



Grain Boundary Segregation Engineering **:A pathway to the design of interfaces**

MIN SEOK KIM

Solute segregation in alloys

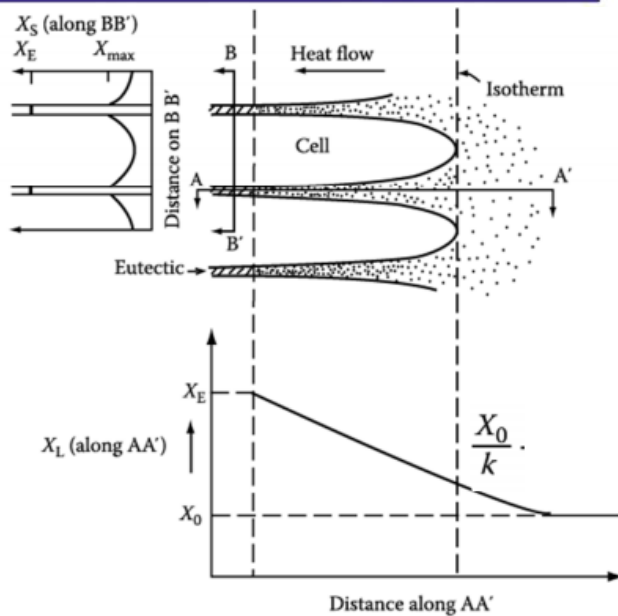
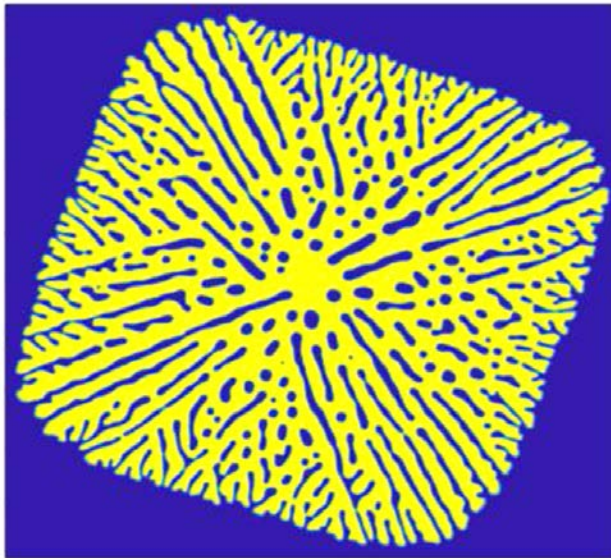
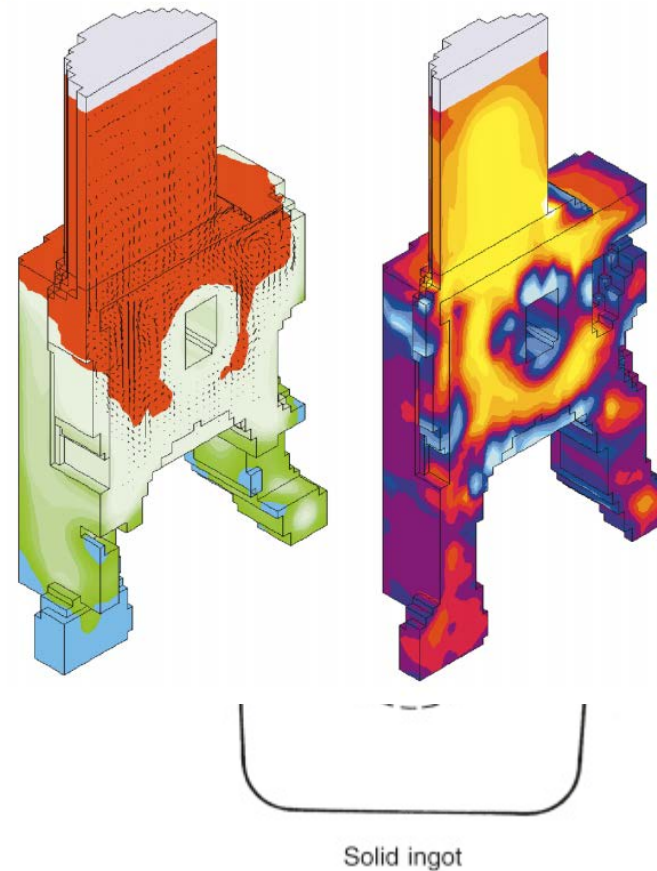
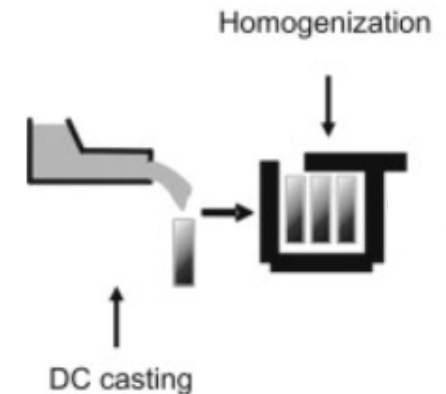
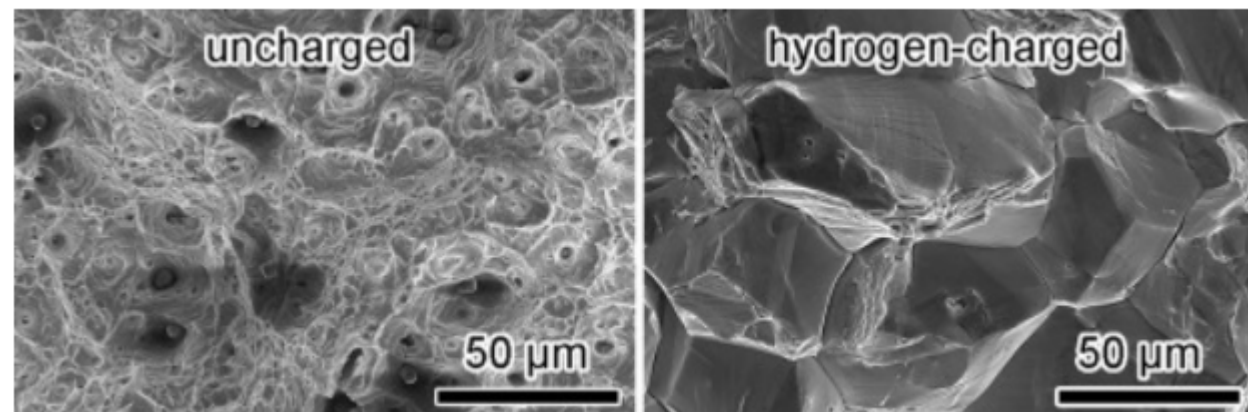
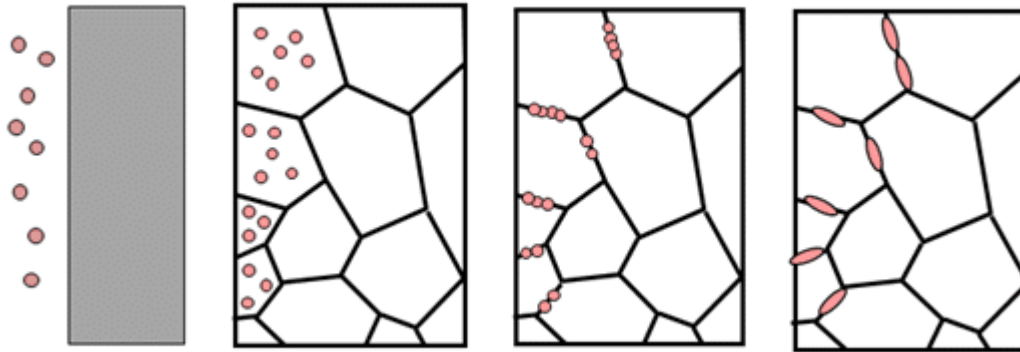


Fig. Simulation of macrosegregation formation in a large steel casting, showing liquid velocity vectors during solidification (left) and final carbon macrosegregation pattern (right).



Hydrogen embrittlement in compositionally complex FeNiCoCrMn FCC solid solution alloy



Gibbs isotherm

$$-d\gamma = \Gamma_1 d\mu_1 + \Gamma_2 d\mu_2 ,$$

where

γ is the surface tension,

Γ_i is the surface excess of component i ,

μ_i is the chemical potential of component i .

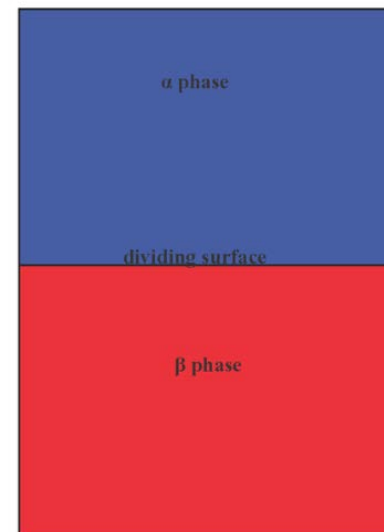
$$G = G^\alpha + G^\beta + G^S$$

$$G = U + pV - TS + \sum_{i=1}^k \mu_i n_i ,$$

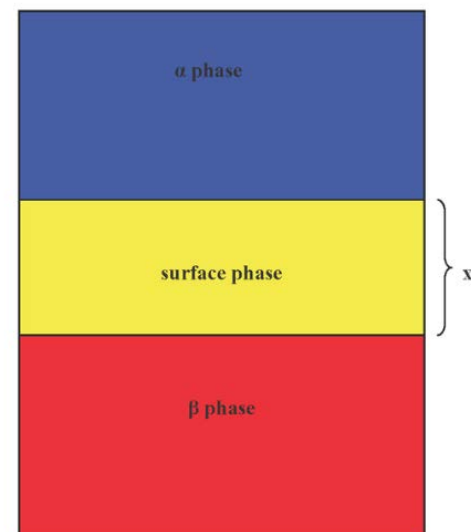
$$dG = Vdp - SdT + \sum_{i=1}^k \mu_i dn_i .$$

$$\sum_{i=1}^k n_i^\alpha d\mu_i + \sum_{i=1}^k n_i^\beta d\mu_i + \sum_{i=1}^k n_i^S d\mu_i + Ad\gamma = 0 .$$

$$\sum_{i=1}^k n_i^S d\mu_i + Ad\gamma = 0 .$$

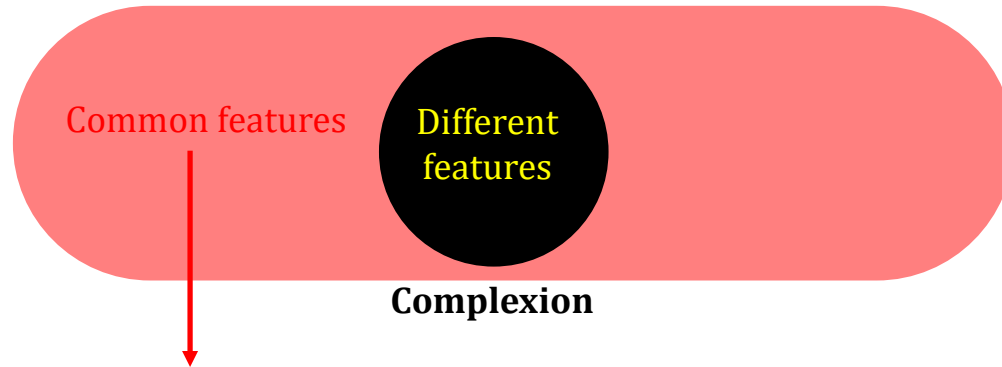


IDEAL SYSTEM



REAL SYSTEM

Segregation Engineering



Interface designing utilizing segregation at **defects(GB, dislocations ...)** , constituting new phase



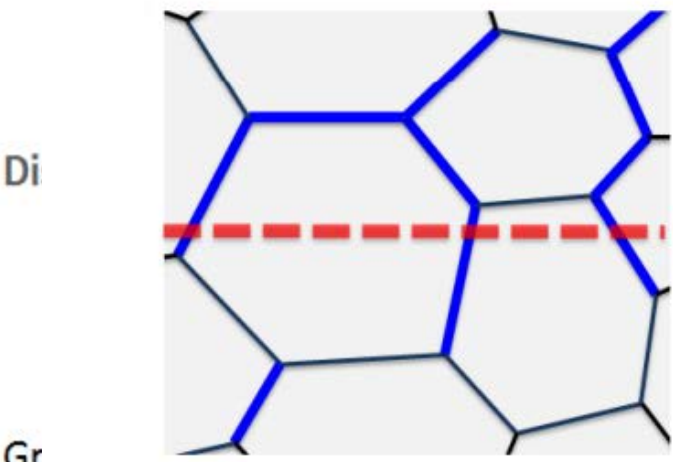
Phase transformation = **Nucleation** & **Growth**

Nucleation

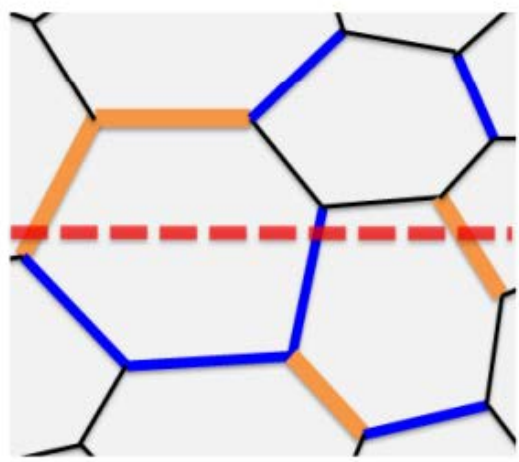
Thermodynamically : Can change G free energy(strain field, Surface energy...)

Kinetically : High Diffusivity , Can act as heterogeneous nucleation site

Segregation Engineering

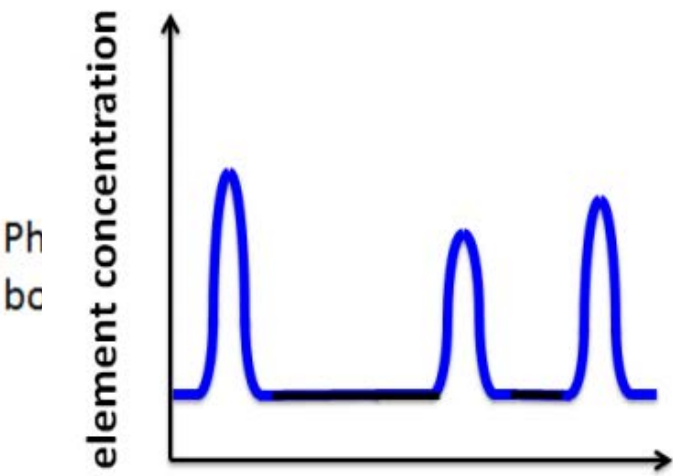


Di
Gr
Bc
Grain boundary segregation

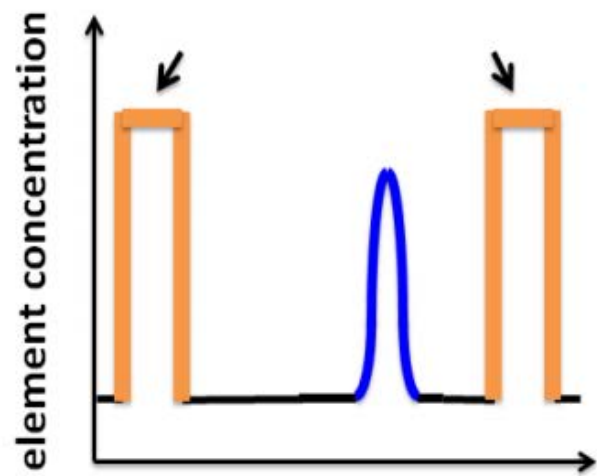


Confined ordering

Heat
treat-
ment



a) spatial coordinate



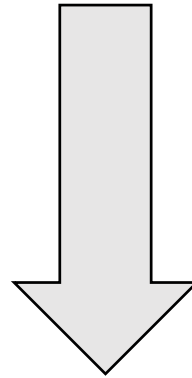
b) spatial coordinate



**Q. How to applicate grain boundary
segregation engineering?**

**Considering effect of Segregated solution in GB local area
(Phase stability, GB cohesion...)**

Grain boundary segregation tendency



Solute element, fraction...

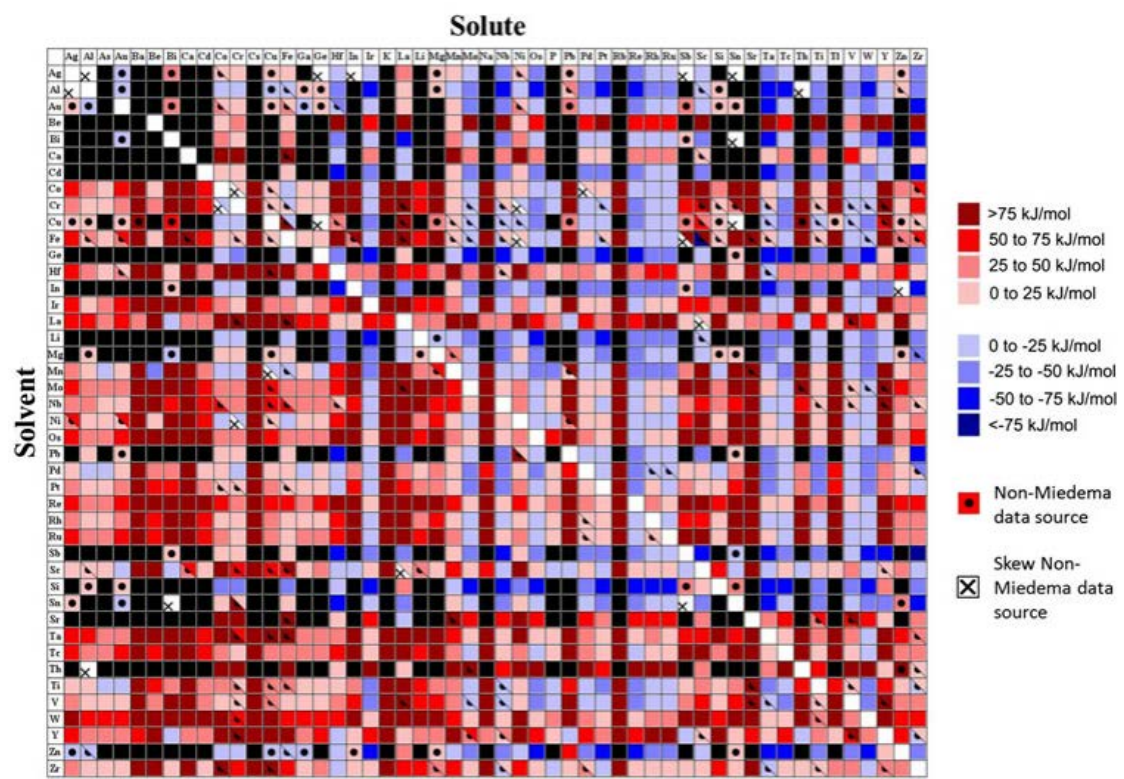
Annealing condition (time, temperature...)

Estimation of Grain boundary Segregation tendency



Estimation of grain boundary segregation enthalpy and its role in stable nanocrystalline alloy design

Heather A. Murdoch and Christopher A. Schuh^{a)}
Department of Materials Science and Engineering, Massachusetts Institute of Technology, Cambridge, Massachusetts 02139



$$\Delta H_{0,M}^{seg} = -0.71 \times \frac{1}{3} \times v \times \left[-\Delta H_{BinA}^{int} - c_0 \gamma_A^S V_A^{2/3} + c_0 \gamma_B^S V_B^{2/3} \right] + \Delta E_{el}$$

Enhancing mechanical property of Martensitic steel

Phase nucleation through confined spinodal fluctuations at crystal defects evidenced in Fe-Mn alloys

A. Kwiatkowski da Silva¹, D. Ponge¹, Z. Peng¹, G. Inden¹, Y. Lu², A. Breen¹, B. Gault¹ & D. Raabe¹

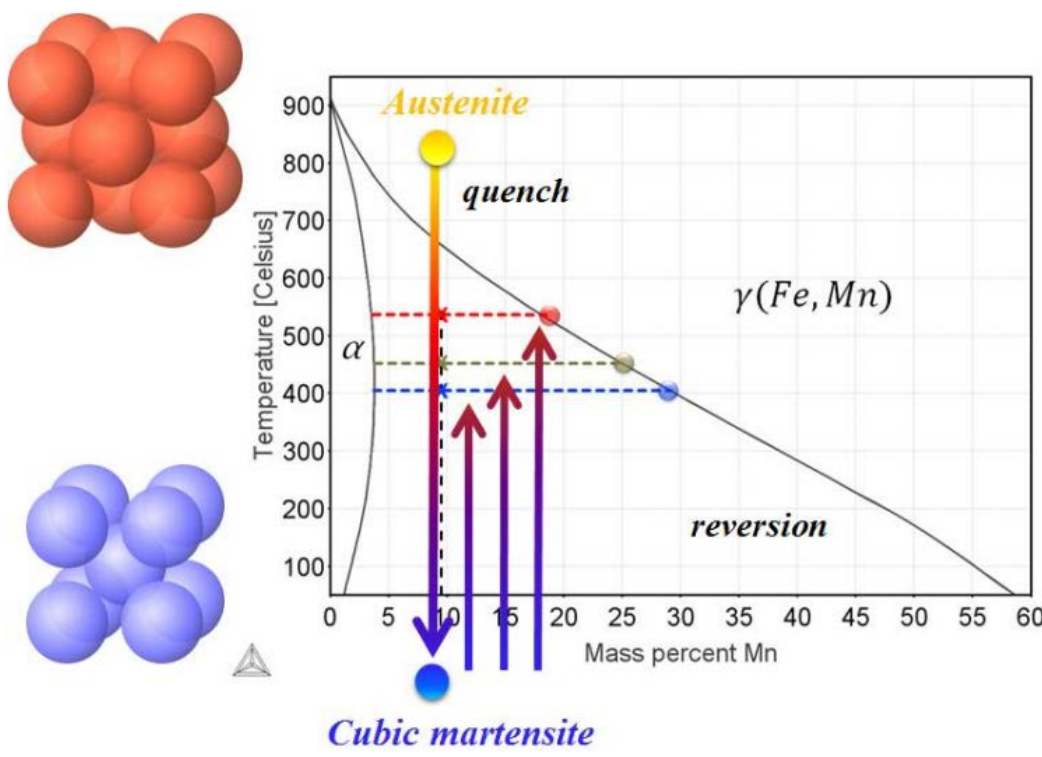
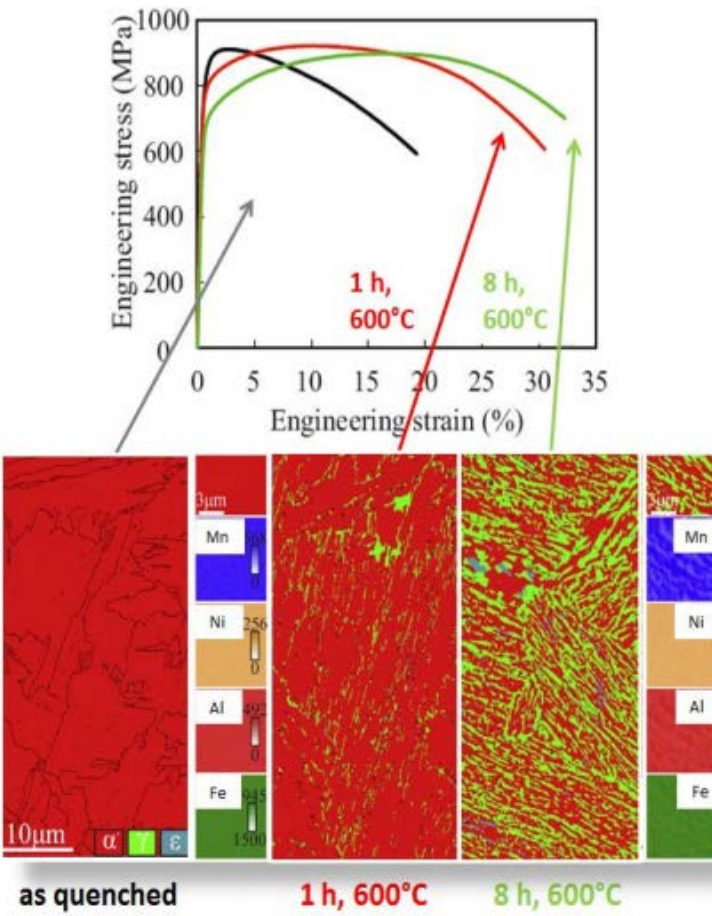
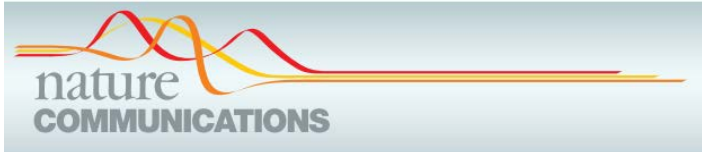


Figure 5. Martensite-to-austenite reversion heat treatment [1,3,4].



**Segregation-driven grain boundary spinodal
decomposition as a pathway for
phase nucleation in a high-entropy alloy**

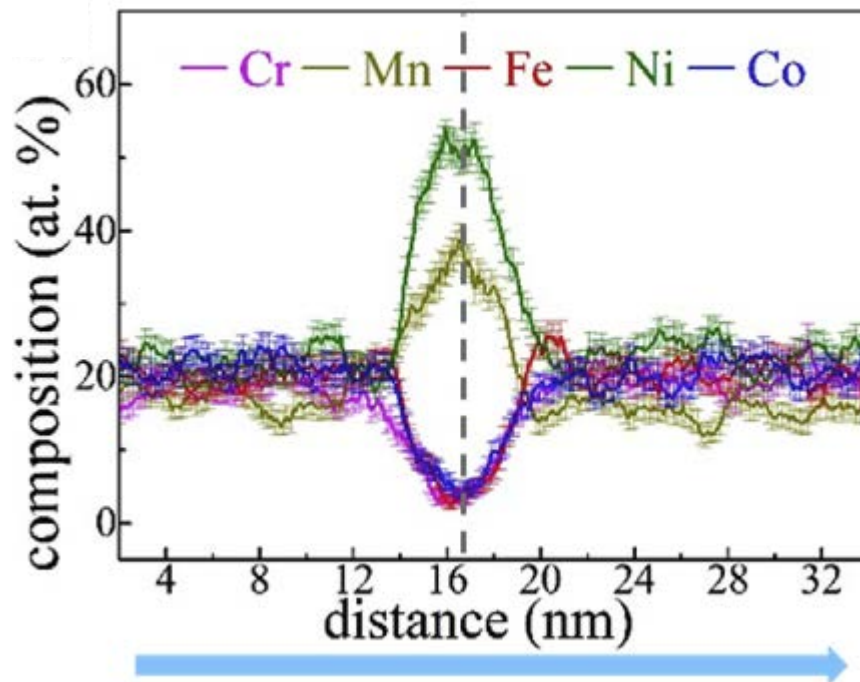
Segregation-driven grain boundary spinodal decomposition as a pathway for phase nucleation in a high-entropy alloy

Linlin Li ^{a, b, *}, Zhiming Li ^a, Alisson Kwiatkowski da Silva ^a, Zirong Peng ^a, Huan Zhao ^a, Baptiste Gault ^{a, c}, Dierk Raabe ^{a, **}

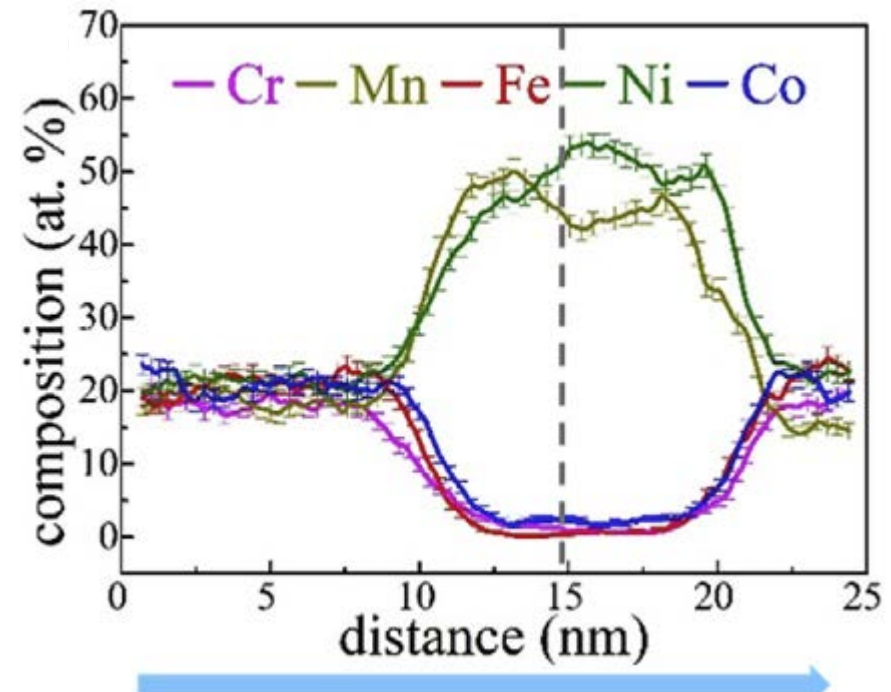
^a Max-Planck-Institut für Eisenforschung, Max-Planck-Strasse 1, 40237, Düsseldorf, Germany

^b Institute of Metal Research, Chinese Academy of Science, Wenhua Road 72, Shenyang, 110016, PR China

^c Department of Materials, Royal School of Mine, Imperial College London, London, SW7 2AZ, UK



450°C, 6hr



450°C, 18hr

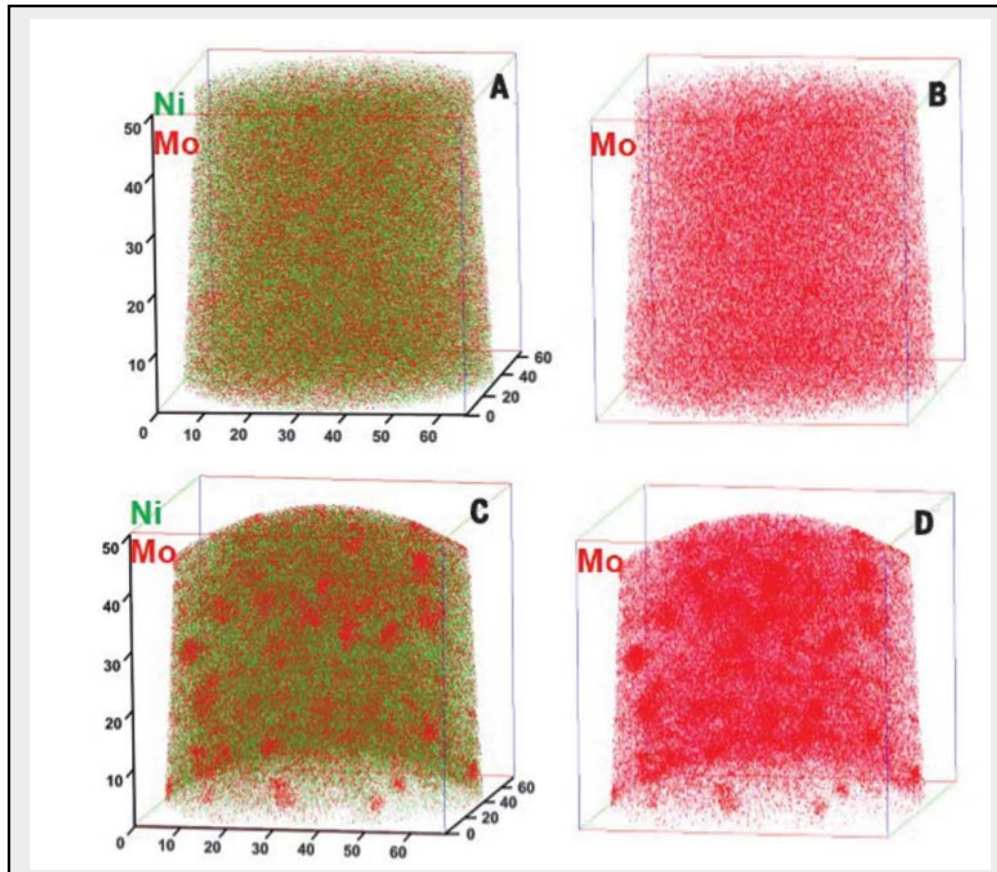
**Grain boundary stability governs
hardening and softening in extremely
fine nano grained metals**

METALLURGY

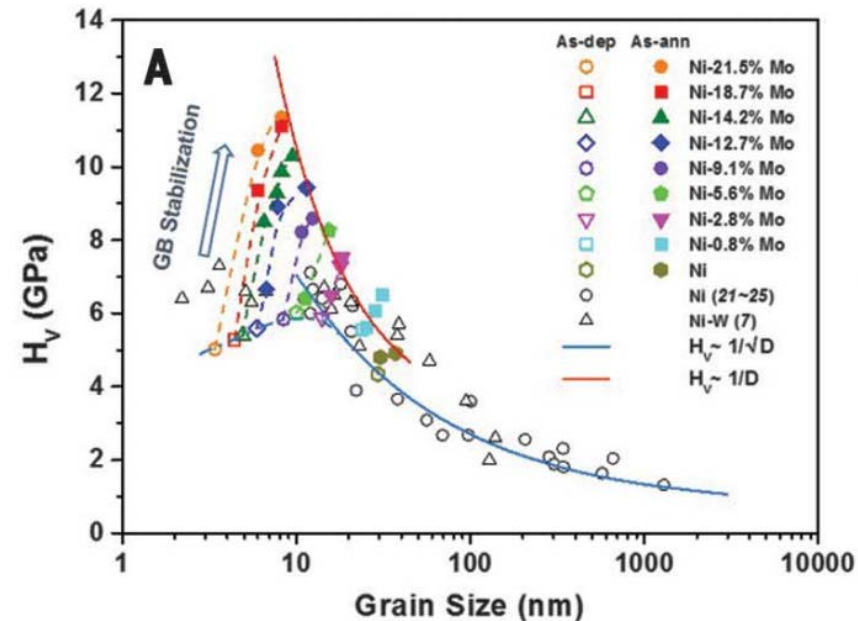
Grain boundary stability governs hardening and softening in extremely fine nanograined metals

J. Hu,^{1*} Y. N. Shi,^{1*} X. Sauvage,² G. Sha,³ K. Lu^{1,3†}

500°C, 1hr



Grain size, $d^{-1/2}$



Stability criteria for nano crystalline alloys

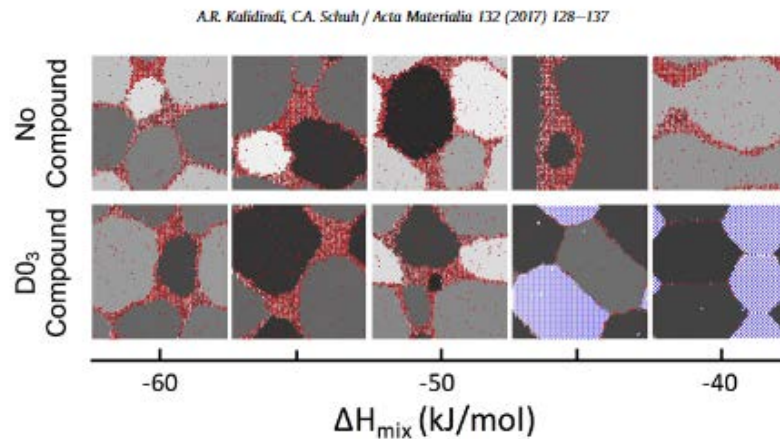
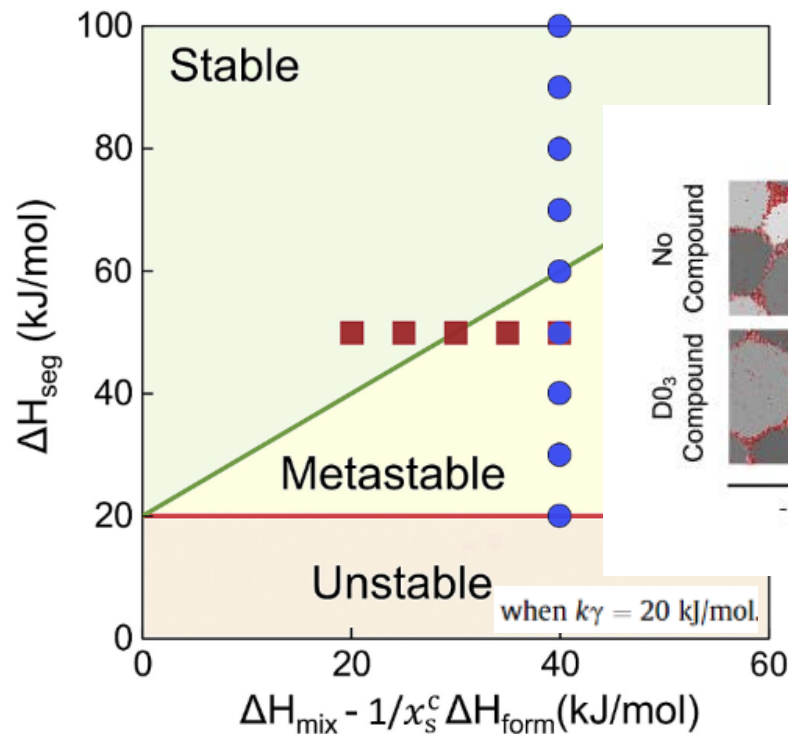
Full length article

Stability criteria for nanocrystalline alloys

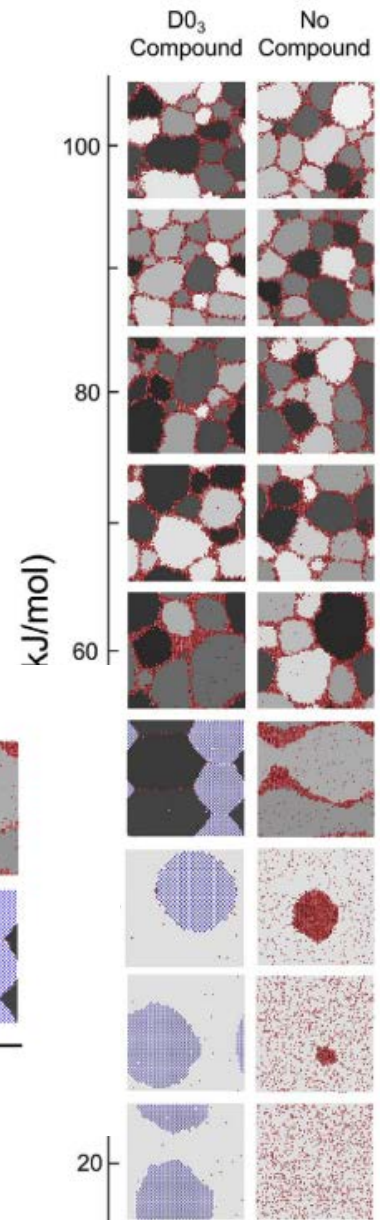
Arvind R. Kalidindi, Christopher A. Schuh*

Department of Materials Science and Engineering, Massachusetts Institute of Technology, 77 Massachusetts Avenue, Cambridge, MA, 02139, USA

$$\Delta H_{\text{seg}} > \underbrace{\Delta H_{\text{mix}} - \frac{1}{\chi_S^c} \Delta H_{\text{form}}}_{\text{Compound formation}} + \underbrace{k\gamma}_{\text{Grain growth}}$$



A.R. Kalidindi, C.A. Schuh / Acta Materialia 132 (2017) 128–137



Segregation has been accepted as a phenomenon to be avoided, which adversely affects the properties of the alloy.

However, it can be used as a methodology for interface design by controlling the segregation phenomenon in nanoscale.

Indeed, studies such as improving the physical properties of TRIP-assisted maraging steel or improving the phase stability of nano crystalline have recently attracted attention, and through this, there is a possibility that the existing alloy design method will overcome limitations that cannot be overcome.

THANK YOU FOR
YOUR KIND ATTENTION