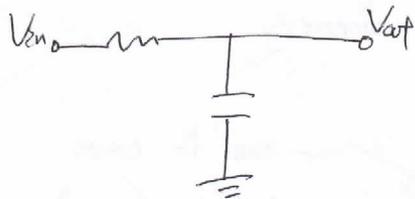


Integrator



$$\frac{V_{out}}{V_{in}} = \frac{1}{1 + j\omega RC}$$

if $\omega RC \gg 1$, $\frac{1}{j\omega RC}$

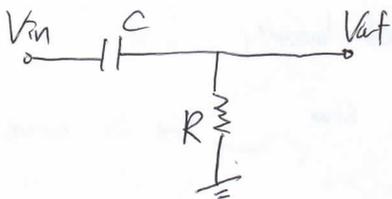
$$\therefore V_{out} = \frac{1}{RC} \int V_{in} dt$$

if $\omega RC = \frac{\omega}{\omega_{2dB}} \gg 1$

LPF becomes integrator.

Not in the case of op-Amp. better design.

Differentiator



$$\frac{V_{out}}{V_{in}} = \frac{R}{1 + j\omega C R} = \frac{j\omega RC}{1 + j\omega RC}$$

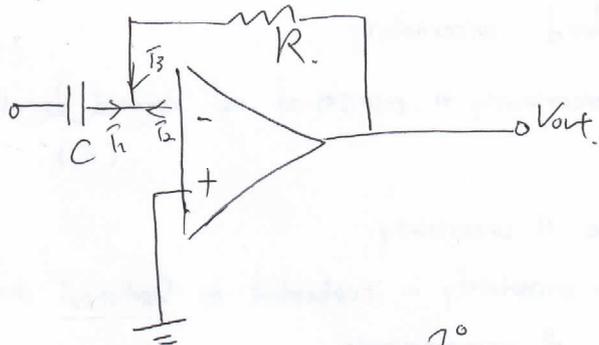
if $\omega RC = \frac{\omega}{\omega_{2dB}} \ll 1$

$$\rightarrow \frac{V_{out}}{V_{in}} = j\omega RC$$

$$\therefore V_{out} = j\omega RC V_{in} = RC \frac{dV_{in}}{dt}$$

HPF with $\frac{\omega}{\omega_{2dB}} \ll 1$

Op-Amp Differentiator



$$\bar{I}_1 = C \frac{d[V_{in} - V_{out}]}{dt} = C \frac{dV_{in}}{dt}$$

$$\bar{I}_2 = 0$$

$$\bar{I}_3 = \frac{V_{out} - V_{out}}{R} = \frac{V_{out}}{R}$$

$$\therefore C \frac{dV_{in}}{dt} + \frac{V_{out}}{R} = 0$$

$$\therefore V_{out} = -RC \frac{dV_{in}}{dt}$$

\therefore differentiation better design.

In practice

$$|V_{out}| \ll V_{cc}$$

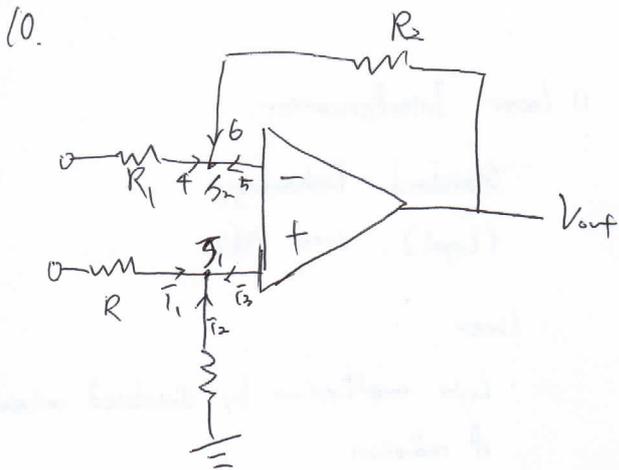
but if $|V_{out}| \ll V_{cc}$

V_{in} has big noise? \Rightarrow "Roll-off of circuit"

\rightarrow suppress.. by C_2, R_2

HW 6.

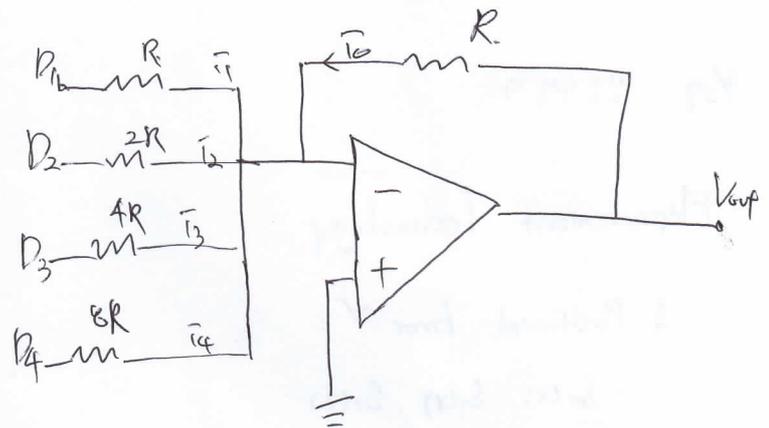
derive the C_2, R_2 addition, gives "R.I.C.F" function to differentiator



$$+ \frac{R_2}{R_1} = \text{Gain} \begin{matrix} > \\ \geq \\ < \end{matrix} 1.$$

11. D/A Converter.

$$[D_1, D_2, D_3, D_4] \xrightarrow{\text{D/A}} V$$



J1

$$\bar{I}_1 = \frac{V_2 - V^+}{R_1}$$

$$\bar{I}_2 = \frac{0 - V^+}{R_2}$$

$$\bar{I}_3 = 0.$$

$$\therefore \frac{V_2 - V^+}{R_1} + \frac{-V^+}{R_2} = 0.$$

$$\therefore V^+ = \frac{R_2 V_2}{R_1 + R_2}$$

J2

$$\bar{I}_4 = \frac{V_1 - (V^-)}{R_1} = V^+$$

$$\bar{I}_5 = 0$$

$$\bar{I}_6 = \frac{V_{out} - V^-}{R_2}$$

$$\therefore \bar{I}_4 + \bar{I}_5 + \bar{I}_6 = 0.$$

$$V_{out} = + \left(\frac{R_2}{R_1} \right) (V_2 - V_1)$$

amplification difference

Differential Amplifier.

$$\bar{I}_1 = \frac{D_1 - V^-}{R} = \frac{D_1}{R}$$

$$\bar{I}_2 = \frac{D_2}{2R}$$

$$\bar{I}_3 = \frac{D_3}{4R}$$

$$\bar{I}_4 = \frac{D_4}{8R}$$

$$\bar{I}_0 = \frac{V_{out} - V^-}{R} = \frac{V_{out}}{R}$$

$$\therefore \frac{D_1}{R} + \frac{D_2}{2R} + \frac{D_3}{4R} + \frac{D_4}{8R} + \frac{V_{out}}{R} = 0.$$

$$\therefore V_{out} = -R \left[\frac{D_1}{R} + \frac{D_2}{2R} + \frac{D_3}{4R} + \frac{D_4}{8R} \right]$$

$$= - \left[D_1 + \frac{D_2}{2} + \frac{D_3}{4} + \frac{D_4}{8} \right]$$

$$D_i = [0, 1]$$

$$\text{if } [1, 1, 1, 1] \Rightarrow \left[1 + \frac{1}{2} + \frac{1}{4} + \frac{1}{8} \right].$$

Digital \Rightarrow Analog

③ 11/20

if 5 bit D/A.

$$V_{out} = -R \left[\frac{D_1}{R} + \frac{D_2}{2R} + \frac{D_3}{4R} + \frac{D_4}{8R} + \frac{D_5}{16R} \right]$$

R tolerance = 10%
due to manufacturing

if R of D_1 is $0.9R$
instead of R.

$$V_{out} = - \left[\frac{R_1}{0.9} + \frac{R_2}{2} + \frac{R_3}{4} + \frac{D_4}{8} + \frac{D_5}{16} \right]$$

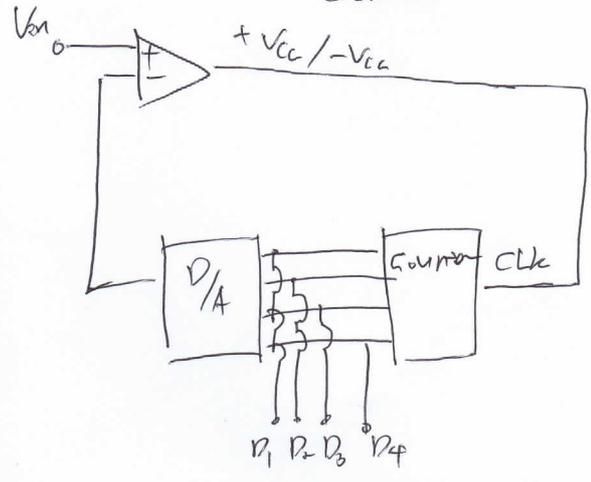
⊕

if [1, 0, 0, 0, 0] $\Rightarrow V_{out} = - \left[\frac{1}{0.9} + 0 \right] = -1.01$

if [1, 0, 0, 0, 1] $\Rightarrow V_{out} = - \left[1 + \dots + \frac{1}{16} \right] =$
 \Rightarrow 4bit maximum //
 ($\because > 10\%$ tolerance)

13. A/D converter.

D/A converter + Analogue comparison + Counter

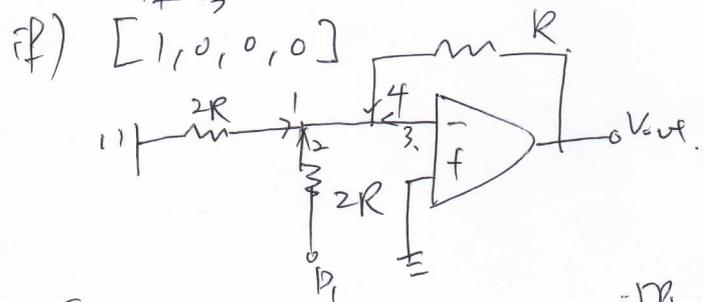
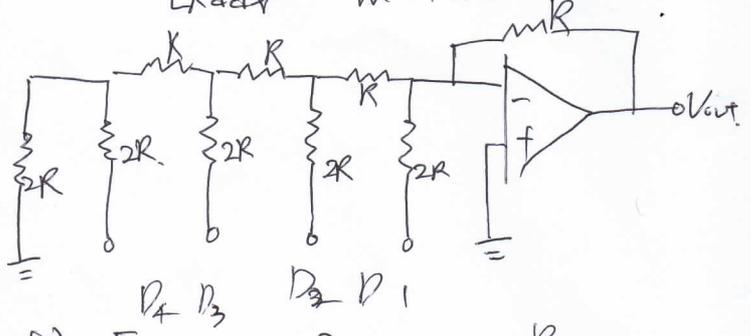


"Successive Approximation Method"

- slow response than D/A
- counter/CLK required.
- Resolution \ll LSB.

12. D/A converter ⊕

"Ladder method"



$\bar{I}_1 = 0$
 $\bar{I}_2 = \frac{V_1}{2R}$
 $\bar{I}_3 = 0$
 $\bar{I}_4 = \frac{V_{out}}{R}$
 $\therefore V_{out} = - \left[\frac{D_1}{2} + \frac{D_2}{4} + \frac{D_3}{8} + \frac{D_4}{16} \right]$
 \hookrightarrow only use $R, 2R$.
 tolerance $\approx 1\%$