

**Development of a Microstructural Rapid Solidification Model  
for Additive Manufacturing Process**

**A.R.S.M.  
03. 18. 2019**

# What is the Additive Manufacturing(AM)?

2

: a manufacturing process of making three dimensional solid objects by building up additives

## Pros

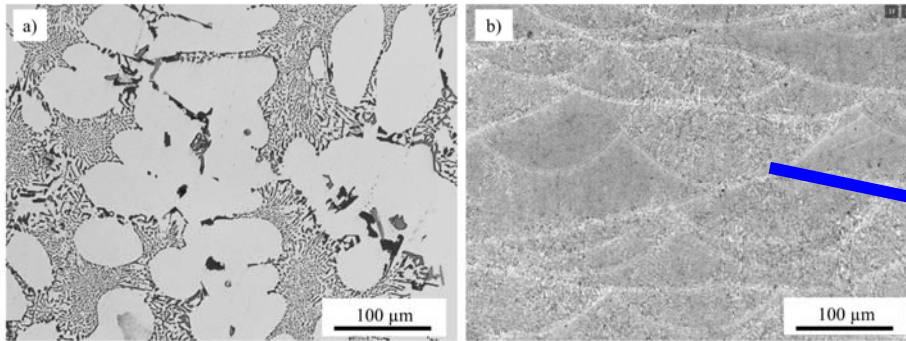
- Lower costs of manufacturing (few additional process, no wastes)
- On-demand manufacturing
- A good option for making extremely complex parts
- Reliability

## Cons

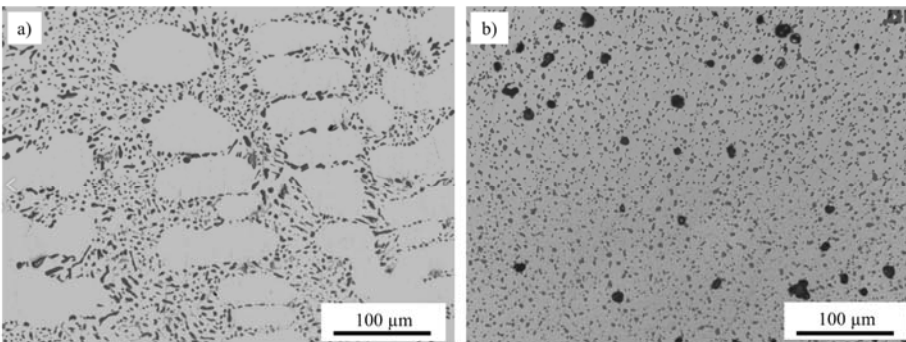
- Low productivity
- Limited materials (e.g. a few steels, Al, Ni, Ti alloys in the case of metal AM)
- Hard to predict mechanical properties (because of dependence of various manufacturing parameters)

→ Solidification model is needed to predict the microstructure which directly decide the mechanical properties of the product

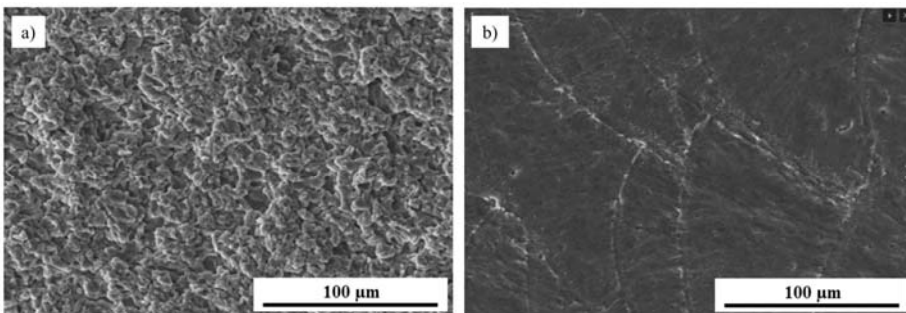
# Foundry vs AM



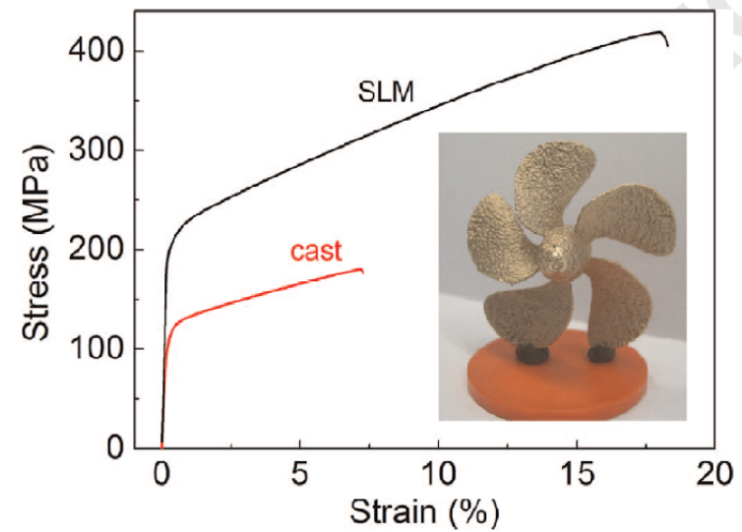
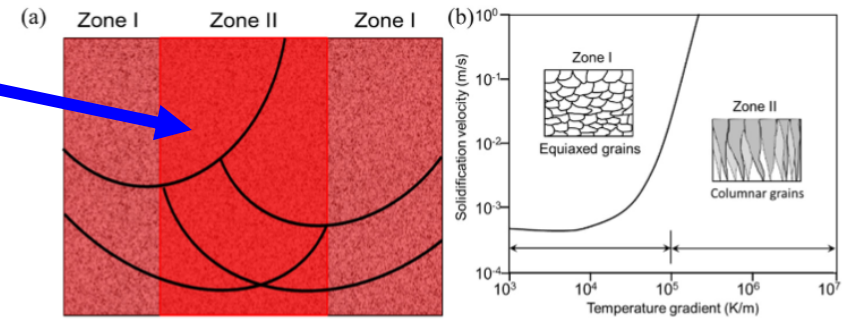
Examples of microstructure under conditions as-produced of AISi10Mg alloy samples obtained through a) gravity casting and b) AM *Item 1 of 4*



Examples of microstructure under T6 conditions of AISi10Mg alloy samples obtained through a) gravity casting and b) AM *Item 2 of 4*



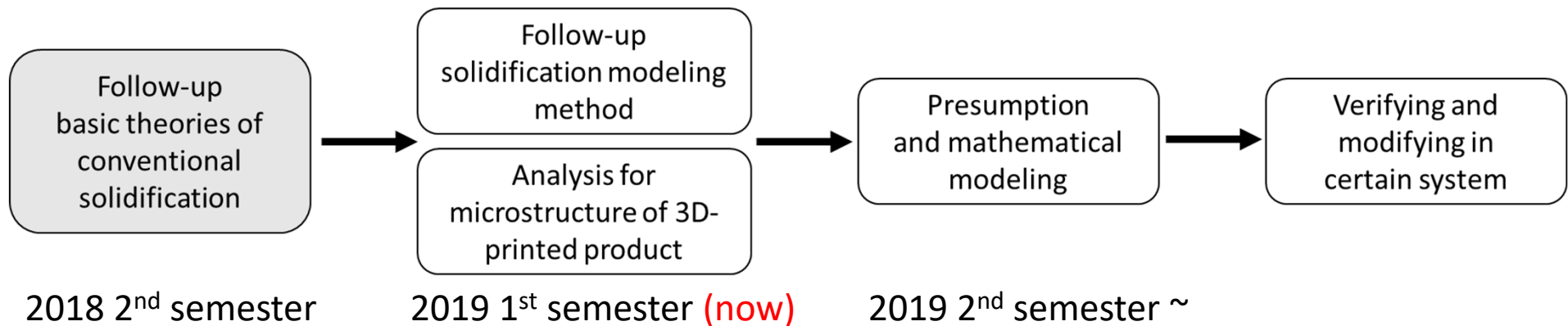
Different morphology of the surface eroded during cavitation tests for AISi10Mg alloy samples obtained through a) gravity casting and b) AM *Item 3 of 4*



## Characteristics of Solidification for AM

- Cooling rate : Conventional casting ( $\sim 10^3$  K/s) vs. Rapid solidification ( $10^3 \sim 10^6$  K/s)
- Dimension : layer thickness = 0.03 ~ 0.1 mm , particle size = 0.01 mm (avg)
- Manufacturing parameters : power, scanning rate, printing path > related to thermal history
- Key input variables for model : Alloy composition( $C_0$ ), Thermal gradient( $G$ ), Growth rate( $V$ )
- Thermodynamic data, Diffusivity and interfacial energy are needed

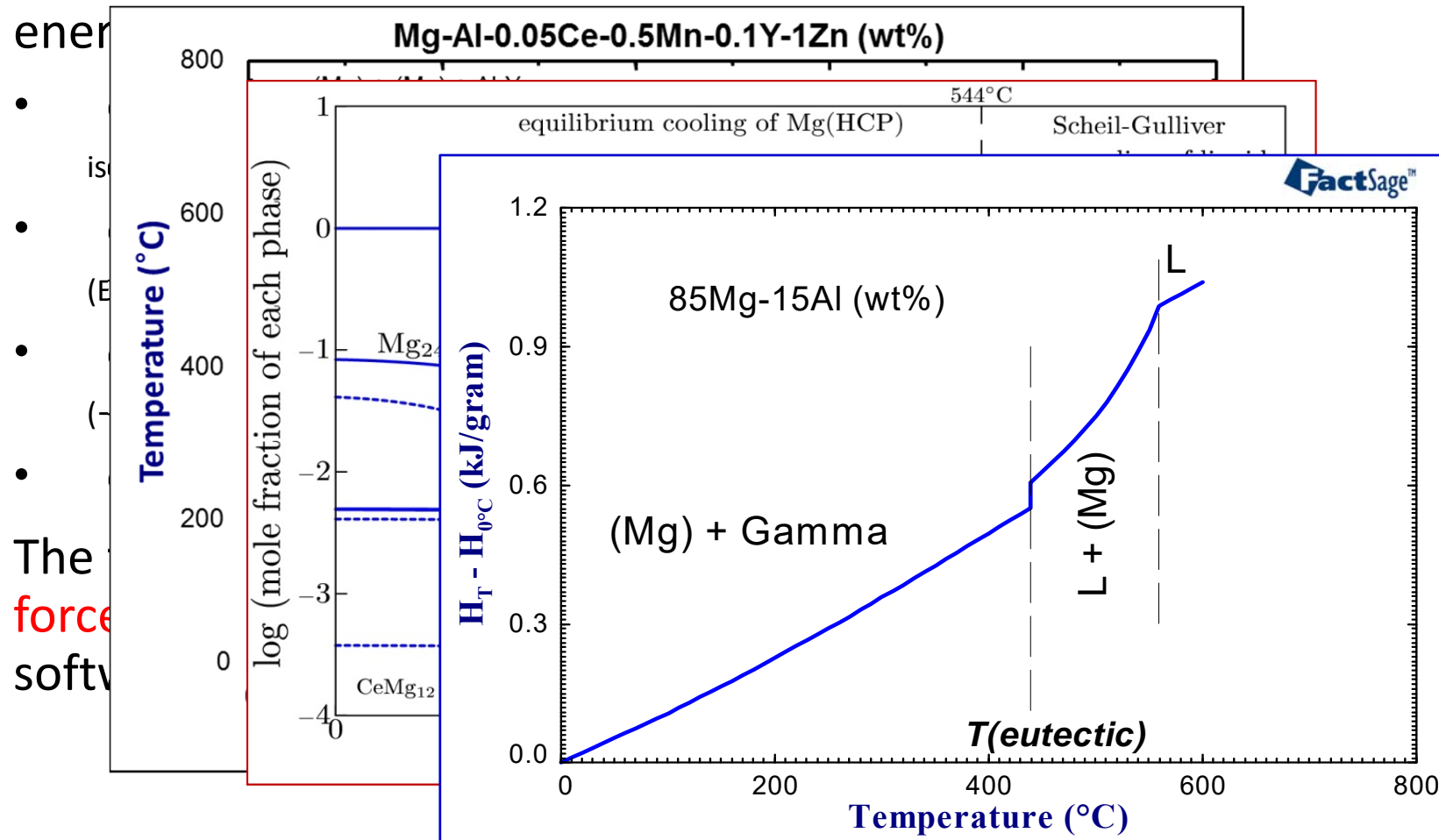
## Research tracks



# What can we do using Thermodynamic Data?

5

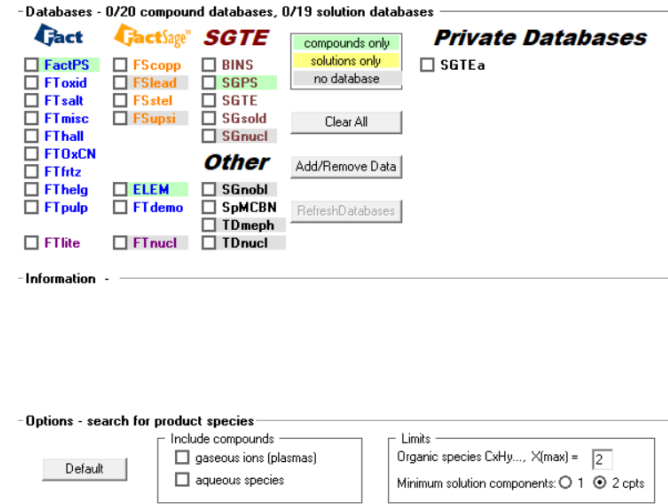
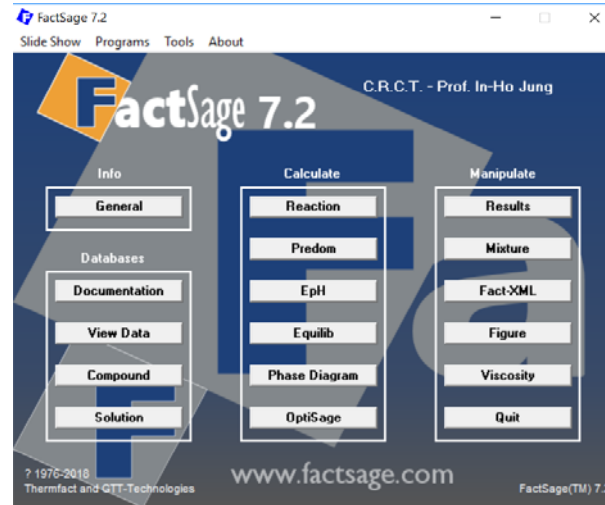
The thermodynamic database can be used along with the Gibbs



<Commercial Software and databases>



## Thermodynamic database



## Microstructural simulation (2009 ~)



Predictions of microstructure evolution : from solidification to annealing

- 1) Matrix composition distribution
- 2) Amount and chemistry of Secondary phases and precipitates

Key experiment & simulation code development

Complexity in calculations

## Scheil Cooling Model

> Energy scale (gibbs E)

- Short calculation time (~seconds)
- No morphology
- No cooling rate
- No diffusion

## Solidification Model (1D)

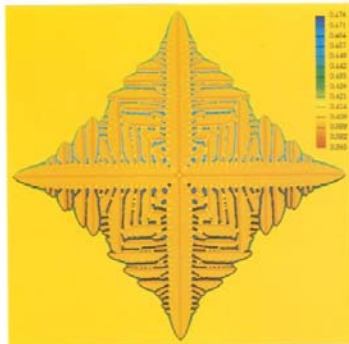
> Energy scale + Time scale

- Short calculation time (~ minutes)
- Cooling rate (G·V)
- Concentration profile in dendrite
- Morphology Calc. (+SDAS/PDAS, fraction)
- Multicomponent system
- Based on FVM, FEM code

## Phase Field Model

> Energy scale + Time scale + Length(Dimension) scale

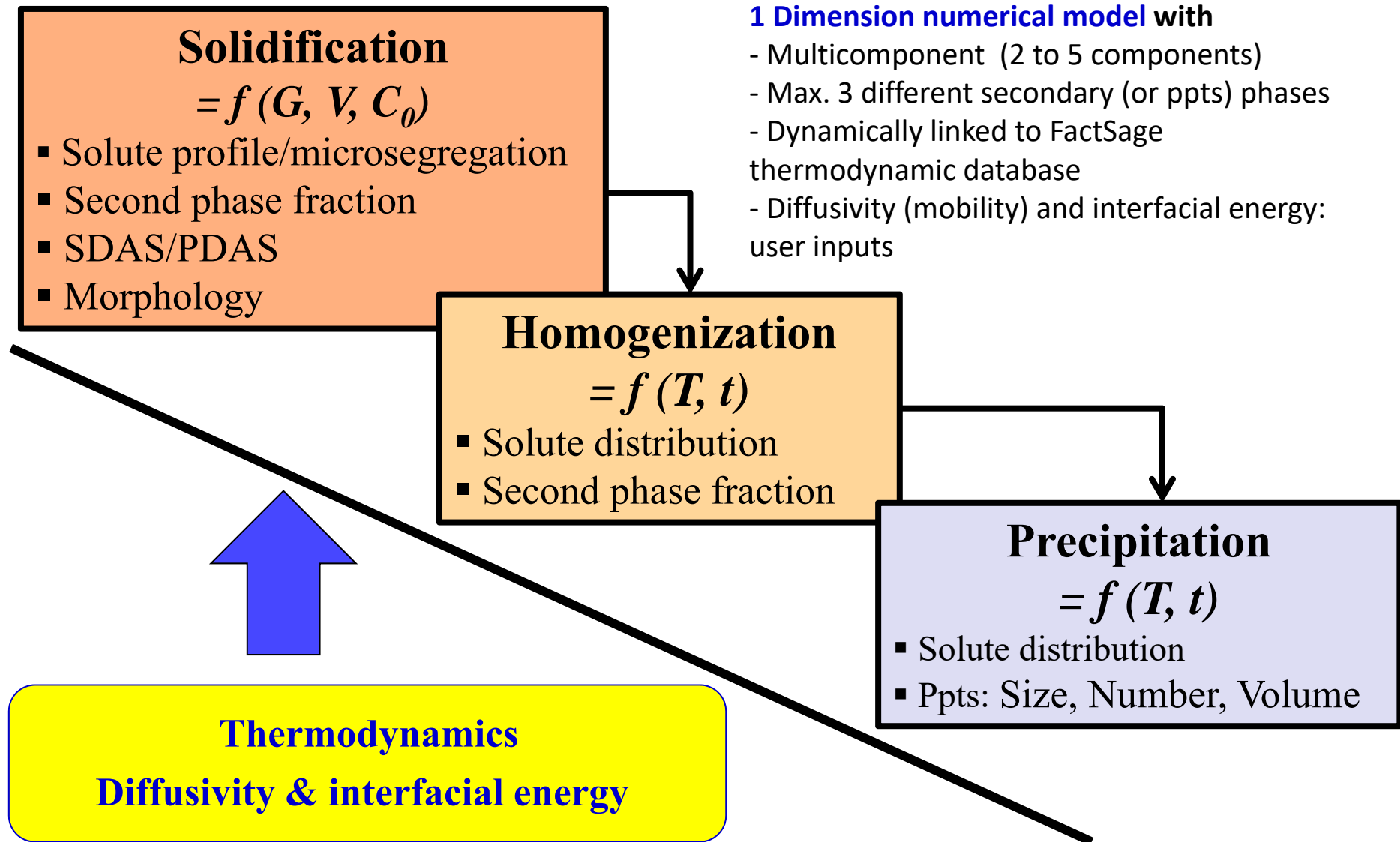
- Calculation of morphology
- Concentration profile (diffusion)
- Long calculation time (~ hours, days)
- Difficulty in Multicomponent system





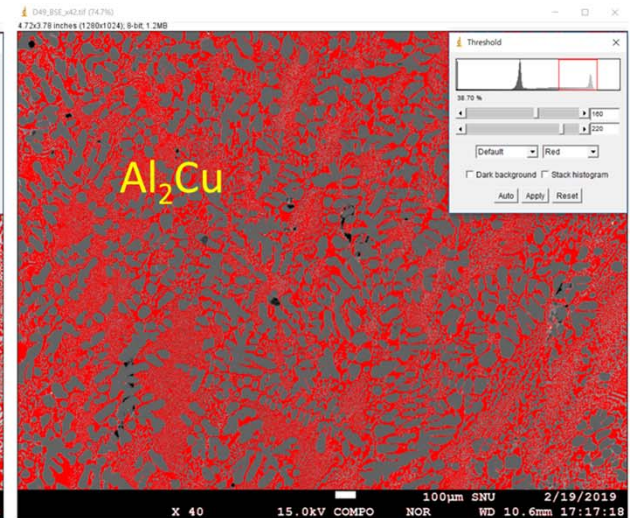
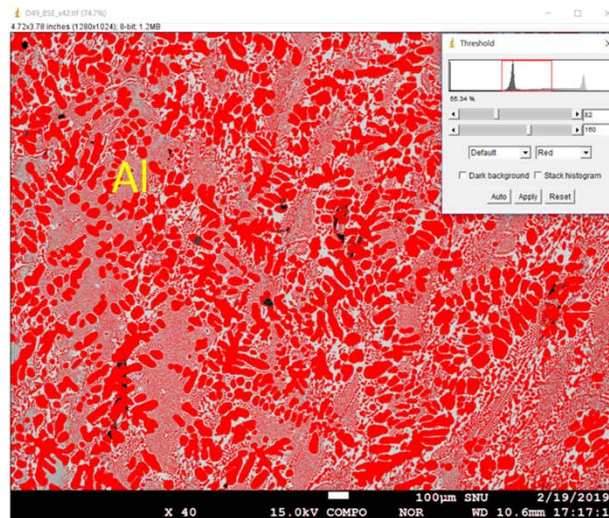
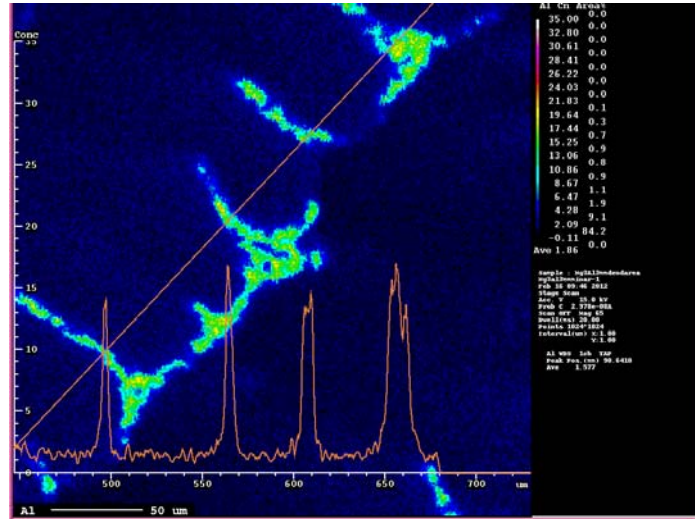
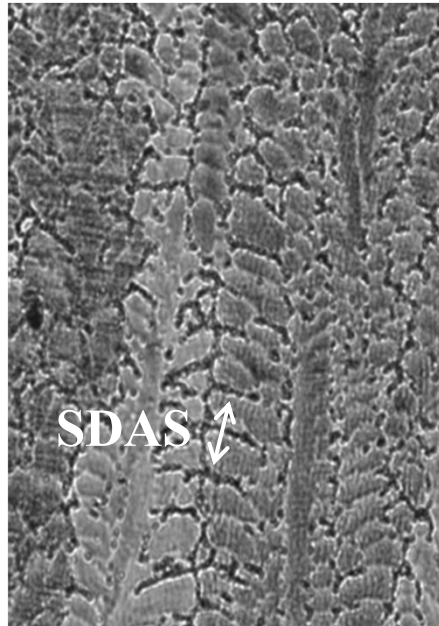
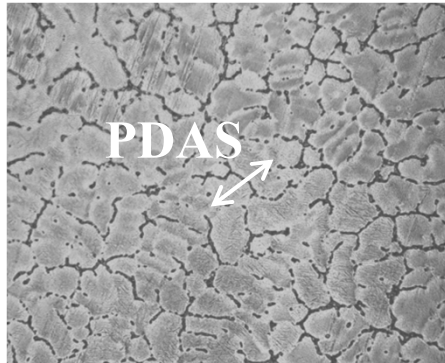
# An Integrated tool for microstructure prediction

9

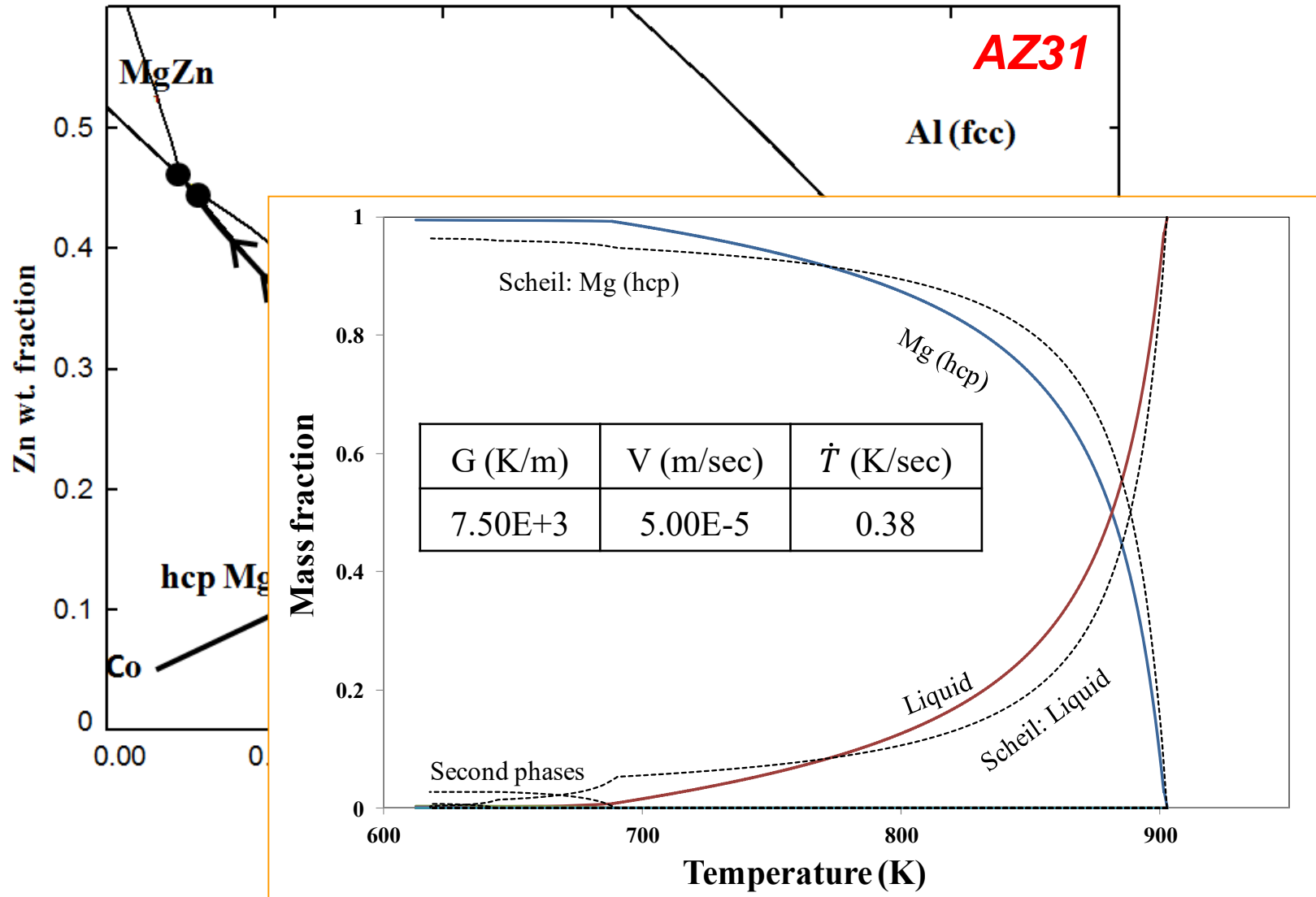


# As-cast microstructure

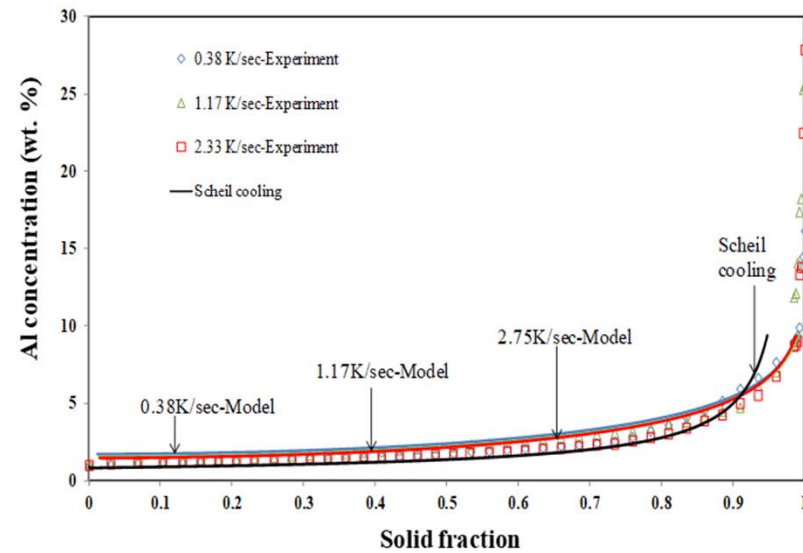
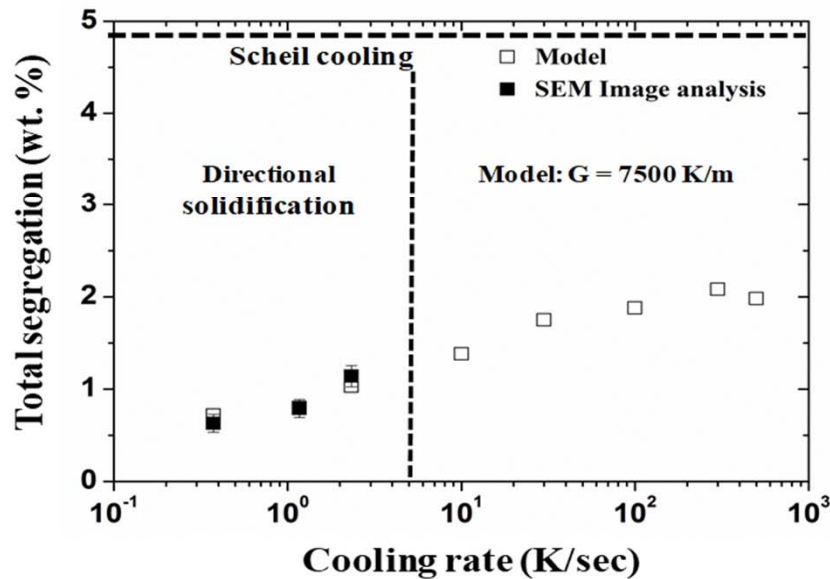
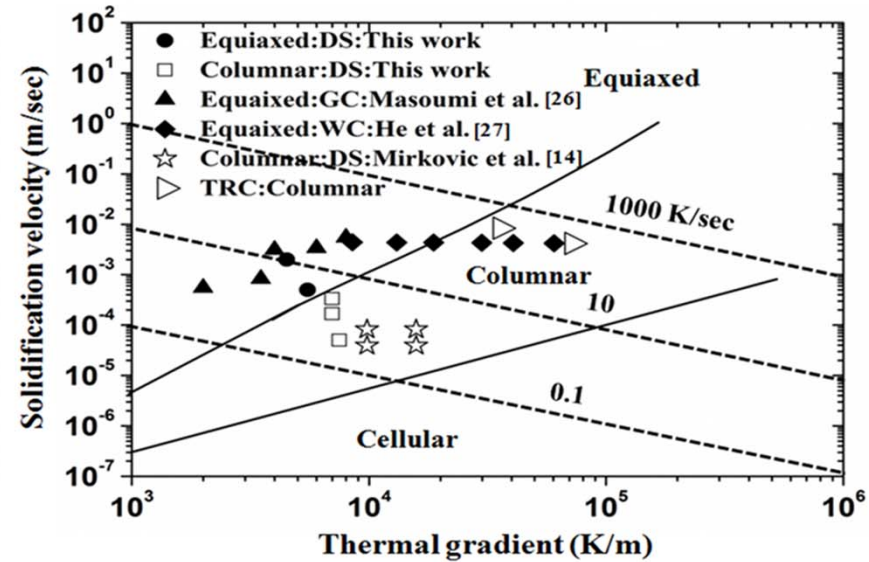
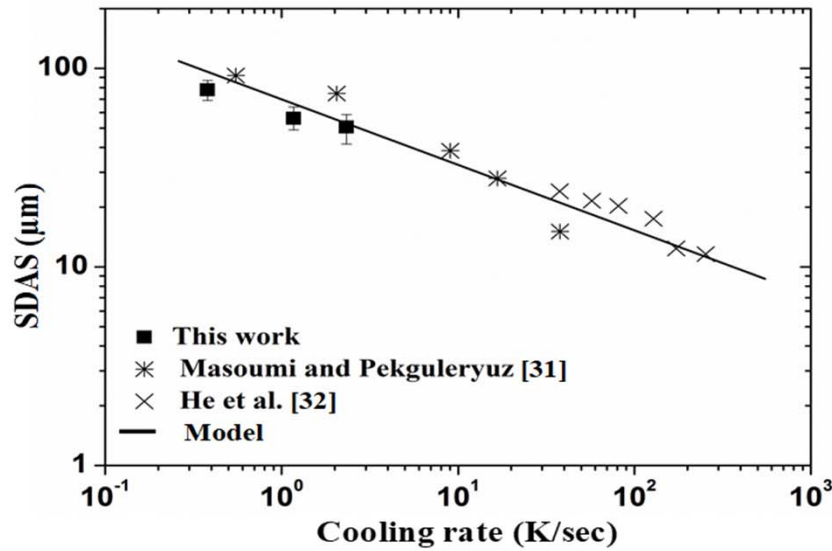
10



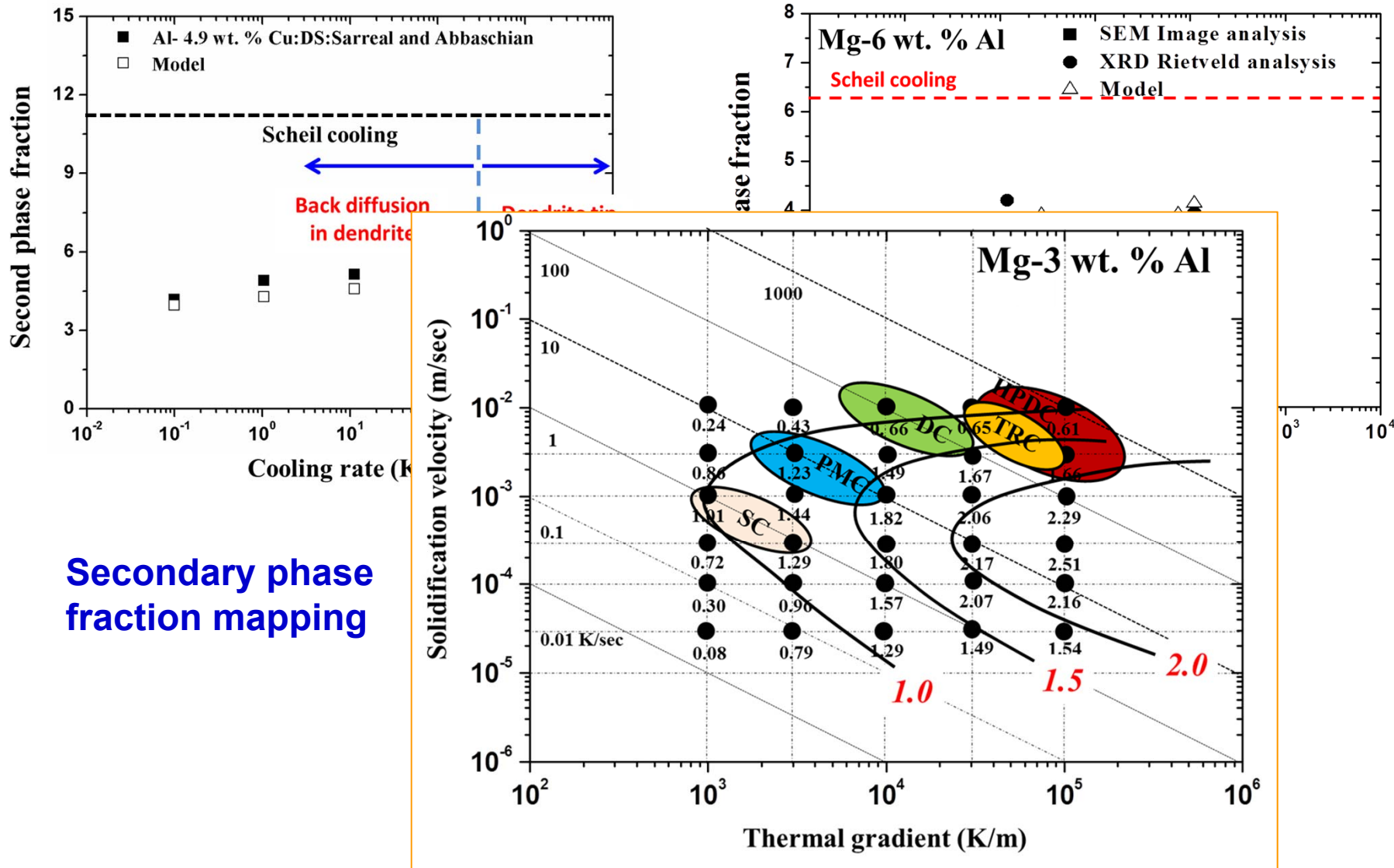
# Some previous results



# Solidification model: AZ31



# Solidification model: Second phase fractions



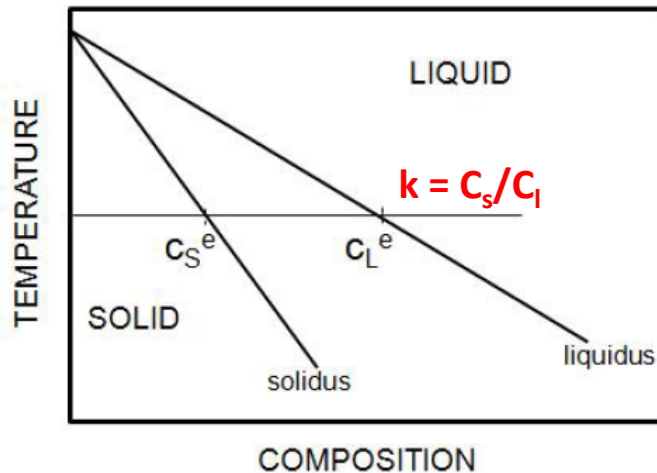
Secondary phase fraction mapping

# Rapid Solidification: Departure from Equilibrium

14

Slow vs Rapid or Equil'm vs Non-equil'm

## Thermodynamics of solidification



Local thermodynamic equilibrium at S/L interface

VS

## Experimental evidences of non-equil'm

TABLE II. Comparison of distribution coefficients under equilibrium ( $k_e$ ) and laser-annealed ( $k'$ ) regrowth conditions.

Dopant	(a) Tetrahedral covalent radius (Å)	(b)		
		$k_e$	$k'$	$\frac{k'}{k_e}$
As	1.18	0.3	1.0	3.3
Sb	1.36	0.023	0.7	30
Bi	1.46	0.0007	0.4	571
Ga	1.26	0.008	0.2	25
In	1.44	0.0004	0.15	375

White et al. Ion implantation followed by laser annealing of solutes in Si

# Theories: Aziz's model for solute trapping

Michael J. Aziz 1981

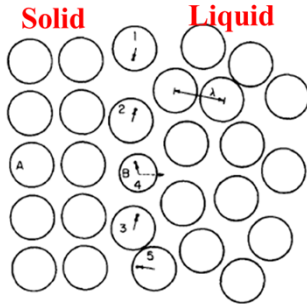


FIG. 1. Choreography of solute trapping.

$$\tau = \frac{\lambda}{v}$$

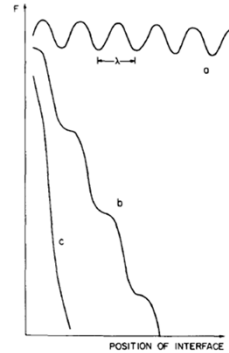


FIG. 2. Free energy of system as a function of interface position. (a) Small driving force, (b) critical driving force, and (c) large driving force.

**Stepwise growth model**  
**Continuous growth model**

Laser melting experiments

Materials	$V_D$ (m/s)
Si-As	0.46
Si-Ge	2.03
Si-Bi	32
Si-Sn	17
Si-Ge	22
Si-In	57
Si-Sb	0.64
Al-Sn	36
Al-In	38
Al-Ge	6.1
Al-Cu	6.7
Ni-Zr	26

$v_d$ : Obtained by fitting solute profile with Aziz's model

Chemical rate theory

Flux balance at interface

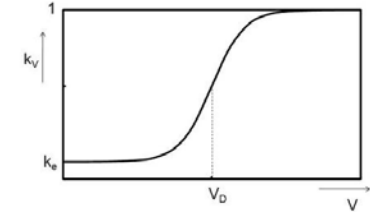
$$k^{non-eqb} = \frac{k + v/v_d}{v/v_d + 1}$$

$v$  = solidification velocity

$v_d = \frac{D}{\lambda}$  = diffusive velocity of a solute atom

$k$  = equilibrium partition coefficient

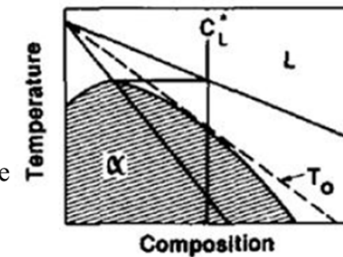
**No dependence on composition**



Boettinger-Coriell-Sekerka 1984

Turnbull's collision limited growth model

The rate at which atoms attach on the solid phase is limited by the rate of collision with the solid phase



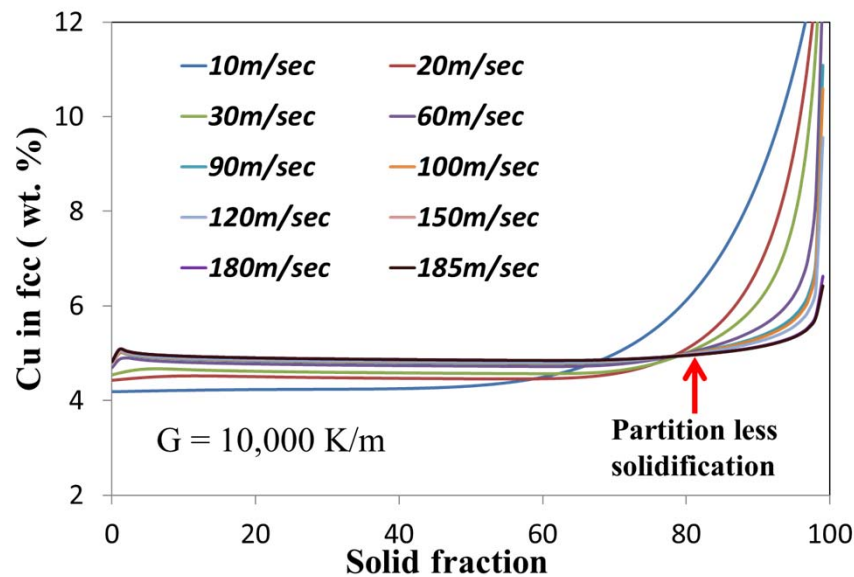
$$m^{non-eqb} = m_e \left( 1 + \frac{k - k^{non-eqbm} \left( 1 - \ln \frac{k^{non-eqbm}}{k} \right)}{1 - k} \right)$$

# Theories: Aziz's model for solute trapping

16

\* Some experimental evidences

Solute distribution: Al- 4.9 wt. % Cu



TOF-SIMS analysis AA2199 alloy

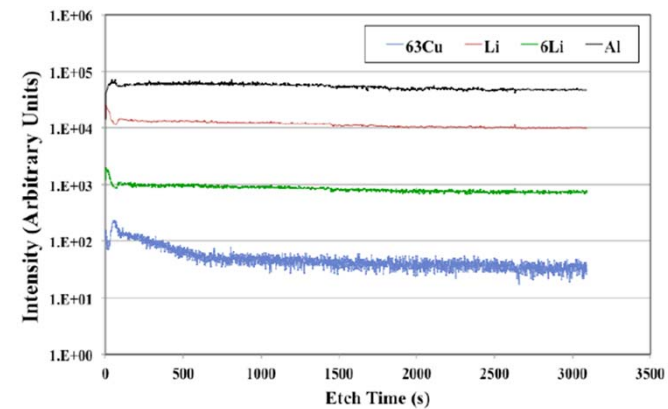
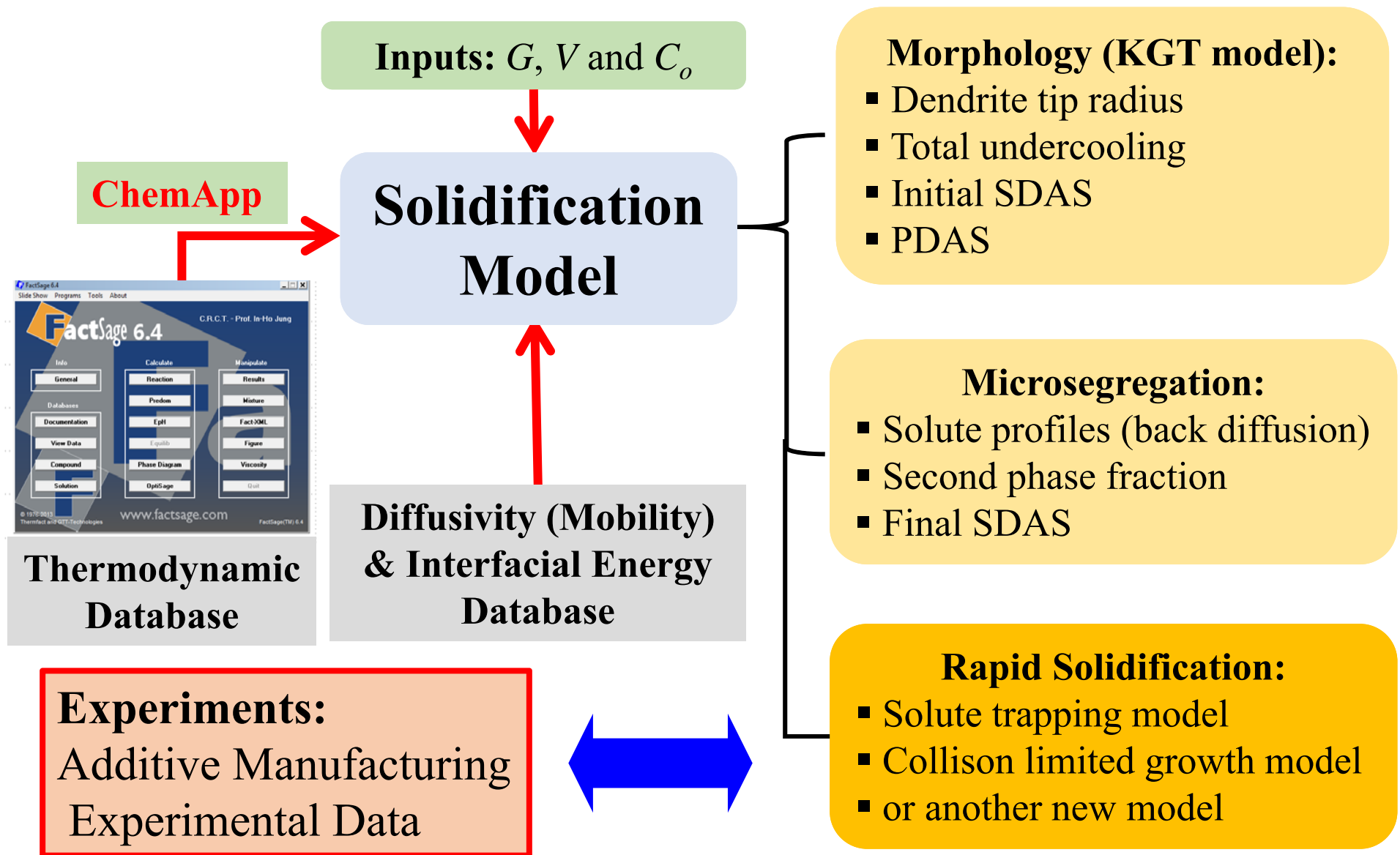


Figure 6-7- TOF-SIMS depth profile revealing homogeneous solute (lithium and copper) distribution.

Phd Thesis Dave Heard, McGill 2013





Thank you for listening!

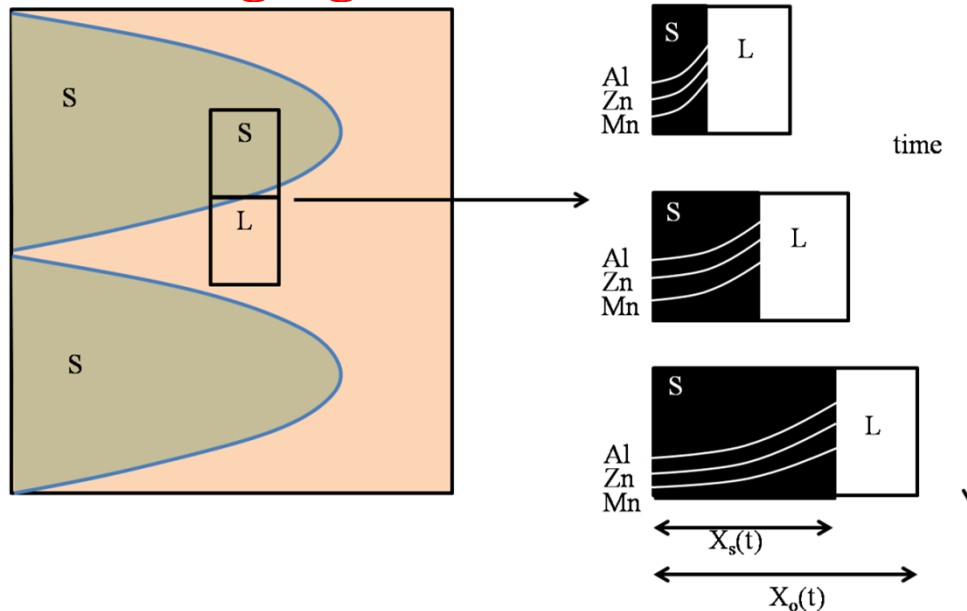
# APPENDIX

# Solidification modeling

## Morphology

Kurz, Giovanola and Trivedi (KGT model)<sup>1</sup>

## Microsegregation



### Back diffusion

$$\frac{\partial C_{si}}{\partial t} = D_{si} \frac{\partial^2 C_{si}}{\partial x^2}$$

### Solute balance

$$\int_0^{X_{si}} C_{si} dx + \int_{X_{si}}^{X_o} C_{li} dx = X_o C_{oi}$$

### Coarsening<sup>2</sup>

$$X_o(t)^3 - X_o(0)^3 = \int_0^t M_i dt$$

Local thermodynamic Equilib  
at solid/liquid interface. (TD database)

$$C_{si} = k_i C_{li}$$

<sup>1</sup>Kurz W, Giovanola B, Trivedi R. Acta Metall. 1986:34:823

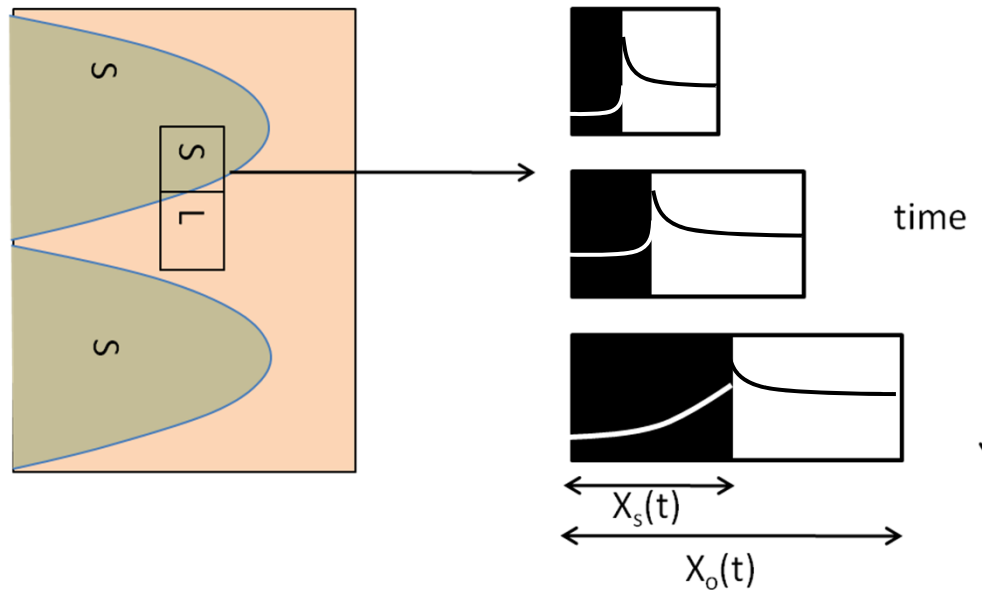
<sup>2</sup>Roosz et al. Mat. Sci. Tech. 1986:2:1149

# Solidification modeling-diffusion in liquid phase

$$\frac{dC_l}{dt} = \frac{cr}{m}$$

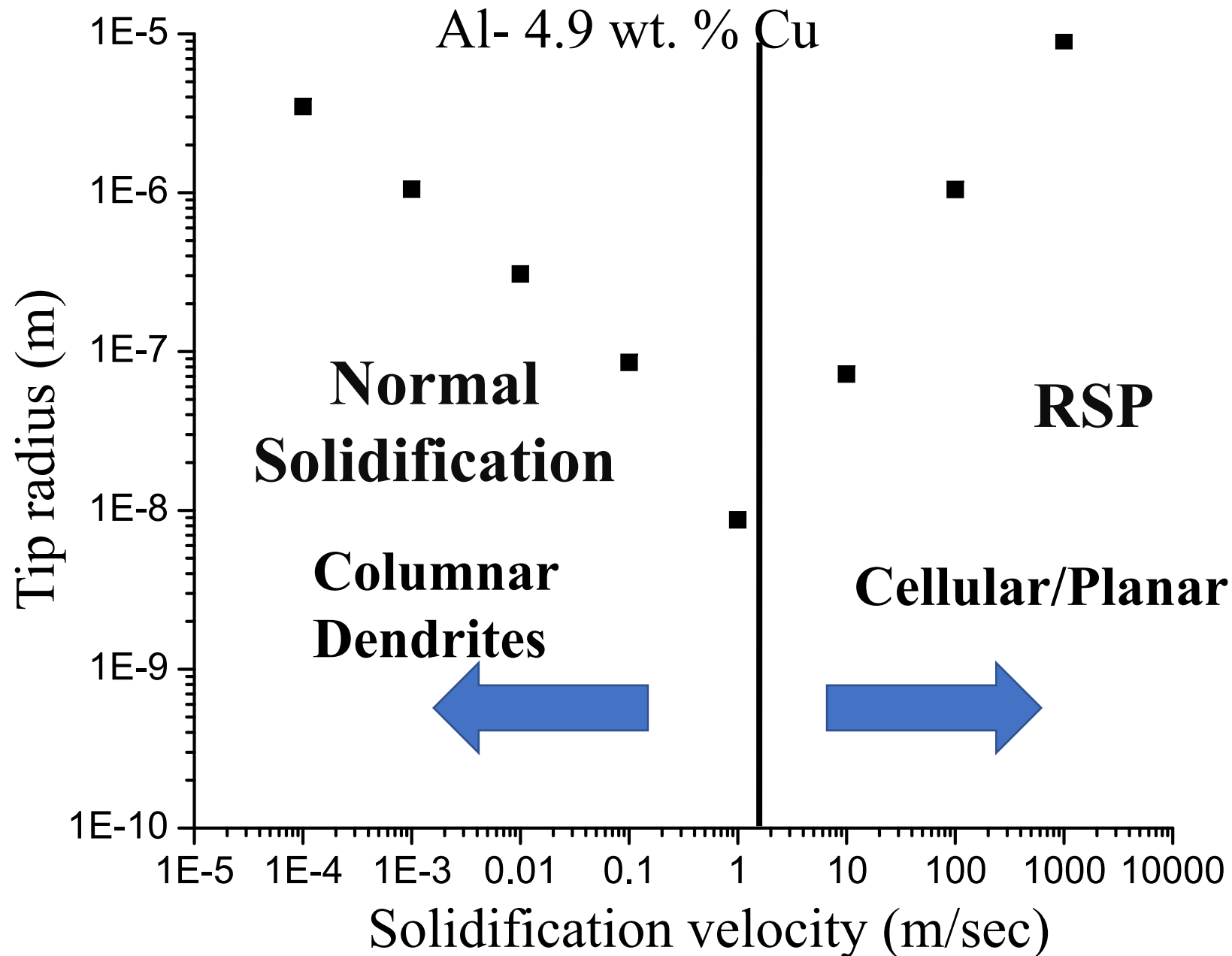
$$\frac{\partial C_s}{\partial t} = D_s \frac{\partial^2 C_s}{\partial x^2}$$

$$\frac{\partial C_l}{\partial t} = D_l \frac{\partial^2 C_l}{\partial x^2}$$



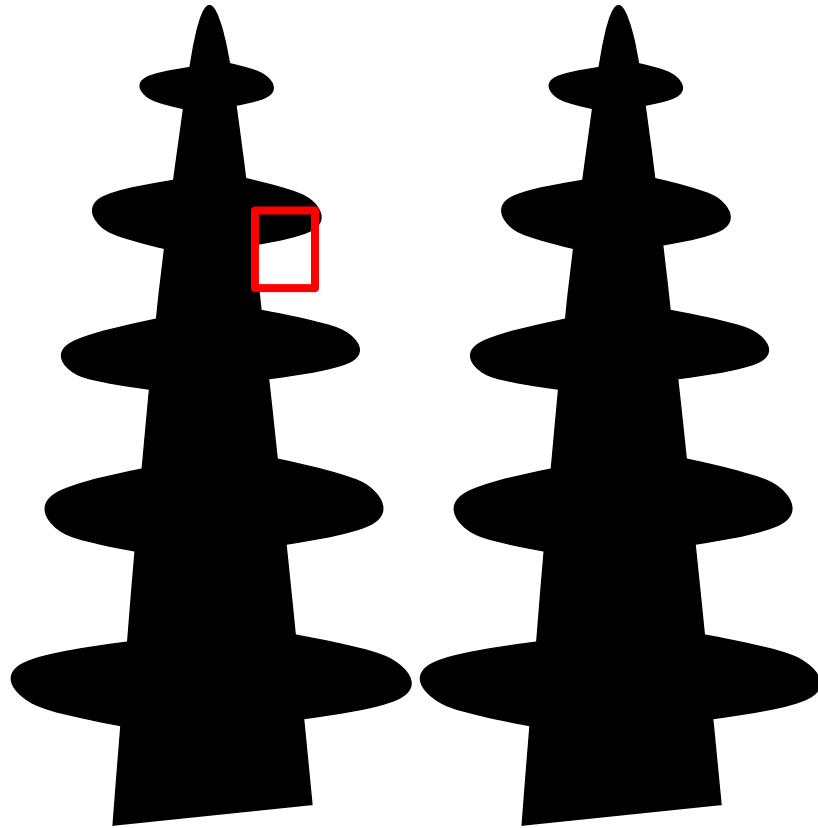
$$x_s^{new} = x_s^{old} + \Delta t \left[ \frac{\left| D_s \frac{\partial C_s}{\partial x} \right|_{x=x_s}^{old} - \left| D_l \frac{\partial C_l}{\partial x} \right|_{x=x_s}^{old} (C_l - C_o) \frac{dx_o}{dt}}{(1-k)C_l} \right]$$

# Solidification modeling-Morphology consideration

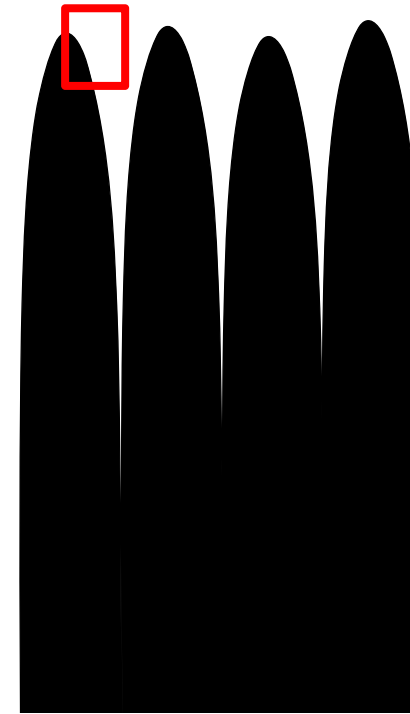


# Solidification modeling-Morphology consideration

---



Columnar dendrite

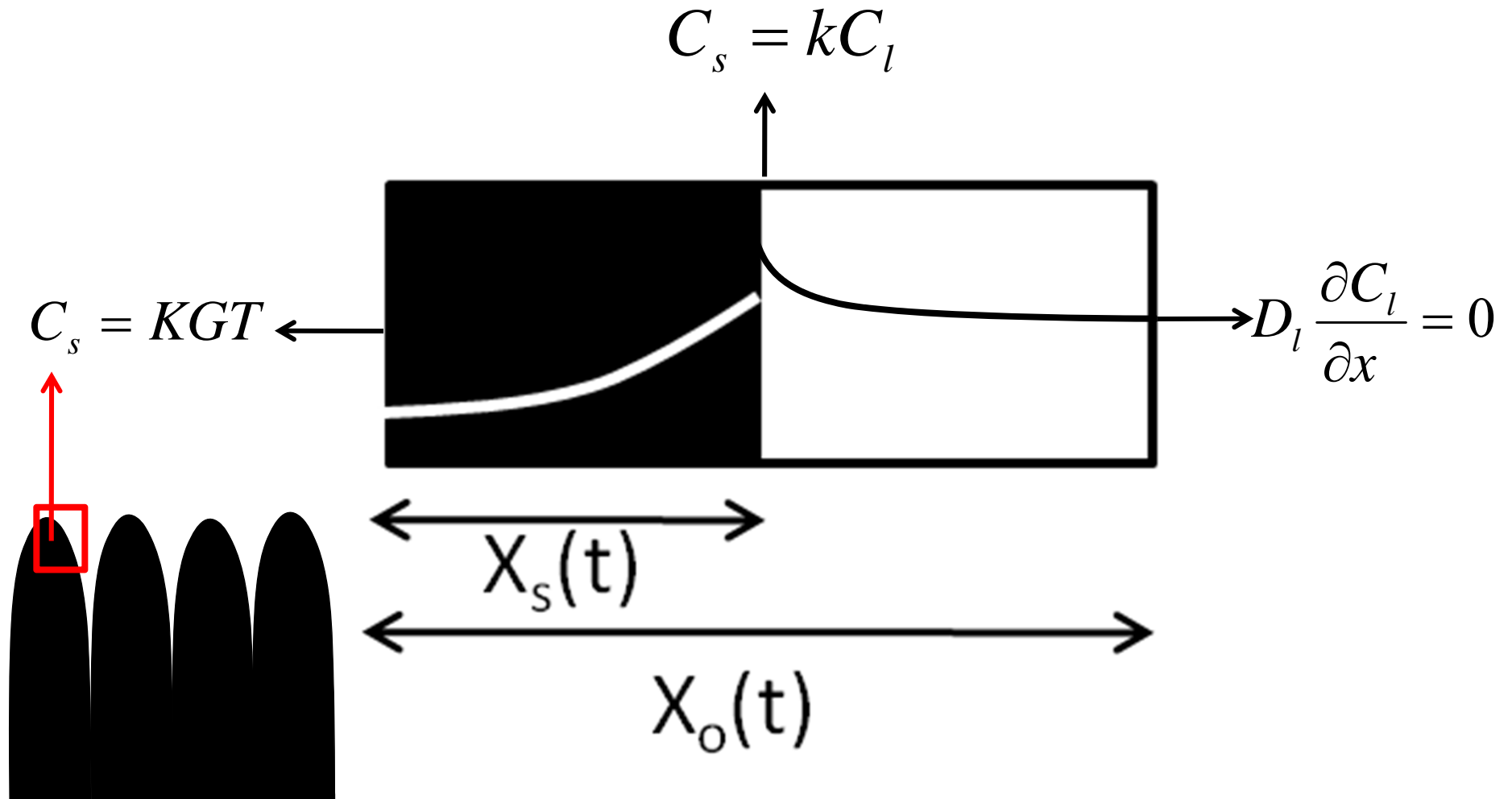


Cellular

**Length scale of the microsegregation calculation changes**

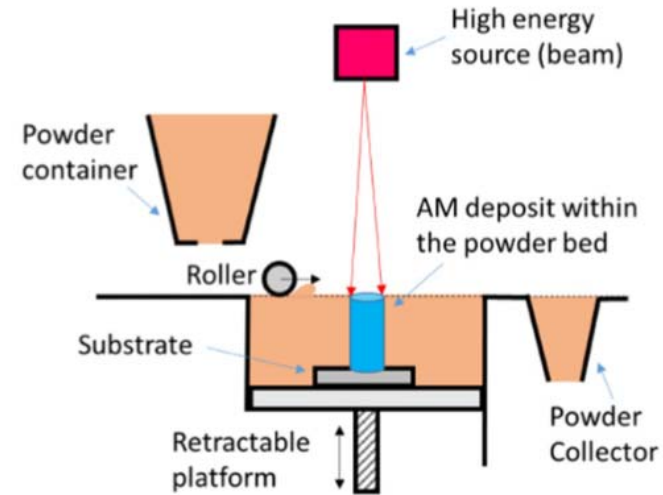
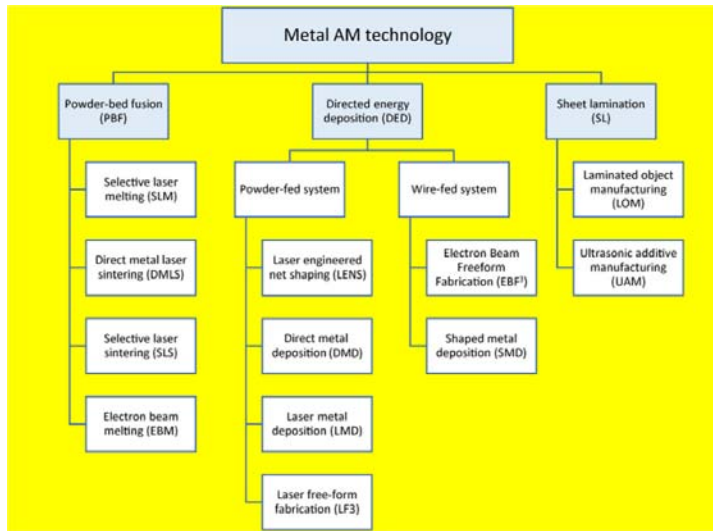
# Solidification model with diffusion ( solid, liquid phases and morphology considerations )

---



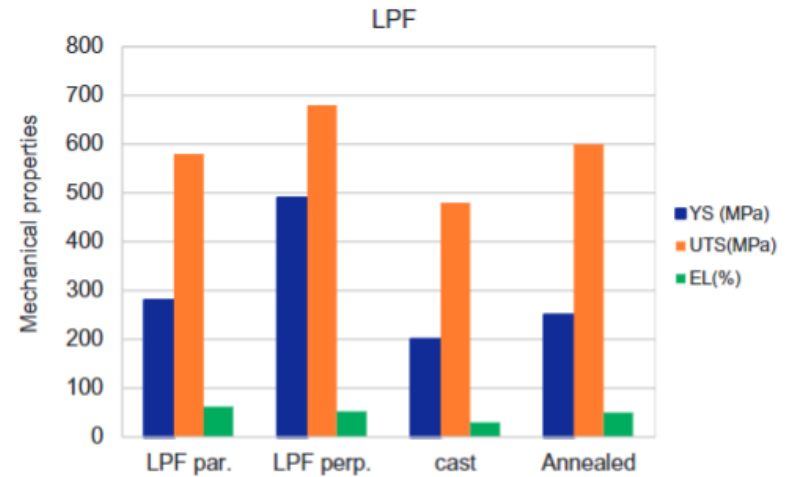
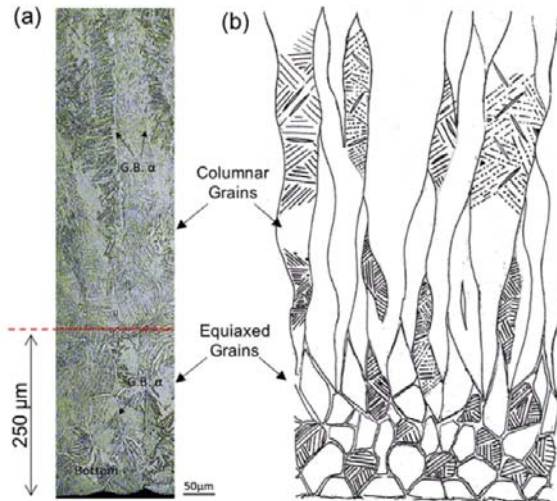


# Additive Manufacturing(AM)?

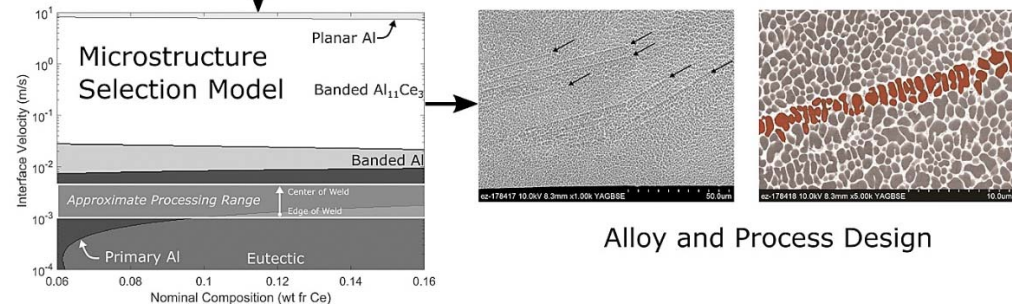
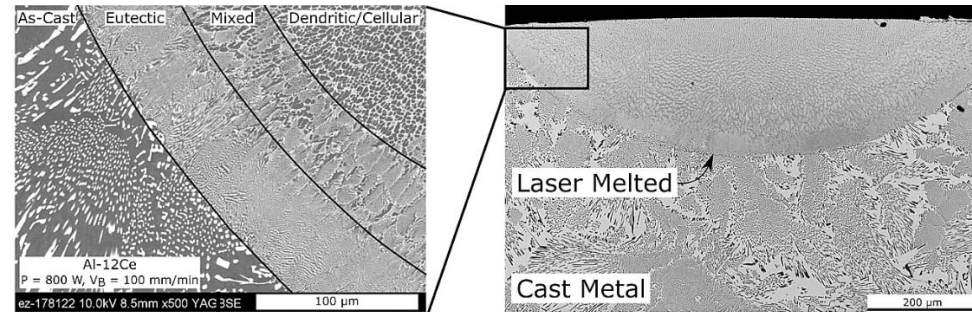
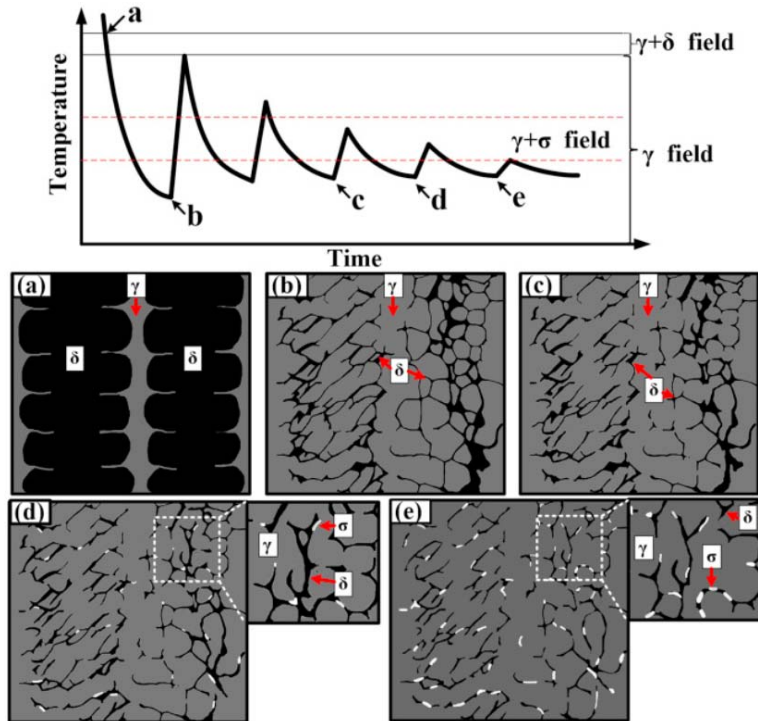


Y. Kok et al. / Materials and Design 139 (2018) 565–586

Equiaxed-to-columnar grain transition



# Additive Manufacturing(AM)?



Alloy and Process Design