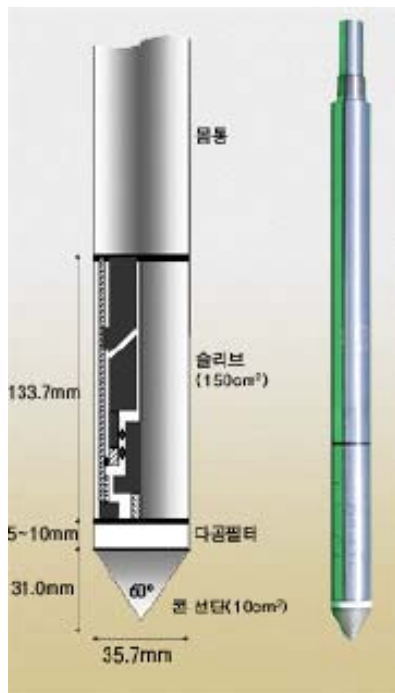


### 3.3 Cone Penetration Test (CPT)

#### (1) General

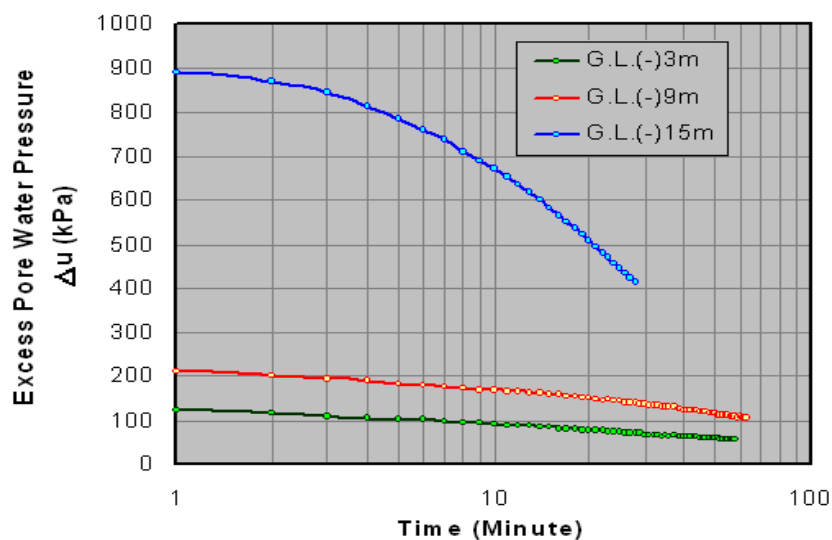


The CPT is carried out by pushing a 60° cone with a face area of 10 cm<sup>2</sup> into the ground at a constant speed ( $2 \pm 0.5$  cm/s), whilst measuring the force to do so. The shear force on a 150 cm<sup>2</sup> 'friction sleeve' and pore pressure are then also measured.

- Type of cone
  - Piezocone
  - Environmental cone
  - Seismic cone
  - Visual cone

- Dissipation test with piezocone

In clays, the horizontal coefficient of consolidation  $C_v$  can be determined by stopping the cone, and measuring pore pressure dissipation as a function of time.



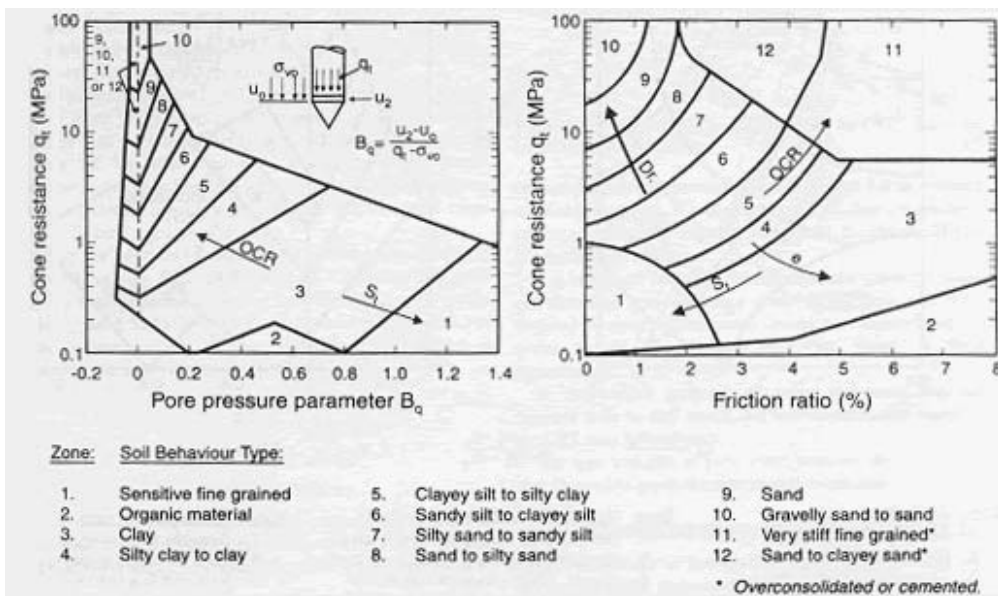
(2) Interpretation and use

i) soil classification

- Robertson and Campanella (1986)

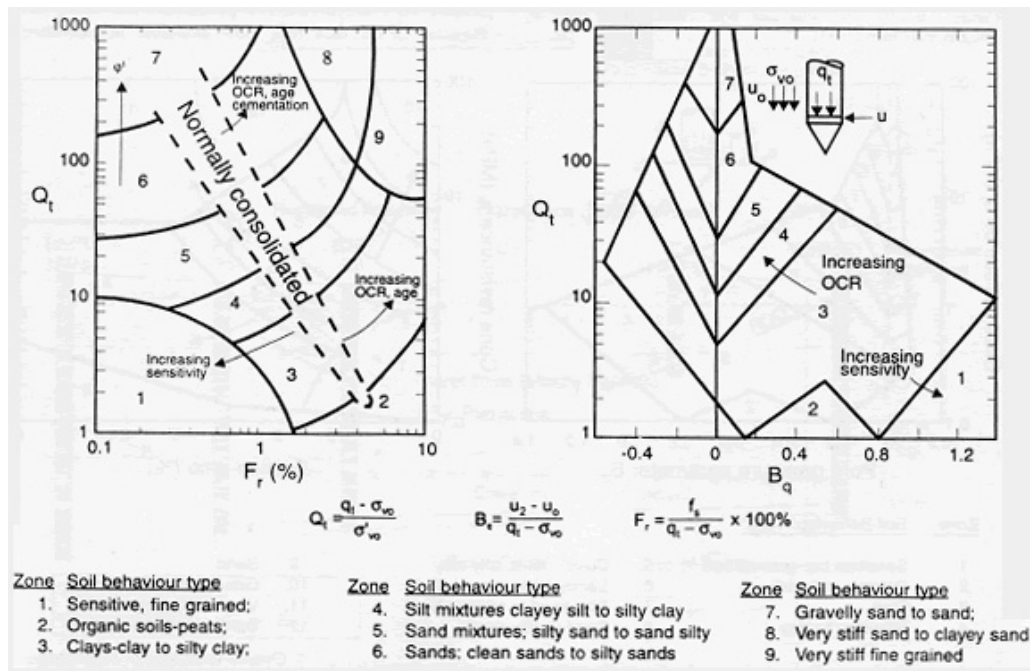
$$B_q = \frac{\Delta u}{q_t - \sigma_{vo}} \quad \text{vs} \quad q_t$$

$$F_r = \frac{f_s}{q_t - \sigma_{vo}} \quad \text{vs} \quad q_t$$



- Robertson (1990)

$$B_q \text{ vs } Q_t = \frac{q_t - \sigma_{vo}}{\sigma'_{vo}}, \quad F_r \text{ vs } Q_t$$



ii) Undrained strength

- $S_u$  is evaluated with cone factors ( $N_{kt}$ ,  $N_{ke}$ ,  $N_{\Delta u}$ )

- Schmertmann(1978), Lunne et al(1985) 
$$s_u = \frac{q_T - \sigma_{v0}}{N_{kt}}$$

- Senneset et al (1982), Campanella et al (1982) 
$$s_u = \frac{q_T - u}{N_{ke}}$$

- Lunne et al (1985) 
$$s_u = \frac{\Delta u}{N_{\Delta u}}$$

regions	The test to evaluate cone factor	Cone factor
England	CIUC	$N_{kt} = 12 \sim 20$
Norway	FVT	$N_{kt} = 12 \sim 19$
Italy	FVT	$N_{kt} = 8 \sim 16$
	CKOUC	$N_{kt} = 8 \sim 10$
Vancouver, Canada	FVT	$N_{kt} = 8 \sim 10$
	SBPT	
Japan	UCT	$N_{kt} = 8 \sim 16$
	FVT	$N_{kt} = 9 \sim 14$
Taiwan	CIUC	$N_{qu} = 5.0 \sim 6.8$
	CAUC	$N_{qu} = 6.0 \sim 7.2$
Canada	FVT	$N_{Du} = 6.2 \sim 7.0$

- Cone factor are very site –specific.

iii) The horizontal coefficient of consolidation

- Based on dissipation test

Torstensson(1975, 1977)

$$c_h = \frac{R^2 \cdot T_{50}}{t_{50}}$$

Baligh & Levadoux(1980)

$$c_h = \frac{R^2 \cdot T}{t}$$

U (%)	A								B	C
	Spherical shape				Cylindrical shape					
	$I_R=30$	$I_R=70$	$I_R=100$	$I_R=130$	$I_R=30$	$I_R=70$	$I_R=100$	$I_R=130$		
40	0.18	0.26	0.34	0.40	0.74	1.14	1.48	1.78	3.0	0.142
50	0.29	0.44	0.58	0.69	1.47	2.19	2.90	3.55	5.6	0.245
60	0.46	0.73	0.98	1.17	2.49	3.83	5.36	6.63	10	0.439

A : Torstensson (1975), B : Baligh와 Levadoux (1986), C : Teh와 Houlsby (1991)

iv) Friction angle,  $\phi$  in sandy soil

Robertson and Campanella (1983)

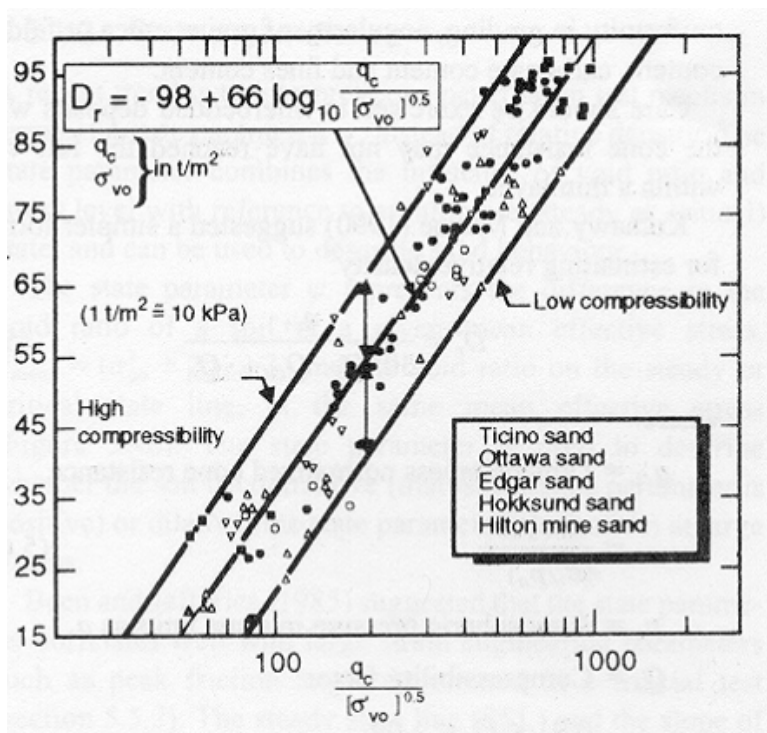
$$\phi = \tan^{-1} \left[ 0.1 + 0.38 \log \left( \frac{q_c}{\sigma'_{v0}} \right) \right]$$

$q_c/\sigma'_{v0}$	Soil state	Friction angle ( $\phi'$ )
< 20	Very loose	< 30
20 ~ 40	Loose	30 ~ 35
40 ~ 120	Medium	35 ~ 40
120 ~ 200	Dense	40 ~ 45
> 200	Very dense	> 45

v)  $D_r$  in sandy soil

Jamiolkovski et al (1985)

$$D_r(\%) = 66 \log \left( \frac{q_c}{\sqrt{\sigma'_{v0}}} \right) - 98$$



vi) Other usage

- OCR
- $E_s$
- Sensitivity
- Bearing capacity of foundation
- Liquefaction potential