

# Peak Shape Modelling

Structure Analysis  
Materials Science & Engineering  
Seoul National University  
CHAN PARK

Bish & Post Chap 8

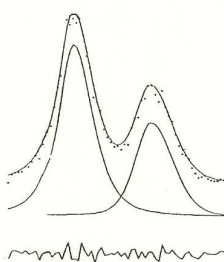
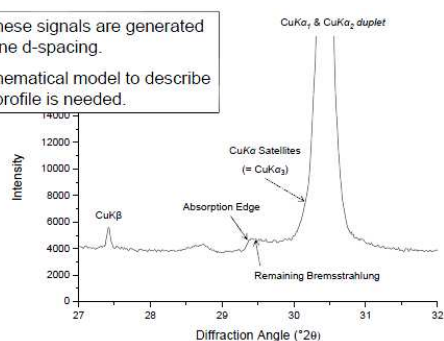
Young Chap 7

Jenkins & Snyder page 302

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## Peak shape modelling

All these signals are generated by one d-spacing.  
Mathematical model to describe the profile is needed.



- Analytical profile fitting
- Direct convolution approach

The Rietveld Method, RA Young

From presentation of Nicola Döbelin,  
RMS Foundation, Switzerland

### Analytical profile fitting

- fit a numerical function (profile shape function; PSF) to a measured diffraction pattern
- PSF  $\rightarrow 2\theta, I, \text{FWHM}$
- An optimization algorithm is employed to adjust parameters of PSF until the difference between the measured and calculated lines are minimized

### Direct convolution approach

#### (Fundamental Parameters Approach)

- profiles are generated by convolution where various functions are convoluted to form the observed profile shape
- Calculate peak profile from device configuration

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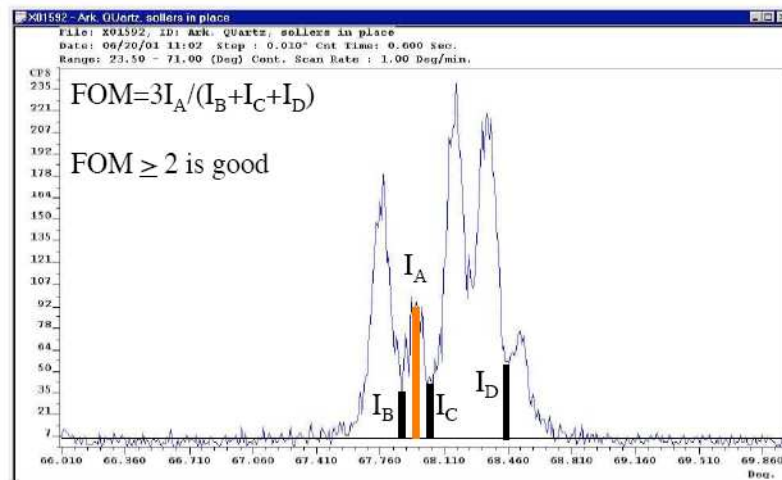
## Precision vs. Accuracy

- Precision - reproducibility
- Accuracy - approach to the "true" value
- Improperly calibrated instruments, inadequate correction for systematic errors → highly precise but inaccurate measurement

Resolution test:

Five fingers of quartz: FOM= 2.29

- Profile constraints



Cullity page 465

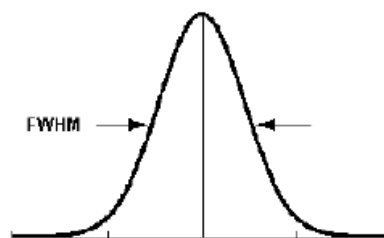
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## Full Width Half Maximum

- All peak shape functions incorporate dependence on half width of Bragg peaks or FWHM
- FWHM shows angular dependence expressed by the **Caglioti** function

$$H^2 = U \tan^2 \theta + V \tan \theta + W$$

- ✓  $H$  = half width
- ✓  $U, V, W$  = refinable parameters



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➤ Convolution - product of two functions is integrated over all spaces

➤ Deconvolution  $(f * g)(t) = f(t) * g(t)$

$$= \int_0^t f(t-\tau)g(\tau) d\tau = \int_0^t f(\tau)g(t-\tau) d\tau$$

➤ Intrinsic profile (specimen profile) (S)

➤ Spectral distribution (radiation source contribution) (W)

➤ Instrumental contribution (G)

➤ Observed profile;  $h(x)$

➤  $h(x) = (W * G) * S + \text{background}$

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## Intrinsic profile (specimen profile) (S)

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➤ Darwin width

✓ Inherent width of a diffraction peak

✓ Result of uncertainty principle ( $\Delta p \Delta x = h$ )

- Location of a photon in a crystal is restricted to a small volume ( $\leftarrow$  absorption coefficient)  $\rightarrow \Delta p$  must be finite  $\rightarrow \Delta \lambda$  ( $\Delta p = h/\Delta \lambda$ ; de Broglie relation) must be finite  $\rightarrow$  produces a finite width to a diffraction peak

➤ Two sample effects which broaden the profile shape functions

✓ Size  $\beta_{\text{size}} = 1/(t \cos \theta)$

✓ Microstrain  $\beta_{\text{strain}} = 4e \tan \theta$

## Spectral Distribution (radiation source contribution) (W)

- The inherent spectral profile of the K-alpha1 line from a Cu target has a breadth of  $0.518 \times 10^{-3} \text{ \AA}$  (approximately Lorentzian and asymmetric).
- The inherent width & asymmetry is usually overwhelmed by the fact that various components of radiation ( $K_{\alpha 1}, K_{\alpha 2}, K_{\alpha 3,4}, \dots$ ) in a polychromatic beam will each spread out as  $2\theta$  increases.
- This spectral dispersion is so great that it can dominate the diffraction profiles at high angle, making them quite broad & relatively symmetric.
- Monochromatization can limit the breadth of W to the Darwin width of the monochromator crystal and its mosaicity.

$$H^2 = U \tan^2 \theta + V \tan \theta + W$$

## Instrumental contribution (G), Observed profile h(x)

- 5 principal non-spectral contribution to the instrumental profile (G)

X-ray source image

Flat specimen → asymmetry

Axial divergence of incident beam → asymmetry

Specimen transparency → asymmetry

Receiving slit

- Intrinsic profile (S)
- Spectral distribution (radiation source contribution) (W)
- Instrumental contribution (G)
- $h(x) = (W * G) * S + \text{background}$  (\*; convolution)
- $(W * G)$ ; fixed for a particular instrument/target system → instrumental profile  $g(x)$
- $h(x) = g(x) * S + \text{background}$
- Very asymmetric profile in sealed tube parafocusing system
- Symmetric Gaussian profile in neutron & synchrotron X-ray

# Analytical profile shape functions (PSFs)

**Table 1.2** Some symmetric analytical profile functions that have been used<sup>a</sup>

Function	Name
(a) $\frac{C_0^{1/2}}{H_K \pi^{1/2}} \exp(-C_0(2\theta_i - 2\theta_K)^2/H_K^2)$	Gaussian ('G')
(b) $\frac{C_1^{1/2}}{\pi H_K} \frac{1}{\left[1 + C_1 \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]}$	Lorentzian ('L')
(c) $\frac{2C_2^{1/2}}{\pi H_K} \frac{1}{\left[1 + C_2 \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]^2}$	Mod 1 Lorentzian
(d) $\frac{C_3^{1/2}}{2H_K} \frac{1}{\left[1 + C_3 \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]^{3/2}}$	Mod 2 Lorentzian
(e) $\eta L + (1 - \eta)G$	pseudo-Voigt ('pV')
The mixing parameter, $\eta$ , can be refined as a linear function of $2\theta$ wherein the refinable variables are $NA$ and $NB$ : $\eta = NA + NB*(2\theta)$	
(f) $\frac{C_4}{H_K} \left[1 + 4^m(2^{1/m} - 1) \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]^{-m}$	Pearson VII
$m$ can be refined as a function of $2\theta$ , $m = NA + NB/2\theta + NC/(2\theta)^2$ , where the refinable variables are $NA$ , $NB$ , and $NC$ .	
(g) Modified Thompson-Cox-Hastings pseudo-Voigt, 'TCHZ'	(Mod-TCH pV)
TCHZ = $\eta L + (1 - \eta)G$ where $\eta = 1.36603q - 0.47719q^2 + 0.1116q^3$ $q = \Gamma_L/\Gamma$ $\Gamma = (\Gamma_G^5 + A\Gamma_G^4\Gamma_L + B\Gamma_G^3\Gamma_L^2 + C\Gamma_G^2\Gamma_L^3 + D\Gamma_G\Gamma_L^4 + \Gamma_L^5)^{0.2} = H_K$ $A = 2.69269$ $B = 2.42843$ $C = 4.47163$ $D = 0.07842$ $\Gamma_G = (U \tan^2 \theta + V \tan \theta + W + Z/\cos^2 \theta)^{1/2}$ $\Gamma_L = X \tan \theta + Y/\cos \theta$	

- Gaussian
- Lorentzian
- Modified Lorentzian
- Intermediate Lorentzian
- Pseudo-Voigt
- Pearson VII
- Split Pearson VII

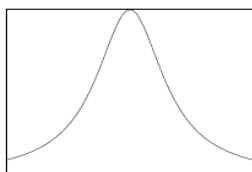
## Analytical profile fitting ➤ Gaussian, Lorentzian, Pseudo Voigt profile

➤ Most instruments are more Gaussian at low angles and more Lorentzian at high angles (wavelength dispersion)

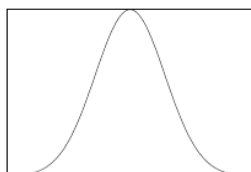
Pseudo Voigt profile;  $nL + (1-n)G$

Lorentzian profile

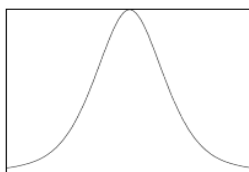
Gaussian profile



Lorentzian (n = 1.0)

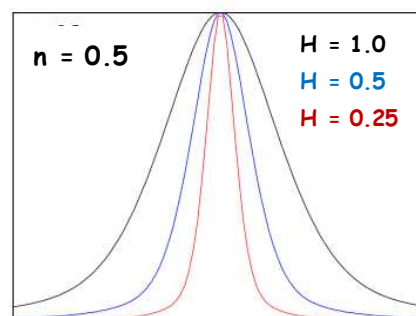


Gaussian (n = 0)



Pseudo Voigt (n = 0.5)

Same FWHM (H) in  
 $H^2 = U \tan^2 \theta + V \tan \theta + W$



# Analytical profile shape functions

(a)  $\frac{C_0^{1/2}}{H_K \pi^{1/2}} \exp(-C_0(2\theta_i - 2\theta_K)^2/H_K^2)$

Gaussian ('G')

(e)  $\eta L + (1 - \eta)G$

pseudo-Voigt ('pV')

The mixing parameter,  $\eta$ , can be refined as a linear function of  $2\theta$  wherein the refinable variables are  $NA$  and  $NB$ :

$\eta = NA + NB*(2\theta)$

(b)  $\frac{C_1^{1/2}}{\pi H_K} \frac{1}{\left[1 + C_1 \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]}$

Lorentzian ('L')

(c)  $\frac{2C_2^{1/2}}{\pi H_K} \frac{1}{\left[1 + C_2 \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]^2}$

Mod 1 Lorentzian

(d)  $\frac{C_3^{1/2}}{2H_K} \frac{1}{\left[1 + C_3 \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]^{3/2}}$

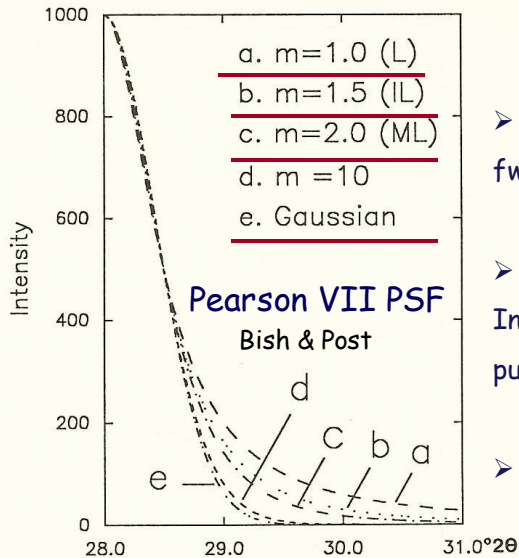
Mod 2 Lorentzian

(f)  $\frac{C_4}{H_K} \left[1 + 4*(2^{1/m} - 1) \frac{(2\theta_i - 2\theta_K)^2}{H_K^2}\right]^{-m}$  Pearson VII

$m$  can be refined as a function of  $2\theta$ ,

$m = NA + NB/2\theta + NC/(2\theta)^2$ ,

where the refinable variables are  $NA$ ,  $NB$ , and  $NC$ .

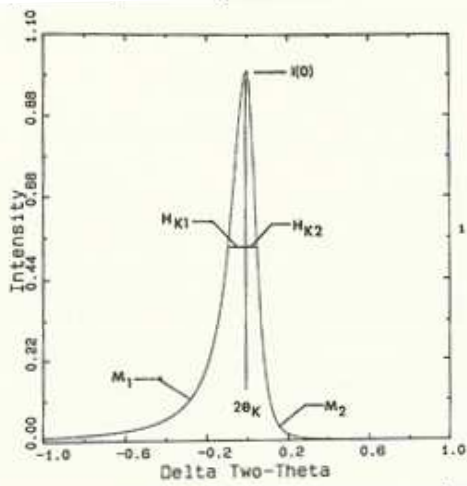


➤ A series of Pearson VII profiles generated with the same fwhm but with different values of exponent  $m$

➤ Depending on the value of  $m$ , the function replicates the Intermediate Lorentzian (IL), Modified Lorentzian (ML), and pure Lorentzian (L) profiles.

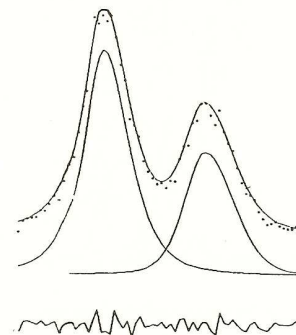
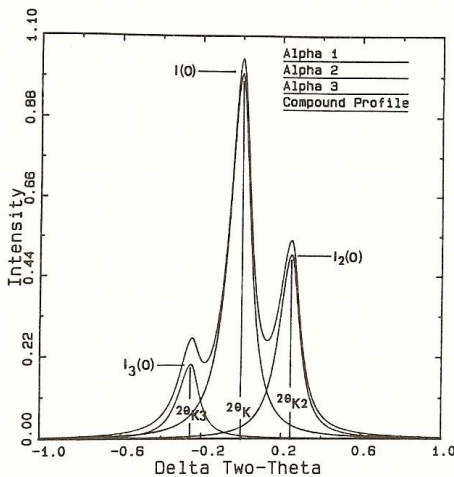
➤ The shape is essentially Gaussian when  $m > \sim 10$

## Split Pearson VII

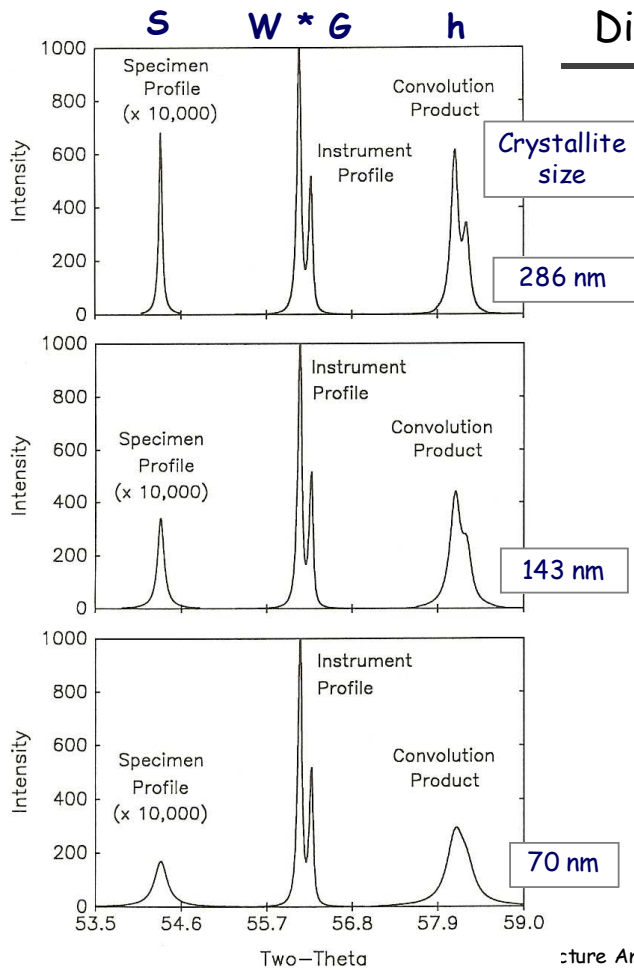


➤ The two half profiles share a common Bragg angle  $2\theta_K$  and peak intensity  $I(0)$ .

➤ Their different fwhm's  $H_K$ , and exponents  $M$ , allow the profile to model an asymmetric line



## Direct convolution approach



$$h = (W * G) * S$$

➤ Line shape ← convolution of  $(W*G)$  and  $(S)$  contributions

$W*G$ ; instrument  
 $S$ ; specimen

$S$ ; Intrinsic profile (specimen profile)  
 $W$ ; Spectral distribution (radiation source contribution)  
 $G$ ; Instrumental contribution

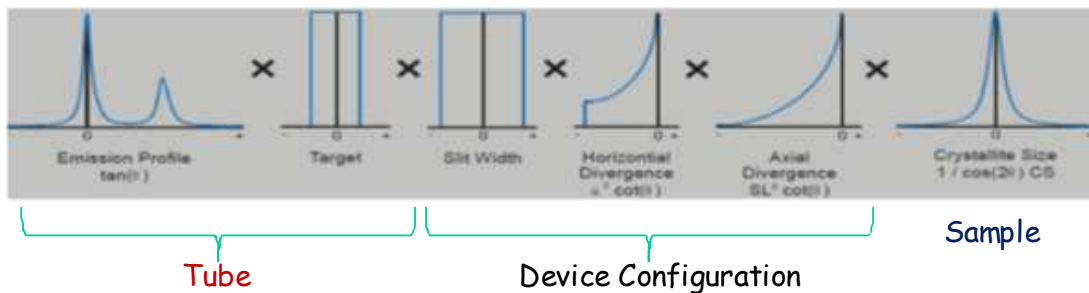
Integrated intensity of the peak remains the same while the peak broadens and the peak intensity decreases

Need to know precisely the nature of contributions from both instrument & specimen

Bish & Post

## Direct convolution approach > Fundamental Parameters Approach (FPA)

- Calculate the peak profile from the device configuration
- Take into account the contributions of:
  - ✓ Source emission profile (X-ray wavelength distribution from Tube)
  - ✓ Every optical element in the beam path (position, size, etc.)
  - ✓ Sample contributions (peak broadening due to crystallite size & strain)



FPA needs:

- Very detailed and complete description of the instrument configuration
- Very well aligned instrument

- Background fitting (this should not affect the apparent Bragg intensities if it is done correctly)
- Extinction
- Preferred Orientation (Texture)
- Absorption & Surface Roughness
- Other Geometric Factors

- 
- Need to know precisely the nature of contributions from both instrument and specimen
  - PSF representing instrument can be obtained by measuring a set of lines from a specimen
    - ✓ Free of crystallite size broadening and lattice defects
    - ✓ Sufficiently small mean particle size and narrow size distribution without having particles so small as to introduce line broadening
    - ✓ Line profile standard, LaB<sub>6</sub> NIST SRM



# Standard Reference Materials (SRMs)

➤ Powder Line Position + Line Shape Std for Powder Dif

✓ **Silicon (SRM 640e); \$741/7.5g**

➤ Line position - Fluorophlogopite mica (SRM 675); \$721/7.5g

➤ Line profile - **LaB<sub>6</sub> (SRM 660c); \$1,002/6g**

➤ Intensity

✓ ZnO, TiO<sub>2</sub> (rutile), Cr<sub>2</sub>O<sub>3</sub>, CeO<sub>2</sub> (SRM 674b); \$916/10g

➤ Quantitative phase analysis

✓ Al<sub>2</sub>O<sub>3</sub> (SRM 676a ); "notify me"/20g, Silicon Nitride (SRM 656); \$492/20g

➤ Instrument Response Std

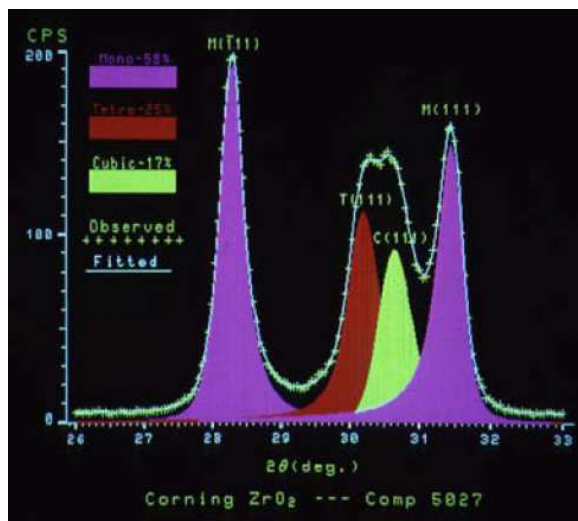
✓ Alumina plate (SRM 1976b); \$700/1 disc

Prices; 2017-12-28

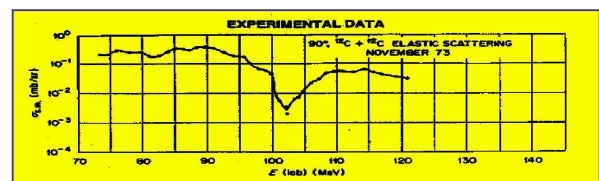
[www.nist.gov/srm/index.cfm](http://www.nist.gov/srm/index.cfm)

Gold  
\$41.46 / gram  
(2017-12-28)  
[goldprice.org](http://goldprice.org)

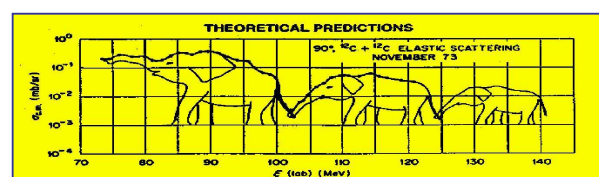
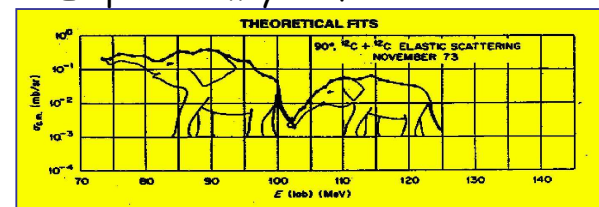
## Line (peak) profile analysis



## The danger of profile fitting



Elephants may be fit to data



Extrapolation ?????