

# Real Variance Estimation in Monte Carlo Wielandt Calculations

**Shim, Hyung Jin**

**Nuclear Engineering Department,  
Seoul National University**

- **Based on the presentation at PHYSOR'08 Interlaken, Switzerland**
- **Another Ref.:**  
Hyung Jin Shim and Chang Hyo Kim, "Tally Efficiency Analysis for Monte Carlo Wielandt Method," *Ann. Nucl. Eng.*, 36, 1694-1701 (2009).



# Objectives of This Study

- Recently, the **Monte Carlo (MC) Wielandt method** for the eigenvalue calculations was proposed **to accelerate fission source convergence**. [1]  
( [1] T. Yamamoto and Y. Miyoshi, “Reliable Method for Fission Source Convergence of Monte Carlo Criticality Calculation with Wielandt’s Method,” *J. Nucl. Sci. Technol.* **41**, No. 2, pp. 99~107 (2004). )
- And it was reported that this method has **the potential to eliminate most of the underprediction bias** in confidence intervals for MC eigenvalue calculations. [2]  
( [2] F. Brown, “Wielandt Acceleration for MCNP5 Monte Carlo Eigenvalue Calculations,” Joint International Topical Meeting on Mathematics & Computation and Supercomputing in Nuclear Applications (M&C+SNA 2007), Monterey, CA, April 15-19 (2007). )
- **However, the variance bias or the calculation efficiency using the real variance was not quantitatively evaluated for the MC Wielandt calculations.**
- **The objectives of this paper are**
  - to develop a real variance estimation method for the MC Wielandt calculations and
  - to analyze the efficiency of the MC Wielandt method by the FOM based on the real variance.

# Approaches

- We have ever developed a real variance estimation method by using the inter-cycle correlations of the fission source distribution (FSD) for the conventional MC eigenvalue calculations. [3]

([3] Hyung Jin Shim and Chang Hyo Kim, “Real Variance Estimation Using an Inter-Cycle Fission Source Correlation for Monte Carlo Eigenvalue Calculations,” *Nucl. Sci. Eng.*, 162, 98-108 (2009).)

- **And we found that this method can be readily applicable to the MC Wielandt calculations, even in MC runs with the small number of active cycles.**
- The presentation contents are
  1. introduction to the real variance estimation method using the FSD’s inter-cycle covariance,
  2. derivation of the real variance for the MC Wielandt method,
  3. efficiency analysis of the MC Wielandt method for a very slow convergence problem.

# Variance Bias

- Let us consider an MC eigenvalue calculation based on  $N$  active cycles with  $M$  neutron histories per cycle.
- Suppose that  $Q_j^i$  is the estimate of a tally  $Q$  from the  $j$ -th neutron history at active cycle  $i$ .
- Then the sample variance of the tally mean,  $\bar{Q}$ , is calculated by

$$\sigma_s^2[\bar{Q}] = \frac{1}{NM(NM-1)} \sum_{i=1}^N \sum_{j=1}^M (Q_j^i - \bar{Q})^2, \quad \text{..... (1)}$$

$$\bar{Q} = \frac{1}{NM} \sum_{i=1}^N \sum_{j=1}^M Q_j^i \quad \text{or} \quad \bar{Q} = \frac{1}{N} \sum_{i=1}^N Q^i, \quad Q^i = \frac{1}{M} \sum_{j=1}^M Q_j^i \quad \text{..... (2)}$$

$Q^i$  means the MC estimate of  $Q$  at active cycle  $i$ .

- However,  $\sigma_s^2[\bar{Q}]$  is quite different from its real variance for slow convergence problems or problems with dominance ratios very close to 1.**

$$\boxed{\sigma^2[\bar{Q}] = E[\sigma_s^2[\bar{Q}]] + \text{'Bias'}}$$
..... (3)

$\sigma^2[\bar{Q}]$  denotes the real or true variance.

# Derivation of Variance Bias

- The real or true variance of  $\bar{Q}$  can be written as

$$\begin{aligned}\sigma^2[\bar{Q}] &= E[\bar{Q}^2] - E[\bar{Q}]^2 \\ &= E\left[\left(\frac{1}{NM} \sum_{i=1}^N \sum_{j=1}^M Q_j^i\right)^2\right] - E\left[\frac{1}{NM} \sum_{i=1}^N \sum_{j=1}^M Q_j^i\right]^2 \\ &= \frac{1}{NM} \sigma^2[Q_j^i] + \frac{1}{(NM)^2} \sum_{i,j} \sum_{i',j' \neq i,j} \text{cov}[Q_j^i, Q_{j'}^{i'}] \quad \dots\dots\dots (4)\end{aligned}$$

- On the other hand, the apparent variance of  $Q$  is defined as the expected value of the sample variance.

$$\sigma_A^2[\bar{Q}] = E[\sigma_S^2[\bar{Q}]] \quad \dots\dots\dots (5)$$

- As Ueki et al. [4] derived the relation between the real variance and the apparent variance of the eigenvalue  $k$ , the variance bias of  $\sigma_S^2[\bar{Q}]$  can be quantified as

$$\sigma^2[\bar{Q}] - \sigma_A^2[\bar{Q}] = \frac{1}{N(N-1/M)} \sum_{l=1}^{N-1} (N-l) \text{cov}[Q^j, Q^{j+l}] \quad \dots\dots\dots (6)$$

( [4] T. Ueki et al, "Error Estimations and Their Biases in Monte Carlo Eigenvalue Calculations," *Nucl. Sci. Eng.*, **125**, 1 (1997). )

## Relation Betw. FSD and Tally

- The tally  $Q$  is calculated by using the corresponding detector response in the MC simulation as follows:

where

$$Q = \mathbf{R}^Q S \quad \text{..... (7)}$$

$$\mathbf{R}^Q S = \int dP R^Q(P) S(P) \quad \text{..... (8)}$$

$$R^Q(P) \equiv \sum_{j=0}^{\infty} \int_{\chi} dP'' g(P'') \int dP' K_j(P' \rightarrow P'') T(P \rightarrow P') \quad \text{..... (9)}$$

$$P \equiv (\mathbf{r}, E, \boldsymbol{\Omega}),$$

$g(P)$  = response function for the tally  $Q$  at  $P$ ,

$$K_0(P' \rightarrow P) = \delta(P' - P),$$

$$K_j(P' \rightarrow P) = \int dP_1 \cdots \int dP_{j-1} K(P_{j-1} \rightarrow P) \cdots K(P' \rightarrow P_1),$$

$$K(P' \rightarrow P) \equiv C(\mathbf{r}'; E', \boldsymbol{\Omega}' \rightarrow E, \boldsymbol{\Omega}) T(E, \boldsymbol{\Omega}; \mathbf{r}' \rightarrow \mathbf{r}) = \text{transport kernel}$$

$$S(P) = \text{fission source distribution.}$$

- $R^Q(P)$  means a  $Q$  contribution from the unit fission source generated at  $P$ .

# How to Quantify Tally's Inter-cycle Covariance

- Because a finite number of histories is simulated,  $R^Q(P)$  and  $S(P)$  in Eq. (8) cannot be measured in a continuous form. Therefore, one may divide the whole region into small nonoverlapping cells with a spatial volume,  $V_m$  ( $m = 1, 2, \dots, N_m$ ), and define their cell-wise discrete functions.
- Then Eq. (7) can be described in a discrete form:

$$Q = \sum_m^{N_m} R_m^Q S_m \quad \text{----- (10)}$$

$$S_m = \int_{V_m} \int_E \int_{\Omega} S(\mathbf{r}, E, \Omega) d\mathbf{r} dE d\Omega = \int_{V_m} S(P) dP$$

$$R_m^Q = \int_{V_m} R^Q(P) S(P) dP / \int_{V_m} S(P) dP$$

- From the definition of covariance, tally's inter-cycle covariance can be written as

$$\begin{aligned} \text{cov}[Q^i, Q^{i+l}] &= E \left[ \left( \sum_{m=1}^{N_m} R_m S_m^i - \sum_{m=1}^{N_m} R_m E[S_m] \right) \left( \sum_{m'=1}^{N_m} R_{m'} S_{m'}^{i+l} - \sum_{m'=1}^{N_m} R_{m'} E[S_{m'}] \right) \right] \\ &= \sum_{m=1}^{N_m} \sum_{m'=1}^{N_m} R_m R_{m'} \text{cov}[S_m^i, S_{m'}^{i+l}] \quad \text{----- (11)} \end{aligned}$$

# How to Quantify FSD's Inter-cycle Covariance

- By the cycle-by-cycle error propagation model [5] and the direct posterior estimation method for the stochastic error's covariance [6],  $\text{cov}[S_m^i, S_{m'}^{i+l}]$  of Eq. (11) can be expressed as

$$\begin{aligned} \text{cov}[S_m^i, S_{m'}^{i+l}] &= \sum_{i'=0}^{\infty} \sum_{n=1}^{N_m} \sum_{n'=1}^{N_m} a_{mn}^{i'} a_{m'n'}^{i'+l} \text{cov}[\varepsilon_n, \varepsilon_{n'}] \\ &= \frac{1}{M} \sum_{i'=0}^{\infty} \sum_{n=1}^{N_m} \sum_{n'=1}^{N_m} a_{mn}^{i'} a_{m'n'}^{i'+l} \text{cov}[\varepsilon_{n,j}, \varepsilon_{n',j}] \end{aligned} \quad \text{----- (12)}$$

$$\text{cov}[\varepsilon_{n,j}, \varepsilon_{n',j}] = E\left[\left(S_{n,j}^i - E[S_n^i | \mathbf{S}^{i-1}]\right) \cdot \left(S_{n',j}^i - E[S_{n'}^i | \mathbf{S}^{i-1}]\right)\right] \quad \text{----- (13)}$$

$a_{mn}^j$  is  $m$ -th row and  $n$ -th column element of the matrix  $\mathbf{A}^j$  and the matrix  $\mathbf{A}$  is defined by

$$\mathbf{A} = \frac{1}{k_0} (\mathbf{H} - \mathbf{S}_0 \cdot \boldsymbol{\tau}^T \cdot \mathbf{H}), \quad \text{----- (14)}$$

$\boldsymbol{\tau} = N_m$  dimensional row vector  $(1, 1, \dots, 1)$ ,  $\mathbf{H}$  = fission matrix,

$\mathbf{S}_0$  = main mode fission source distribution,  $k_0$  = main mode eigenvalue.

( [5] E. M. Gelbard and R. E. Prael, "Monte Carlo Work at Argonne National Laboratory, ANL-75-2(NEACRP-L-118) (1974).

( [6] H. J. Shim and C. H. Kim, "Stopping Criteria of Inactive Cycle Monte Carlo Calculations," *Nucl. Sci. Eng.*, **157**, pp.132-141 (2007). )



# Transport Equation

- The time-independent Boltzmann transport equation for neutrons can be written in operator notation as

$$\mathbf{T} \psi = \frac{1}{k} \mathbf{F} \psi \quad \text{----- (15)}$$

where

$$\mathbf{T} \psi = [\boldsymbol{\Omega} \cdot \nabla + \Sigma_t(\mathbf{r}, E)] \psi(\mathbf{r}, E, \boldsymbol{\Omega}) - \int dE' \int d\boldsymbol{\Omega}' \Sigma_s(\mathbf{r}; E', \boldsymbol{\Omega}' \rightarrow E, \boldsymbol{\Omega}) \psi(\mathbf{r}, E', \boldsymbol{\Omega}') \quad \text{----- (16)}$$

$$\mathbf{F} \psi = \frac{\chi(E)}{4\pi} \int dE' \int d\boldsymbol{\Omega}' \nu(E') \Sigma_f(\mathbf{r}, E') \psi(\mathbf{r}, E', \boldsymbol{\Omega}') \quad \text{----- (17)}$$

$\Sigma_t(\mathbf{r}, E)$  = total cross section

$\Sigma_s(\mathbf{r}; E', \boldsymbol{\Omega}' \rightarrow E, \boldsymbol{\Omega})$  = scattering cross section from  $E', \boldsymbol{\Omega}'$  to  $E, \boldsymbol{\Omega}$

$\chi(E)$  = fission spectrum

$\nu(E')$  = mean number of fission neutrons produced in a fission

$\Sigma_f(\mathbf{r}, E')$  = fission cross section

$k$  = multiplication factor

# Conventional MC Power Method

- By inverting  $\mathbf{T}$  and operating with  $\mathbf{F}$  on both sides of Eq. (15), we obtain the following form

$$\mathbf{F}\psi = \frac{1}{k} [\mathbf{F}\mathbf{T}^{-1}] \mathbf{F}\psi \quad \text{..... (18)}$$

- And the FSD,  $S$  and fission operator,  $\mathbf{H}$  are defined as follows

$$S = \mathbf{F}\psi \quad \text{..... (19)}$$

$$\mathbf{H} = \mathbf{F}\mathbf{T}^{-1} \quad \text{..... (20)}$$

- The fission operator  $\mathbf{H}(\mathbf{r}', E', \boldsymbol{\Omega}' \rightarrow \mathbf{r}, E, \boldsymbol{\Omega})$  denotes the number of first-generation fission neutrons born per unit volume about  $(\mathbf{r}, E, \boldsymbol{\Omega})$ , due to a parent neutron born per unit volume at  $(\mathbf{r}', E', \boldsymbol{\Omega}')$ .
- Inserting Eqs. (19) and (20) into Eq. (18) leads the following eigenvalue equation

$$S = \frac{1}{k} \mathbf{H}S \quad \text{..... (21)}$$

- In the conventional MC eigenvalue calculations, the FSD is iteratively updated as

$$S^i = \frac{1}{k^{i-1}} \mathbf{H}S^{i-1} + \varepsilon^i \quad \text{..... (22)}$$

# MC Wielandt Method

- The Wielandt method is characterized by rewriting Eq. (15) as

$$\mathbf{T}\psi - \frac{1}{k_e}\mathbf{F}\psi = \left(\frac{1}{k} - \frac{1}{k_e}\right)\mathbf{F}\psi \quad \text{..... (23)}$$

$k_e$  is an estimated eigenvalue.

- By inverting  $(\mathbf{T} - \mathbf{F}/k_e)$  and operating with  $\mathbf{F}$  on both sides of Eq. (23), we obtain the following equation

$$\mathbf{F}\psi = \left(\frac{1}{k} - \frac{1}{k_e}\right) \left[ \mathbf{F} \left( \mathbf{M} - \frac{1}{k_e}\mathbf{F} \right)^{-1} \right] \mathbf{F}\psi \quad \text{..... (24)}$$

- Inserting Eq. (19) into Eq. (24) leads the following eigenvalue equation

$$S = \left(\frac{1}{k} - \frac{1}{k_e}\right) \mathbf{H}'S \quad \text{..... (25)} \quad \mathbf{H}' = \mathbf{F} \left( \mathbf{M} - \frac{1}{k_e}\mathbf{F} \right)^{-1} \quad \text{..... (26)}$$

- Applying the power method to Eq. (25), the FSD is updated iteratively in the Wielandt method as

$$S^i = \left(\frac{1}{k^{i-1}} - \frac{1}{k_e}\right) \mathbf{H}'S^{i-1} + \varepsilon^i \quad \text{..... (27)}$$

## Algorithm for MC Wielandt Method (1/2)

- Using Eq. (20), the fission operator  $\mathbf{H}'$  in the Wielandt's method can be expressed as

$$\begin{aligned}\mathbf{H}' &= \mathbf{F} \left[ \mathbf{M} - \frac{1}{k_e} \mathbf{F} \right]^{-1} = \mathbf{F} \left[ \mathbf{M} - \frac{1}{k_e} \mathbf{H} \mathbf{M} \right]^{-1} = \mathbf{F} \left[ \left( \mathbf{I} - \frac{\mathbf{H}}{k_e} \right) \mathbf{M} \right]^{-1} = \mathbf{F} \mathbf{M}^{-1} \left( \mathbf{I} - \frac{\mathbf{H}}{k_e} \right)^{-1} \\ &= \mathbf{H} \left( \mathbf{I} - \frac{\mathbf{H}}{k_e} \right)^{-1}\end{aligned}\quad \text{..... (28)}$$

- By the Taylor's series expansion,  $\left( \mathbf{I} - \mathbf{H}/k_e \right)^{-1}$  in Eq. (28) can be written as

$$\left( \mathbf{I} - \frac{\mathbf{H}}{k_e} \right)^{-1} = \mathbf{I} + \frac{\mathbf{H}}{k_e} + \left( \frac{\mathbf{H}}{k_e} \right)^2 + \dots \quad \text{..... (29)}$$

- Inserting Eq. (29) into Eq. (28) leads to

$$\mathbf{H}' = \mathbf{H} \left( \mathbf{I} + \frac{\mathbf{H}}{k_e} + \left( \frac{\mathbf{H}}{k_e} \right)^2 + \dots \right) \quad \text{..... (30)}$$

## Algorithm for MC Wielandt Method (2/2)

- Substitution of Eq. (30) into Eq. (27) leads

$$\begin{aligned}
 S^i = & \left( \frac{1}{k^{i-1}} - \frac{1}{k_e} \right) \mathbf{H} S^{i-1} + \left( \frac{1}{k^{i-1}} - \frac{1}{k_e} \right) \mathbf{H} \left( \left( \frac{\mathbf{H}}{k_e} \right) S^{i-1} \right) \\
 & + \left( \frac{1}{k^{i-1}} - \frac{1}{k_e} \right) \mathbf{H} \left( \left( \frac{\mathbf{H}}{k_e} \right)^2 S^{i-1} \right) + \dots + \varepsilon^i \quad \text{..... (31)}
 \end{aligned}$$

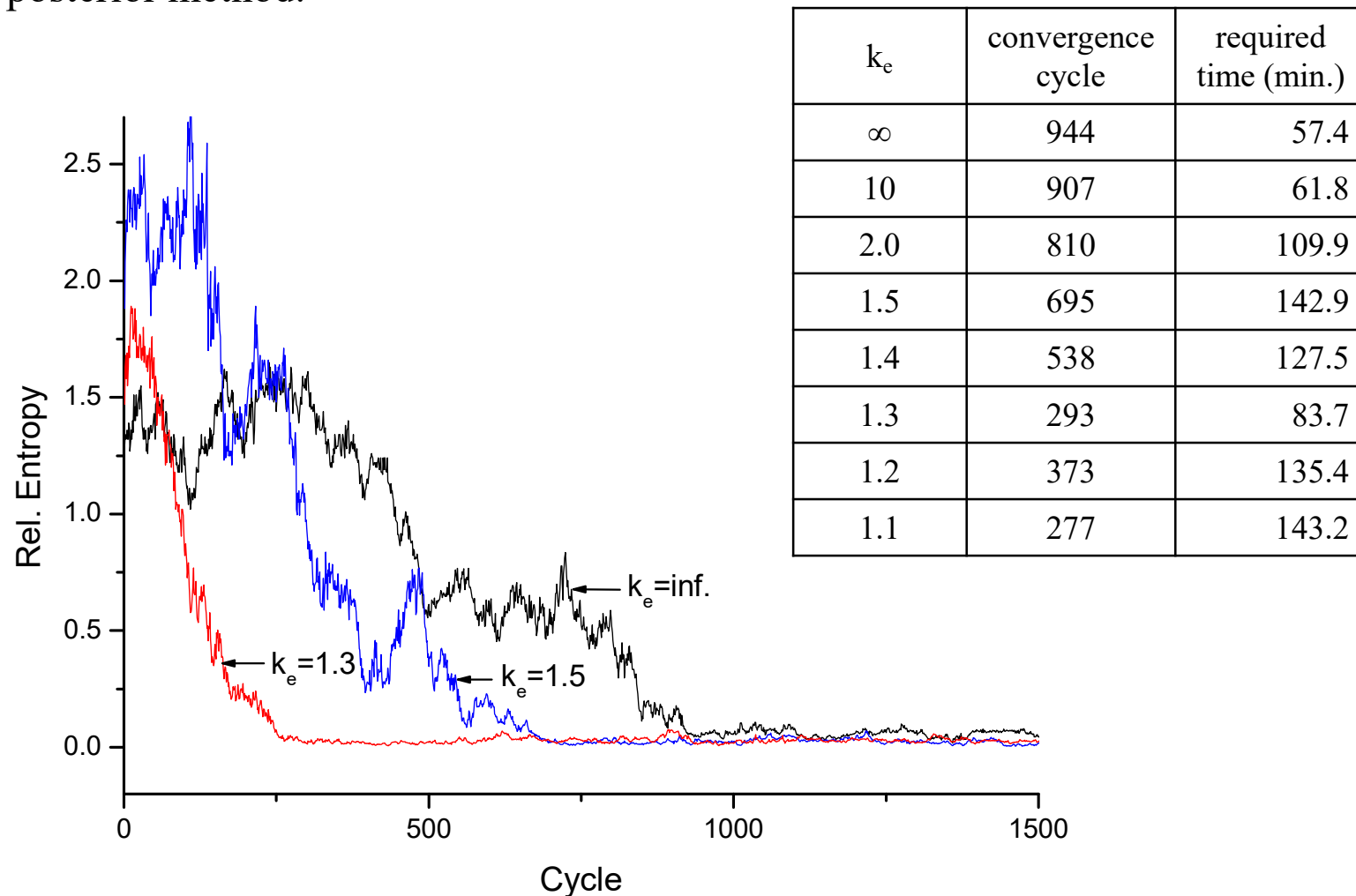
- The first term in the RHS of Eq. (31) means the number of first next-cycle fission sites generated from  $S^{i-1}$ . From comparing this term with the RHS of Eq. (22), one can see that it is less by as much as  $\mathbf{H} S^{i-1} / k_e$ . And these fission sources of  $\mathbf{H} S^{i-1} / k_e$  generate the second next-cycle fission sites as much as the second term in the RHS of Eq. (31).
- In the same way, the next-cycle fission sites from all the generations are sampled. This process is exactly the same as the algorithm described in Ref. [1].  
( [1] T. Yamamoto and Y. Miyoshi, "Reliable Method for Fission Source Convergence of Monte Carlo Criticality Calculation with Wielandt's Method," J. Nucl. Sci. Technol., v. 41, n. 2, pp. 99~107 (2004). )

# Real Variance Estimation In MC Wielandt Calculations

- The sample variance of a tallied nuclear parameter or a tally in the MC Wielandt calculations must be biased because of inter-cycle correlations of FSD by Eq. (27).
- From comparing Eq. (27) with Eq. (22), we can see that the only difference is the change from the operator  $\mathbf{H}$  into  $\mathbf{H}'$ .
- Therefore the real variance estimation method using FSD's inter-cycle correlation can be directly applied to the MC Wielandt calculations by changing  $\mathbf{H}$  into  $\mathbf{H}'$ .

# Results of Source Convergence

- Cycle number of the fission source convergence were diagnosed by the Ueki's posterior method.



# Application Results of the IAEA Source Conv. Problem #1 ( 10,000 histories X 1,000 active cycles )

$k_e$	CPU Time (min.)	power	sample variance		estimated real variance	
			$R$	FOM	$R$	FOM
(1,3) Assembly						
$\infty$	128	5.38E-04	0.00080	12204.17	0.10200	0.75
10.0	142	6.42E-04	0.00073	13186.95	0.05566	2.27
2.0	279	6.36E-04	0.00070	7318.43	0.04230	2.00
1.5	421	6.41E-04	0.00073	4456.24	0.03673	1.76
1.4	484	6.34E-04	0.00075	3676.01	0.03411	1.78
1.3	581	6.54E-04	0.00076	2979.90	0.02930	2.01
1.2	734	6.54E-04	0.00081	2075.54	0.02801	1.74
1.1	1046	6.46E-04	0.00094	1081.90	0.02160	2.05
(3,3) Assembly						
$\infty$	128	1.55E-04	0.00158	3128.77	0.08420	1.10
10.0	142	1.85E-04	0.00144	3388.95	0.07174	1.37
2.0	279	1.65E-04	0.00145	1705.60	0.05005	1.43
1.5	421	1.66E-04	0.00150	1055.44	0.03806	1.64
1.4	484	1.70E-04	0.00151	906.87	0.03629	1.57
1.3	581	1.56E-04	0.00162	655.84	0.03281	1.60
1.2	734	1.52E-04	0.00171	465.70	0.02878	1.64
1.1	1046	1.64E-04	0.00183	285.46	0.02301	1.81



# Application Results of the IAEA Source Conv. Problem #1 ( 100,000 histories X 1,000 active cycles )

$k_e$	CPU Time (min.)	power	sample variance		estimated real variance	
			$R$	FOM	$R$	FOM
(1,3) Assembly						
$\infty$	1253	6.41E-04	0.00023	15082.05	0.02034	1.93
10.0	1395	6.56E-04	0.00023	13548.18	0.01803	2.20
2.0	2774	6.65E-04	0.00021	8174.50	0.01251	2.30
1.5	4215	6.62E-04	0.00023	4484.60	0.01055	2.13
1.4	4859	6.61E-04	0.00023	3890.80	0.00963	2.22
1.3	5824	6.57E-04	0.00024	2981.21	0.00900	2.12
1.2	7430	6.50E-04	0.00026	1991.06	0.00815	2.03
1.1	10591	6.55E-04	0.00029	1122.66	0.00680	2.04
(3,3) Assembly						
$\infty$	1253	1.59E-04	0.00049	3322.95	0.02374	1.42
10.0	1395	1.62E-04	0.00049	2985.00	0.02194	1.49
2.0	2774	1.61E-04	0.00047	1631.94	0.01523	1.55
1.5	4215	1.61E-04	0.00048	1029.67	0.01231	1.57
1.4	4859	1.59E-04	0.00049	857.24	0.01139	1.59
1.3	5824	1.60E-04	0.00050	686.87	0.01030	1.62
1.2	7430	1.61E-04	0.00053	479.16	0.00902	1.65
1.1	10591	1.62E-04	0.00058	280.67	0.00741	1.72

# Conclusion

- A variance-bias estimation method using an inter-cycle FSD's correlation in the conventional MC eigenvalue calculations is applied to the MC Wielandt calculations.
- **From the FOM's based on the estimated real variance for the slow-convergence benchmark problem, it was shown that the tally efficiency is enhanced by the MC Wielandt calculations.**