

Variational Principle

❖ Vectorial Approach

$$\vec{F} = m\vec{a}$$

❖ Energy or Variational Approach

- scalars
- governing principle
- correct condition is defined by

$$\delta(\text{scalar}) = 0, \text{stationary}$$

- integral

❖ Calculus of variation

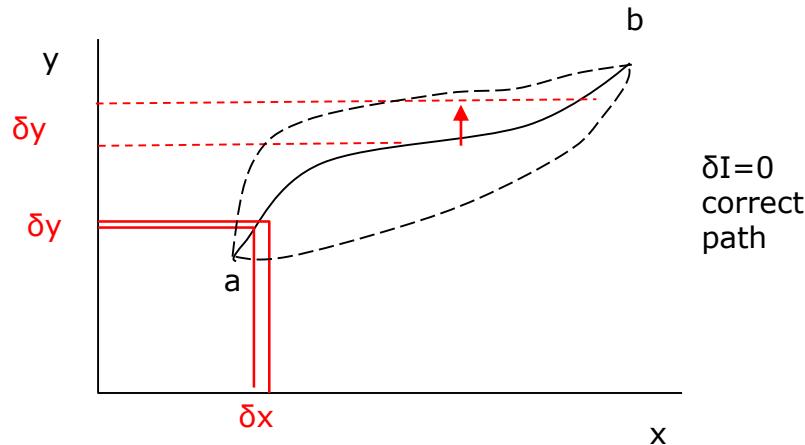
- Chap. 2. Lanczos, "Variational Principles of Mechanics"
- Chap. 2. Hildebrand, "Methods of Applied Mathematics"
- Chap. 3. Langhaar, "Energy Methods in Applied Mechanics"

Variational Principle

❖ Calculus of variation (continued)

Behavior described by finding condition when certain meaningful quantity is stationary

$$I = \int_a^b F(y, y', x) dx$$



δy is called "variation in y ", y is a dependent variable.

$$\delta I = \int_a^b \delta F(y, y', x) dx$$

$$\delta F(y, y', x) = \frac{\partial F}{\partial y} \delta y + \frac{\partial F}{\partial y'} \delta y' + \frac{\partial F}{\partial x} \delta x = 0$$

Variational Principle

in operations

$$\delta g(y) = \frac{dg(x)}{dy} \delta y = g'(y) \delta y$$

$$\delta(y^2) = 2y \delta y$$

$$\delta \sin y = \cos y \delta y$$

$$\delta \left(\frac{dw}{dx} \right) = \frac{d\delta w}{dx}, \quad \delta \left(\frac{d^n w}{dx^n} \right) = \frac{d^n (\delta w)}{dx^n}$$

$$\delta \left(\int_a^b F dx \right) = \int_a^b \delta F dx$$

consider

$$I = \int_a^b F(y, y', x) dx$$

$$\delta I = \int_a^b \delta F dx = \int_a^b \left[\frac{\partial F}{\partial y} \delta y' + \frac{\partial F}{\partial y'} \delta y' \right] dx$$

$$= \int_a^b \left[\frac{\partial F}{\partial y} \delta y \right] dx + \frac{\partial F}{\partial y} \delta y'|_a^b - \int_a^b \delta y \frac{d}{dx} \left(\frac{\partial F}{\partial y'} \right) dx$$

Variational Principle

$$\delta I = - \int_a^b \left[\frac{d}{dx} \left(\frac{\partial F}{\partial y'} \right) - \frac{\partial F}{\partial y} \right] \delta y dx = 0$$

$\delta I = 0$, if and only if

$$\frac{d}{dx} \left(\frac{\partial F}{\partial y'} \right) - \frac{\partial F}{\partial y} = 0 : Euler's Equations$$

If $F = T - U + W$

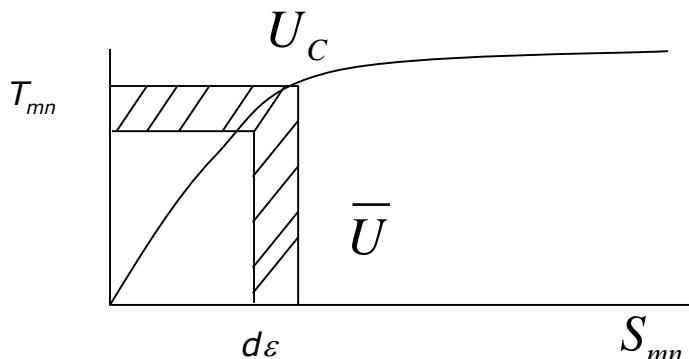
$x = f(\text{time}) \Rightarrow$ Lagrange's Egn.

Variational Principle

❖ Structural mechanics

- scalars of interest
 - Strain Energy Density
 - Complementary Strain Energy Density

$$\begin{aligned}\bar{U} &= \bar{U}(S_{mn}) \\ \overline{U}_c &= \bar{U}(T_{mn})\end{aligned}$$



$$\bar{U} = \int_0^{\varepsilon_{mn}} F_{mn}(S_{mn}') dS_{mn}'$$

- For linear system

$$U = \frac{1}{2} T_{mn} S_{mn} = \frac{1}{2} T^T S$$

Tensor

Voight

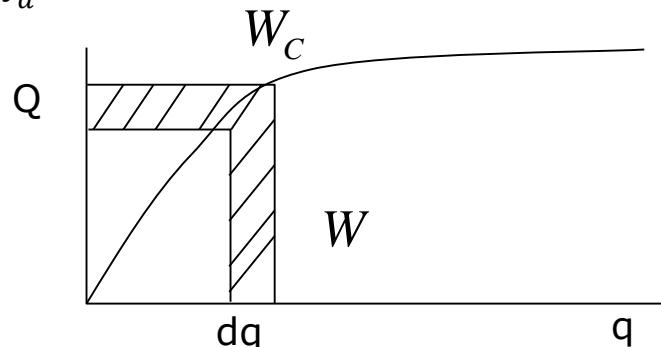
$$U = \iiint \bar{U}(S_{mn}) dV = U$$

$$U_c = \int_0^{T_{mn}} S_{mn}(T_{mn}') dT_{mn}$$

Variational Principle

- ❖ Work = Force times distance

$$\int_a^b \vec{F} \cdot d\vec{r}$$



$$W = \int_0^q Q(q') dq'$$

$$W_C = \int_0^Q q(Q') dQ'$$

- ❖ Variation of Strain Energy

$$U(S_{mn}) = \iiint \left\{ \int_0^{S_{mn}} T_{mn}(S'_{mn}) dS'_{mn} \right\}$$

-perturbation in strain $S_{mn} + \delta S_{mn}$

consider

$$\begin{aligned} & U(S_{mn} + \delta S_{mn}) - U(S_{mn}) \\ &= \iiint \left\{ \int_{S_{mn}}^{S_{mn} + \delta S_{mn}} T_{mn}(S'_{mn}) \delta S'_{mn} \right\} = \Delta U(S_{mn}) \\ &= \underbrace{\iiint \{ T_{mn}(S_{mn}) \delta S_{mn} \} dV}_{\delta U} \end{aligned}$$

Variational Principle

❖ Variation in Work

$$\delta W = \iiint_A \hat{T}_{mn} \delta U_n dA + \iiint_V f_n \delta U_n dV$$

❖ Derivation of Principle of Minimum Total Potential Energy

given loaded body in equilibrium

$$\iiint_V \left\{ \frac{\partial T_{mn}}{\partial x_m} + f_n \right\} \delta U_n dV = 0$$

$$1st \ term : \iiint \frac{\partial T_{mn}}{\partial x_m} \delta U_n dV = \iiint \left\{ \frac{\partial}{\partial x_m} (T_{mn} \delta U_n) - T_{mn} \frac{\partial}{\partial x_m} (\delta U_n) \right\} dx$$

$$\vec{B} = \hat{i}_n (T_{mn} \delta U_n)$$

$$= \iiint \left\{ \nabla \vec{B} - T_{mn} \delta \left(\frac{\partial U_n}{\partial x_m} \right) \right\} dV$$

$$\iiint_V \nabla \vec{B} dV = \iint_A \vec{B} \cdot \vec{N} dA$$

$$\iint_A T_{mn} \cos(Nx_m) \delta U_n dA - \iiint_V T_{mn} \delta S_{mn} dV + \iiint_V f_n \delta U_n dV = 0$$

$$\iiint_V T_{mn} \delta S_{mn} dV = \iint_A \hat{T}_{mn} \delta U_n dA + \iiint_V f_n \delta U_n dV$$

δU

δW

$$\delta(U - W) = 0$$

$I = \text{variational indicator}$

Variational Principle

- ❖ **Principle of stationary total potential energy of all displacement of a loaded structure satisfying geometric B.C's – the right ones(equilibrium) are those that minimize Π**

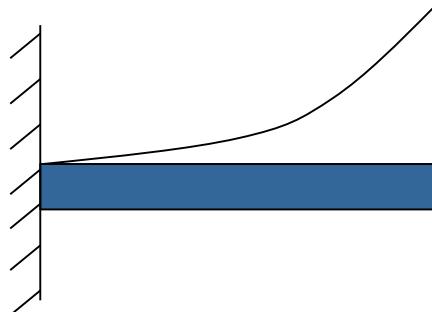
$$\Pi = V - W$$

$$\delta\Pi = \delta(V - W) = 0$$

$$U = \iiint \left\{ \int_0^{S_{mn}} T_{mn}(S_{mn}) dS_{mn} \right\} dV$$

$$W = \iint_A \hat{T}_{sn} u_n dA + \iiint_V f_n u_n dV$$

- Solution by minimization usually considers certain subset.

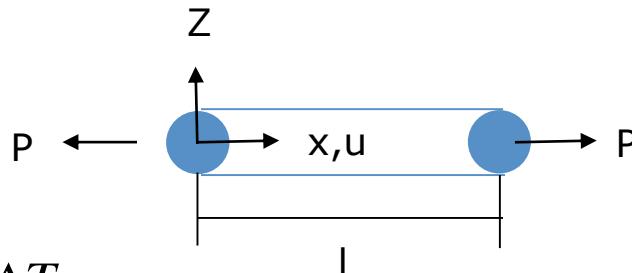


 *approximate solution*

Variational Principle

❖ **V of a typical structure**

i) Rod



$$T_{11} = ES_{11} - E\alpha\Delta T$$

$$S_{11} = \frac{du}{dx}$$

$$\delta U = \iiint T_{11} \delta S_{11} dV$$

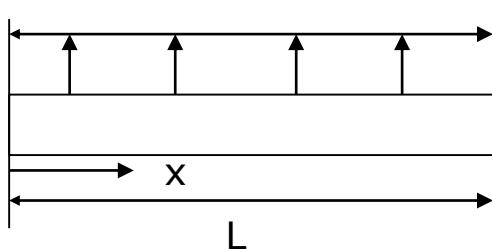
$$U = \iiint_V \left\{ \frac{1}{2} ES_{11}^2 - E\alpha\Delta T S_{11} \right\} dA dx$$

$$= \frac{1}{2} \int_0^l EA \left(\frac{du}{dx} \right)^2 dx - \int_0^l \left(\iint E\alpha\Delta T \frac{du}{dx} dA \right) dx$$

Variational Principle

❖ ***U* of a typical structure**

ii) Beam in Bending



$$T_{11} = ES_{11} - E\alpha\Delta T$$

$$S_{11} = -z \frac{d^2 w}{dx^2}$$

$$U = \iiint \left\{ \frac{1}{2} ES_{11}^2 - E\alpha\Delta T S_{11} \right\} dAdx$$

$$U = \frac{1}{2} \int_0^l EI \left(\frac{d^2 w}{dx^2} \right)^2 dx + \int_0^l (E\alpha\Delta T z dA) \frac{d^2 w}{dx^2} dx$$

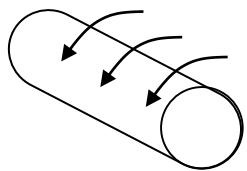
$$W = \int_0^l f_w(x) w(x) dx$$

$I = \int z^2 dA$

Variational Principle

❖ **V of a typical structure**

iii) Torsion of Bar



$$\frac{d\alpha}{dx} = \frac{T}{GJ}, \quad T = GJ \frac{d\alpha}{dx}$$

$$U = \frac{1}{2} \int_0^l T \frac{d\alpha}{dx} dx = \frac{1}{2} \int_0^l GJ \left(\frac{d\alpha}{dx} \right)^2 dx$$

Variational Principle

❖ Rayleigh-Ritz Approach

$$\vec{U}(x, y, z, t) = \sum_{i=1}^N a_i(t) \varphi_i(x, y, z)$$

$\rightarrow \varphi \Rightarrow$ satisfy only the geometric B.C.'s

φ should be twice differentiable

$$\Pi_p = (U - W) = \Pi_p(a_1, a_2, \dots, a_n)$$

$$\delta \Pi_p = \frac{\partial \Pi_p}{\partial a_1} \delta a_1 + \frac{\partial \Pi_p}{\partial a_2} \delta a_2 + \dots,$$

$$\frac{\partial \Pi_p}{\partial a_1} = o, \frac{\partial \Pi_p}{\partial a_2} = 0, \dots etc.$$

For linear elastic problem,

$$[K]\{q\} = \{f\}$$

Variational Principle

❖ Note on dynamics

- d'Alembert's Force

$$\vec{f}_I = -\rho \ddot{\vec{u}}_n$$

PSTPE (Principle of the stationarity total potential energy)

$$\int_{t_1}^{t_2} \left(\underbrace{\iiint_V T_{mn} \delta S_{mn} dV}_{\delta U} + \iiint_V \rho \ddot{u}_n \delta u_n dV - \underbrace{\iiint_V f_{nB} \delta u_n dV - \iint_A \hat{T}_{sn} \delta u_n dA}_{\delta W} \right) dt = 0$$

$$\int_{t_1}^{t_2} \iiint_V \rho \ddot{u}_n \delta u_n dV dt = \int_{t_1}^{t_2} \iiint_V \rho \dot{u}_n \delta \dot{u}_n dt \quad \boxed{- \int_{t_1}^{t_2} \iiint_V \rho \dot{u}_n \delta \dot{u}_n dV dt} \quad \begin{matrix} 0 \\ \delta W \\ -\delta T \end{matrix}$$

$\downarrow \dot{u} \quad \downarrow \delta \dot{u}$

$$T = \iiint_V \frac{1}{2} \rho \dot{u}_n \dot{u}_n dV$$

$$\int_{t_1}^{t_2} (\delta U - \delta T - \delta W) dt = 0$$

$$\boxed{\delta \int_{t_1}^{t_2} (T - U) dt + \int_{t_1}^{t_2} \delta W dt = 0}$$

Hamilton's principle

Variational Principle

❖ Principle of the minimum complementary energy

- increments in stress field δT_{mn}

$$\frac{\partial T_{mn}}{\partial X_m} + \cancel{\delta f_n}^0 = 0$$

$$\iiint_V \left\{ S_{mn} - \frac{1}{2} \left(\frac{\partial u_n}{\partial x_m} + \frac{\partial u_m}{\partial x_n} \right) \right\} \delta T_{mn} dV = 0$$

$$\iiint_V S_{mn} \delta T_{mn} dV - \iint_A U_n \delta s_n d\hat{T}_{sn} A = 0$$

$$\delta U^C - \delta W^C = 0$$

$$\delta \hat{T}_{sn} = \delta T_{mn} \cos(Nx_n) dA$$