

Basics of Fluid Flow

Introduction

- Fluids
 - No resistance to external shear forces
 - Regarded as continuum, i.e., continuous substance
- Fluid flow is caused by the action of externally applied forces.
 - Surface forces: pressure or shear forces
 - Body forces: gravity, forces induced by rotation
- Flow speed affects its properties
 - Creeping flow: Speed low enough; inertia ignored
 - Laminar flow: Inertia important, but each fluid particle follows a smooth trajectory
 - Turbulent flow: Speed increase leads to instability; random type of flow

Introduction – Cont.

- Flow speed/Sound speed (Ma: Mach #)
 - Compressibility
 - $Ma < 0.3$: Incompressible flow
 - $Ma > 0.3$: Compressible flow
 - Thermal effects
 - $Ma < 1.0$: Subsonic flow
 - $Ma > 1.0$: Supersonic flow
 - $Ma > 5.0$: Hypersonic flow (change in chemical nature)
 - Viscosity
 - Viscous flow vs. Inviscid flow
 - Newton's law
 - Newtonian flow vs. Non-Newtonian flow
 - Other phenomena
 - Heat transfer, Bouyancy, Multi-phase, ...



Conservation Principles

- Control volume approach
 - In fluid flows, it is more convenient to deal with the flow within a certain spatial region (CV), rather than in a parcel of matter which quickly passes through the region of interest.
- Conservation of two extensive properties
 - Rate of change of the property amount in a given CM to externally determined effects
 - Mass $\frac{dm}{dt} = 0$. (1.1)
 - Momentum (Newton's 2nd law of motion)

$$\frac{d(mv)}{dt} = \sum f, \quad (1.2)$$



Conservation Principles – Cont.

■ Transformation into CV form

- Fundamental variables are intensive, i.e., independent of amount of matter considered. Ex. Density (mass/volume), Velocity (momentum/mass).
- Corresponding extensive property

$$\Phi = \int_{\Omega_{CM}} \rho \phi \, d\Omega, \quad (1.3)$$

- LHS of each conservation equation for a CV (HW#1)

$$\frac{d}{dt} \int_{\Omega_{CM}} \rho \phi \, d\Omega = \frac{d}{dt} \int_{\Omega_{CV}} \rho \phi \, d\Omega + \int_{S_{CV}} \rho \phi (\mathbf{v} - \mathbf{v}_b) \cdot \mathbf{n} \, dS, \quad (1.4)$$

- For a fixed CV, $\mathbf{v}_b = \mathbf{0}$ and the first derivative on RHS becomes a local (partial) derivative.



Mass Conservation

■ Continuity equation

- Set $\phi = 1$:

$$\frac{\partial}{\partial t} \int_{\Omega} \rho \, d\Omega + \int_S \rho \mathbf{v} \cdot \mathbf{n} \, dS = 0. \quad (1.5)$$

- Applying the Gauss' divergence theorem, and allowing CV to become infinitesimally small (HW #2)

$$\frac{\partial \rho}{\partial t} + \text{div}(\rho \mathbf{v}) = 0. \quad (1.6)$$

- Cartesian form in tensor notation

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u_i)}{\partial x_i} = \frac{\partial \rho}{\partial t} + \frac{\partial(\rho u_x)}{\partial x} + \frac{\partial(\rho u_y)}{\partial y} + \frac{\partial(\rho u_z)}{\partial z} = 0, \quad (1.7)$$



Momentum Conservation

■ Momentum conservation equation

- In Eq. (1.2) and (1.4), replace ϕ with v ,

$$\frac{\partial}{\partial t} \int_{\Omega} \rho v \, d\Omega + \int_S \rho v v \cdot \mathbf{n} \, dS = \sum \mathbf{f} . \quad (1.8)$$

- RHS can be expressed in terms of intensive properties by considering
 - Surface forces (pressure, normal and shear stresses, surface tension, etc.)
 - Body forces (gravity, centrifugal and Coriolis forces, electromagnetic forces, etc.)
- To close the system of equations, assume that the fluid is Newtonian (HW #3).

Momentum Conservation – Cont.

- For Newtonian fluids, the stress tensor T ,

$$\boldsymbol{\tau} = - \left(p + \frac{2}{3} \mu \operatorname{div} \mathbf{v} \right) \mathbf{I} + 2\mu \mathbf{D} , \quad (1.9)$$

$$\mathbf{D} = \frac{1}{2} [\operatorname{grad} \mathbf{v} + (\operatorname{grad} \mathbf{v})^T] . \quad (1.10)$$

- OR For incompressible flow

$$T_{ij} = - \left(p + \frac{2}{3} \mu \frac{\partial u_j}{\partial x_j} \right) \delta_{ij} + 2\mu D_{ij} , \quad (1.11)$$

$$D_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) , \quad (1.12)$$

- Viscous part

$$\tau_{ij} = 2\mu D_{ij} - \frac{2}{3} \mu \delta_{ij} \operatorname{div} \mathbf{v} . \quad (1.13)$$

Momentum Conservation – Cont.

- With b representing the body forces, in integral form

$$\frac{\partial}{\partial t} \int_{\Omega} \rho \mathbf{v} \, d\Omega + \int_S \rho \mathbf{v} \mathbf{v} \cdot \mathbf{n} \, dS = \int_S \mathbf{T} \cdot \mathbf{n} \, dS + \int_{\Omega} \rho \mathbf{b} \, d\Omega . \quad (1.14)$$

- By applying Gauss' divergence theorem, in coordinate free vector form

$$\frac{\partial(\rho \mathbf{v})}{\partial t} + \text{div}(\rho \mathbf{v} \mathbf{v}) = \text{div} \mathbf{T} + \rho \mathbf{b} . \quad (1.15)$$

- i -th Cartesian component

$$\frac{\partial(\rho u_i)}{\partial t} + \text{div}(\rho u_i \mathbf{v}) = \text{div} \mathbf{t}_i + \rho b_i . \quad (1.16)$$

Momentum Conservation – Cont.

- Integral form of Eq. (1.16)

$$\frac{\partial}{\partial t} \int_{\Omega} \rho u_i \, d\Omega + \int_S \rho u_i \mathbf{v} \cdot \mathbf{n} \, dS = \int_S \mathbf{t}_i \cdot \mathbf{n} \, dS + \int_{\Omega} \rho b_i \, d\Omega , \quad (1.17)$$

- where

$$\mathbf{t}_i = \mu \text{grad} u_i + \mu (\text{grad} \mathbf{v})^T \cdot \mathbf{i}_i - \left(p + \frac{2}{3} \mu \text{div} \mathbf{v} \right) \mathbf{i}_i = \tau_{ij} \mathbf{i}_j - p \mathbf{i}_i . \quad (1.18)$$

- In Cartesian coordinates

$$\mathbf{t}_i = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \mathbf{i}_j - \left(p + \frac{2}{3} \mu \frac{\partial u_j}{\partial x_j} \right) \mathbf{i}_i . \quad (1.19)$$

Momentum Conservation – Cont.

- The momentum equations are said to be in “strong conservation form” if all terms have the form of the divergence of a vector or tensor. The strong conservation form, when used with a FVM, automatically insures global momentum conservation.
- Eq. (1.16) is a strong conservation form. By employing the continuity equation and based on

$$\operatorname{div}(\rho \mathbf{v} u_i) = u_i \operatorname{div}(\rho \mathbf{v}) + \rho \mathbf{v} \cdot \operatorname{grad} u_i ,$$

- A non-conservation form is obtained

$$\rho \frac{\partial u_i}{\partial t} + \rho \mathbf{v} \cdot \operatorname{grad} u_i = \operatorname{div} \mathbf{t}_i + \rho b_i . \quad (1.20)$$

Momentum Conservation – Cont.

- The pressure gradient is regarded as a body force, i.e., non-conservative treatment of the pressure term, based on

$$\operatorname{div}(p \mathbf{i}_i) = \operatorname{grad} p \cdot \mathbf{i}_i .$$

- If Eq. (1.13) is substituted into Eq. (1.16), and gravity is the only body force, for Cartesian coordinates,

$$\frac{\partial(\rho u_i)}{\partial t} + \frac{\partial(\rho u_j u_i)}{\partial x_j} = \frac{\partial \tau_{ij}}{\partial x_j} - \frac{\partial p}{\partial x_i} + \rho g_i , \quad (1.21)$$

Conservation of Scalar Quantities

- Integral form of the equation describing conservation of a scalar quantity, ϕ ,

$$\frac{\partial}{\partial t} \int_{\Omega} \rho \phi \, d\Omega + \int_S \rho \phi \mathbf{v} \cdot \mathbf{n} \, dS = \sum f_{\phi} , \quad (1.22)$$

- Diffusive transport, by Fourier's law for heat diffusion or Fick's law for mass diffusion

$$f_{\phi}^d = \int_S \Gamma \operatorname{grad} \phi \cdot \mathbf{n} \, dS , \quad (1.23)$$

- Integral form of the generic conservation equation

$$\frac{\partial}{\partial t} \int_{\Omega} \rho \phi \, d\Omega + \int_S \rho \phi \mathbf{v} \cdot \mathbf{n} \, dS = \int_S \Gamma \operatorname{grad} \phi \cdot \mathbf{n} \, dS + \int_{\Omega} q_{\phi} \, d\Omega , \quad (1.26)$$

Cons. of Scalar Quantities – Cont.

- Coordinate-free vector form,

$$\frac{\partial(\rho\phi)}{\partial t} + \operatorname{div}(\rho\phi\mathbf{v}) = \operatorname{div}(\Gamma \operatorname{grad} \phi) + q_{\phi} . \quad (1.27)$$

- In Cartesian coordinates and tensor notation

$$\frac{\partial(\rho\phi)}{\partial t} + \frac{\partial(\rho u_j \phi)}{\partial x_j} = \frac{\partial}{\partial x_j} \left(\Gamma \frac{\partial \phi}{\partial x_j} \right) + q_{\phi} . \quad (1.28)$$

Simplified Mathematical Models

■ Incompressible flow

- Density is assumed constant – liquids or gases if $Ma < 0.3$
- If flow is isothermal, the viscosity is also constant.

$$\operatorname{div} \mathbf{v} = 0, \quad (1.32)$$

$$\frac{\partial u_i}{\partial t} + \operatorname{div}(\mathbf{u}_i \mathbf{v}) = \operatorname{div}(\nu \operatorname{grad} u_i) - \frac{1}{\rho} \operatorname{div}(p \mathbf{i}_i) + b_i, \quad (1.33)$$

- Kinematic viscosity $\nu = \mu/\rho$

Simplified Models – Cont.

■ Inviscid flow

- Viscous effects are neglected altogether (far from solid surfaces)

$$\frac{\partial(\rho u_i)}{\partial t} + \operatorname{div}(\rho u_i \mathbf{v}) = -\operatorname{div}(p \mathbf{i}_i) + \rho b_i. \quad (1.34)$$

■ Potential flow

- Flow is assumed inviscid + Velocity field is irrotational.
- Define velocity potential $\mathbf{v} = -\operatorname{grad} \Phi$.
- Governing equation

$$\operatorname{div}(\operatorname{grad} \Phi) = 0. \quad (1.36)$$

Simplified Models – Cont.

■ Stokes flow

- When the flow velocity is very small, the fluid is very viscous, or the geometric dimensions are very small, i.e., Re is very small, the convective (inertial) terms play a minor role and can be neglected.
- Momentum equation becomes (for steady non-convection flows)

$$\text{div} (\mu \text{grad } u_i) - \frac{1}{\rho} \text{div} (p \mathbf{i}_i) + b_i = 0 . \quad (1.37)$$

Simplified Models – Cont.

■ Boussinesq approximation

- In flows with heat transfer, the fluid properties are normally functions of temperature. The variations may be small and yet be the cause of the fluid motion.
- If the density variation is not large, one may treat the density as constant in the unsteady and convection terms, and treat it as variable only in the gravitational term.

$$(\rho - \rho_0)g_i = -\rho_0 g_i \beta (T - T_0) , \quad (1.38)$$

Simplified Models – Cont.

- Boundary layer approximation
 - When the flow has a predominant direction and the variation of the geometry is gradual
 - Thin shear layer or boundary layer flows
 - Diffusive transport of momentum *in the principal flow direction* is much smaller than convection and can be neglected
 - The velocity component in the main flow direction is much larger than the components in other directions
 - The pressure gradient across the flow is much smaller than in the principal flow direction

Simplified Models – Cont.

- Boundary layer approximation – Cont.
 - 2D BL equations

$$\frac{\partial(\rho u_1)}{\partial t} + \frac{\partial(\rho u_1 u_1)}{\partial x_1} + \frac{\partial(\rho u_2 u_1)}{\partial x_2} = \mu \frac{\partial^2 u_1}{\partial x_2^2} - \frac{\partial p}{\partial x_1}, \quad (1.39)$$

and the momentum equation normal to the principal flow direction $\partial p / \partial x_2 = 0$.

Mathematical Classification of Flows

- Hyperbolic flows
- Parabolic flows
- Elliptic flows
- Mixed flow types
(HW)