



[2008] [06-1]

Planning Procedure of Naval Architecture & Ocean Engineering

October, 2008

Prof. Kyu-Yeul Lee

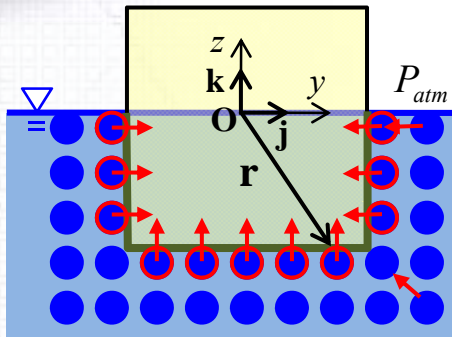
Department of Naval Architecture and Ocean Engineering,
Seoul National University of College of Engineering



Part 1. Stability & Trim

[06-1] Pressure integration technique (1)

유체 중에 잠긴 물체가 받는 힘과 모멘트



S_B : 침수표면

V : 침수부피

유체 입자가 주위 유체 입자에 작용하는 정적인 압력

Bernoulli Eq.

$$\rho \frac{\partial \Phi}{\partial t} + \frac{1}{2} |\nabla \Phi|^2 + \rho g z + P = C$$

$$P = -\rho \frac{\partial \Phi}{\partial t} - \frac{1}{2} |\nabla \Phi|^2 - \rho g z + C$$

정수 \rightarrow 유체의 속도 = 0 $\rightarrow P_{Static}$

$$P_{Static} = -\rho g z + C \rightarrow P_{atm}$$

$$P_{Static} = -\rho g z + P_{atm}$$

$$P_{Fluid}(z) + P_{atm}$$

$$P_{Fluid}(z) = -\rho g z$$

유체 입자들이 유체 중에 잠긴 물체에 작용하는 정적인 힘과 모멘트

$$\mathbf{F} = \iint_{S_B} (-\rho g z) d\mathbf{S} = -\rho g \iint_{S_B} z(\mathbf{n} dS) = -\rho g \iint_{S_B} \mathbf{n} z dS$$

$$\mathbf{M} = \iint_{S_B} \mathbf{r} \times (-\rho g z) d\mathbf{S} = -\rho g \iint_{S_B} \mathbf{r} \times z(\mathbf{n} dS) = -\rho g \iint_{S_B} (\mathbf{r} \times \mathbf{n}) z dS$$

Divergence Theorem

$$\mathbf{F} = \mathbf{k} \rho g \iiint_V dV$$

$$\mathbf{M} = \rho g \iiint_V [\mathbf{i}y - \mathbf{j}x] dV$$

선박의 자세와 힘, 모멘트와의 관계

- Pressure Integration Technique¹⁾

1) J.N.Newman, Marine Hydrodynamics, 1977, pp.290-295

선박이 유체 중에서 받는 정적인 힘과 모멘트

$$\mathbf{F} = \mathbf{k}\rho g \iiint dV \quad \mathbf{M} = \rho g \iiint [\mathbf{i}y - \mathbf{j}x] dV$$

\downarrow $V(\xi_3, \xi_4, \xi_5)$ \downarrow $V(\xi_3, \xi_4, \xi_5)$

$$\mathbf{F} = \mathbf{F}(\xi_3, \xi_4, \xi_5) \quad \mathbf{M} = \mathbf{M}(\xi_3, \xi_4, \xi_5)$$

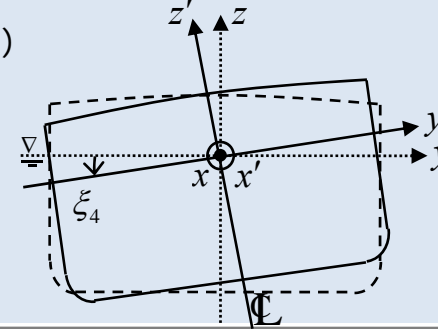
(Q) 침수부피(중심)가 변하는 자세는?
 대경사 경우 미소경사 경우

$$\mathbf{F} \approx -\mathbf{k}\rho g \xi_4 T_{WP}(z')$$

$$\mathbf{M} \approx \mathbf{i}(-\rho g \xi_4 V_0 z'_{B0} - \rho g \xi_4 I_T + mgz'_G \xi_4) + \mathbf{j}\rho g \xi_4 I_P$$

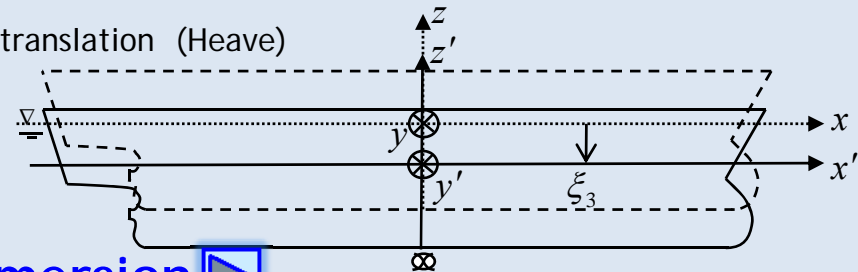
x 축 rotation (Roll)

Heel ▶



z 축 translation (Heave)

Immersion ▶

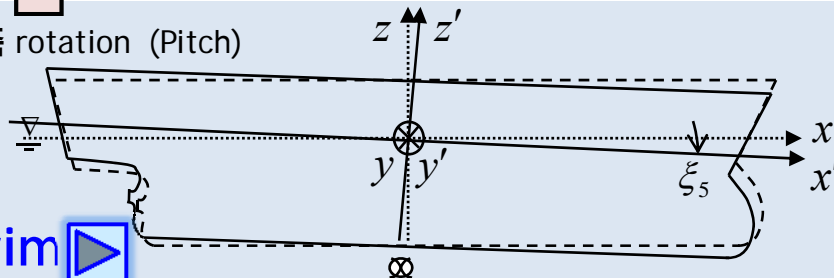


$$\mathbf{F} \approx \mathbf{k}\rho g \xi_5 L_{WP}(z')$$

$$\mathbf{M} \approx \mathbf{i}\rho g \xi_5 I_P + \mathbf{j}(-\rho g \xi_5 V_0 z'_{B0} - \rho g \xi_5 I_L + mgz'_G \xi_5)$$

y 축 rotation (Pitch)

Trim ▶



$$\mathbf{F} \approx -\mathbf{k}\rho g \xi_3 A_{WP}(z')$$

$$\mathbf{M} \approx -\mathbf{i}\rho g \xi_3 T_{WP}(z') + \mathbf{j}\rho g \xi_3 L_{WP}(z')$$

복원력(모멘트)의 선형화 (Taylor series expansion) [1]



초기 자세(ξ_3, ξ_4, ξ_5)에서 복원력(F), 횡 방향 복원 모멘트(M_T), 종 방향 복원 모멘트(M_L)를 알고 있을 때, 미소 변화된 자세($\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5$)에서의 복원력(F), 횡 방향 복원 모멘트(M_T), 종 방향 복원 모멘트(M_L)는?

$F(\xi_3, \xi_4, \xi_5)$	➔	$F(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5)$
$M_T(\xi_3, \xi_4, \xi_5)$	➔	$M_T(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5)$
$M_L(\xi_3, \xi_4, \xi_5)$	➔	$M_L(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5)$

Taylor series expansion

$$F(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) = F(\xi_3, \xi_4, \xi_5) + \frac{\partial F}{\partial \xi_3} \Delta\xi_3 + \frac{\partial F}{\partial \xi_4} \Delta\xi_4 + \frac{\partial F}{\partial \xi_5} \Delta\xi_5 + \dots \text{선형화}$$

$$M_T(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) = M_T(\xi_3, \xi_4, \xi_5) + \frac{\partial M_T}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_T}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_T}{\partial \xi_5} \Delta\xi_5 + \dots \text{선형화}$$

$$M_L(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) = M_L(\xi_3, \xi_4, \xi_5) + \frac{\partial M_L}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_L}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_L}{\partial \xi_5} \Delta\xi_5 + \dots \text{선형화}$$

복원력(모멘트)의 선형화 (Taylor series expansion) (2)

✓ Taylor series 1차항까지 전개

$$F(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) = F(\xi_3, \xi_4, \xi_5) + \frac{\partial F}{\partial \xi_3} \Delta\xi_3 + \frac{\partial F}{\partial \xi_4} \Delta\xi_4 + \frac{\partial F}{\partial \xi_5} \Delta\xi_5$$

$$M_T(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) = M_T(\xi_3, \xi_4, \xi_5) + \frac{\partial M_T}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_T}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_T}{\partial \xi_5} \Delta\xi_5$$

$$M_L(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) = M_L(\xi_3, \xi_4, \xi_5) + \frac{\partial M_L}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_L}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_L}{\partial \xi_5} \Delta\xi_5$$



$$F(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) - F(\xi_3, \xi_4, \xi_5) = \frac{\partial F}{\partial \xi_3} \Delta\xi_3 + \frac{\partial F}{\partial \xi_4} \Delta\xi_4 + \frac{\partial F}{\partial \xi_5} \Delta\xi_5$$

$$M_T(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) - M_T(\xi_3, \xi_4, \xi_5) = \frac{\partial M_T}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_T}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_T}{\partial \xi_5} \Delta\xi_5$$

$$M_L(\xi_3 + \Delta\xi_3, \xi_4 + \Delta\xi_4, \xi_5 + \Delta\xi_5) - M_L(\xi_3, \xi_4, \xi_5) = \frac{\partial M_L}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_L}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_L}{\partial \xi_5} \Delta\xi_5$$



$$\Delta F = \frac{\partial F}{\partial \xi_3} \Delta\xi_3 + \frac{\partial F}{\partial \xi_4} \Delta\xi_4 + \frac{\partial F}{\partial \xi_5} \Delta\xi_5$$

$$\Delta M_T = \frac{\partial M_T}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_T}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_T}{\partial \xi_5} \Delta\xi_5$$

$$\Delta M_L = \frac{\partial M_L}{\partial \xi_3} \Delta\xi_3 + \frac{\partial M_L}{\partial \xi_4} \Delta\xi_4 + \frac{\partial M_L}{\partial \xi_5} \Delta\xi_5$$

복원력(모멘트)의 선형화 (Taylor series expansion) [3]

✓ Taylor series 1차항까지 전개

$$\Delta F = \frac{\partial F}{\partial \xi_3} \Delta \xi_3 + \frac{\partial F}{\partial \xi_4} \Delta \xi_4 + \frac{\partial F}{\partial \xi_5} \Delta \xi_5$$

$$\Delta M_T = \frac{\partial M_T}{\partial \xi_3} \Delta \xi_3 + \frac{\partial M_T}{\partial \xi_4} \Delta \xi_4 + \frac{\partial M_T}{\partial \xi_5} \Delta \xi_5$$

$$\Delta M_L = \frac{\partial M_L}{\partial \xi_3} \Delta \xi_3 + \frac{\partial M_L}{\partial \xi_4} \Delta \xi_4 + \frac{\partial M_L}{\partial \xi_5} \Delta \xi_5$$

✓ Matrix로 표현 $\mathbf{b} = \mathbf{A}\mathbf{x}$

변수 3개, 식 3개



$$\begin{pmatrix} \Delta F \\ \Delta M_T \\ \Delta M_L \end{pmatrix} = \begin{pmatrix} \frac{\partial F}{\partial \xi_3} & \frac{\partial F}{\partial \xi_4} & \frac{\partial F}{\partial \xi_5} \\ \frac{\partial M_T}{\partial \xi_3} & \frac{\partial M_T}{\partial \xi_4} & \frac{\partial M_T}{\partial \xi_5} \\ \frac{\partial M_L}{\partial \xi_3} & \frac{\partial M_L}{\partial \xi_4} & \frac{\partial M_L}{\partial \xi_5} \end{pmatrix} \begin{pmatrix} \Delta \xi_3 \\ \Delta \xi_4 \\ \Delta \xi_5 \end{pmatrix}$$

1. **자세**의 변화량이 주어져 있을 때,
힘(모멘트)의 변화량을 구하는 경우

$$\begin{pmatrix} \Delta F \\ \Delta M_T \\ \Delta M_L \end{pmatrix} = \begin{pmatrix} \frac{\partial F}{\partial \xi_3} & \frac{\partial F}{\partial \xi_4} & \frac{\partial F}{\partial \xi_5} \\ \frac{\partial M_T}{\partial \xi_3} & \frac{\partial M_T}{\partial \xi_4} & \frac{\partial M_T}{\partial \xi_5} \\ \frac{\partial M_L}{\partial \xi_3} & \frac{\partial M_L}{\partial \xi_4} & \frac{\partial M_L}{\partial \xi_5} \end{pmatrix} \begin{pmatrix} \Delta \xi_3 \\ \Delta \xi_4 \\ \Delta \xi_5 \end{pmatrix}$$

Find ← Given Given

$\mathbf{b} = \mathbf{A}\mathbf{x}$ 를 풀면 됨

2. **힘(모멘트)**의 변화량이 주어져 있을 때,
자세의 변화량을 구하는 경우

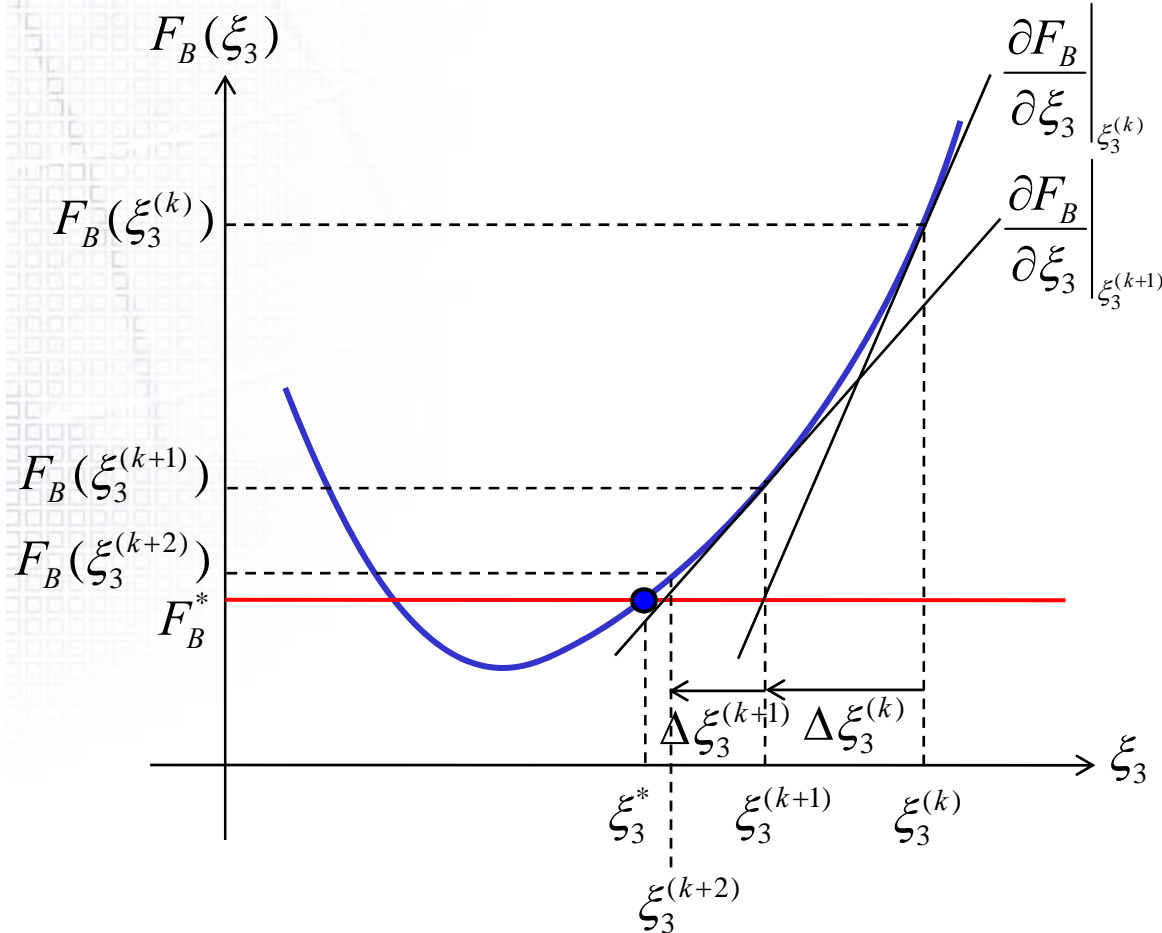
$$\begin{pmatrix} \Delta F \\ \Delta M_T \\ \Delta M_L \end{pmatrix} = \begin{pmatrix} \frac{\partial F}{\partial \xi_3} & \frac{\partial F}{\partial \xi_4} & \frac{\partial F}{\partial \xi_5} \\ \frac{\partial M_T}{\partial \xi_3} & \frac{\partial M_T}{\partial \xi_4} & \frac{\partial M_T}{\partial \xi_5} \\ \frac{\partial M_L}{\partial \xi_3} & \frac{\partial M_L}{\partial \xi_4} & \frac{\partial M_L}{\partial \xi_5} \end{pmatrix} \begin{pmatrix} \Delta \xi_3 \\ \Delta \xi_4 \\ \Delta \xi_5 \end{pmatrix}$$

Given Given Find →

$\mathbf{x} = \mathbf{A}^{-1}\mathbf{b}$ 를 풀면 됨

※ \mathbf{A} 가 선형화되어 있기 때문에
반복 계산(iteration)을 해야 함

목표 힘(F^*)에 대한 선박의 자세 계산 (1 변수 예)



Taylor series 1차 항까지 전개

$$F_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) = F_B(\xi_3^{(k)}) + \left. \frac{\partial F_B}{\partial \xi_3} \right|_{\xi_3^{(k)}} \cdot \Delta \xi_3^{(k)} = F_B^*$$

힘의 변화량과 자세의 변화량 관계

$$F_B^* - F_B(\xi_3^{(k)}) = \left. \frac{\partial F_B}{\partial \xi_3} \right|_{\xi_3^{(k)}} \cdot \Delta \xi_3^{(k)}$$

자세의 변화량에 대해 표현

$$\Delta \xi_3^{(k)} = \left(\left. \frac{\partial F_B}{\partial \xi_3} \right|_{\xi_3^{(k)}} \right)^{-1} (F_B^* - F_B(\xi_3^{(k)}))$$

자세 변화

$$\xi_3^{(k+1)} = \xi_3^{(k)} + \Delta \xi_3^{(k)}$$

$$|\xi_3^{(k+1)} - \xi_3^{(k)}| < \epsilon$$

No $k = k + 1$

Yes

종료 $\xi_3^* = \xi_3^{(k+1)}$

목표 힘(F^*, M_T^*, M_L^*)에 대한 선박의 자세 계산

힘의 변화량과 자세의 변화량 관계

$$F_B^* - F_B(\xi_3^{(k)}, \xi_4^{(k)}, \xi_5^{(k)}) = \frac{\partial F_B}{\partial \xi_3} \Big|_{\xi_3^{(k)}} \cdot \Delta \xi_3^{(k)} + \frac{\partial F_B}{\partial \xi_4} \Big|_{\xi_4^{(k)}} \cdot \Delta \xi_4^{(k)} + \frac{\partial F_B}{\partial \xi_5} \Big|_{\xi_5^{(k)}} \cdot \Delta \xi_5^{(k)}$$

$$M_T^* - M_T(\xi_3^{(k)}, \xi_4^{(k)}, \xi_5^{(k)}) = \frac{\partial M_T}{\partial \xi_3} \Big|_{\xi_3^{(k)}} \cdot \Delta \xi_3^{(k)} + \frac{\partial M_T}{\partial \xi_4} \Big|_{\xi_4^{(k)}} \cdot \Delta \xi_4^{(k)} + \frac{\partial M_T}{\partial \xi_5} \Big|_{\xi_5^{(k)}} \cdot \Delta \xi_5^{(k)}$$

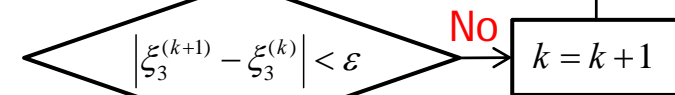
$$M_L^* - M_L(\xi_3^{(k)}, \xi_4^{(k)}, \xi_5^{(k)}) = \frac{\partial M_L}{\partial \xi_3} \Big|_{\xi_3^{(k)}} \cdot \Delta \xi_3^{(k)} + \frac{\partial M_L}{\partial \xi_4} \Big|_{\xi_4^{(k)}} \cdot \Delta \xi_4^{(k)} + \frac{\partial M_L}{\partial \xi_5} \Big|_{\xi_5^{(k)}} \cdot \Delta \xi_5^{(k)}$$

자세의 변화량에 대해 표현

$$\begin{bmatrix} \Delta \xi_3^{(k)} \\ \Delta \xi_4^{(k)} \\ \Delta \xi_5^{(k)} \end{bmatrix} = \begin{bmatrix} \frac{\partial F_B}{\partial \xi_3} \Big|_{\xi_3^{(k)}} & \frac{\partial F_B}{\partial \xi_4} \Big|_{\xi_4^{(k)}} & \frac{\partial F_B}{\partial \xi_5} \Big|_{\xi_5^{(k)}} \\ \frac{\partial M_T}{\partial \xi_3} \Big|_{\xi_3^{(k)}} & \frac{\partial M_T}{\partial \xi_4} \Big|_{\xi_4^{(k)}} & \frac{\partial M_T}{\partial \xi_5} \Big|_{\xi_5^{(k)}} \\ \frac{\partial M_L}{\partial \xi_3} \Big|_{\xi_3^{(k)}} & \frac{\partial M_L}{\partial \xi_4} \Big|_{\xi_4^{(k)}} & \frac{\partial M_L}{\partial \xi_5} \Big|_{\xi_5^{(k)}} \end{bmatrix}^{-1} \begin{bmatrix} F_B^* - F_B(\xi_3^{(k)}, \xi_4^{(k)}, \xi_5^{(k)}) \\ M_T^* - M_T(\xi_3^{(k)}, \xi_4^{(k)}, \xi_5^{(k)}) \\ M_L^* - M_L(\xi_3^{(k)}, \xi_4^{(k)}, \xi_5^{(k)}) \end{bmatrix}$$

자세 변화

$$\xi_3^{(k+1)} = \xi_3^{(k)} + \Delta \xi_3^{(k)}$$



종료 $\xi_3^* = \xi_3^{(k+1)}$

미소 자세와 미소 힘, 모멘트와의 관계식¹⁾

$$\begin{pmatrix} \Delta F \\ \Delta M_T \\ \Delta M_L \end{pmatrix} = \begin{pmatrix} \left. \frac{\partial F}{\partial \xi_3} \right|_{\xi_3^{(k)}} & \left. \frac{\partial F}{\partial \xi_4} \right|_{\xi_4^{(k)}} & \left. \frac{\partial F}{\partial \xi_5} \right|_{\xi_5^{(k)}} \\ \left. \frac{\partial M_T}{\partial \xi_3} \right|_{\xi_3^{(k)}} & \left. \frac{\partial M_T}{\partial \xi_4} \right|_{\xi_4^{(k)}} & \left. \frac{\partial M_T}{\partial \xi_5} \right|_{\xi_5^{(k)}} \\ \left. \frac{\partial M_L}{\partial \xi_3} \right|_{\xi_3^{(k)}} & \left. \frac{\partial M_L}{\partial \xi_4} \right|_{\xi_4^{(k)}} & \left. \frac{\partial M_L}{\partial \xi_5} \right|_{\xi_5^{(k)}} \end{pmatrix} \begin{pmatrix} \Delta \xi_3 \\ \Delta \xi_4 \\ \Delta \xi_5 \end{pmatrix}$$

Jacobian matrix
(자세 변화량을 힘과 모멘트의 변화량으로 변환)

$$= \begin{pmatrix} -\rho g A_{WP}(\xi_3^{(k)}) & -\rho g T_{WP}(\xi_3^{(k)}) & \rho g L_{WP}(\xi_3^{(k)}) \\ -\rho g T_{WP}(\xi_4^{(k)}) & -\rho g I_T(\xi_4^{(k)}) - \rho g V(\xi_4^{(k)}) z_B^{(k)} + mg \cdot z_G^{(k)} & \rho g I_P(\xi_4^{(k)}) \\ \rho g L_{WP}(\xi_5^{(k)}) & \rho g I_P(\xi_5^{(k)}) & -\rho g I_L(\xi_5^{(k)}) - \rho g V(\xi_5^{(k)}) z_B^{(k)} + mg \cdot z_G^{(k)} \end{pmatrix} \cdot \begin{pmatrix} \Delta \xi_3 \\ \Delta \xi_4 \\ \Delta \xi_5 \end{pmatrix}$$



Linked Slides

Advanced
Ship
Design
Automation
Laboratory

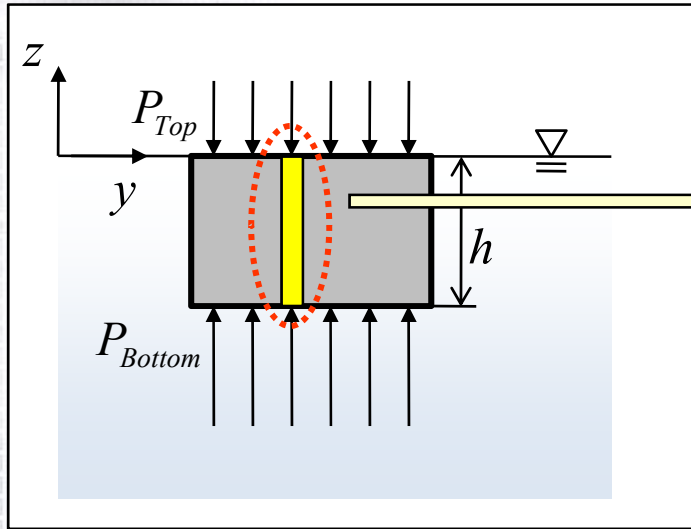
압력

$$P_{Static} = P_{atm} - \rho g z$$

$$P_{Fluid} = -\rho g z$$

※ 압력(Pressure) : 단위 면적에 수직으로 작용하는 힘 즉, 힘을 구하기 위해서는 압력에 면적과 그 작용면의 법선 벡터(Normal Vector)를 곱해야 함

✓ 아래 물체에 작용하는 수직방향의 정적인 힘은?



: 물체 윗면의 미소 면적에 작용하는 힘

$$dF_{Top} = P_{Top} \cdot \mathbf{n}_1 dS \quad \left(\begin{array}{l} P_{Top} = P_{atm} - \rho g \cdot 0 \\ \mathbf{n}_1 = -\mathbf{k} \end{array} \right)$$

\mathbf{n}_1 : Normal vector
 dS : Area

$$dF_{Bottom} = P_{Bottom} \cdot \mathbf{n}_2 dS \quad \left(\begin{array}{l} P_{Bottom} = P_{atm} - \rho g h \\ \mathbf{n}_2 = \mathbf{k} \end{array} \right)$$

: 물체 아랫면의 미소 면적에 작용하는 힘

$$\begin{aligned} dF &= dF_{Top} + dF_{Bottom} \\ &= P_{Top} \cdot \mathbf{n}_1 dS + P_{Bottom} \cdot \mathbf{n}_2 dS \\ &= \cancel{P_{atm}} (-\mathbf{k}) dS + (\cancel{P_{atm}} - \rho g h) \mathbf{k} dS \\ &= -\rho g h \mathbf{k} dS = \mathbf{k} (-\rho g h \cdot dS) \end{aligned}$$

: 대기압에 의한 힘이 서로 상쇄됨

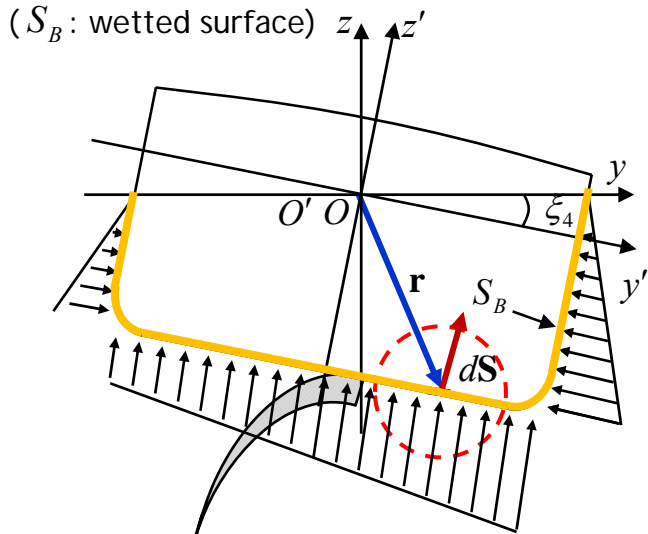
✓ Bernoulli Equation : (where $P_{Static} = P_{atm} + P_{Fluid}$)

$$\begin{aligned} \rho \frac{\partial \Phi}{\partial t} + P + \frac{1}{2} \rho |\nabla \Phi|^2 + \rho g z &= P_{atm} \\ \rho \frac{\partial \Phi}{\partial t} + (P_{atm} + P_{Fluid}) + \frac{1}{2} \rho |\nabla \Phi|^2 + \rho g z &= P_{atm} \\ \rho \frac{\partial \Phi}{\partial t} + P_{Fluid} + \frac{1}{2} \rho |\nabla \Phi|^2 + \rho g z &= 0 \end{aligned}$$

선박에 작용하는 정적인 힘과 모멘트

$$P_{Fluid} = -\rho g z$$

좌현으로 기울어진 상태 (횡 경사)
(선박을 선수에서 선미 방향으로 바라봄)



(미소 면적에 작용하는 힘)
 $d\mathbf{F} = P_{Fluid} d\mathbf{S} = P_{Fluid} \mathbf{n} dS$
 $= -\rho g z \mathbf{n} dS$

$d\mathbf{M} = \mathbf{r} \times d\mathbf{F}$ (미소 면적)
 (미소 면적에 작용하는 모멘트)
 \mathbf{r}

Hydrostatic force
: 침수표면에 작용하는 모든 정적인 힘을 적분하여 구함



✓ 미소 면적에 작용하는 힘 :

$$d\mathbf{F} = P_{Fluid} \cdot d\mathbf{S} = P_{Fluid} \cdot \mathbf{n} dS = -\rho g z \cdot \mathbf{n} dS$$

✓ Total force :

$$\mathbf{F} = \iint_{S_B} P_{Fluid} \mathbf{n} dS \Rightarrow \mathbf{F} = -\rho g \iint_{S_B} \mathbf{n} z dS$$

Hydrostatic Moment : (모멘트) = (거리) X (힘)

✓ 미소 면적에 작용하는 모멘트 :

$$d\mathbf{M} = \mathbf{r} \times d\mathbf{F} = \mathbf{r} \times P_{Fluid} \mathbf{n} dS = (\mathbf{r} \times \mathbf{n}) P_{Fluid} dS$$

✓ Total moment :

$$\mathbf{M} = \iint_{S_B} P_{Fluid} (\mathbf{r} \times \mathbf{n}) dS \Rightarrow \mathbf{M} = -\rho g \iint_{S_B} (\mathbf{r} \times \mathbf{n}) z dS$$

왜 r이 먼저 오는가? (좌표축에서 양의 방향을 고려함)

Hydrostatic Force

✓ Hydrostatic force (Surface force)

$$\mathbf{F} = -\rho g \iint_{S_B} \mathbf{n} z dS$$



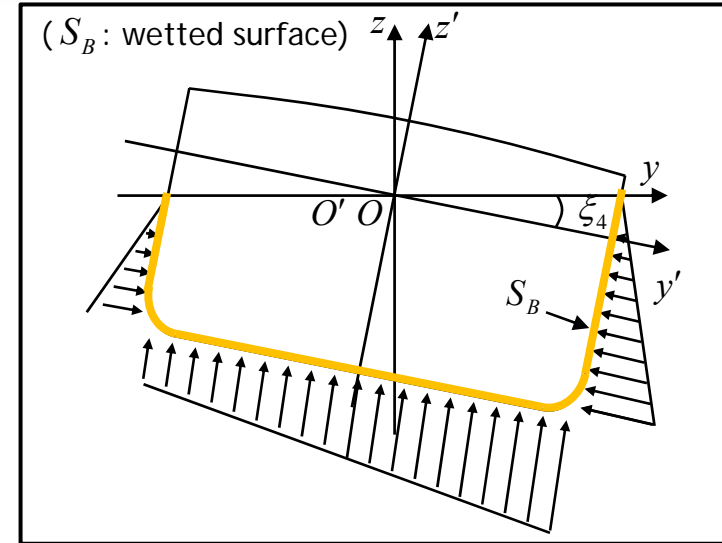
Divergence theorem¹⁾ 사용하면,

$$\left(\iiint_V \nabla f dV = \iint_S f \cdot \mathbf{n} dA \right)$$

$$\mathbf{F} = \rho g \iiint_V \nabla z dV \quad \left(\nabla z \stackrel{2)}{=} \frac{\partial z}{\partial x} \mathbf{i} + \frac{\partial z}{\partial y} \mathbf{j} + \frac{\partial z}{\partial z} \mathbf{k} = \mathbf{k} \right)$$

$$= \mathbf{k} \rho g \iiint_V dV$$

$$= \mathbf{k} \rho g V(t)$$



$$\therefore \mathbf{F} = \mathbf{k} \rho g \iiint_V dV$$

: 유체에 잠긴 물체가 배제한(displaced) 유체의 무게만큼의 위쪽 방향으로 받는 힘(부력)
 (Archimedes' Principle)

※ [-]부호가 사라진 이유

: Divergence theorem은 면의 외향 단위 벡터를 기준으로 한다.
 부력 계산시 사용하는 Normal vector는 내향 단위 벡터이므로,
 (-)를 곱한 뒤, Divergence theorem을 적용해야 한다.

Hydrostatic Moment

✓ Hydrostatic moment

$$\mathbf{M} = -\rho g \iint_{S_B} (\mathbf{r} \times \mathbf{n}) z dS = \rho g \iint_{S_B} (\mathbf{n} \times \mathbf{r}) z dS$$



Divergence theorem¹⁾ 사용하면,

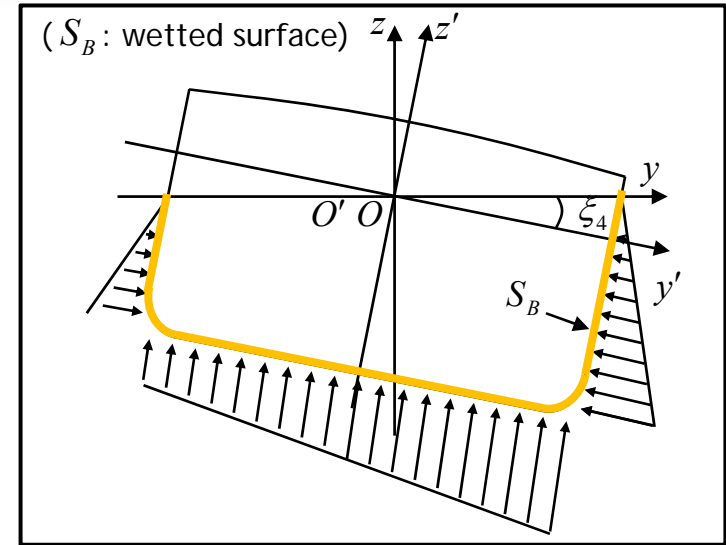
$$\left(\iiint_V \nabla \times \mathbf{F} dV = \iint_S \mathbf{n} \times \mathbf{F} dA \right)$$

$$\mathbf{M} = -\rho g \iiint_V (\nabla \times \mathbf{r}) z dV$$

Normal Vector의 방향이 반대이므로 (-)부호를 붙여줌

$$\left(\begin{array}{l} \text{2)} \\ \nabla \times \mathbf{r} z = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xz & yz & z^2 \end{vmatrix} = \mathbf{i} \left(\frac{\partial}{\partial y} z^2 - \frac{\partial}{\partial z} yz \right) + \mathbf{j} \left(\frac{\partial}{\partial z} xz - \frac{\partial}{\partial x} z^2 \right) + \mathbf{k} \left(\frac{\partial}{\partial x} yz - \frac{\partial}{\partial y} xz \right) = -\mathbf{i}y + \mathbf{j}x \end{array} \right)$$

$$\therefore \mathbf{M} = -\rho g \iiint_V [-\mathbf{i}y + \mathbf{j}x] dV$$



← 의미 ?

Hydrostatic Moment (횡 경사)

✓ Hydrostatic moment



$$\mathbf{M} = -\rho g \iiint_V [-\mathbf{i}y + \mathbf{j}x] dV = \rho g \iiint_V [\mathbf{i}y - \mathbf{j}x] dV$$

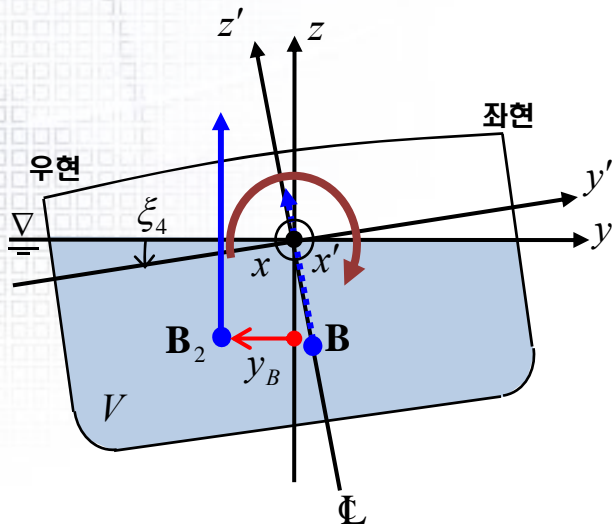
$$= \rho g \iiint_V \mathbf{i}y dV - \rho g \iiint_V \mathbf{j}x dV = \mathbf{i}\rho g V y_B - \mathbf{j}\rho g V x_B = \mathbf{i}M_{BT} + \mathbf{j}M_{BL}$$

부력에 의한 횡 방향 모멘트 | 부력에 의한 종 방향 모멘트

부력의 횡 방향 중심 | 부력의 종 방향 중심

$(M_{BL} = \rho g V \cdot x_B)$

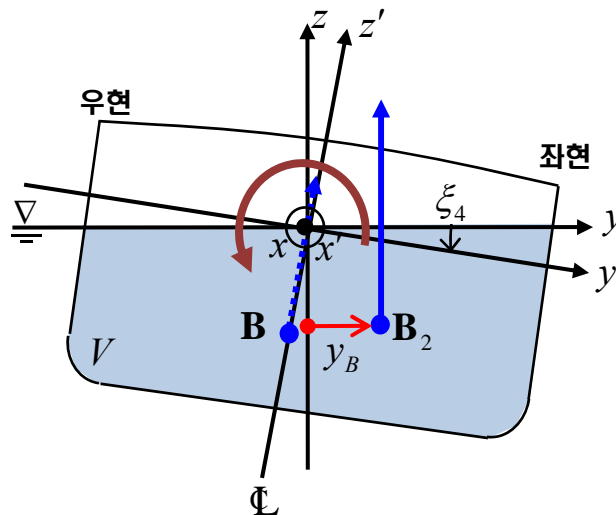
< 우현으로 기울었을 경우(+방향) >



$$\mathbf{M}_{BT} < 0$$

$y_B < 0$ 이므로, 음의 모멘트

< 좌현으로 기울었을 경우(-방향) >



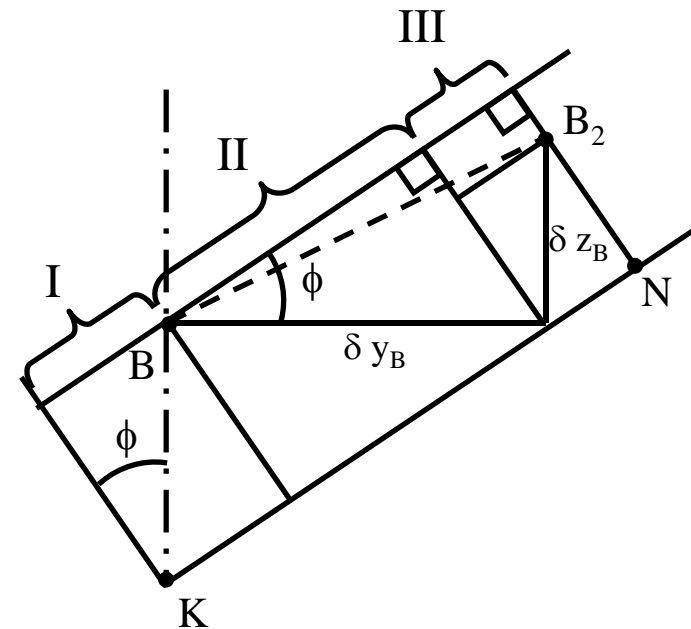
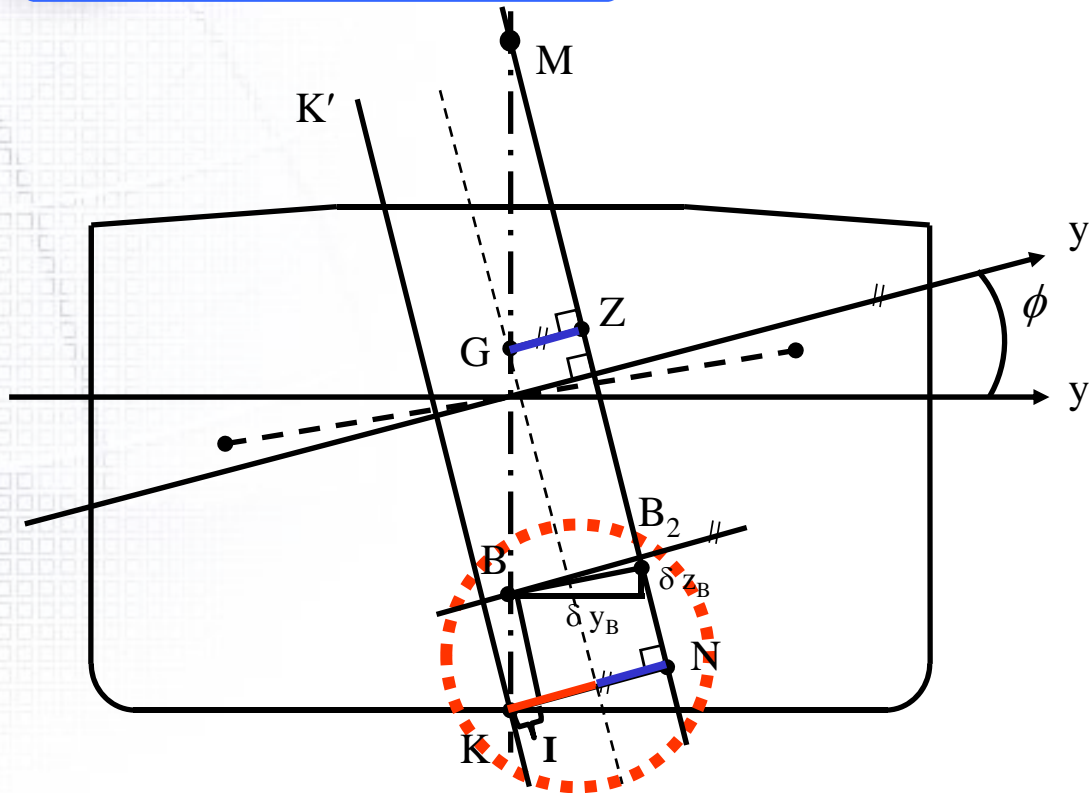
$$\mathbf{M}_{BT} > 0$$

$y_B > 0$ 이므로, 양의 모멘트

선박 안정론¹⁾ [선박계산법]의 횡방향 부력 모멘트

1) 이규열, 노명일, 안재운, 선박안정론, 5th, pp.96-97

부심 이동에 따른 복원 아암 KN



$$\begin{aligned}
 KN(\phi) &= I + II + III \\
 &= KB \sin \phi + \delta y_B \cos \phi + \delta z_B \sin \phi \\
 &= KG \sin \phi + GZ
 \end{aligned}$$

Hydrostatic Moment (횡 경사)

✓ Hydrostatic moment



$$\mathbf{M} = -\rho g \iiint_V [-\mathbf{i}y + \mathbf{j}x] dV = \rho g \iiint_V [\mathbf{i}y - \mathbf{j}x] dV$$

$$= \rho g \iiint_V \mathbf{i}y dV - \rho g \iiint_V \mathbf{j}x dV = \mathbf{i}\rho g V y_B - \mathbf{j}\rho g V x_B = \mathbf{i}M_{BT} + \mathbf{j}M_{BL}$$

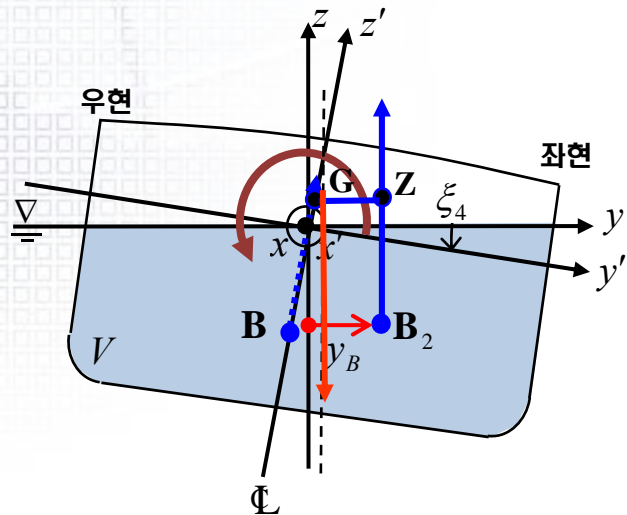
부력에 의한 횡 방향 모멘트 | 부력에 의한 종 방향 모멘트

부력

부력의 횡 방향 중심 | 부력의 종 방향 중심

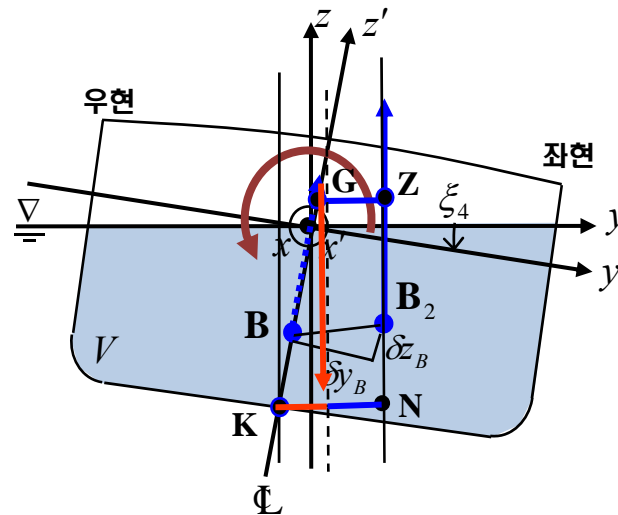
$(M_{BL} = \rho g V \cdot x_B)$

< 좌현으로 기울었을 경우(-방향) >



y_B : 수선면 고정 좌표계의 x축을 기준으로 한 부력의 횡 방향 모멘트 암

< 선박 안정론 > $KN = KG \sin \phi + GZ$



KN : 배 밑면의 중심 K를 통과하는 축을 기준으로 한 부력의 횡 방향 모멘트 암

(Q) 다른 것인가?

(A) 중력에 의한 모멘트를 고려해 보면, 모두 GZ 가 횡 복원 모멘트 암이 된다.

즉, 선박이 받는 횡 복원 모멘트는 동일하다.

Hydrostatic Moment (중 경사)



✓ Hydrostatic moment



$$\mathbf{M} = -\rho g \iiint_V [-\mathbf{i}y + \mathbf{j}x] dV = \rho g \iiint_V [\mathbf{i}y - \mathbf{j}x] dV$$

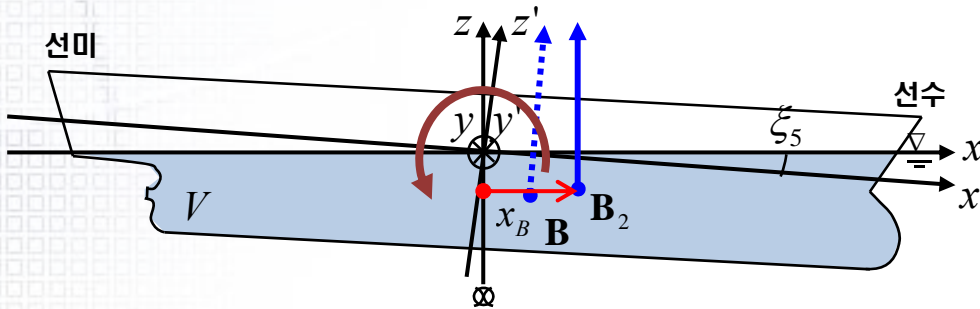
$$= \rho g \iiint_V \mathbf{i}y dV - \rho g \iiint_V \mathbf{j}x dV = \mathbf{i}\rho g V y_B - \mathbf{j}\rho g V x_B = \mathbf{i}M_{BT} + \mathbf{j}M_{BL}$$

부력에 의한
횡 방향 모멘트 | 부력에 의한
종 방향 모멘트

부력의 횡 방향 중심 | 부력의 종 방향 중심

$(M_{BL} = \rho g V \cdot x_B)$

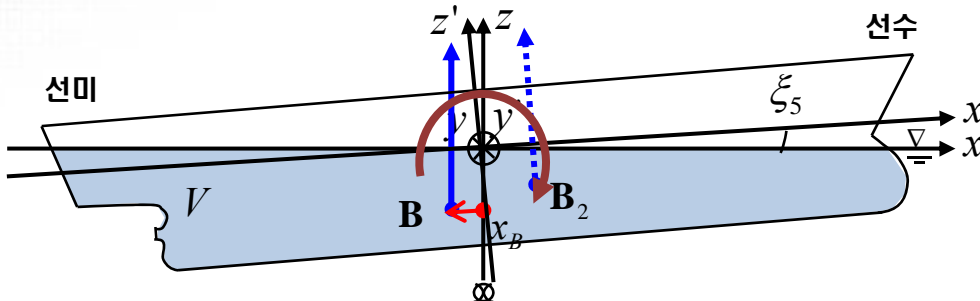
< 선수쪽으로 기울었을 경우(+방향) >



$$\mathbf{M}_{BL} < 0$$

$x_B > 0$ 이므로, 음의 모멘트

< 선미쪽으로 기울었을 경우(-방향) >



$$\mathbf{M}_{BL} > 0$$

$x_B < 0$ 이므로, 양의 모멘트

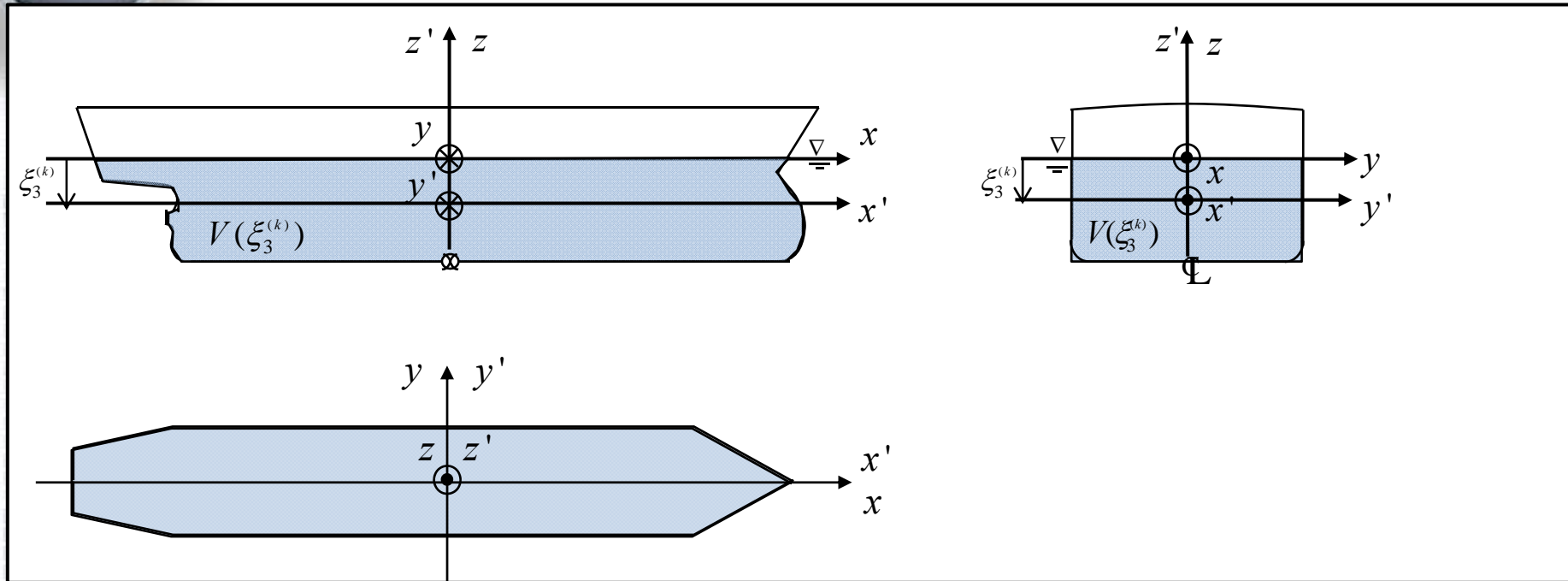


Linked Slides

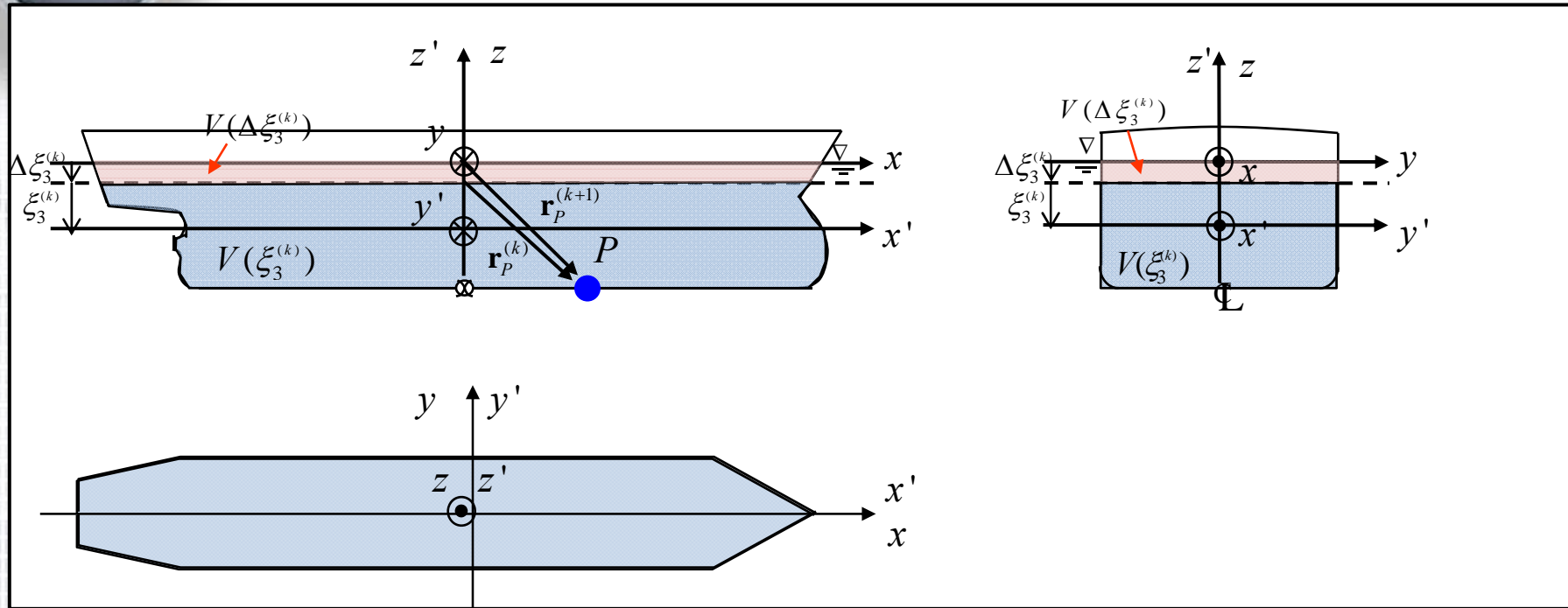
– Pressure Integration Technique을 이용한
부력, 횡 방향 모멘트, 종 방향 모멘트 계산

J.N.Newman, Marine Hydrodynamics, 1977,
pp.290~295

Immersion에 의한 좌표계 변환



Immersion에 의한 좌표계 변환



ex) 선박이 immersion하고 있다. k번째 immersion 상태에서 흘수가 20 m 였다면, k+1번째 상태에서 1m 가라 앉았을 때, 각각 k번째 와 k+1번째의 배 밑면의 좌표를 구하시오.

sol) k번째 에서는 $z_P^{(k)} = -20$

k+1번째 에서는 배가 아래로 1m 내려간 것이므로, $z_P^{(k+1)} = -21$

즉, 변위 $\Delta \xi_3^{(k)} = -1$ 이라고 할 때, $z_P^{(k)}$ 와 $z_P^{(k+1)}$ 사이에는 다음 관계가 성립한다.

$$z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)}$$

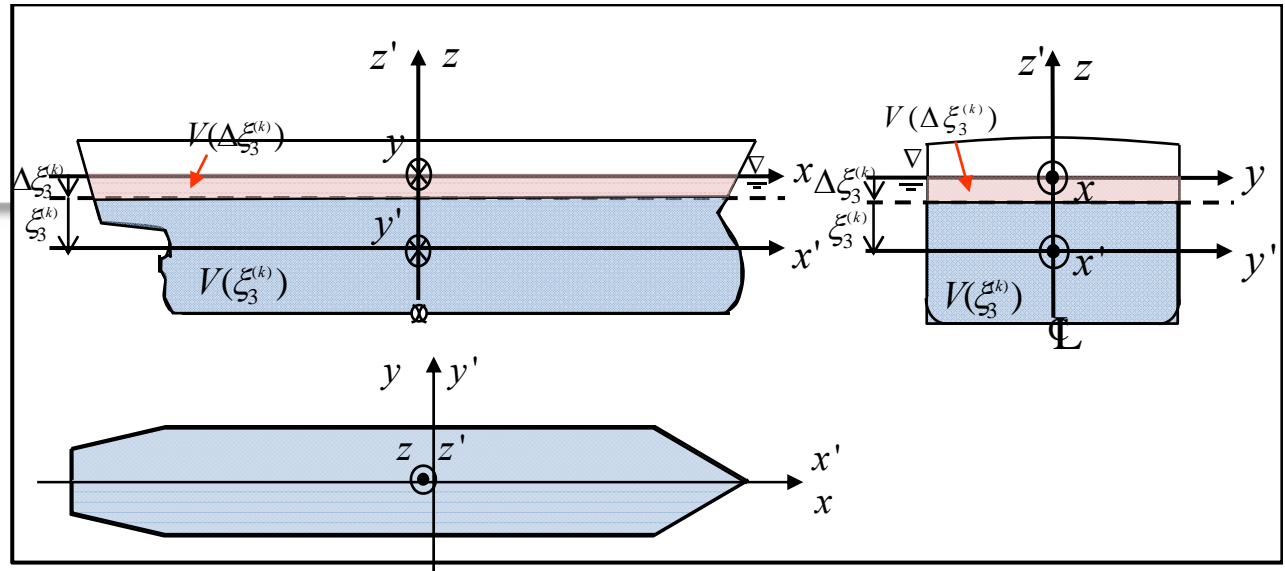
$$\left(x_P^{(k+1)} = x_P^{(k)}, y_P^{(k+1)} = y_P^{(k)} \right)$$

x,y는 좌표 동일함

Immersion에 의한 힘 (부력) (1)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$



$\mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$ (k)번째 상태의 부피와
변화된 부피에 의한
힘으로 분리 (k)번째 상태의 부피

$$= \mathbf{k}\rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} dV = \mathbf{k}\rho g \left\{ \iiint_{V(\xi_3^{(k)})} dV + \iiint_{V(\Delta \xi_3^{(k)})} dV \right\}$$

$$\iiint_{V(\xi_3^{(k)})} dV = \iiint_{V(\xi_3^{(k)})} dx dy dz = V(\xi_3^{(k)})$$

Immersion에 의한 힘 (부력) (2)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$\mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$ (k)번째 상태의 부피와
변화된 부피에 의한
힘으로 분리

$$= \mathbf{k}\rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} dV = \mathbf{k}\rho g \left\{ \iiint_{V(\xi_3^{(k)})} dV + \iiint_{V(\Delta \xi_3^{(k)})} dV \right\}$$

적분하기 편리하게 적분 순서를 변경

$$\iiint_{V(\Delta \xi_3^{(k)})} dV = \iiint_{V(\Delta \xi_3^{(k)})} dx dy dz = \int_{x_A^{(k)}}^{x_F^{(k)}} \int_{y_S^{(k)}}^{y_P^{(k)}} \int_{z_L^{(k)}}^{z_U^{(k)}} dz dy dx$$

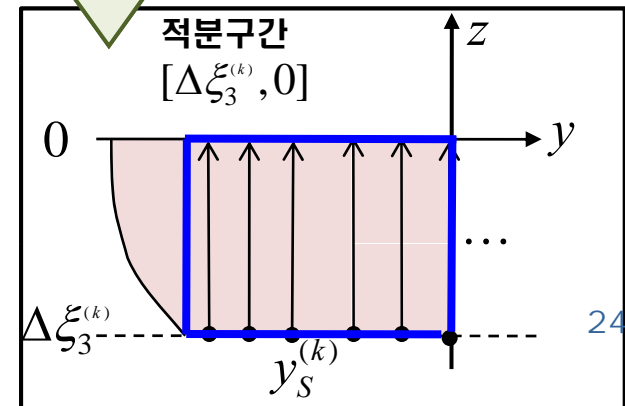
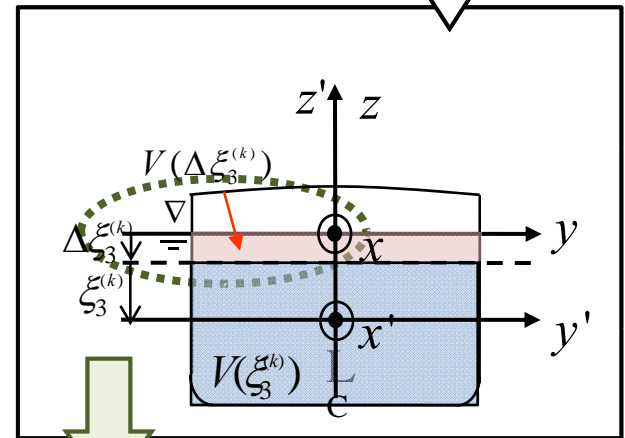
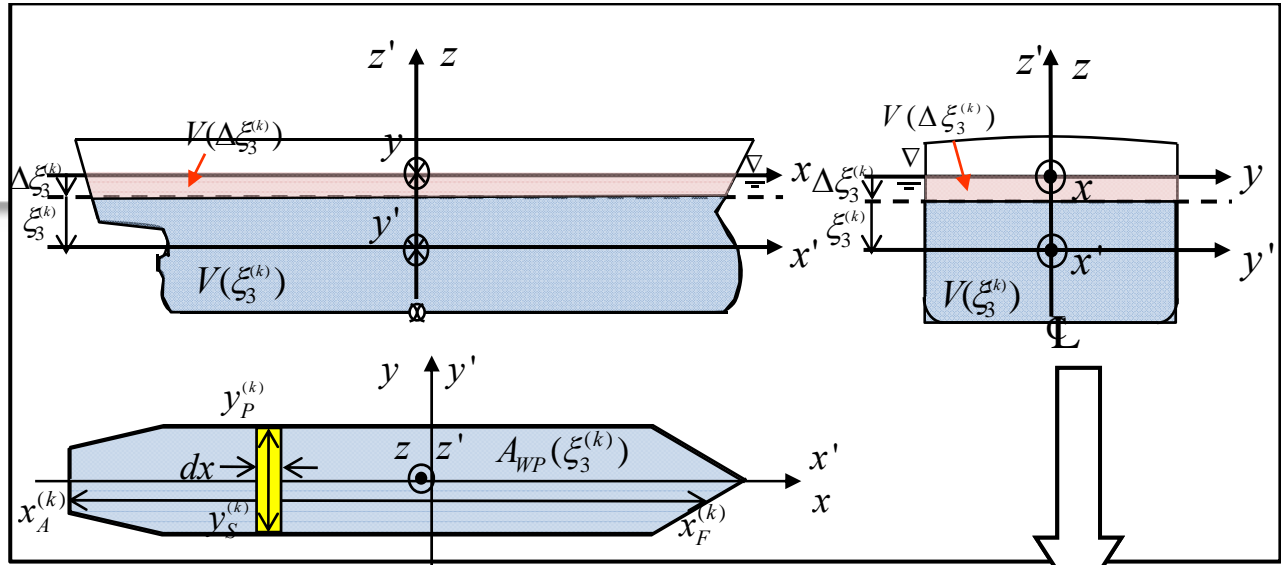
만약 $\Delta \xi_3^{(k)}$ 가 작다면,

$$\approx \int_{x_A^{(k)}}^{x_F^{(k)}} \int_{y_S^{(k)}}^{y_P^{(k)}} \int_{\Delta \xi_3^{(k)}}^0 dz dy dx = \int_{x_A^{(k)}}^{x_F^{(k)}} \int_{y_S^{(k)}}^{y_P^{(k)}} (-\Delta \xi_3^{(k)}) dy dx$$

$$= \int_{x_A^{(k)}}^{x_F^{(k)}} (-\Delta \xi_3^{(k)}) [y_P^{(k)} - y_S^{(k)}] dx = -\Delta \xi_3^{(k)} \int_{x_A^{(k)}}^{x_F^{(k)}} [y_P^{(k)} - y_S^{(k)}] dx$$

$$= -\Delta \xi_3^{(k)} A_{WP}(\xi_3^{(k)})$$

(k)번째 상태의 수선면적



Immersion에 의한 힘 (부력) (3)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$\mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$ (k)번째 상태의 부피와
변화된 부피에 의한
힘으로 분리

$$= k\rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} dV = k\rho g \left\{ \iiint_{V(\xi_3^{(k)})} dV + \iiint_{V(\Delta \xi_3^{(k)})} dV \right\}$$

변화된 부피

$$\iiint_{V(\Delta \xi_3^{(k)})} dV \approx \frac{-\Delta \xi_3^{(k)}}{(-)} \frac{A_{WP}(\xi_3^{(k)})}{(+)}$$

(+)

부호 검증

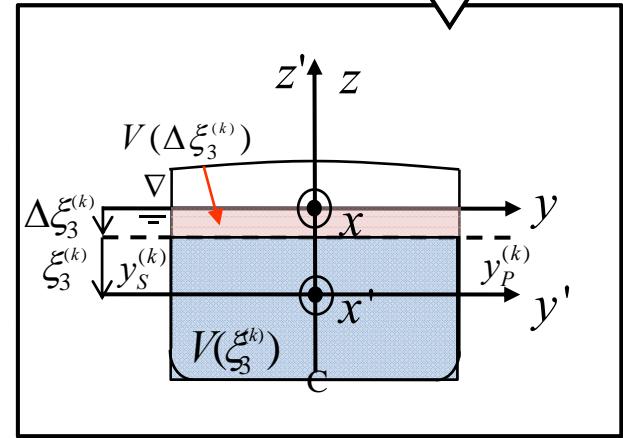
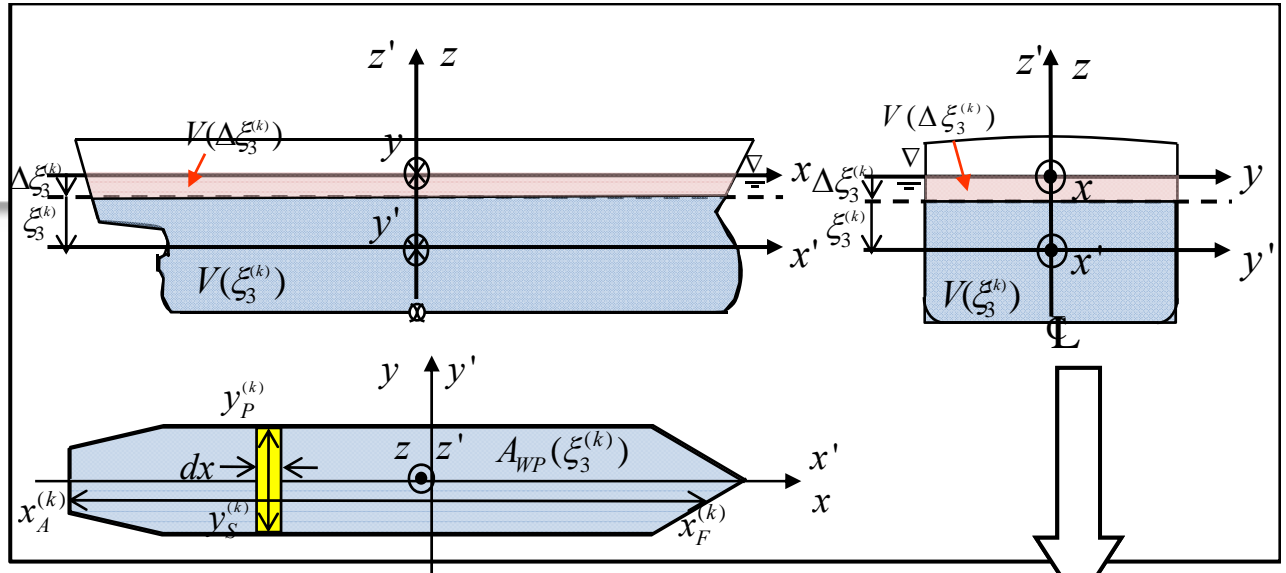
$A_{WP}(\xi_3^{(k)})$ 는 항상 (+)



$\Delta \xi_3^{(k)}$ 이 (-)이면, 가라앉는 것임.



이 때 \mathbf{F} 는 (+) → 부력 증가



Immersion에 의한 힘 (부력) (4)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$$\mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$$

$$= \mathbf{k}\rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} dV = \mathbf{k}\rho g \left\{ \iiint_{V(\xi_3^{(k)})} dV + \iiint_{V(\Delta \xi_3^{(k)})} dV \right\}$$

만약 $\Delta \xi_3^{(k)}$ 가 작다면,

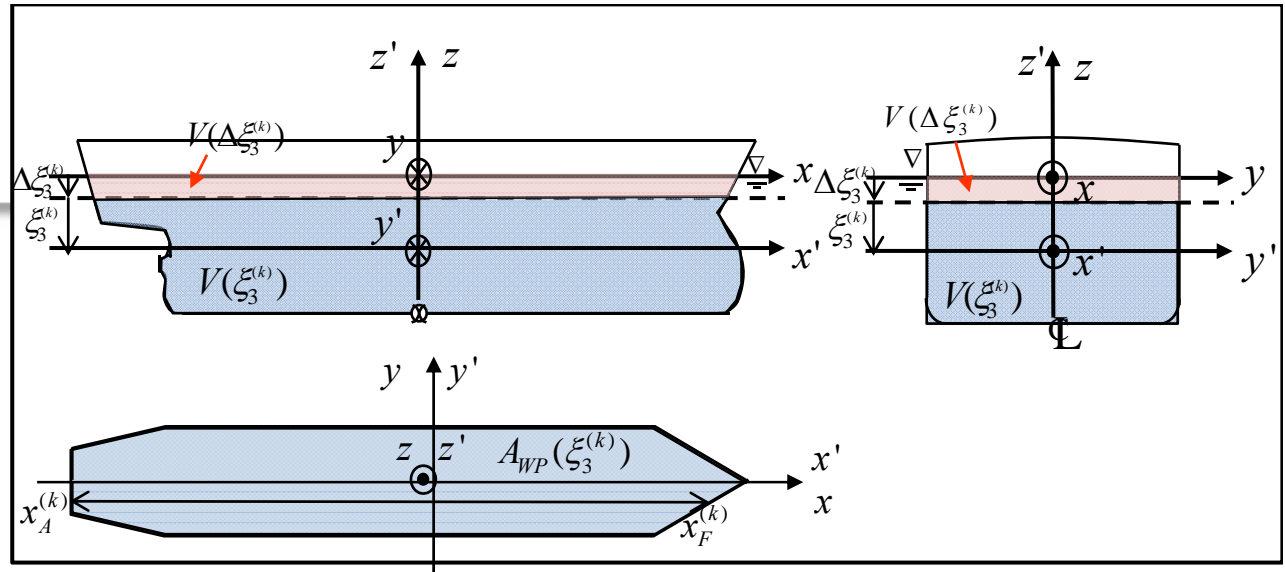
$$\approx \mathbf{k}\rho g (V(\xi_3^{(k)}) - \Delta \xi_3^{(k)} \underbrace{A_{WP}(\xi_3^{(k)})}_{(k)\text{번째 상태의 수선면적}})$$

(k)번째 상태의 수선면적

$$\mathbf{F}_B(\xi_3^{(k)}) = \mathbf{k}\rho g V(\xi_3^{(k)})$$

대입하면,

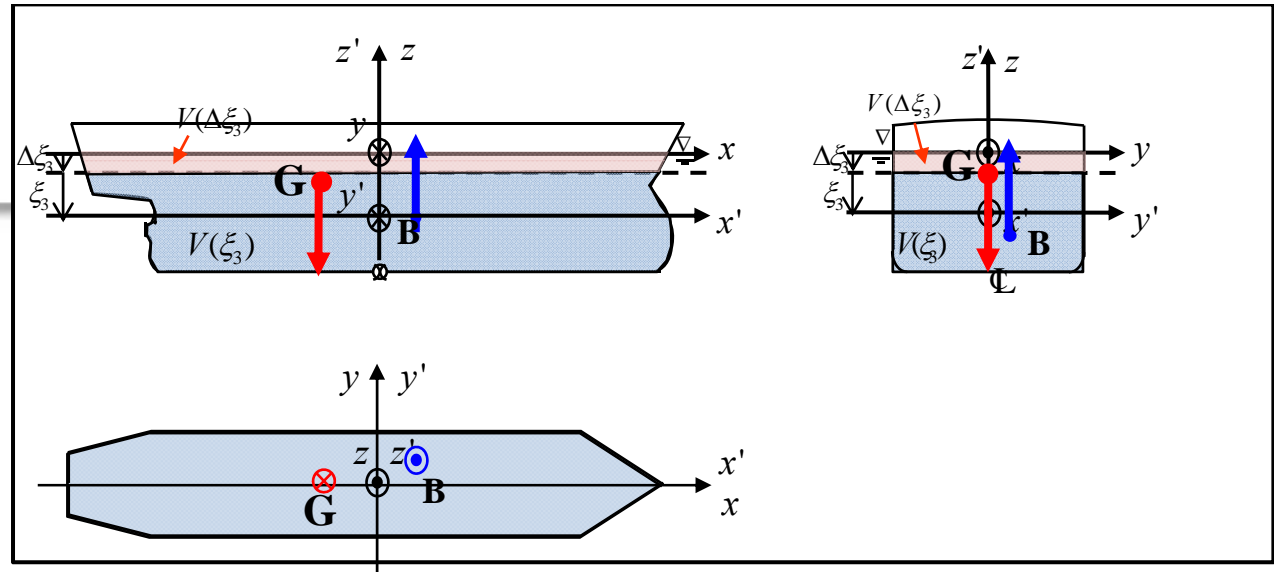
$$\mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) = \mathbf{F}_B(\xi_3^{(k)}) - \mathbf{k}\rho g A_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)}$$



Immersion에 의한 힘 (부력) (5)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$



✓ 부력

$$\mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) = \mathbf{F}_B(\xi_3^{(k)}) - \mathbf{k} \rho g A_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)}$$

✓ 중력

$$\mathbf{F}_G(\xi_3^{(k)} + \Delta \xi_3^{(k)}) = -\mathbf{k} m g = \mathbf{F}_G(\xi_3^{(k)})$$

✓ 선박이 받는 힘

$$\begin{aligned} \mathbf{F}(\xi_3^{(k)} + \Delta \xi_3^{(k)}) &= \mathbf{F}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) + \mathbf{F}_G(\xi_3^{(k)} + \Delta \xi_3^{(k)}) \\ &= \mathbf{F}_B(\xi_3^{(k)}) + \mathbf{F}_G(\xi_3^{(k)}) - \mathbf{k} \rho g A_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} = \mathbf{F}(\xi_3^{(k)}) - \mathbf{k} \rho g A_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} \end{aligned}$$

$$\mathbf{F}(\xi_3^{(k)} + \Delta \xi_3^{(k)}) - \mathbf{F}(\xi_3^{(k)}) = \mathbf{k} \left\{ -\rho g A_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} \right\}$$

$$\Delta \mathbf{F}(\xi_3^{(k)}) = \mathbf{k} \left. \frac{\partial \mathbf{F}}{\partial \xi_3} \right|_{\xi_3^{(k)}} \Delta \xi_3^{(k)}$$

$$\left. \frac{\partial \mathbf{F}}{\partial \xi_3} \right|_{\xi_3^{(k)}} = -\rho g A_{WP}(\xi_3^{(k)})$$

Immersion에 의한 모멘트 (1)

좌표 변환

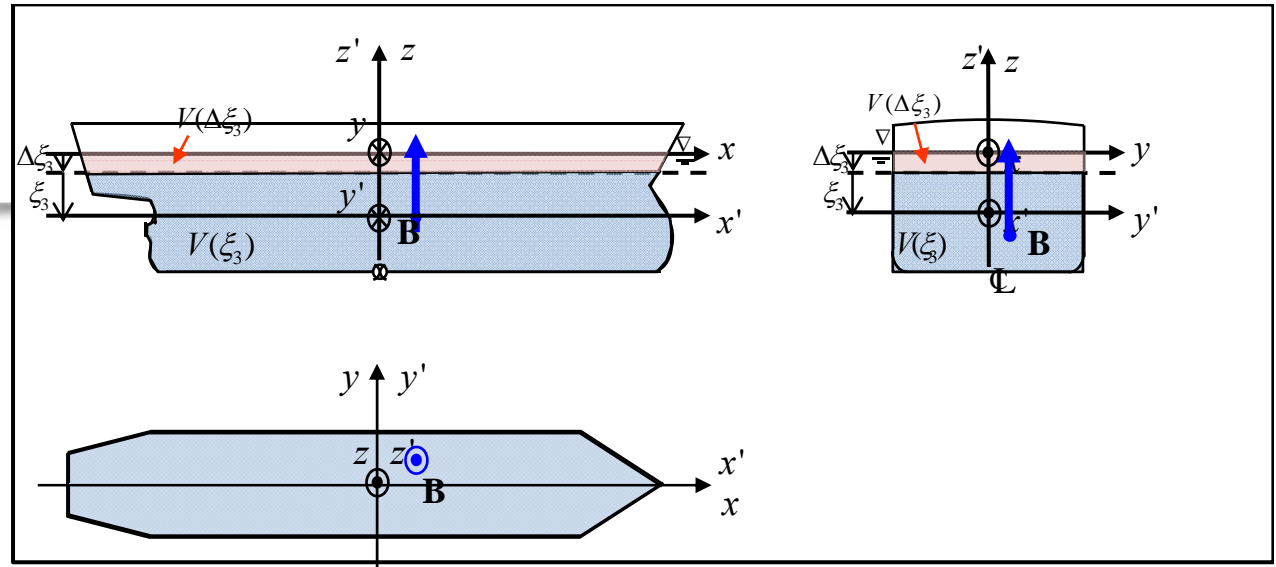
$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$$\mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$$

$$= \rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \rho g \left\{ \underbrace{\iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV}_{\text{K번째 상태의 부피}} + \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV \right\}$$

$$\iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dx dy dz = \mathbf{i} \iiint_{V(\xi_3^{(k)})} y dx dy dz - \mathbf{j} \iiint_{V(\xi_3^{(k)})} x dx dy dz$$

$$= \mathbf{i}V(\xi_3^{(k)})y_B^{(k+1)} - \mathbf{j}V(\xi_3^{(k)})x_B^{(k+1)} = \mathbf{i}V(\xi_3^{(k)})y_B^{(k)} - \mathbf{j}V(\xi_3^{(k)})x_B^{(k)}$$



Immersion에 의한 모멘트 (2)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$$\mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$$

$$= \rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \rho g \left\{ \iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV + \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV \right\}$$

변화된 부피

$$\iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dx dy dz$$

만약 $\Delta \xi_3^{(k)}$ 가 작다면

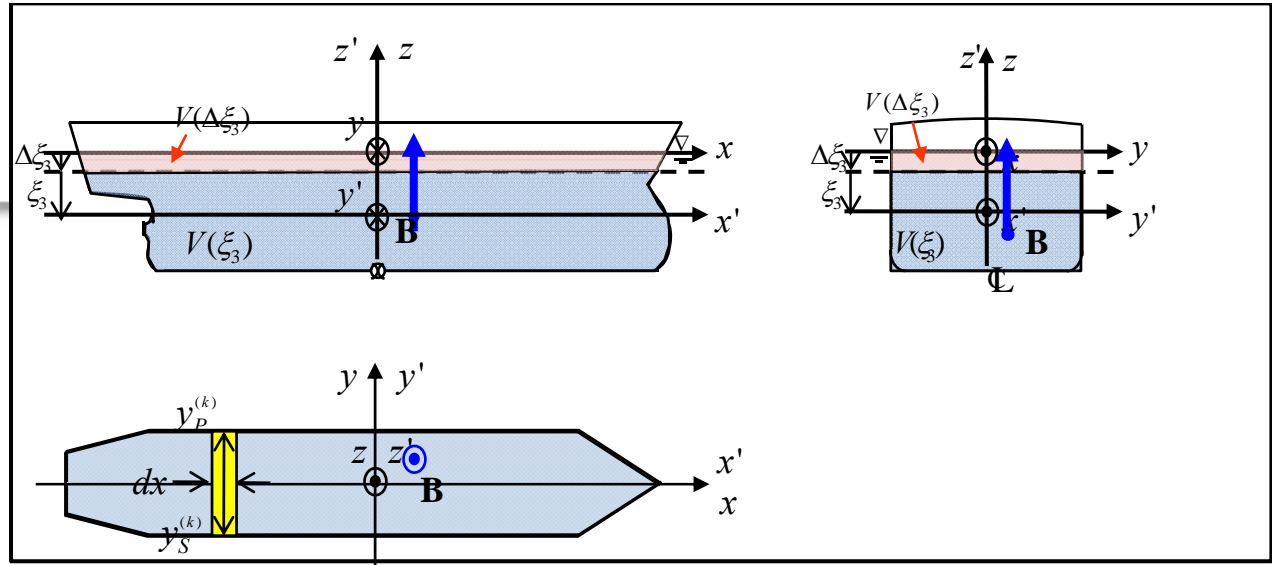
$$\begin{aligned} &\approx \int_{x_A^{(k)}}^{x_F^{(k)}} \int_{y_S^{(k)}}^{y_P^{(k)}} \int_{\Delta \xi_3^{(k)}}^0 [\mathbf{i}y - \mathbf{j}x] dz dy dx = \int_{x_A^{(k)}}^{x_F^{(k)}} \int_{y_S^{(k)}}^{y_P^{(k)}} [\mathbf{i}yz - \mathbf{j}xz]_{\Delta \xi_3^{(k)}}^0 dy dx = \int_{x_A^{(k)}}^{x_F^{(k)}} \int_{y_S^{(k)}}^{y_P^{(k)}} \{ \mathbf{i}y(-\Delta \xi_3^{(k)}) - \mathbf{j}x(-\Delta \xi_3^{(k)}) \} dy dx \\ &= -\Delta \xi_3^{(k)} \int_{x_A^{(k)}}^{x_F^{(k)}} \left\{ \mathbf{i} \frac{y^2}{2} \Big|_{y_S^{(k)}}^{y_P^{(k)}} - \mathbf{j}xy \Big|_{y_S^{(k)}}^{y_P^{(k)}} \right\} dx = -\Delta \xi_3^{(k)} \int_{x_A^{(k)}}^{x_F^{(k)}} \left\{ \mathbf{i} \frac{(y_P^{(k)})^2 - (y_S^{(k)})^2}{2} - \mathbf{j}x(y_P^{(k)} - y_S^{(k)}) \right\} dx \\ &= -\Delta \xi_3^{(k)} \left\{ \int_{x_A^{(k)}}^{x_F^{(k)}} \mathbf{i} \frac{(y_P^{(k)})^2 - (y_S^{(k)})^2}{2} dx - \int_{x_A^{(k)}}^{x_F^{(k)}} \mathbf{j}x(y_P^{(k)} - y_S^{(k)}) dx \right\} = -\Delta \xi_3^{(k)} (\mathbf{i}T_{WP}(\xi_3^{(k)}) - \mathbf{j}L_{WP}(\xi_3^{(k)})) \end{aligned}$$

$\left[\frac{y_P^{(k)} + y_S^{(k)}}{2} \right] \times [y_P^{(k)} - y_S^{(k)}] dx$
 횡 방향 중심 수선면적

$x \times [y_P^{(k)} - y_S^{(k)}] dx$
 종 방향 중심 수선면적

수선면의
 횡 방향 1차 모멘트

수선면의
 종 방향 1차 모멘트



Immersion에 의한 모멘트 (3)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$$\mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$$

$$= \rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \rho g \left\{ \iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV + \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV \right\}$$

변화된 부피

$$\iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dx dy dz$$

만약 $\Delta \xi_3^{(k)}$ 가 작다면,

$$\approx \frac{\text{수선면의 횡 방향 1차 모멘트}}{(-)} \approx \frac{\text{수선면의 종 방향 1차 모멘트}}{(+)} \approx -\Delta \xi_3^{(k)} (\mathbf{i}T_{WP}(\xi_3^{(k)}) - \mathbf{j}L_{WP}(\xi_3^{(k)}))$$

부호 검증

$T_{WP}(\xi_3^{(k)})$ 가 (+)이면, 수선면 중심이 좌현쪽



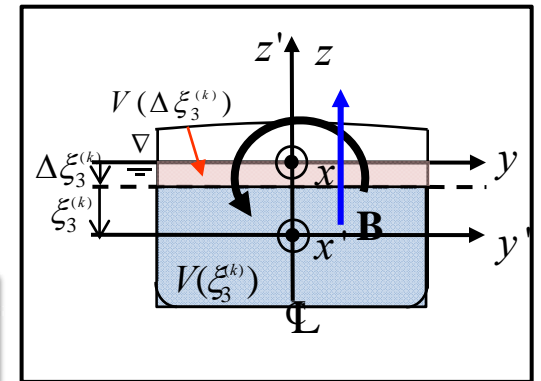
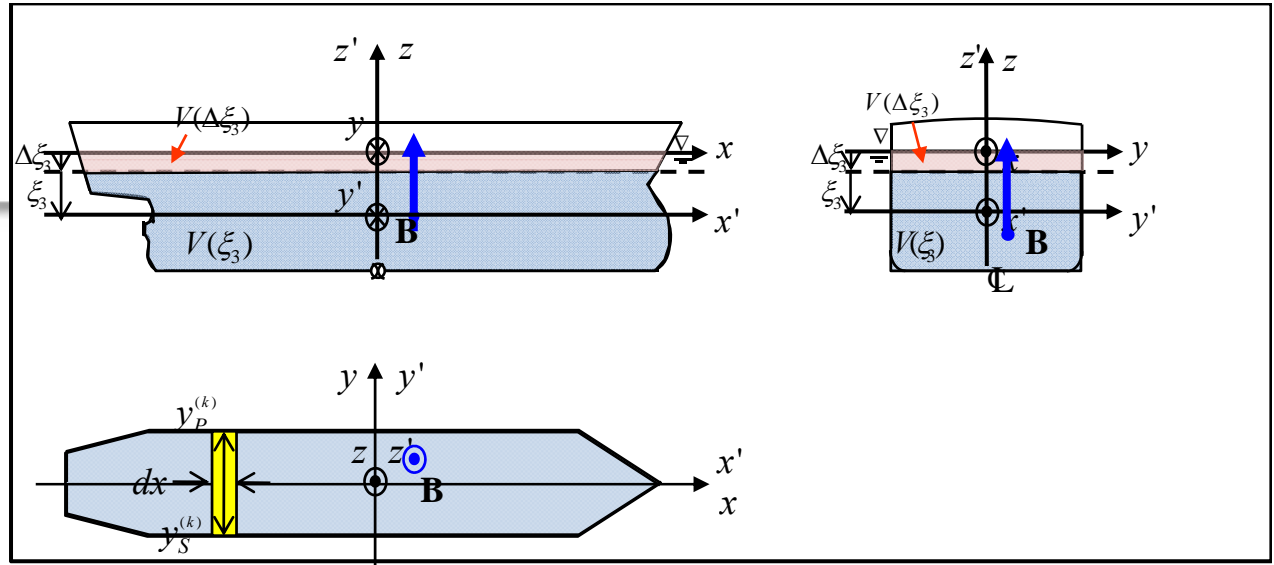
$\Delta \xi_3^{(k)}$ 이 (-)이면, 가라앉는 것임.



이 때, 수선면 중심이 좌현쪽이기 때문에, 부력 중심도 좌현쪽 (미소 자세)



x 축에 대한 (+)의 모멘트



Immersion에 의한 모멘트 (4)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

$$\mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)})$$

$$= \rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \rho g \left\{ \iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV + \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV \right\}$$

$$\iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dx dy dz$$

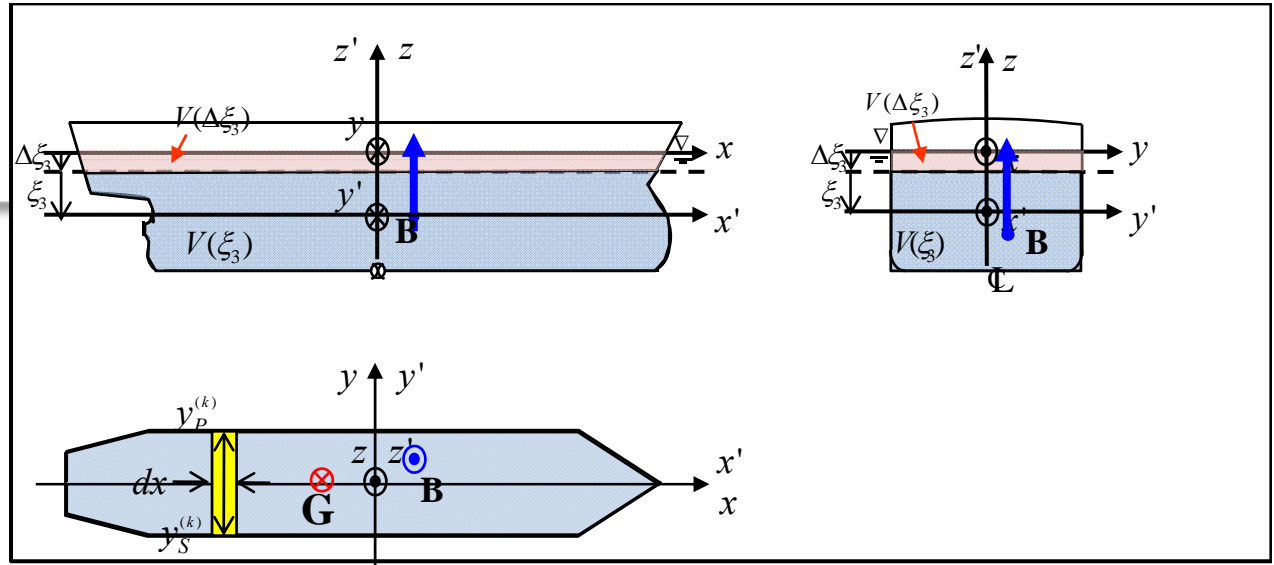
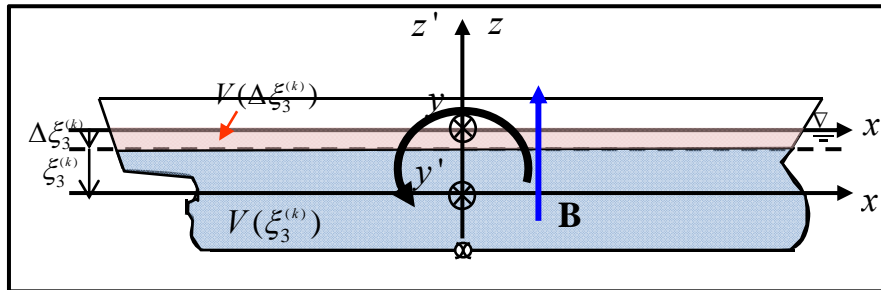
변화된 부피

만약 ξ_3 가 작다면,

$$\approx \frac{-\Delta \xi_3^{(k)} (\mathbf{i}T_{WP}(\xi_3^{(k)}) - \mathbf{j}L_{WP}(\xi_3^{(k)}))}{(-) \quad (+)}$$

(-)

수선면의 횡 방향 1차 모멘트 수선면의 종 방향 1차 모멘트



부호 검증

$L_{WP}(\xi_3^{(k)})$ 가 (+)이면, 수선면 중심이 선수쪽

$\Delta \xi_3^{(k)}$ 이 (-)이면, 가라앉는 것임.

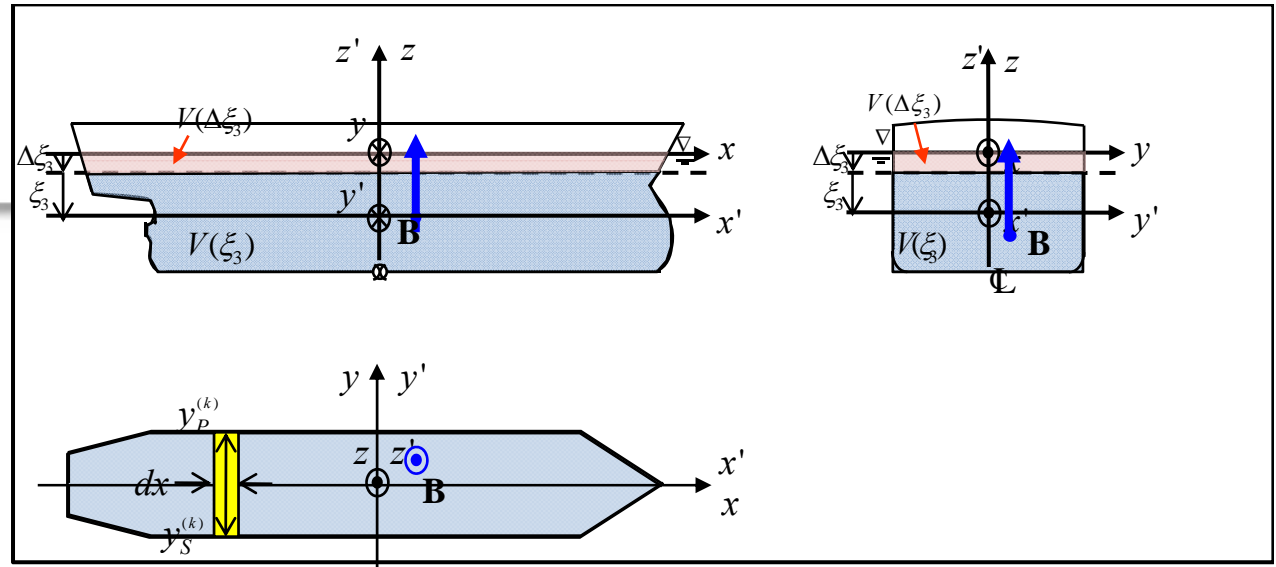
이 때, 수선면 중심이 선수쪽이기 때문에, 부력 중심도 선수쪽 (미소 자세)

y 축에 대한 (-)의 모멘트

Immersion에 의한 모멘트 (5)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$



$$\begin{aligned} \mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) &= \rho g \iiint_{V(\xi_3^{(k)} + \Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV = \rho g \left\{ \iiint_{V(\xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV + \iiint_{V(\Delta \xi_3^{(k)})} [\mathbf{i}y - \mathbf{j}x] dV \right\} \end{aligned}$$

만약 $\Delta \xi_3^{(k)}$ 가 작다면,

$$\approx \rho g \left\{ \left[\mathbf{i}V(\xi_3^{(k)})y_B^{(k)} - \mathbf{j}V(\xi_3^{(k)})x_B^{(k)} \right] - \Delta \xi_3^{(k)} \left[\mathbf{i}T_{WP}(\xi_3^{(k)}) - \mathbf{j}L_{WP}(\xi_3^{(k)}) \right] \right\}$$

대입

수선면의 횡 방향 1차 모멘트 | 수선면의 종 방향 1차 모멘트

$$\mathbf{M}_B(\xi_3^{(k)}) = \rho g \left\{ \mathbf{i}V(\xi_3^{(k)})y_B^{(k)} - \mathbf{j}V(\xi_3^{(k)})x_B^{(k)} \right\}$$

$$\mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) = \mathbf{M}_B(\xi_3^{(k)}) - \mathbf{i}\rho g T_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} + \mathbf{j}\rho g L_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)}$$

Immersion에 의한 모멘트 (6)

좌표 변환

$$\begin{pmatrix} x_P^{(k+1)} = x_P^{(k)} \\ y_P^{(k+1)} = y_P^{(k)} \\ z_P^{(k+1)} = z_P^{(k)} + \Delta \xi_3^{(k)} \end{pmatrix}$$

✓ 부력에 의한 모멘트

$$\mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) = \mathbf{M}_B(\xi_3^{(k)}) - \mathbf{i} \rho g T_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} + \mathbf{j} \rho g L_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)}$$



✓ 중력에 의한 모멘트

$$\begin{aligned} \mathbf{M}_G(\xi_3^{(k)} + \Delta \xi_3^{(k)}) &= \mathbf{r}_G^{(k+1)} \times (-\mathbf{k}mg) = -\mathbf{i}mg \cdot y_G^{(k+1)} + \mathbf{j}mg \cdot x_G^{(k+1)} \\ &= -\mathbf{i}mg \cdot y_G^{(k)} + \mathbf{j}mg \cdot x_G^{(k)} = \mathbf{M}_G(\xi_3^{(k)}) \end{aligned}$$

$$\mathbf{r}_G^{(k+1)} \times (-\mathbf{k}) = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ x_G^{(k+1)} & y_G^{(k+1)} & z_G^{(k+1)} \\ 0 & 0 & -1 \end{vmatrix} = -\mathbf{i}y_G^{(k+1)} + \mathbf{j}x_G^{(k+1)}$$

✓ 선박이 받는 모멘트

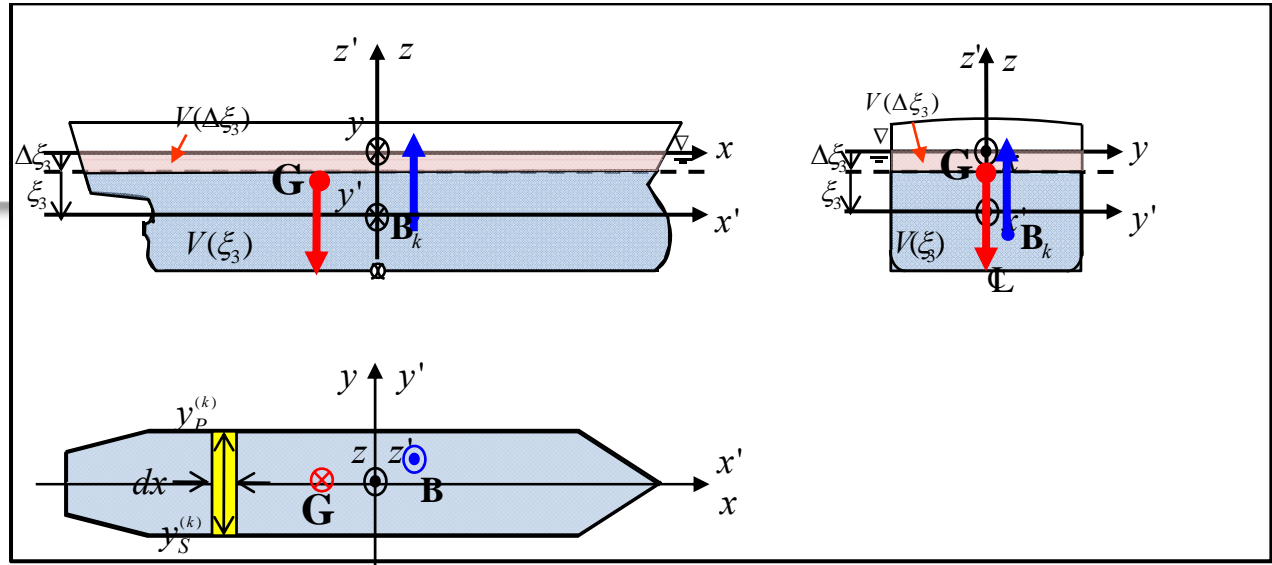
$$\begin{aligned} \mathbf{M}(\xi_3^{(k)} + \Delta \xi_3^{(k)}) &= \mathbf{M}_B(\xi_3^{(k)} + \Delta \xi_3^{(k)}) + \mathbf{M}_G(\xi_3^{(k)} + \Delta \xi_3^{(k)}) \\ &= \mathbf{M}_B(\xi_3^{(k)}) + \mathbf{M}_G(\xi_3^{(k)}) - \mathbf{i}T_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} + \mathbf{j}L_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} \\ &= \mathbf{M}(\xi_3^{(k)}) - \mathbf{i}T_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} + \mathbf{j}L_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} \end{aligned}$$

$$\mathbf{M}(\xi_3^{(k)} + \Delta \xi_3^{(k)}) - \mathbf{M}(\xi_3^{(k)}) = \mathbf{i} \{ -\rho g T_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} \} + \mathbf{j} \{ \rho g L_{WP}(\xi_3^{(k)}) \Delta \xi_3^{(k)} \}$$

$$\Delta \mathbf{M} = \mathbf{i} \left. \frac{\partial \mathbf{M}_T}{\partial \xi_3} \right|_{\xi_3^{(k)}} \Delta \xi_3^{(k)} + \mathbf{j} \left. \frac{\partial \mathbf{M}_L}{\partial \xi_3} \right|_{\xi_3^{(k)}} \Delta \xi_3^{(k)}$$

$$\left. \frac{\partial \mathbf{M}_T}{\partial \xi_3} \right|_{\xi_3^{(k)}} = -\rho g T_{WP}(\xi_3^{(k)})$$

$$\left. \frac{\partial \mathbf{M}_L}{\partial \xi_3} \right|_{\xi_3^{(k)}} = \rho g L_{WP}(\xi_3^{(k)})$$





Supplementary Slides

Advanced
Ship
Design
Automation
Laboratory

Coordinate System

x' 축 - 원점: Midship, (+): 선수
 y' 축 - 원점: Centerline, (+): 좌현
 z' 축 - 원점: 수선면, (+): 선박의 위

x 축 - 원점: Midship, (+): x' 축을 포함하고 수선면과 직교인 평면과 수선면 사이의 교선
 y 축 - 원점: Centerline, (+): z 축과 x 축의 외적 방향
 z 축 - 원점: 수면, (+): 수선면에 수직한 위 방향

