

[2008][01-1]

# Engineering Mathematics 2

September, 2008

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Department of Naval Architecture and Ocean Engineering,  
Seoul National University of College of Engineering



# Mathematical Modeling & Linearization



# Why Mathematics?

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# Why Mathematics?

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사회·철학적 현상



# Why Mathematics?

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사회·철학적 현상

물리적 현상



# Why Mathematics?

역학적/사회적 이해  
통찰력

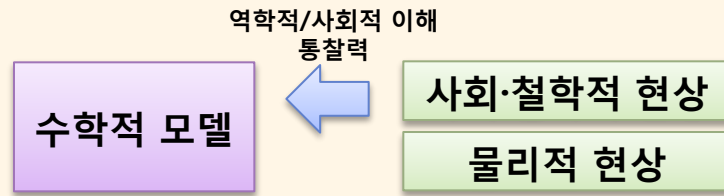


사회·철학적 현상

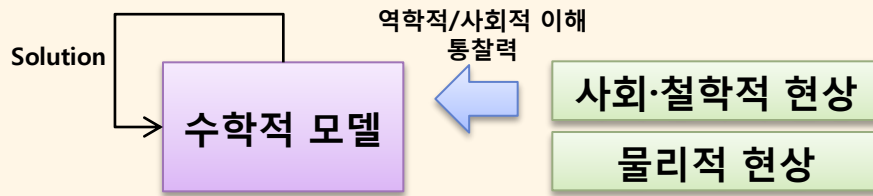
물리적 현상



# Why Mathematics?

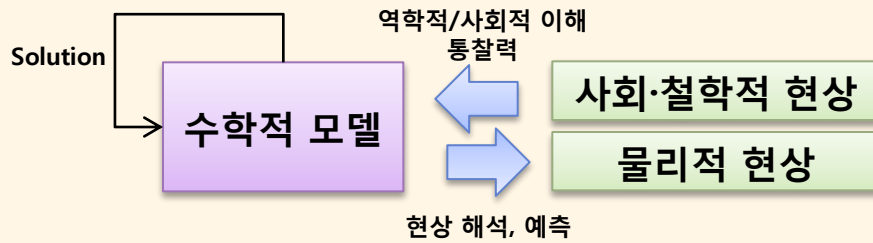


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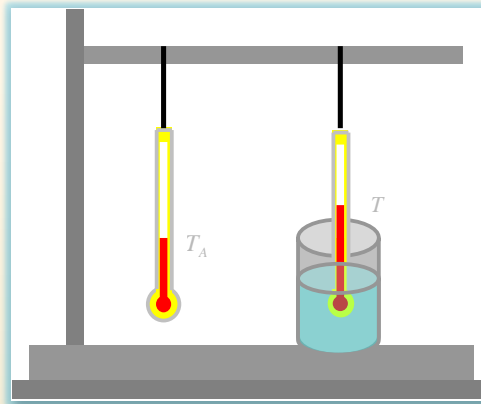
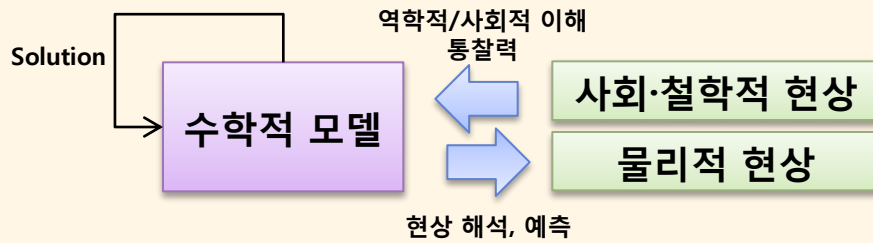




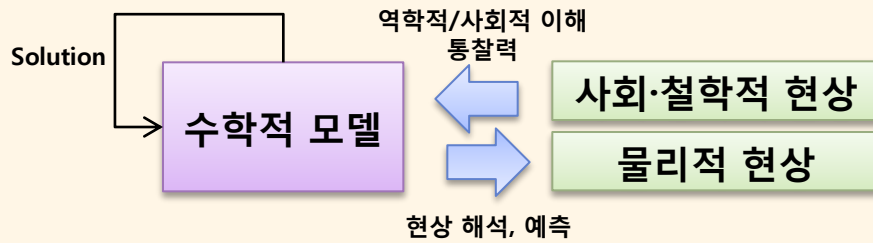
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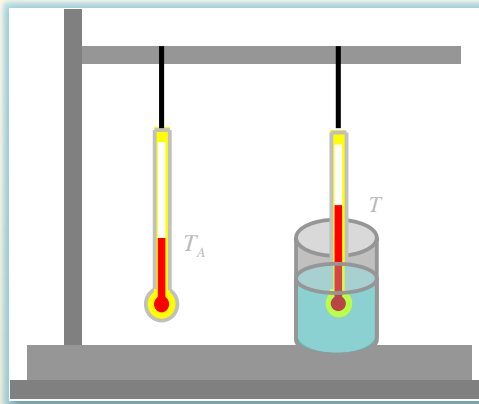
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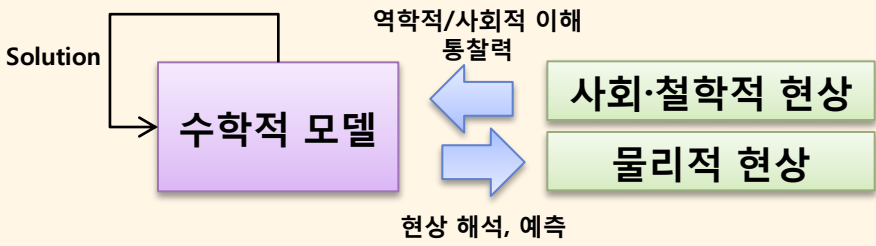
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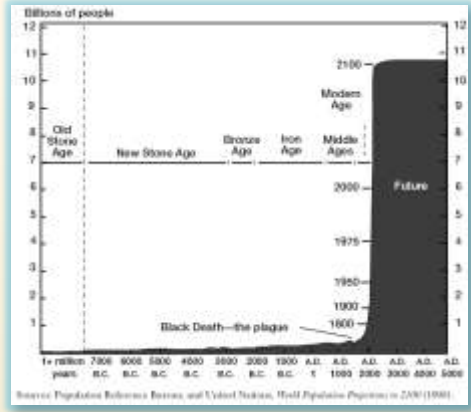
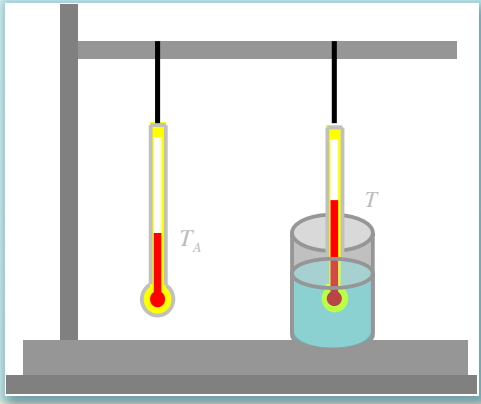
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시간이 얼마나  
걸릴까?



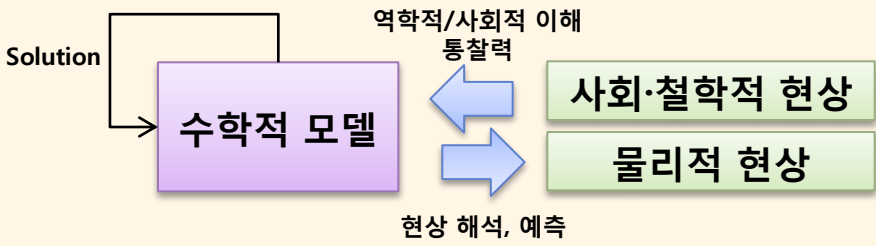
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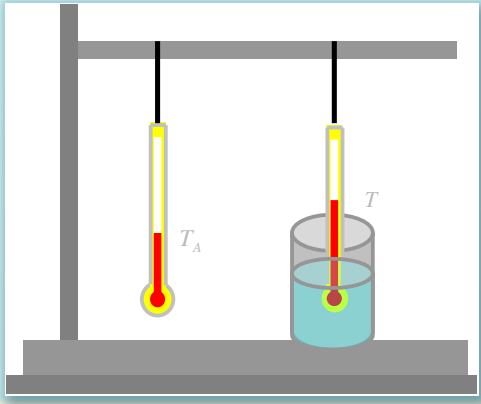
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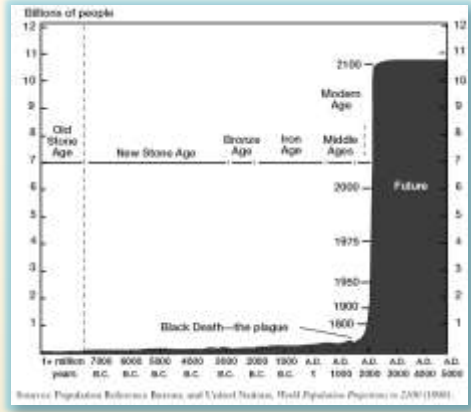
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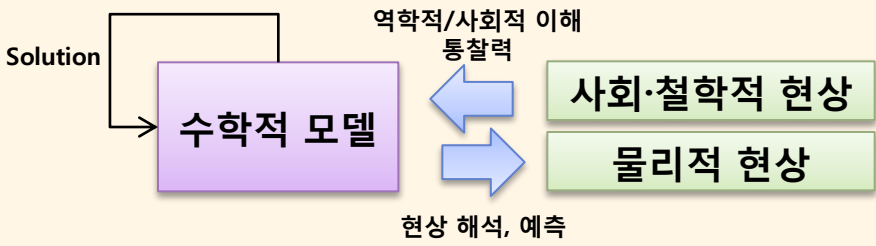
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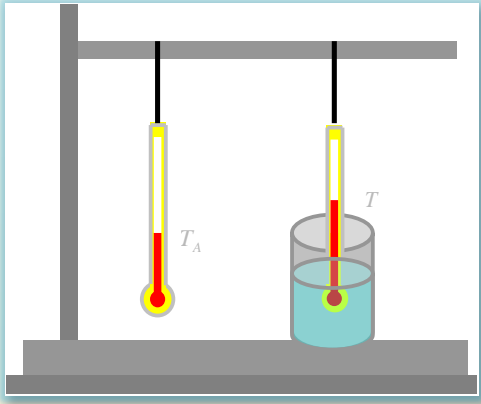
미래에는 인구가 얼마나 증가할까?



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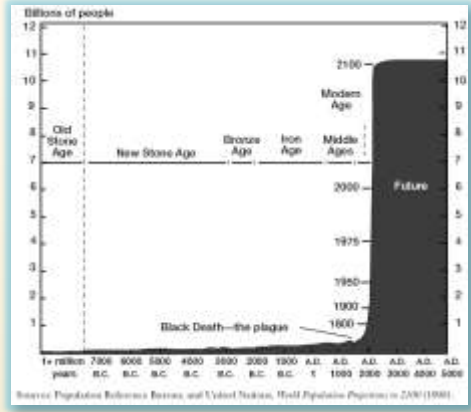


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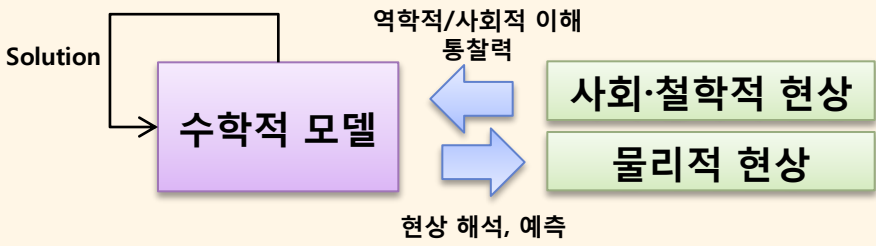


Changing **rate** of water temperature  $\propto$  Temperature difference between water and outside

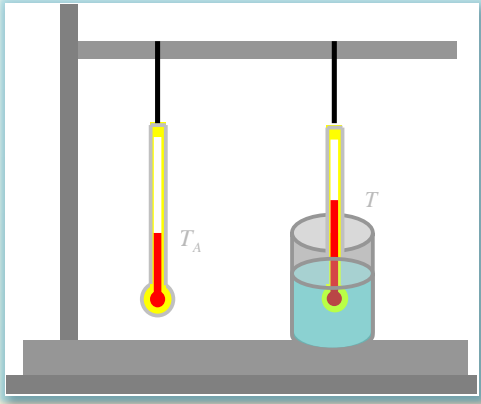
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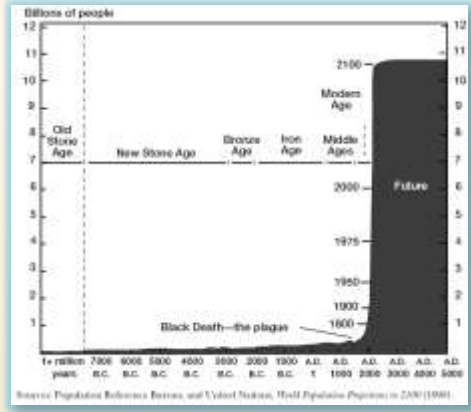
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Changing **rate** of water temperature

$\propto$

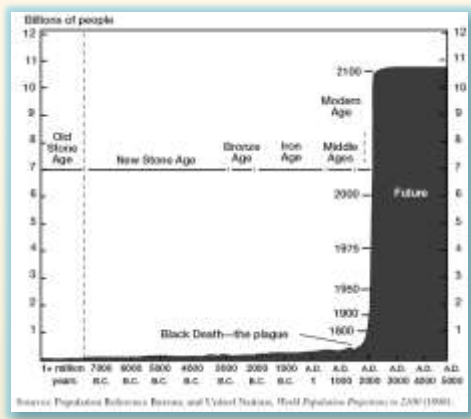
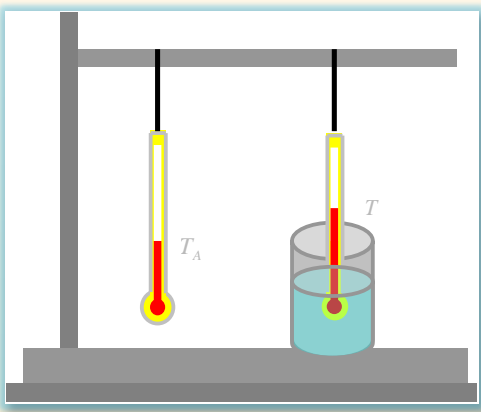
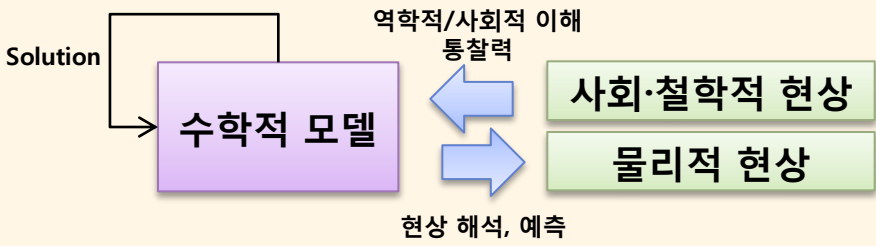
Temperature difference between water and outside

$$\frac{dT(t)}{dt} = k(T - T_A), k < 0$$

$T$  : Water temperature  
 $T_A$  : Outside temperature (constant)



# Why Mathematics?



Changing **rate** of water temperature  $\propto$  Temperature difference between water and outside

Increasing **rate** of population  $\propto$  Present Population

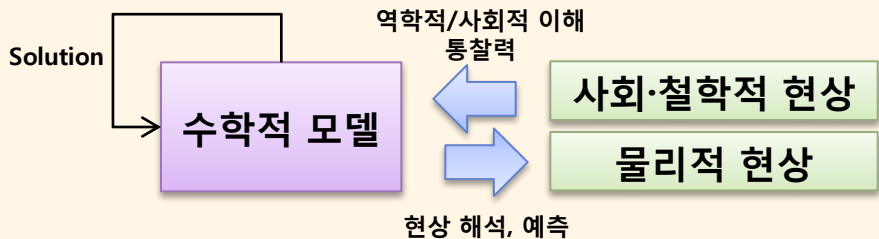
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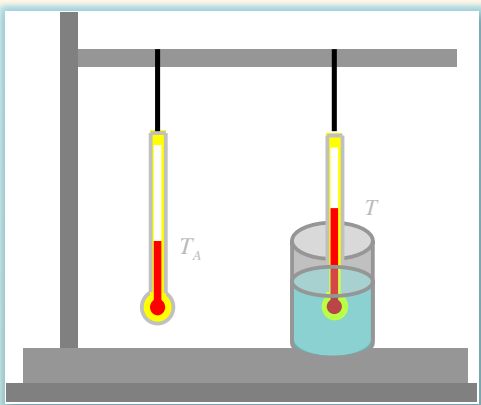




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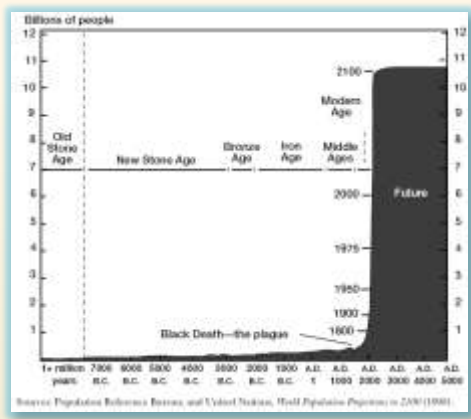


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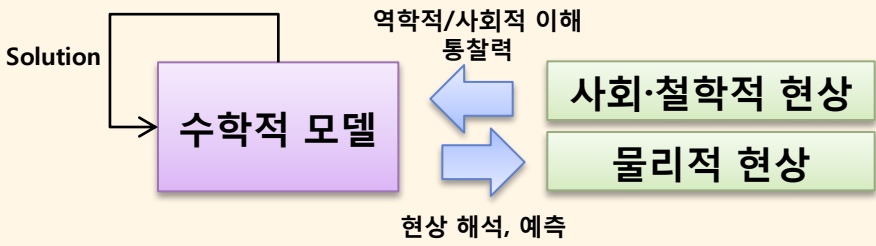
Increasing **rate** of population  $\propto$  Present Population

$$\frac{dy(t)}{dt} = k \cdot y(t)$$

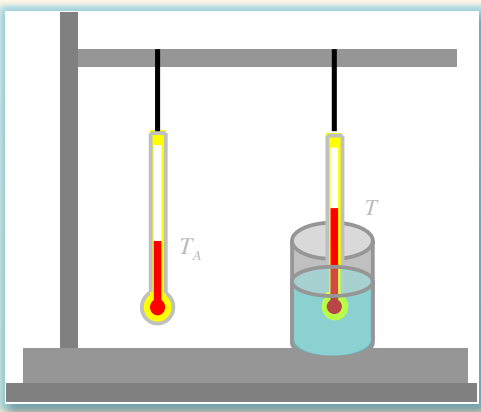
$y$  : population  
 $t$  : time  
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# Why Mathematics?



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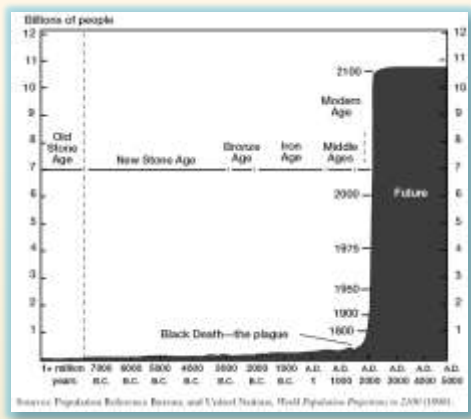


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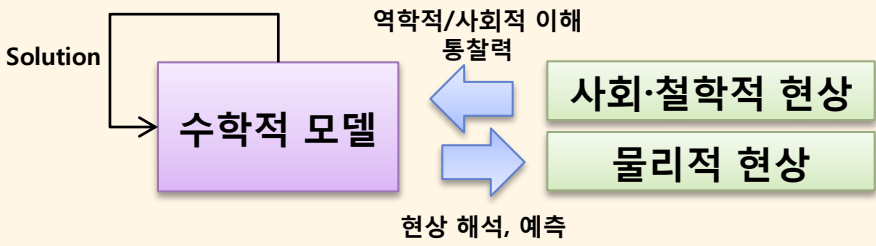
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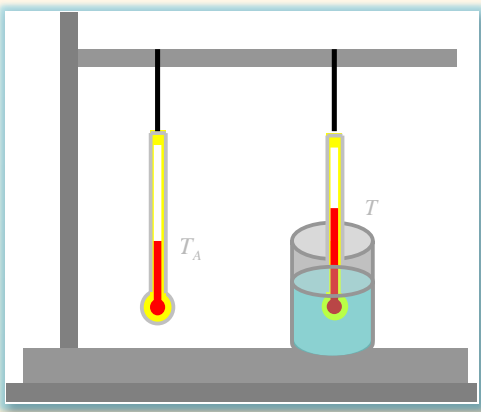
## <Newton's law of cooling>



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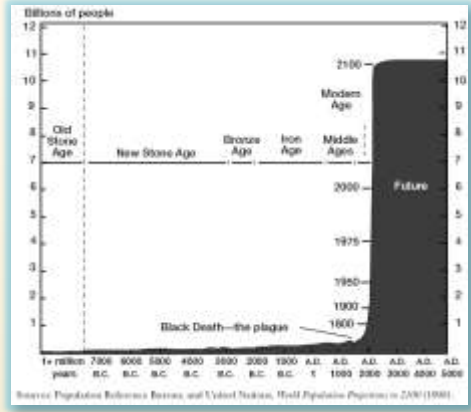
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 $t$  : time  
 $k$  : proportional constant

<Malthus Law>



# Linear O.D.E

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# Linear O.D.E

**Linear** Model  
(Linear Equation)

Linear/Nonlinear O.D.E

**Nonlinear** Model  
(Nonlinear Equation)



# Linear O.D.E

**Linear Model**  
(Linear Equation)

Linear/Nonlinear O.D.E

**Nonlinear Model**  
(Nonlinear Equation)

$$ex) \quad mz'' + cz' + kz = F_0 \cos \omega t$$

$z_1$

$z_2$

Try:  
 $z = e^{\lambda t}$

-Basis  
Linearly Independent



# Linear O.D.E

**Linear Model**  
(Linear Equation)

Linear/Nonlinear O.D.E

**Nonlinear Model**  
(Nonlinear Equation)

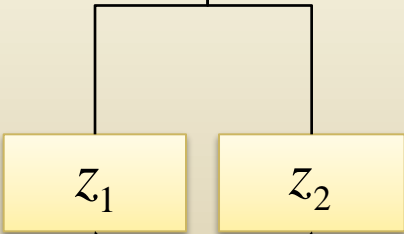
$$ex) mz'' + cz' + kz = F_0 \cos \omega t$$

$$ex) mz'' + cz' + kz = 0 \quad z_h$$

**General Solution**  
- Homogeneous

$$z_h = C_1 z_1 + C_2 z_2$$

-Linear Combination  
-Superposition



Try:  
 $z = e^{\lambda t}$

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# Linear O.D.E

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Linear/Nonlinear O.D.E

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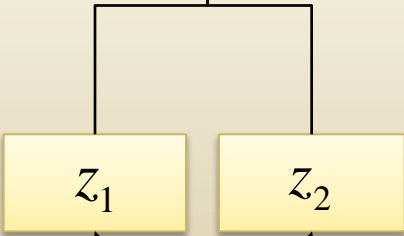
$z_p$

General Solution  
- Homogeneous

Particular  
Solution

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# Linear O.D.E

**Linear Model**  
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Linear/Nonlinear O.D.E

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ex)  $mz'' + cz' + kz = F_0 \cos \omega t$

**General Solution**  
-Nonghomogeneous

$z = z_h + z_p$   
-Superposition

ex)  $mz'' + cz' + kz = 0$

$z_h$

$z_p$

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**Particular Solution**

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Linear/Nonlinear O.D.E

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**General Solution**  
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ex)  $mz'' + cz' + kz = 0$

$z_h$

$z_p$

**General Solution**  
- Homogeneous

**Particular Solution**

**Another Superposition**

$z_h = C_1 z_1 + C_2 z_2$

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$z_1$

$z_2$

Try:  
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-Basis  
Linearly Independent



# Linear O.D.E

**Linear Model**  
(Linear Equation)

Linear/Nonlinear O.D.E

**Nonlinear Model**  
(Nonlinear Equation)

ex)  $mz'' + cz' + kz = F_0 \cos \omega t$

ex)  $mz'' + kz + k_1 z^3 = 0$

ex)  $(y'')^2 - y^2 = 0$

-Superposition?

**General Solution**  
-Nonghomogeneous

$z = z_h + z_p$   
-Superposition

ex)  $mz'' + cz' + kz = 0$

$z_h$

$z_p$

**General Solution**  
- Homogeneous

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$z_h = C_1 z_1 + C_2 z_2$

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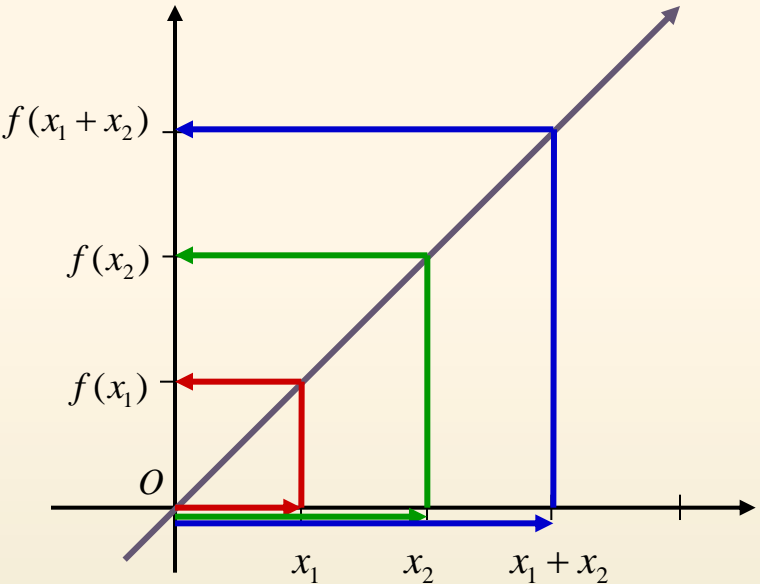
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-Basis  
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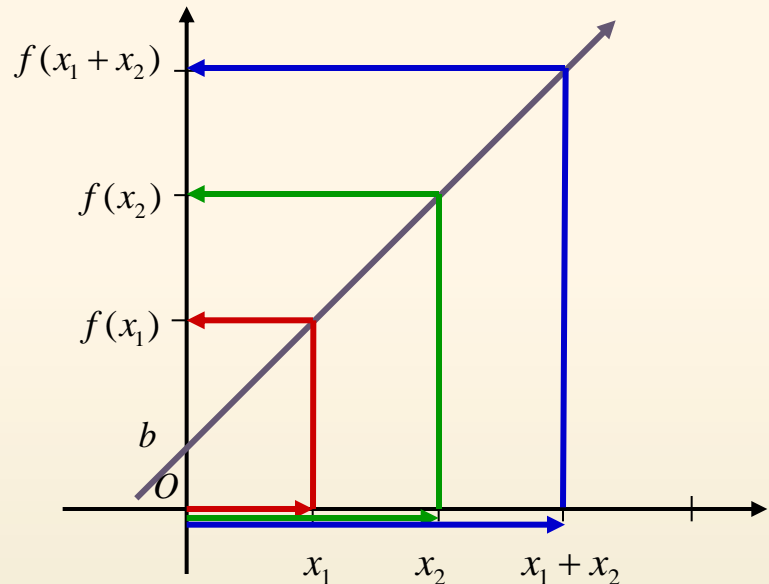


# Linearity, Superposition

$$f(x) = mx$$

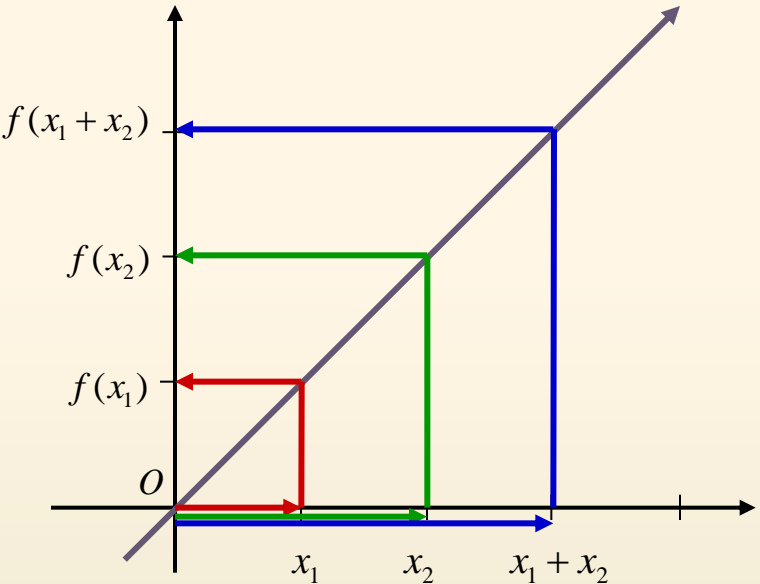


$$f(x) = mx + b$$



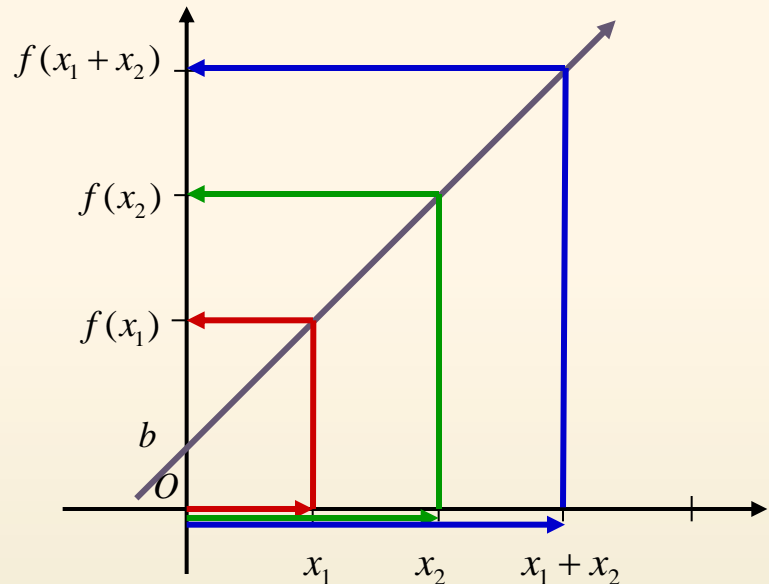
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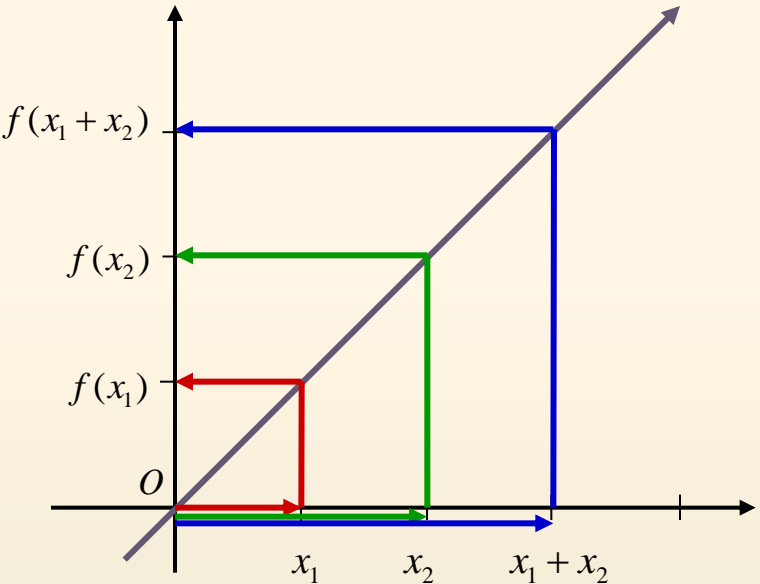
$$f(x_1) = mx_1, \quad f(x_2) = mx_2$$

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# Linearity, Superposition

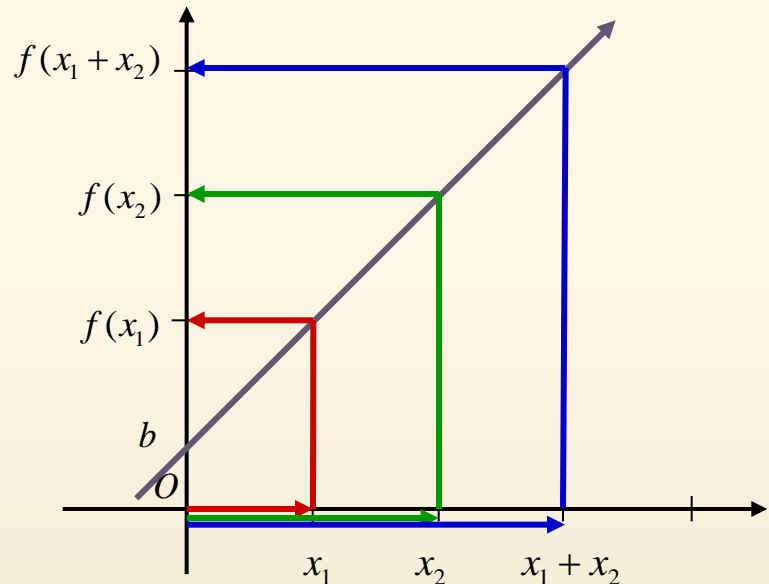
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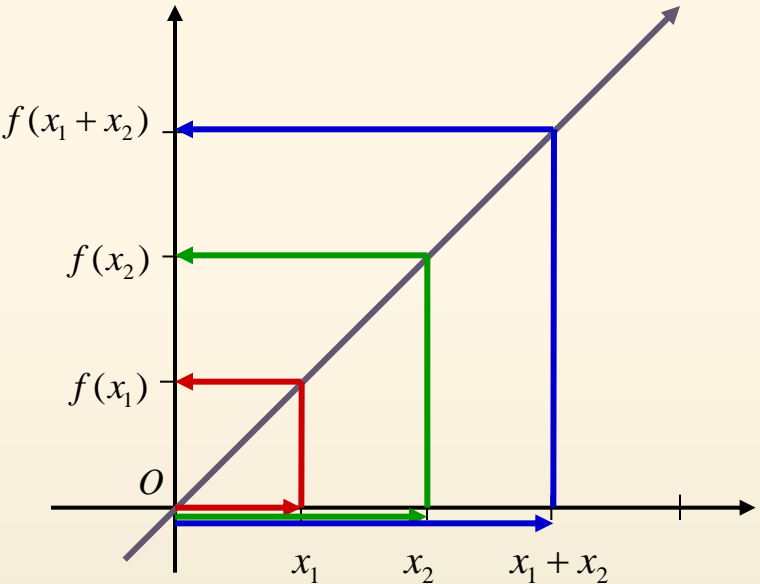
$$f(x_1 + x_2) = m(x_1 + x_2)$$

$$f(x) = mx + b$$



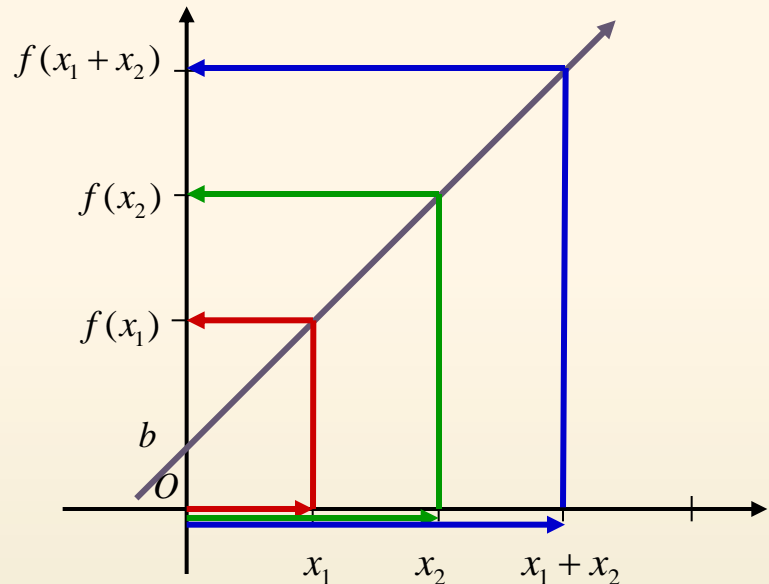
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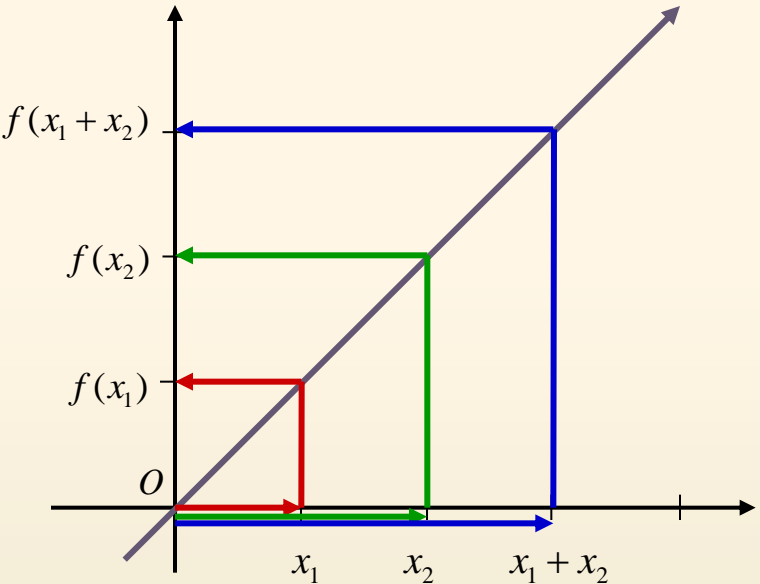
$$f(x_1) = mx_1, \quad f(x_2) = mx_2$$
$$f(x_1 + x_2) = m(x_1 + x_2)$$
$$= mx_1 + mx_2$$
$$= f(x_1) + f(x_2)$$

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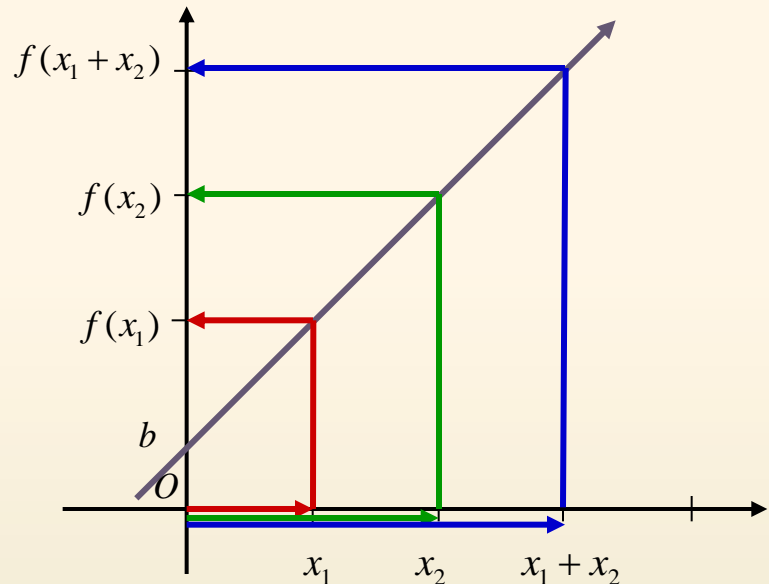
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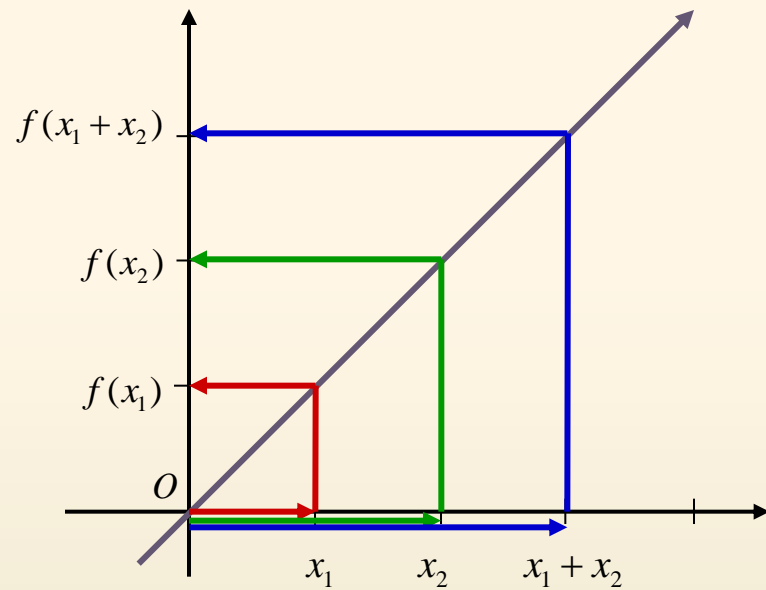
$$f(x_1) = mx_1 + b, \quad f(x_2) = mx_2 + b$$





# Linearity, Superposition

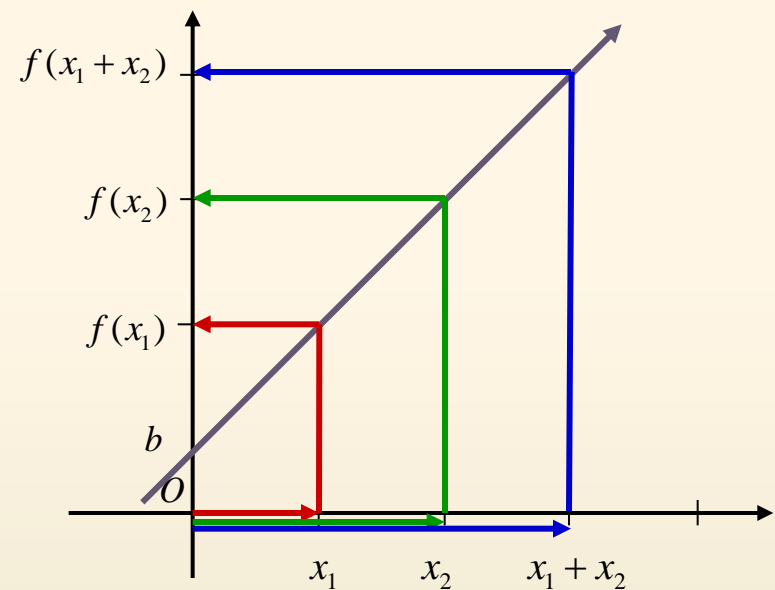
$$f(x) = mx$$



$$f(x_1) = mx_1, \quad f(x_2) = mx_2$$

$$\begin{aligned} f(x_1 + x_2) &= m(x_1 + x_2) \\ &= mx_1 + mx_2 \\ &= f(x_1) + f(x_2) \end{aligned}$$

$$f(x) = mx + b$$



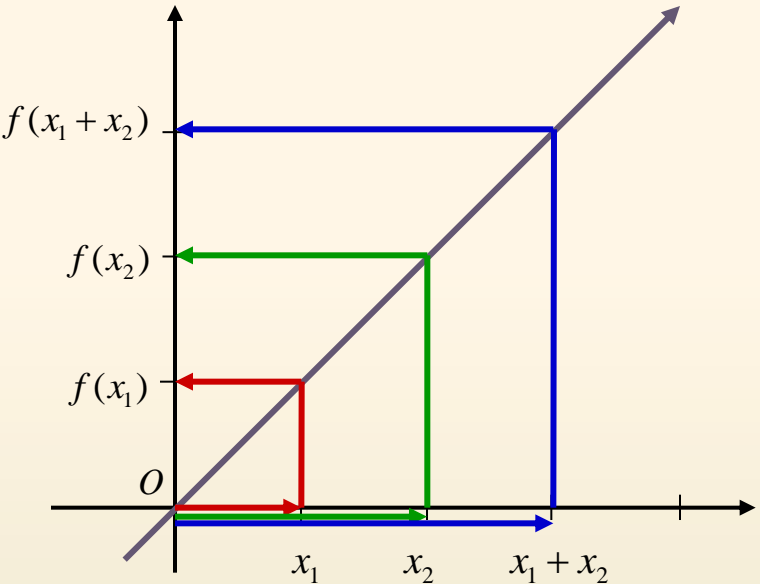
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# Linearity, Superposition

$$f(x) = mx$$



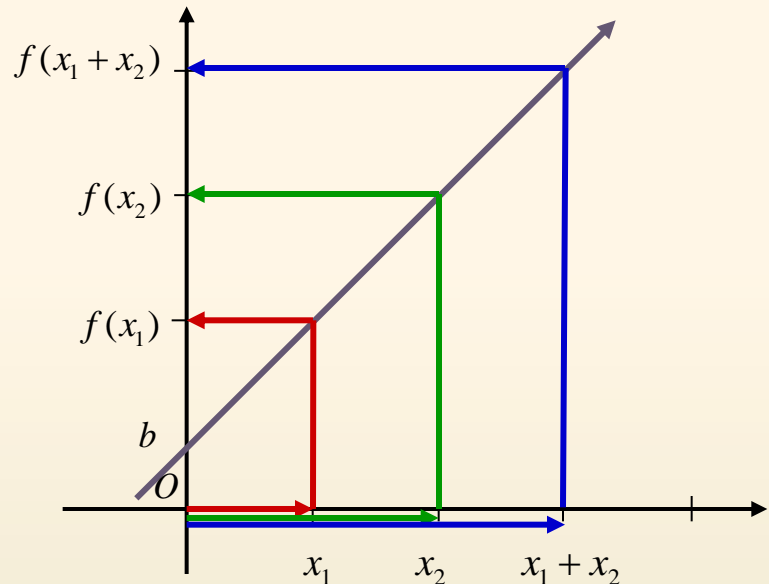
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$$= f(x_1) + f(x_2)$$

$$f(x) = mx + b$$



$$f(x_1) = mx_1 + b, \quad f(x_2) = mx_2 + b$$

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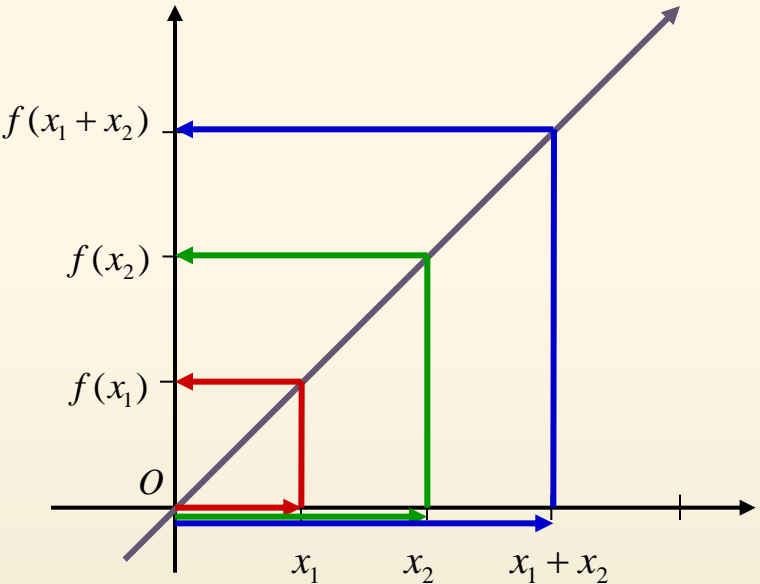
$$= mx_1 + mx_2 + b$$

$$\neq f(x_1) + f(x_2)$$



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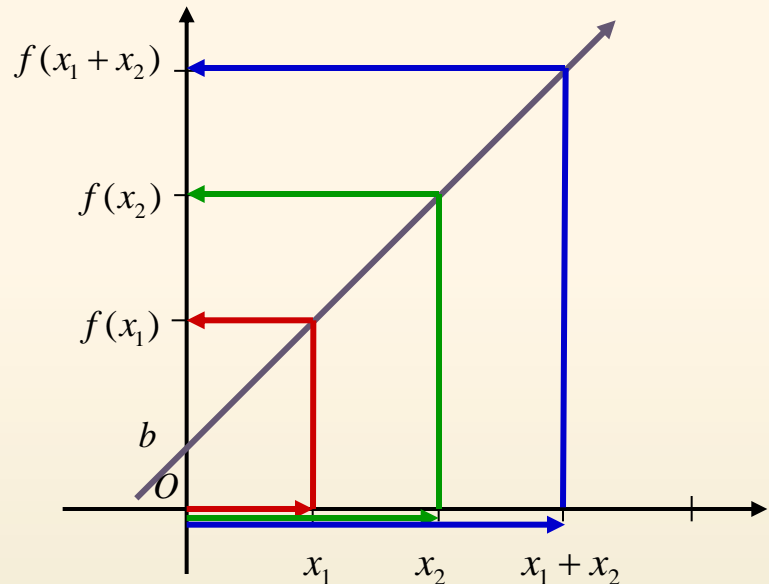
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Linearity,  
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$$f(x) = mx + b$$



$$f(x_1) = mx_1 + b, \quad f(x_2) = mx_2 + b$$

$$f(x_1 + x_2) = m(x_1 + x_2) + b$$

$$= mx_1 + mx_2 + b$$

$$\neq f(x_1) + f(x_2)$$



# Linearity, Superposition

If a function  $f(x)$  has linearity,  
the function  $f(x)$  has these 2 characters.

$$f(ax_1 + bx_2) = af(x_1) + bf(x_2)$$

## Homogeneity

$$(b = 0)$$

$$f(ax_1) = af(x_1)$$

## Additivity

$$(a = b = 1)$$

$$f(x_1 + x_2) = f(x_1) + f(x_2)$$

$x_1, x_2$  : independent variable



# Linear O.D.E

$$f(ax_1 + bx_2) = af(x_1) + bf(x_2)$$

- Linear O.D.E.

The dependent variable  $y$  and all its derivatives  $y', y'', \dots, y^{(n)}$  are of the first degree, that is the power of each term involving  $y$  is 1

The coefficients  $a_0, \dots, a_n$  of  $y', y'', \dots, y^{(n)}$  depend at most on the independent variable  $x$

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# Linear O.D.E

$$f(ax_1 + bx_2) = af(x_1) + bf(x_2)$$

- Linear O.D.E.

The dependent variable  $y$  and all its derivatives  $y', y'', \dots, y^{(n)}$  are of the first degree, that is the power of each term involving  $y$  is 1

The coefficients  $a_0, \dots, a_n$  of  $y', y'', \dots, y^{(n)}$  depend at most on the independent variable  $x$

$$a_n(x)y^{(n)} + a_{n-1}(x)y^{(n-1)} + \dots + a_2(x)y'' + a_1(x)y' + a_0(x)y = g(x)$$

---



# Linear O.D.E

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---

$$\text{ex) } my'' + cy' + ky = f(x)$$

$$y'' + \alpha y = 0$$

$$x^2 y'' + xy' - \alpha y = 0$$

$$xy'' + y' + \alpha^2 y = 0$$

$$(1 - x^2)y'' - 2xy' + n(n+1)y = 0$$

$$\text{where, } y = y(x), y' = \frac{dy}{dx}$$

$$m, c, k = \text{constant}$$

$$n = 0, 1, 2, \dots$$



# Nonlinear O.D.E

$$f(ax_1 + bx_2) \neq af(x_1) + bf(x_2)$$

## •linear O.D.E.

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## •Nonlinear O.D.E.

---

$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots$$





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$$(1 - y)y' + 2y = e^x$$

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$$(1 - y)y' + 2y = e^x \quad y'' + \sin y = e^x$$

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$$(1 - y)y' + 2y = e^x$$

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---

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# Nonlinear O.D.E

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# Nonlinearity

Nonlinearity of the nature

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# Nonlinearity

Nonlinearity of the nature → Nonlinear Mathematical Model

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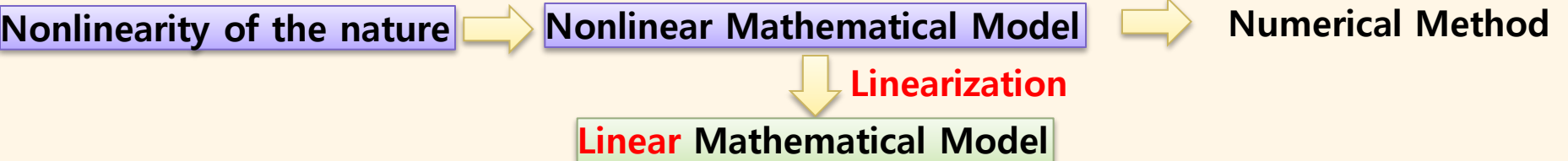
# Nonlinearity

Nonlinearity of the nature → Nonlinear Mathematical Model → Numerical Method

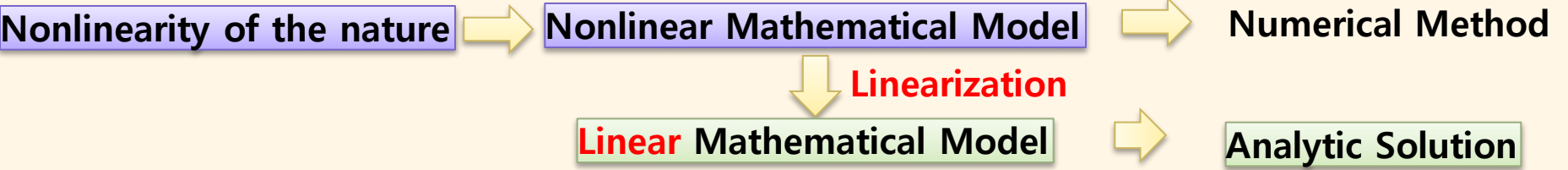
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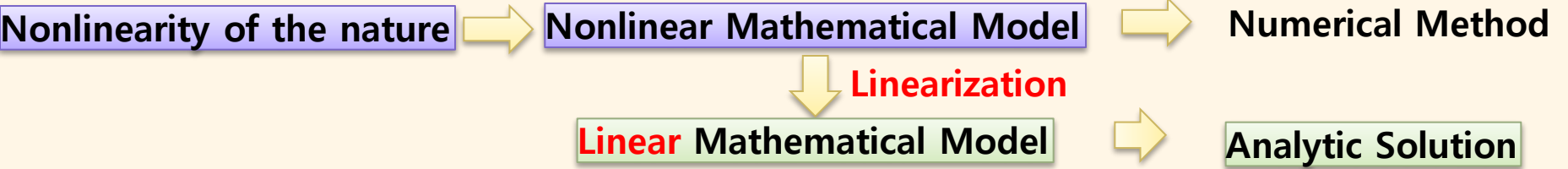
# Nonlinearity



# Nonlinearity



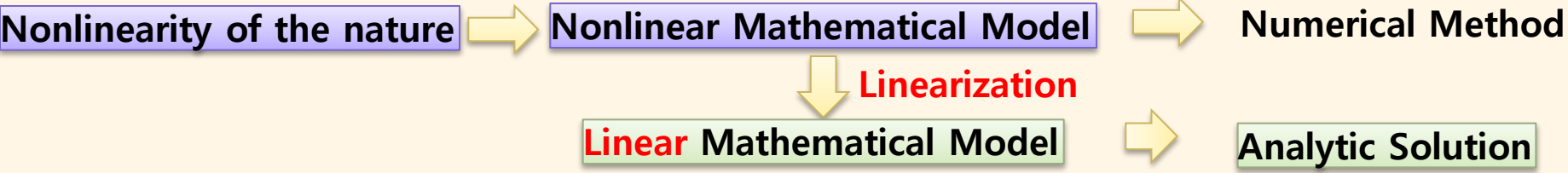
# Nonlinearity




How to linearize the nonlinear model?



# Nonlinearity



## Taylor Series

 How to linearize the nonlinear model?

Taylor Series : 미분 가능한 어떤 함수를 다항식의 형태로 근사하는 방법.  
 $n \geq 0$  인 정수  $n$ 에 대하여,  $x=x^*$ 인 지점에서  $n$ 번 미분 가능한 함수  $f$ 는 아래와 같이 나타낼 수 있다

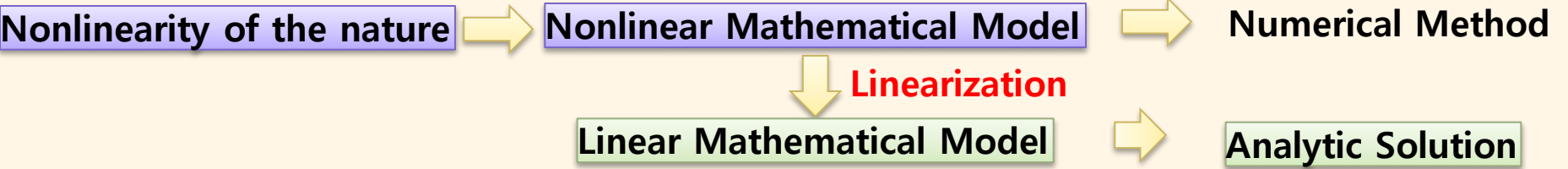
주어진 점  $x^*$  에서  $f(x)$ 의 Taylor Series

$$f(x) = f(x^*) + \frac{df(x^*)}{dx}(x - x^*) + \frac{1}{2} \frac{d^2 f(x^*)}{dx^2}(x - x^*)^2 + R$$

나머지항(Remainder)  
 :  $x$ 가  $x^*$ 에 충분히 가까우면 그 값이 매우 작음



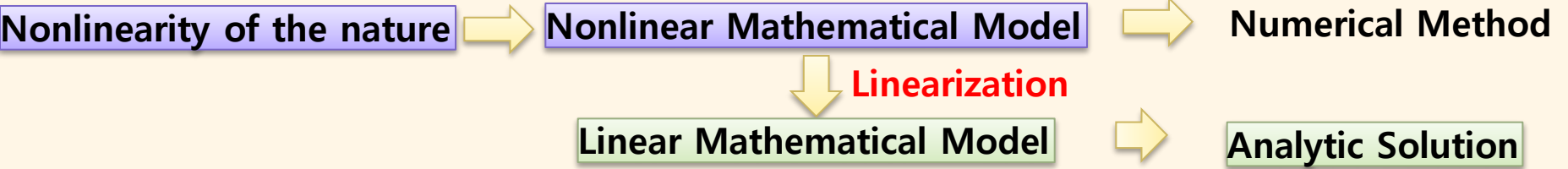
# Nonlinearity



## Taylor Series



# Nonlinearity



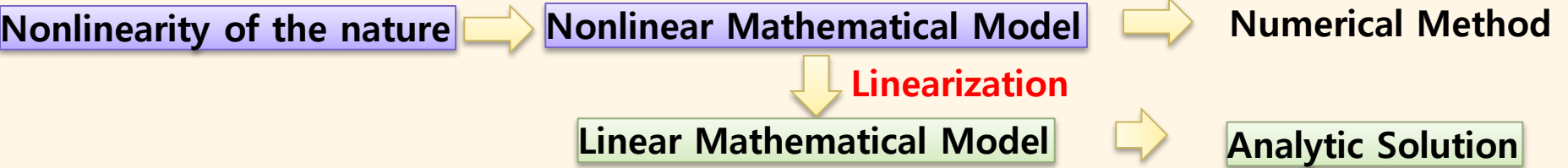
## Taylor Series

Given :  $x^*$ ,  $f(x^*)$ ,  $x^*$  에서의  $i$ 차 미분 계수  $\left( \frac{\partial^i f(x^*)}{\partial x^i} \right)$

Find :  $f(x^* + \Delta x)$



# Nonlinearity



## Taylor Series

Given :  $x^*$ ,  $f(x^*)$ ,  $x^*$  에서의  $i$ 차 미분 계수  $\left( \frac{\partial^i f(x^*)}{\partial x^i} \right)$

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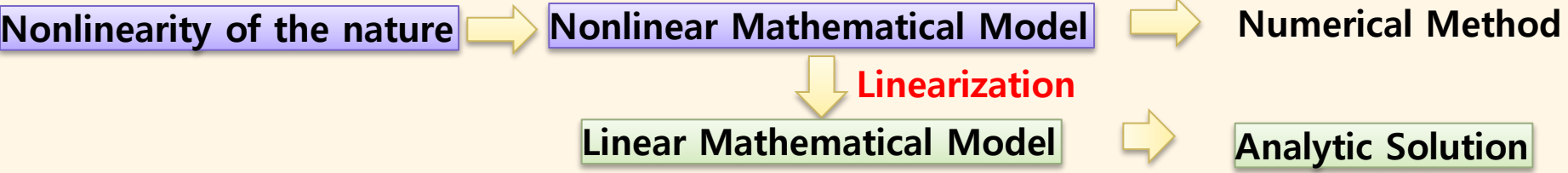
※ 1변수 함수의 Taylor Series Expansion

$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$





# Nonlinearity



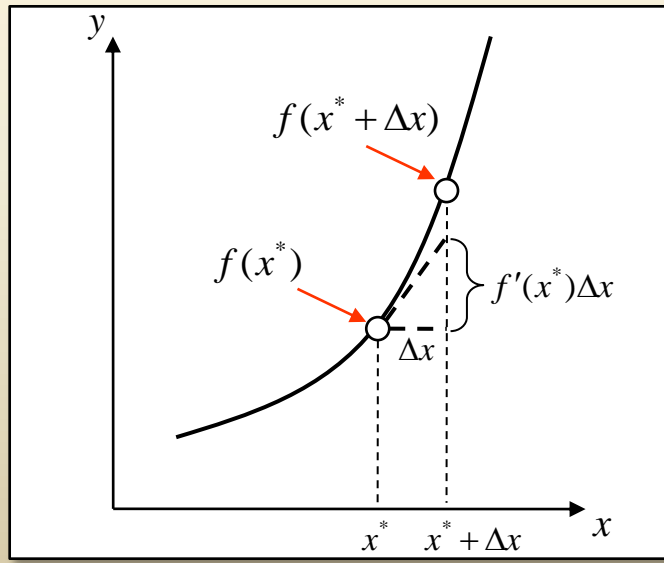
## Taylor Series

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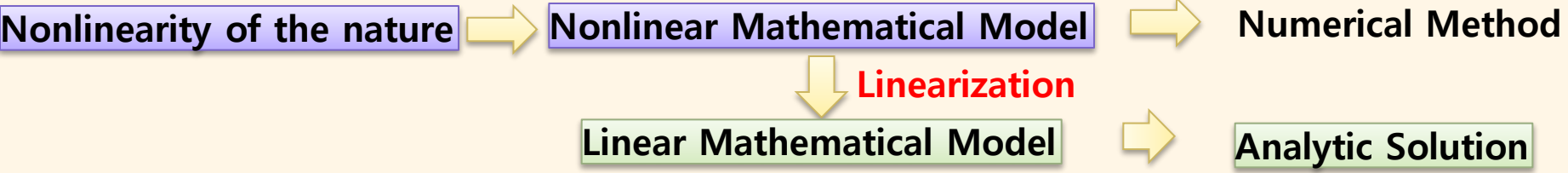
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# Nonlinearity



## Taylor Series

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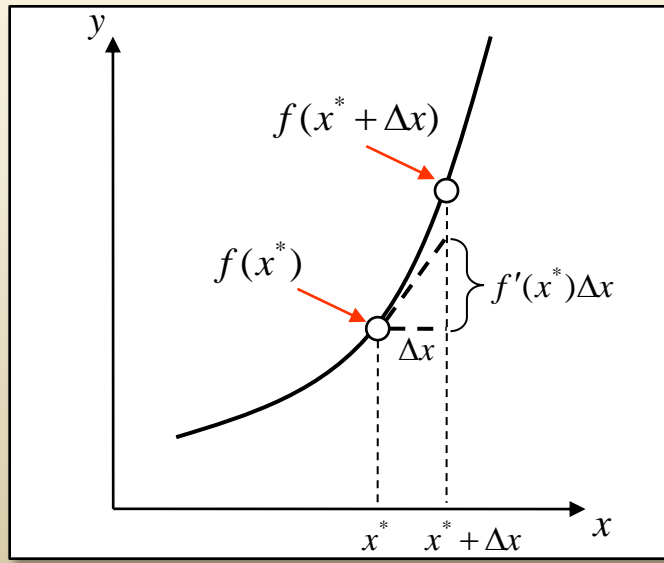
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$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$

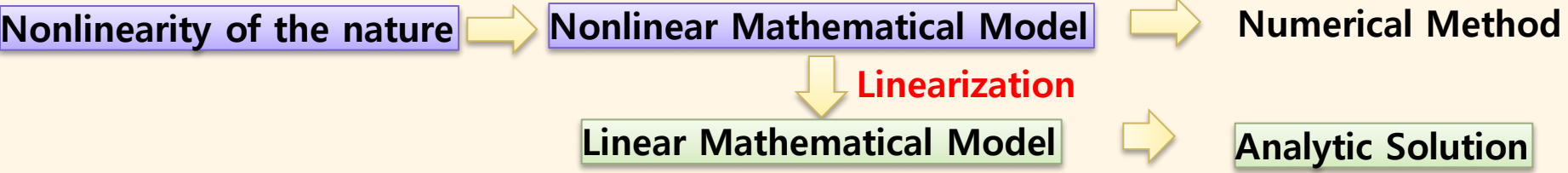
## Maclaurin Series

let  $x^* \rightarrow 0$ ,  $\Delta x \rightarrow x$

$$f(x) = f(0) + f'(0)\Delta x + \frac{1}{2} f''(0)\Delta x^2 + \dots$$



# Nonlinearity



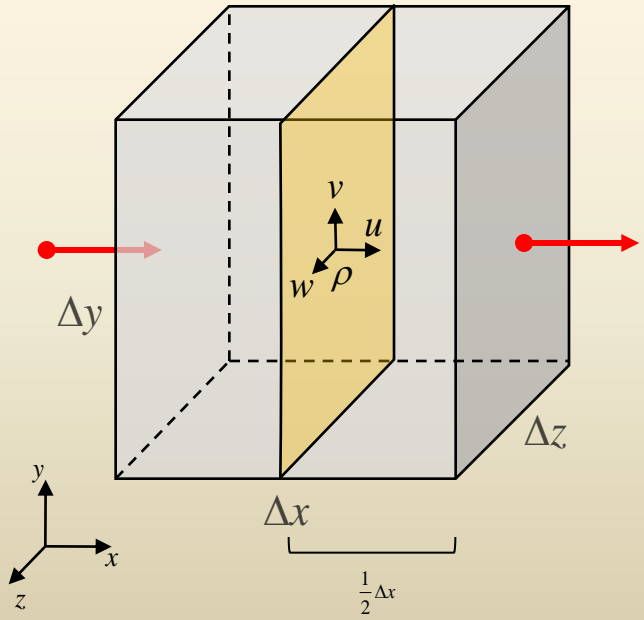
## Taylor Series

$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$

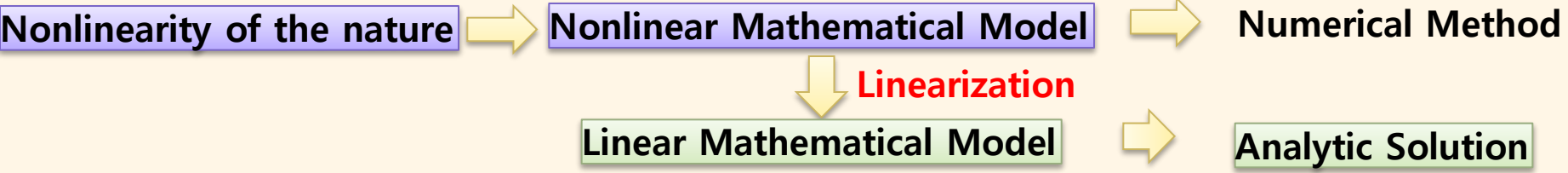
### Maclaurin Series

$$f(x) = f(0) + f'(0)x + \frac{1}{2} f''(0)x^2 + \dots$$

### Ex) Continuity Equation



# Nonlinearity



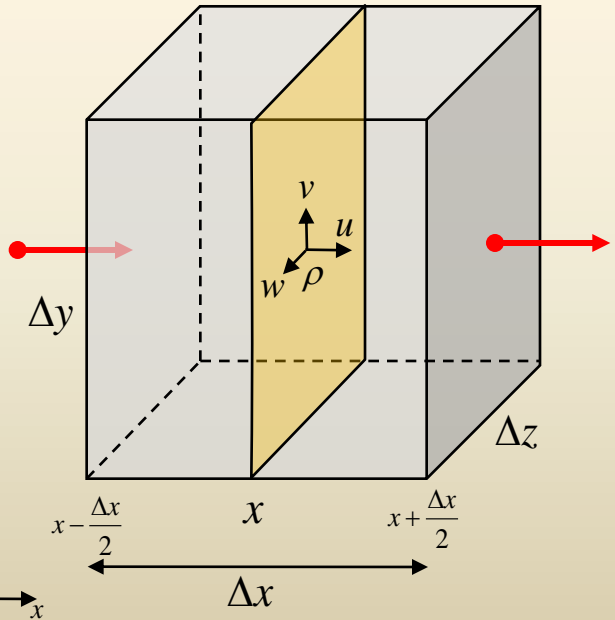
## Taylor Series

$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$

### Maclaurin Series

$$f(x) = f(0) + f'(0)x + \frac{1}{2} f''(0)x^2 + \dots$$

### Ex) Continuity Equation\*



✓ Given :  $\rho(x, y, z)u(x, y, z)$  and  $\frac{\partial(\rho u)}{\partial x}$  at  $(x, y, z)$

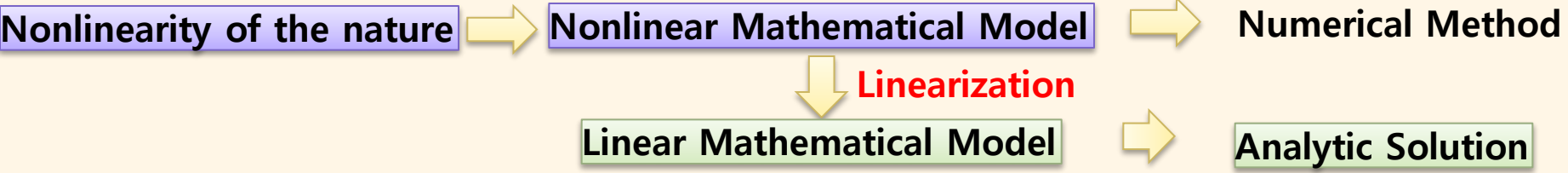
✓ Find : 오른쪽 면을 통해 검사체적으로부터 빠져나간 유체의 질량

$$\begin{aligned} & \rho\left(x + \frac{\Delta x}{2}, y, z\right)u\left(x + \frac{\Delta x}{2}, y, z\right)\Delta y\Delta z \\ & = \left[ \rho(x, y, z)u(x, y, z) + \frac{\partial(\rho u)}{\partial x} \frac{\Delta x}{2} + \dots \right] \Delta y\Delta z \\ & = \left[ \rho u + \frac{\partial(\rho u)}{\partial x} \frac{\Delta x}{2} + \dots \right] \Delta y\Delta z \approx \left[ \rho u + \frac{\partial(\rho u)}{\partial x} \frac{\Delta x}{2} \right] \Delta y\Delta z \end{aligned}$$

✓ 단위 시간당 왼쪽 면을 통해 들어온 유체의 질량

$$\begin{aligned} & \rho\left(x - \frac{\Delta x}{2}, y, z\right)u\left(x - \frac{\Delta x}{2}, y, z\right)\Delta y\Delta z \\ & = \left[ \rho(x, y, z)u(x, y, z) + \frac{\partial(\rho u)}{\partial x} \left(-\frac{\Delta x}{2}\right) + \dots \right] \Delta y\Delta z \\ & = \left[ \rho u + \frac{\partial(\rho u)}{\partial x} \left(-\frac{\Delta x}{2}\right) + \dots \right] \Delta y\Delta z \approx \left[ \rho u + \frac{\partial(\rho u)}{\partial x} \left(-\frac{\Delta x}{2}\right) \right] \Delta y\Delta z \end{aligned}$$

# Nonlinearity



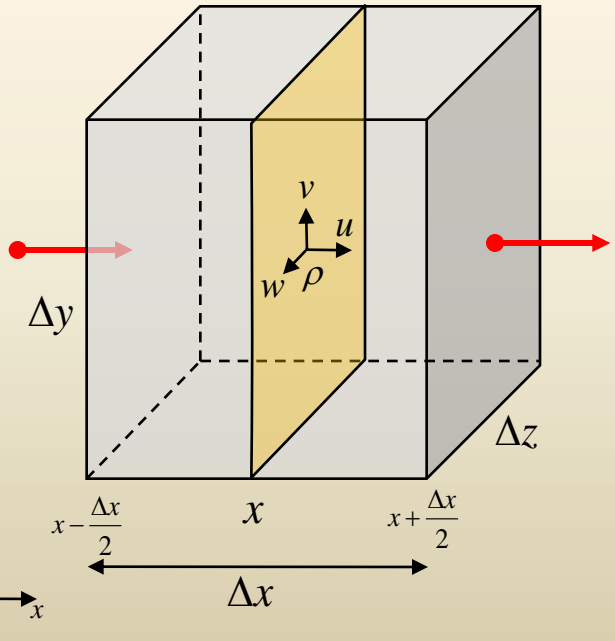
## Taylor Series

$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$

### Maclaurin Series

$$f(x) = f(0) + f'(0)x + \frac{1}{2} f''(0)x^2 + \dots$$

## Ex) Continuity Equation\*



✓ the net flux of mass into the cube in the x direction

(+ : mass flow rate in)

$$\left[ \rho u + \frac{\partial(\rho u)}{\partial x} \left( -\frac{\Delta x}{2} \right) \right] \Delta y \Delta z - \left[ \rho u + \frac{\partial(\rho u)}{\partial x} \frac{\Delta x}{2} \right] \Delta y \Delta z = -\frac{\partial(\rho u)}{\partial x} \Delta x \Delta y \Delta z$$

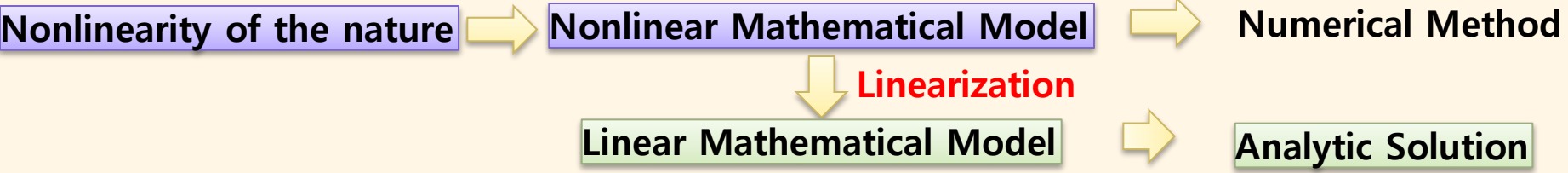
✓ the net flux of mass into the cube in the y direction  $-\frac{\partial(\rho v)}{\partial x} \Delta x \Delta y \Delta z$

✓ the net flux of mass into the cube in the z direction  $-\frac{\partial(\rho w)}{\partial x} \Delta x \Delta y \Delta z$

✓ the net rate of mass accumulation inside the control volume

$$-\left[ \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial x} + \frac{\partial(\rho w)}{\partial x} \right] \Delta x \Delta y \Delta z$$

# Nonlinearity



## Taylor Series

$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$

### Maclaurin Series

$$f(x) = f(0) + f'(0)x + \frac{1}{2} f''(0)x^2 + \dots$$

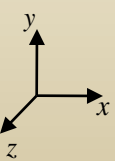
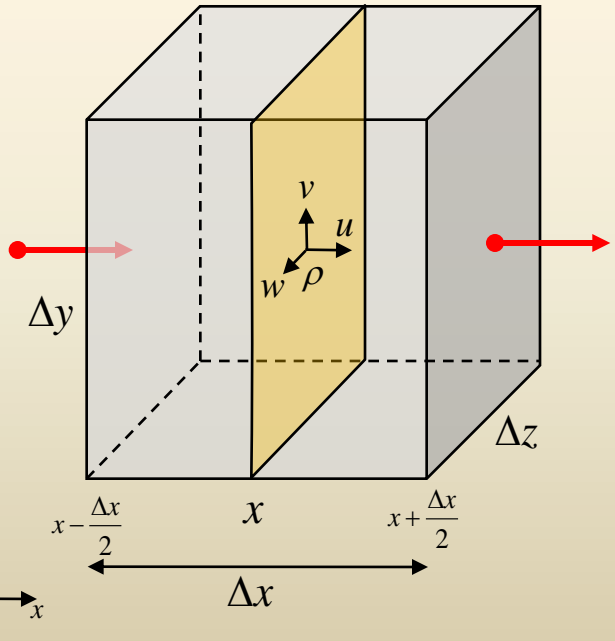
### Ex) Continuity Equation\*

✓Given :  $\rho(t)$  and  $\frac{\partial \rho}{\partial x}$  at  $(t)$

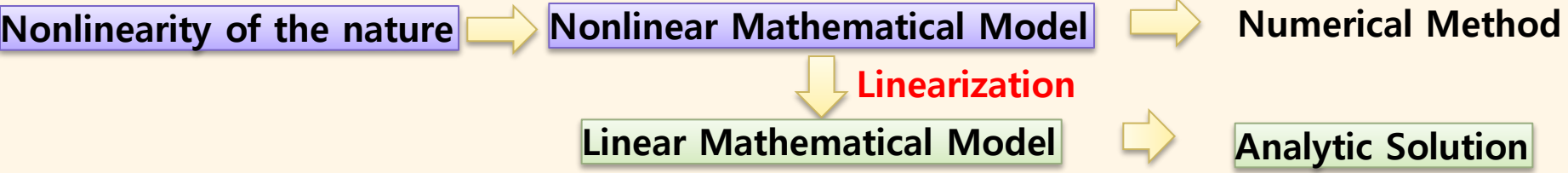
✓Find : the increase in mass for a time increment

$$[\rho(t + \Delta t) - \rho(t)] \Delta x \Delta y \Delta z$$

$$= \left[ \frac{\partial \rho}{\partial t} \Delta t + \dots \right] \Delta x \Delta y \Delta z \approx \left[ \frac{\partial \rho}{\partial t} \Delta t \right] \Delta x \Delta y \Delta z$$



# Nonlinearity



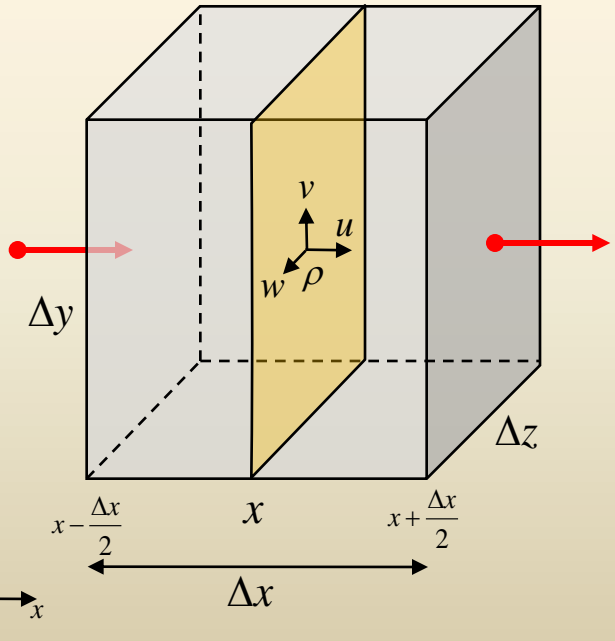
## Taylor Series

$$f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$$

### Maclaurin Series

$$f(x) = f(0) + f'(0)\Delta x + \frac{1}{2} f''(0)\Delta x^2 + \dots$$

## Ex) Continuity Equation\*



✓ Mass conservation

: the increase in mass for a time increment must be due to

the net inflow rate occurring over a time increment

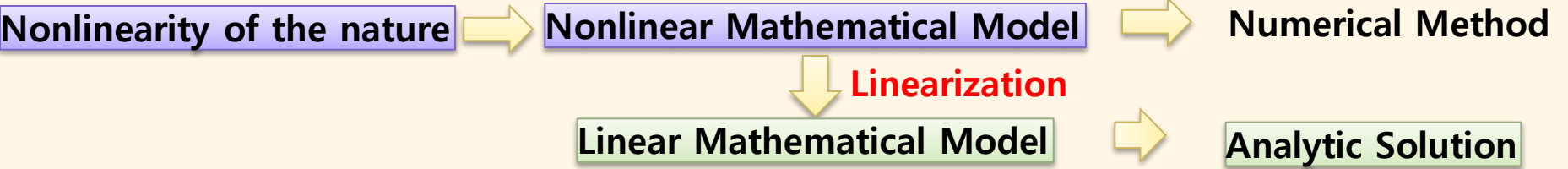
$$\left[ \frac{\partial \rho}{\partial t} \Delta t \right] \Delta x \Delta y \Delta z = - \left[ \frac{\partial \rho}{\partial x} + \frac{\partial(\rho v)}{\partial x} + \frac{\partial(\rho w)}{\partial x} \right] \Delta x \Delta y \Delta z \Delta t$$

$$\therefore \frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial x} + \frac{\partial(\rho w)}{\partial x} = 0$$

↓ ↓ ↓ ↓  
assumed as given at first

but we need to find them in the result.

# Nonlinearity

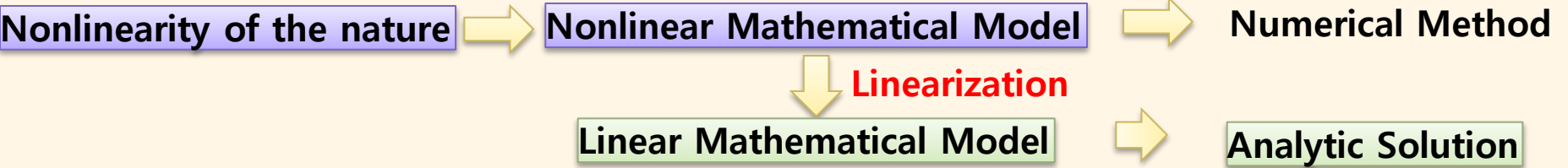


## Taylor Series





# Nonlinearity



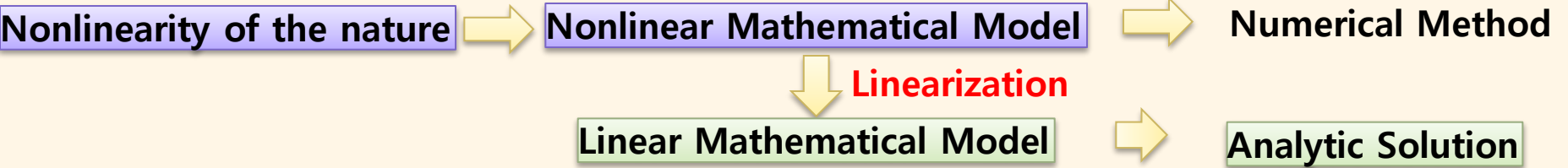
## Taylor Series

Given :  $(x_1^*, x_2^*), f(x_1^*, x_2^*), x^*$  에서의 미분 계수  $\left( \frac{\partial^{i+j} f(x_1^*, x_2^*)}{\partial x_1^i \partial x_2^j} \right)$

Find :  $f(x_1^* + \Delta x_1, x_2^* + \Delta x_2)$



# Nonlinearity



## Taylor Series

Given :  $(x_1^*, x_2^*), f(x_1^*, x_2^*), x^*$  에서의 미분 계수  $\left( \frac{\partial^{i+j} f(x_1^*, x_2^*)}{\partial x_1^i \partial x_2^j} \right)$

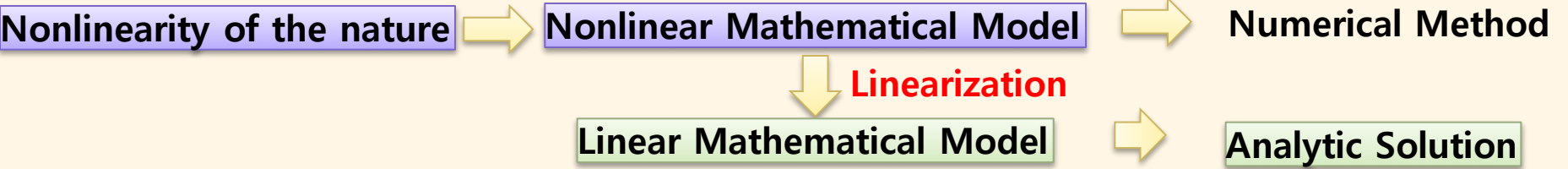
Find :  $f(x_1^* + \Delta x_1, x_2^* + \Delta x_2)$

※ 2변수 함수의 Taylor Series Expansion

$$f(x_1^* + \Delta x_1, x_2^* + \Delta x_2) = f(x_1^*, x_2^*) + \frac{\partial f}{\partial x_1} \Delta x_1 + \frac{\partial f}{\partial x_2} \Delta x_2 + \frac{1}{2} \left( \frac{\partial^2 f}{\partial x_1^2} \Delta x_1^2 + 2 \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_1 \Delta x_2 + \frac{\partial^2 f}{\partial x_2^2} \Delta x_2^2 \right) + \dots$$



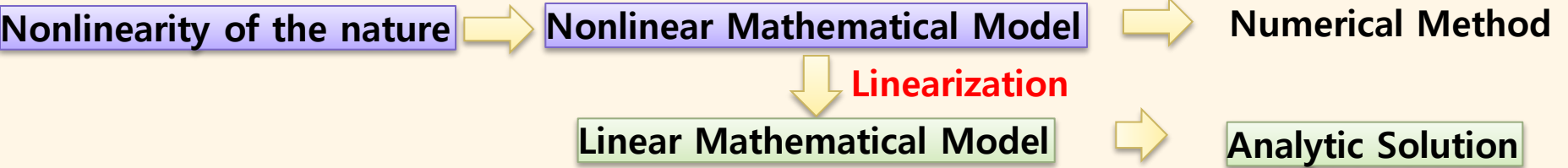
# Nonlinearity



## Taylor Series



# Nonlinearity



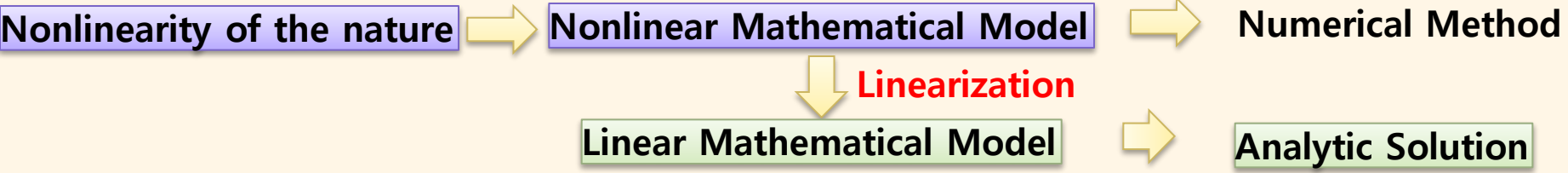
## Taylor Series

※ 2변수 함수의 Taylor Series Expansion

$$f(x_1^* + \Delta x_1, x_2^* + \Delta x_2) = f(x_1^*, x_2^*) + \frac{\partial f}{\partial x_1} \Delta x_1 + \frac{\partial f}{\partial x_2} \Delta x_2 + \frac{1}{2} \left( \frac{\partial^2 f}{\partial x_1^2} \Delta x_1^2 + 2 \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_1 \Delta x_2 + \frac{\partial^2 f}{\partial x_2^2} \Delta x_2^2 \right) + \dots$$



# Nonlinearity



## Taylor Series

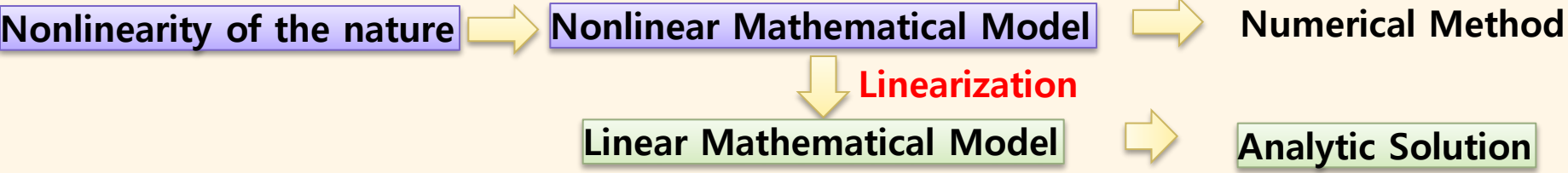
※ 2변수 함수의 Taylor Series Expansion

$$\nabla f(\mathbf{x}^*)^T (\mathbf{x} - \mathbf{x}^*) = \begin{bmatrix} \frac{\partial f}{\partial x_1} \\ \frac{\partial f}{\partial x_2} \end{bmatrix}^T \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

$$f(x_1^* + \Delta x_1, x_2^* + \Delta x_2) = f(x_1^*, x_2^*) + \frac{\partial f}{\partial x_1} \Delta x_1 + \frac{\partial f}{\partial x_2} \Delta x_2 + \frac{1}{2} \left( \frac{\partial^2 f}{\partial x_1^2} \Delta x_1^2 + 2 \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_1 \Delta x_2 + \frac{\partial^2 f}{\partial x_2^2} \Delta x_2^2 \right) + \dots$$



# Nonlinearity



## Taylor Series

※ 2변수 함수의 Taylor Series Expansion

$$\nabla f(\mathbf{x}^*)^T (\mathbf{x} - \mathbf{x}^*) = \begin{bmatrix} \frac{\partial f}{\partial x_1} \\ \frac{\partial f}{\partial x_2} \end{bmatrix}^T \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

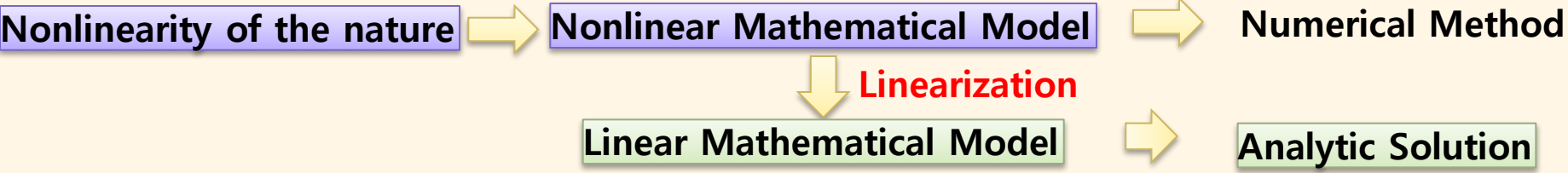
$$f(x_1^* + \Delta x_1, x_2^* + \Delta x_2) = f(x_1^*, x_2^*) + \frac{\partial f}{\partial x_1} \Delta x_1 + \frac{\partial f}{\partial x_2} \Delta x_2 + \frac{1}{2} \left( \frac{\partial^2 f}{\partial x_1^2} \Delta x_1^2 + 2 \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_1 \Delta x_2 + \frac{\partial^2 f}{\partial x_2^2} \Delta x_2^2 \right) + \dots$$

$$\frac{1}{2} (\Delta \mathbf{x})^T \mathbf{H}(\mathbf{x}^*) (\Delta \mathbf{x}) = \frac{1}{2} \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} (\Delta x_1) + \frac{\partial^2 f}{\partial x_2 \partial x_1} (\Delta x_2) & \frac{\partial^2 f}{\partial x_1 \partial x_2} (\Delta x_1) + \frac{\partial^2 f}{\partial x_2^2} (\Delta x_2) \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

$$= \frac{1}{2} \begin{bmatrix} \Delta x_1 & \Delta x_2 \end{bmatrix} \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} & \frac{\partial^2 f}{\partial x_1 \partial x_2} \\ \frac{\partial^2 f}{\partial x_2 \partial x_1} & \frac{\partial^2 f}{\partial x_2^2} \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$



# Nonlinearity



## Taylor Series

※ 2변수 함수의 Taylor Series Expansion

$$\nabla f(\mathbf{x}^*)^T (\mathbf{x} - \mathbf{x}^*) = \begin{bmatrix} \frac{\partial f}{\partial x_1} \\ \frac{\partial f}{\partial x_2} \end{bmatrix}^T \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

$$f(x_1^* + \Delta x_1, x_2^* + \Delta x_2) = f(x_1^*, x_2^*) + \frac{\partial f}{\partial x_1} \Delta x_1 + \frac{\partial f}{\partial x_2} \Delta x_2 + \frac{1}{2} \left( \frac{\partial^2 f}{\partial x_1^2} \Delta x_1^2 + 2 \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_1 \Delta x_2 + \frac{\partial^2 f}{\partial x_2^2} \Delta x_2^2 \right) + \dots$$

$$\frac{1}{2} (\Delta \mathbf{x})^T \mathbf{H}(\mathbf{x}^*) (\Delta \mathbf{x}) = \frac{1}{2} \left[ \frac{\partial^2 f}{\partial x_1^2} (\Delta x_1) + \frac{\partial^2 f}{\partial x_2 \partial x_1} (\Delta x_2) \quad \frac{\partial^2 f}{\partial x_1 \partial x_2} (\Delta x_1) + \frac{\partial^2 f}{\partial x_2^2} (\Delta x_2) \right] \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

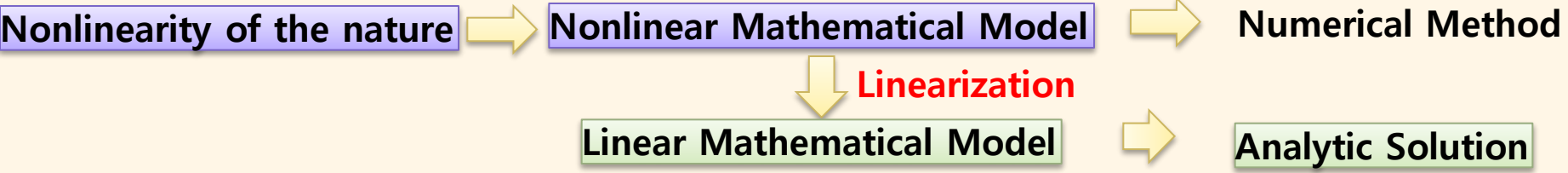
$$= \frac{1}{2} \begin{bmatrix} \Delta x_1 & \Delta x_2 \end{bmatrix} \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} & \frac{\partial^2 f}{\partial x_1 \partial x_2} \\ \frac{\partial^2 f}{\partial x_2 \partial x_1} & \frac{\partial^2 f}{\partial x_2^2} \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

$$\mathbf{H} = \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} & \frac{\partial^2 f}{\partial x_1 \partial x_2} \\ \frac{\partial^2 f}{\partial x_2 \partial x_1} & \frac{\partial^2 f}{\partial x_2^2} \end{bmatrix}$$

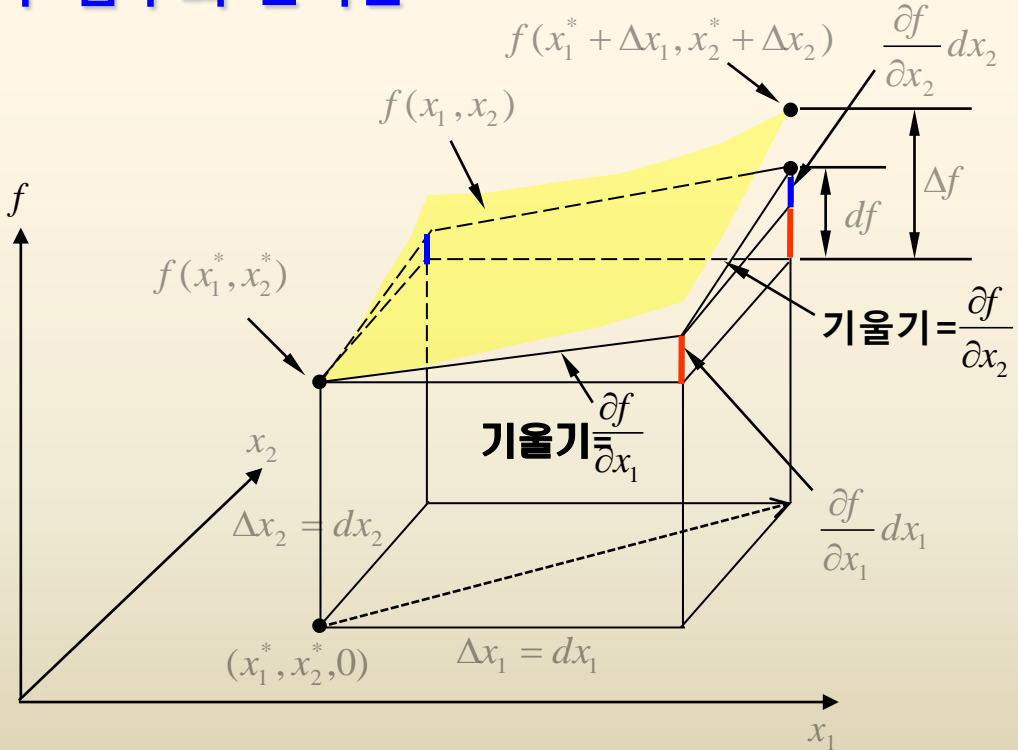
$$\therefore f(\mathbf{x}) = f(\mathbf{x}^*) + \nabla f(\mathbf{x}^*)^T (\Delta \mathbf{x}) + \frac{1}{2} (\Delta \mathbf{x})^T \mathbf{H}(\mathbf{x}^*) (\Delta \mathbf{x}) + R$$



# Nonlinearity



## 2변수 함수의 전미분



주어진 것:  $(x_1^*, x_2^*), f(x_1^*, x_2^*)$

실제 구해야 하는 것:  
 $f(x_1^* + \Delta x_1, x_2^* + \Delta x_2)$   
 $= f(x_1^*, x_2^*) + \Delta f$

근사적으로 구할 수 있는 것:  
 $f(x_1^*, x_2^*) + df$

$\Delta x_1, \Delta x_2$ 가 아주 작다면  
 $\Delta f \cong df$ 라 볼 수 있음

$x_2$  방향의 변화량

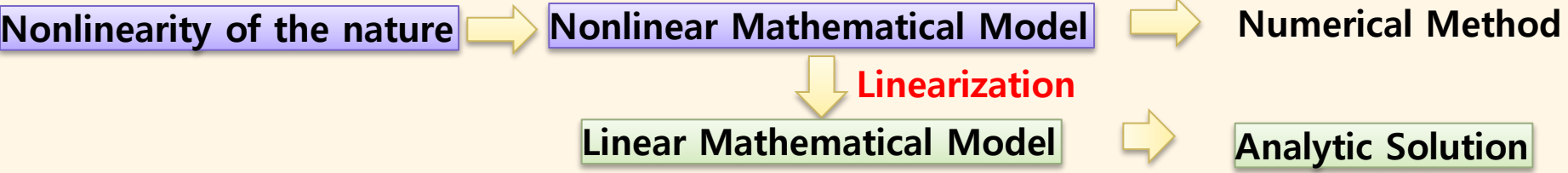
$$df = \frac{\partial f}{\partial x_1} dx_1 + \frac{\partial f}{\partial x_2} dx_2$$

$x_1$  방향의 변화량





# Nonlinearity



## 2변수 함수의 전미분

✓ 2변수 함수의 전미분

$$df = \frac{\partial f}{\partial x_1} dx_1 + \frac{\partial f}{\partial x_2} dx_2$$

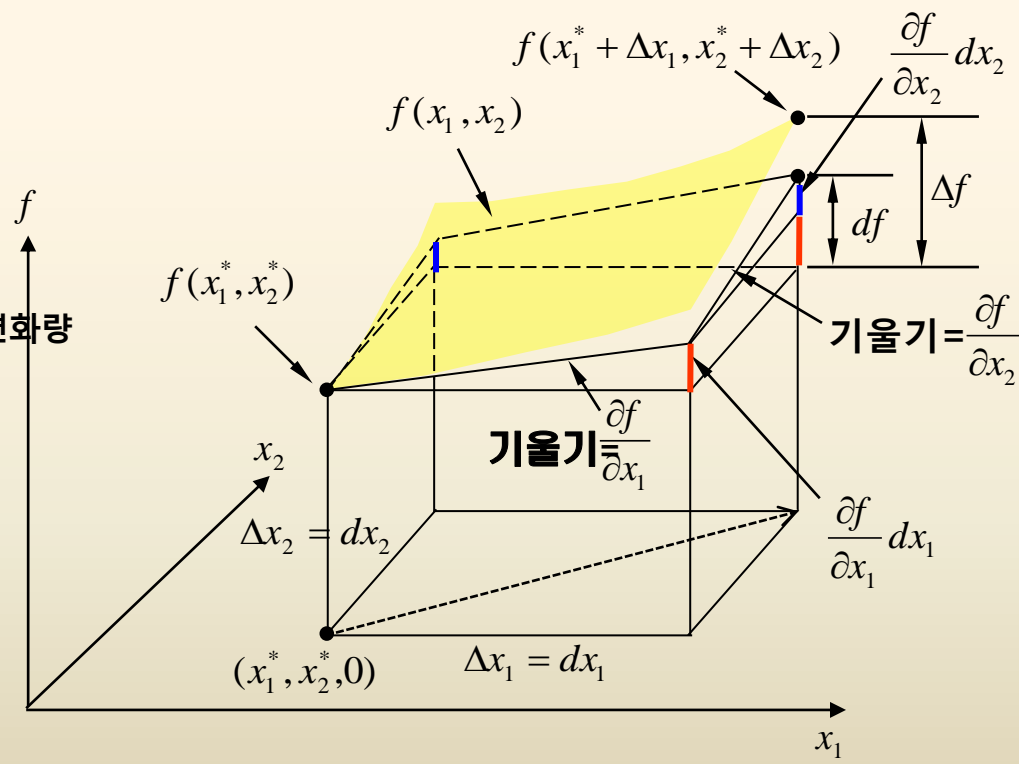
→  $x_2$ 가 고정일 때  $x_1$ 의 변화에 따른  $f$ 의 변화량  
 →  $x_1$ 가 고정일 때  $x_2$ 의 변화에 따른  $f$ 의 변화량

↓

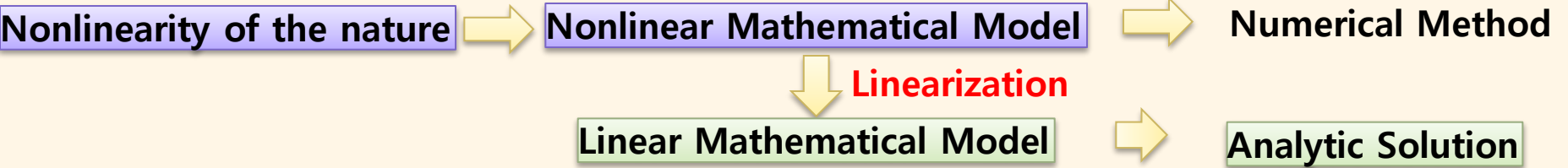
$$f = \mathbf{V}, \quad \frac{x_1}{\text{속도}} = t, \quad \frac{x_2}{\text{시간}} = x$$

$$d\mathbf{V} = \frac{\partial \mathbf{V}}{\partial t} dt + \frac{\partial \mathbf{V}}{\partial x} dx$$

→ 시간이 고정일 때, 위치 변화에 따른 속도 변화량  
 → 위치가 고정일 때, 시간 변화에 따른 속도 변화량



# Nonlinearity



**Taylor Series**  $f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$

## 삼각함수 Taylor 전개

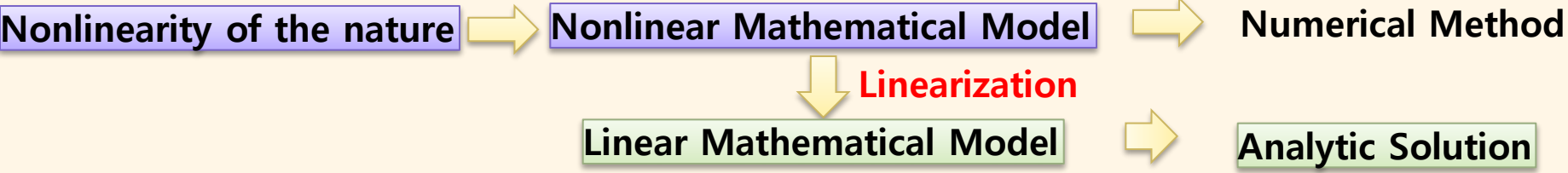
$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots = \sum_{n=0}^{\infty} \frac{(-1)^n}{(2n+1)!} \theta^{2n+1}$$

$$\cos \theta = 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!} - \dots = \sum_{n=0}^{\infty} \frac{(-1)^n}{(2n)!} \theta^{2n}$$

$$\tan \theta = \theta + \frac{\theta^3}{3} + \frac{2\theta^5}{15} + \dots = \sum_{n=0}^{\infty} \frac{B_{2n} (-4)^n (1-4^n)}{(2n)!} \theta^{2n-1}$$



# Nonlinearity



**Taylor Series**  $f(x^* + \Delta x) = f(x^*) + f'(x^*)\Delta x + \frac{1}{2} f''(x^*)\Delta x^2 + \dots$

## 삼각함수 Taylor 전개

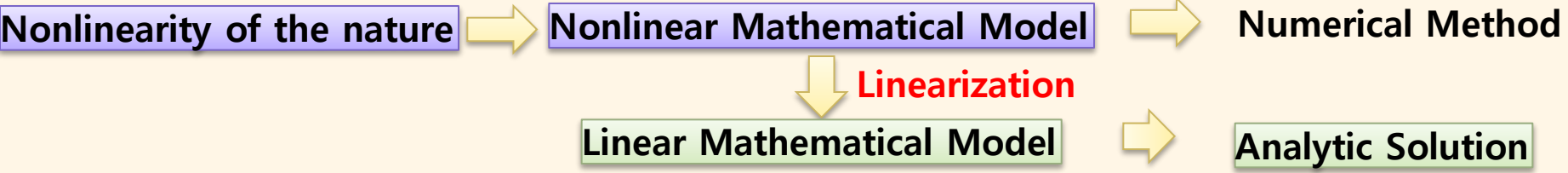
$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots = \sum_{n=0}^{\infty} \frac{(-1)^n}{(2n+1)!} x^{2n+1}$$

$$\cos \theta = 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!} - \dots = \sum_{n=0}^{\infty} \frac{(-1)^n}{(2n)!} x^{2n}$$

$$\tan \theta = \theta + \frac{\theta^3}{3} + \frac{2\theta^5}{15} + \dots = \sum_{n=0}^{\infty} \frac{B_{2n} (-4)^n (1-4^n)}{(2n)!} x^{2n-1}$$

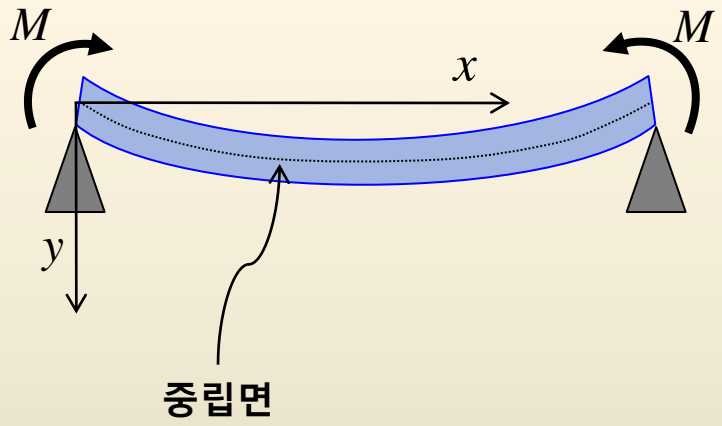


# Nonlinearity



## Ex) 탄성선의 미분 방정식

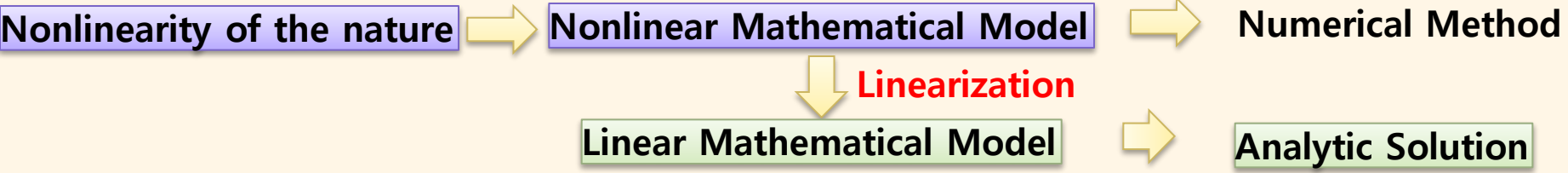
Deflection of a beam



\* 중립면 : 보의 볼록 한 쪽의 재료는 늘어나고, 오목한 쪽의 재료는 줄어든다. 이 때, 보의 상면과 하면 사이의 어딘가는 길이가 변하지 않는 재료들의 층이 존재할 것이다. 그와 같은 섬유들이 이루는 면을 중립면이라 한다.

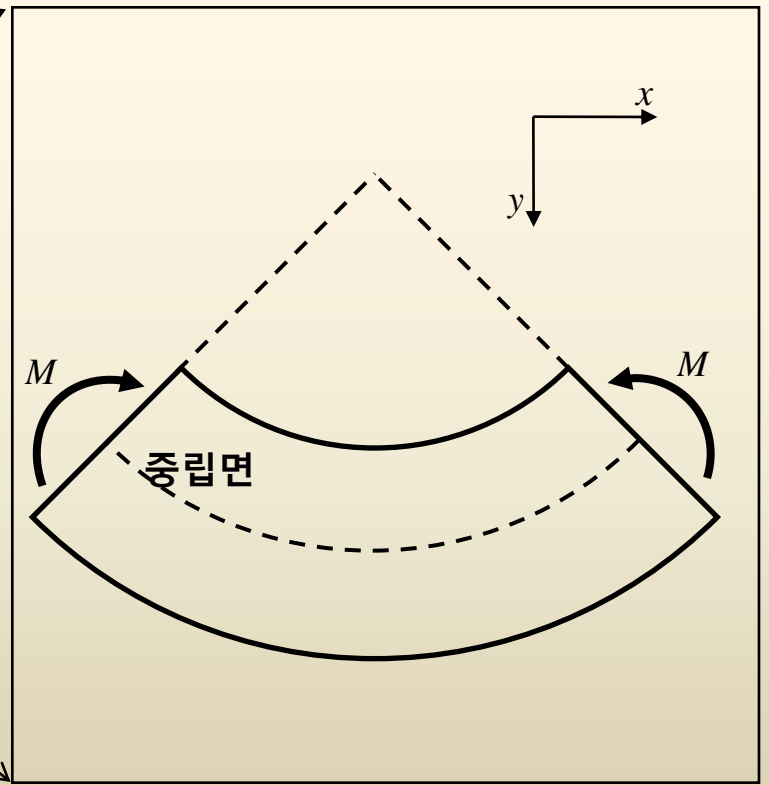
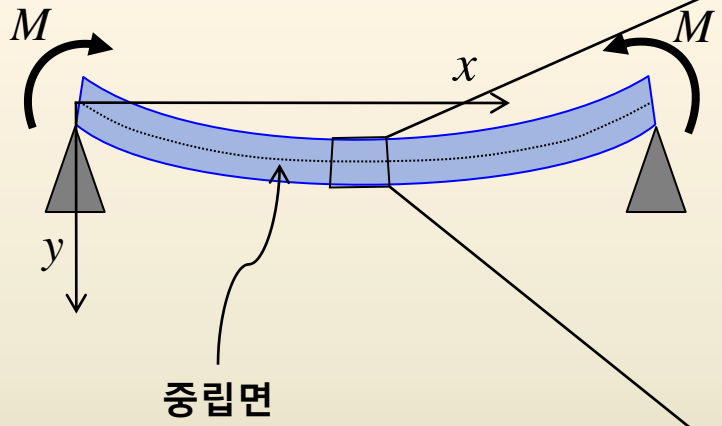


# Nonlinearity



## Ex) 탄성선의 미분 방정식

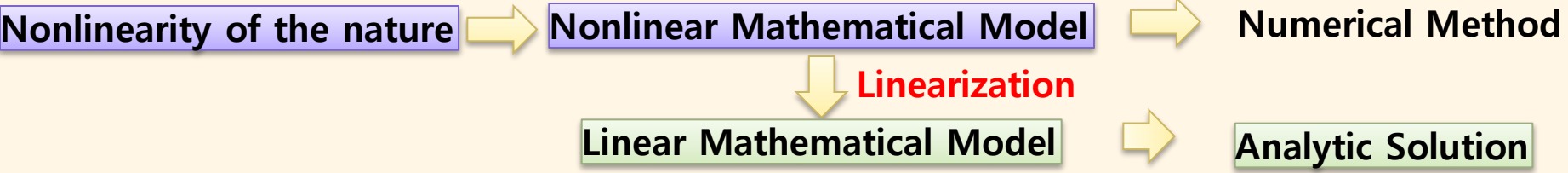
Deflection of a beam



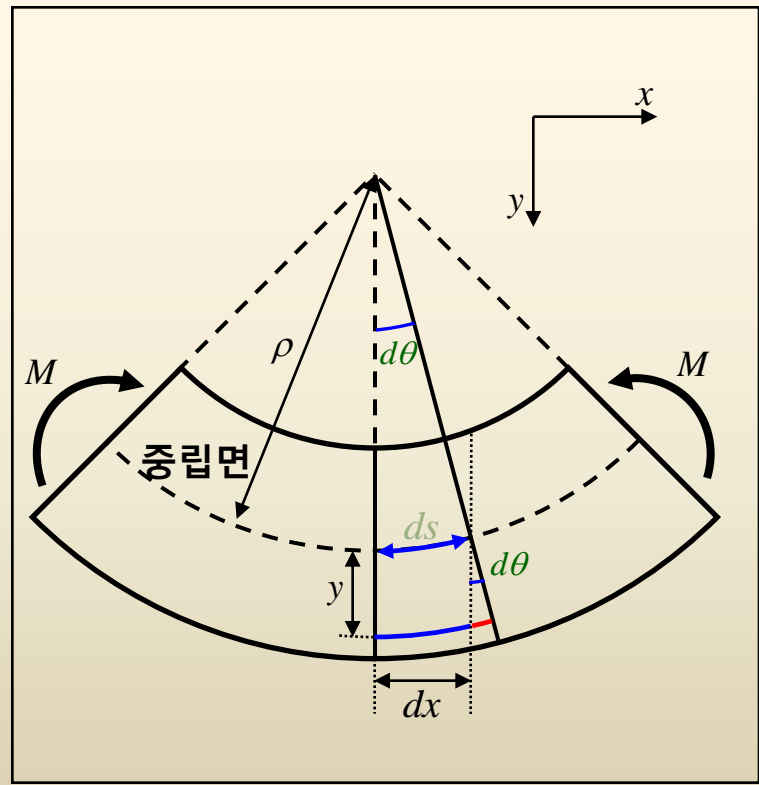
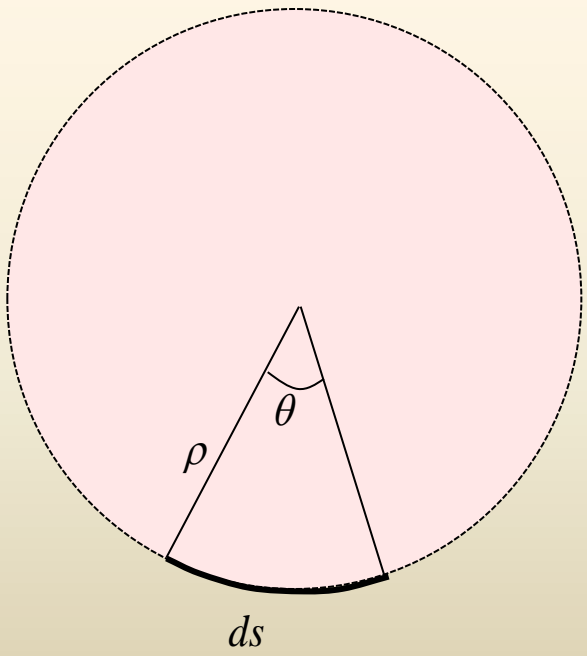
\* 중립면 : 보의 볼록 한 쪽의 재료는 늘어나고, 오목한 쪽의 재료는 줄어든다. 이 때, 보의 상면과 하면 사이의 어딘가는 길이가 변하지 않는 재료들의 층이 존재할 것이다. 그와 같은 섬유들이 이루는 면을 중립면이라 한다.



# Nonlinearity



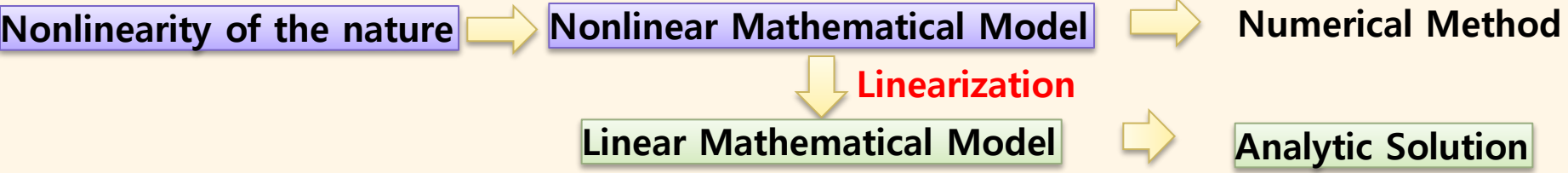
## Ex) 탄성선의 미분 방정식



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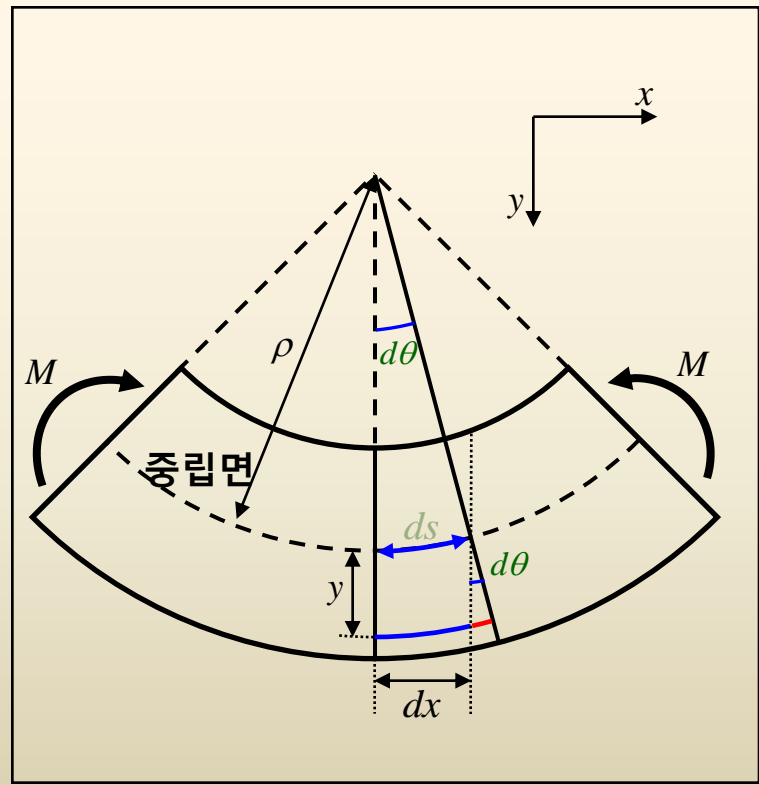


# Nonlinearity

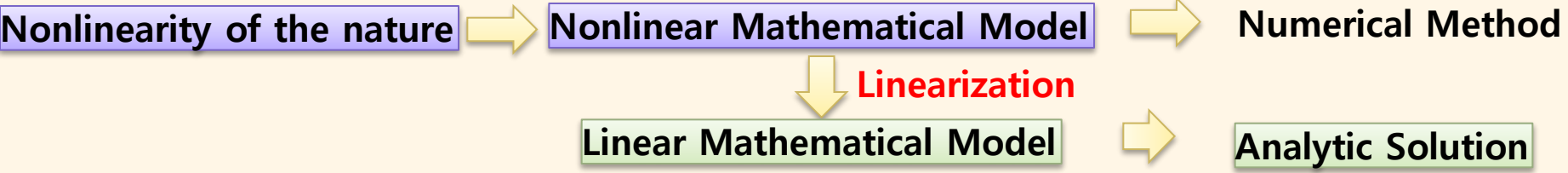


Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$



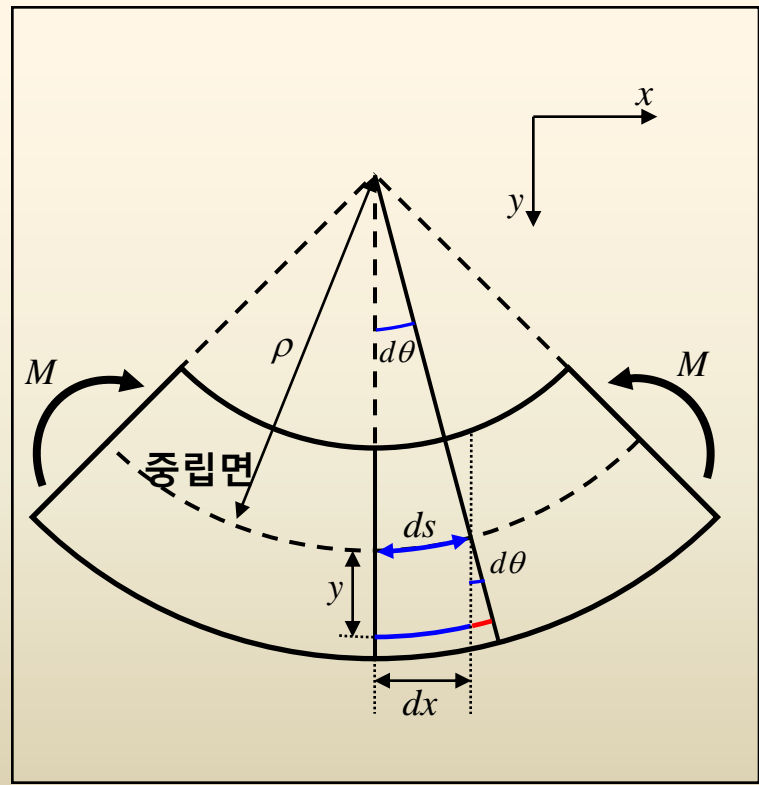
# Nonlinearity



Ex) 탄성선의 미분 방정식

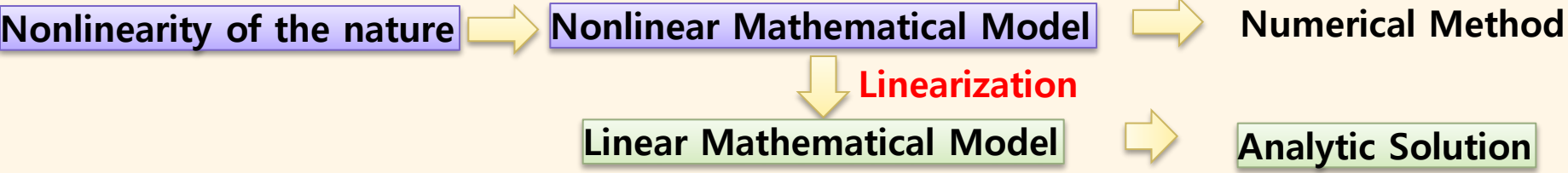
$$\sigma = E\varepsilon$$

$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$





# Nonlinearity

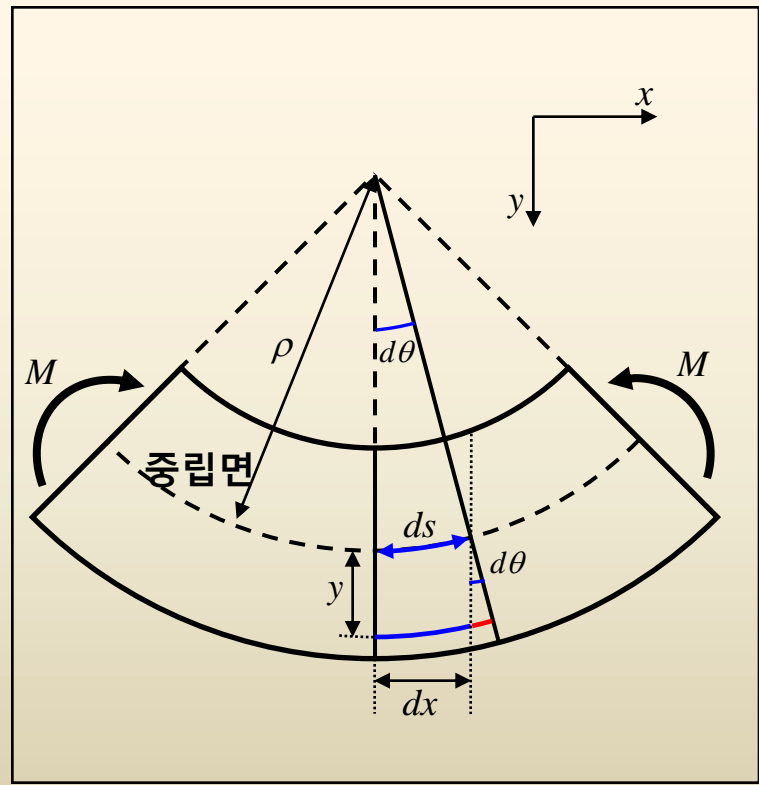


Ex) 탄성선의 미분 방정식

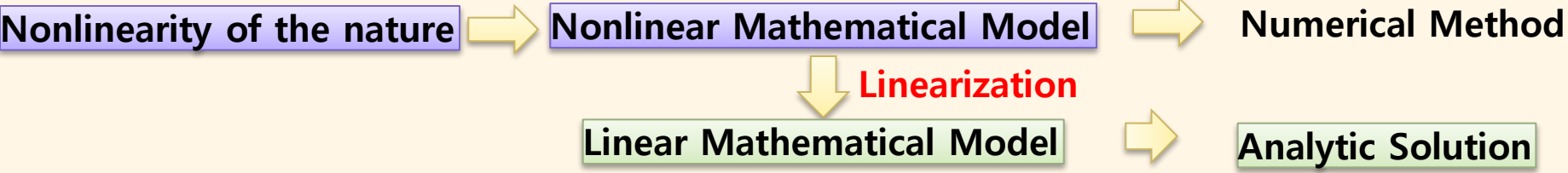
$$\sigma = E\varepsilon$$

$$\textcircled{1} \rho \cdot d\theta = ds \implies \frac{d\theta}{ds} = \frac{1}{\rho}$$

② 중립면에서 y만큼 떨어진 곳의 변형률 (ε)



# Nonlinearity



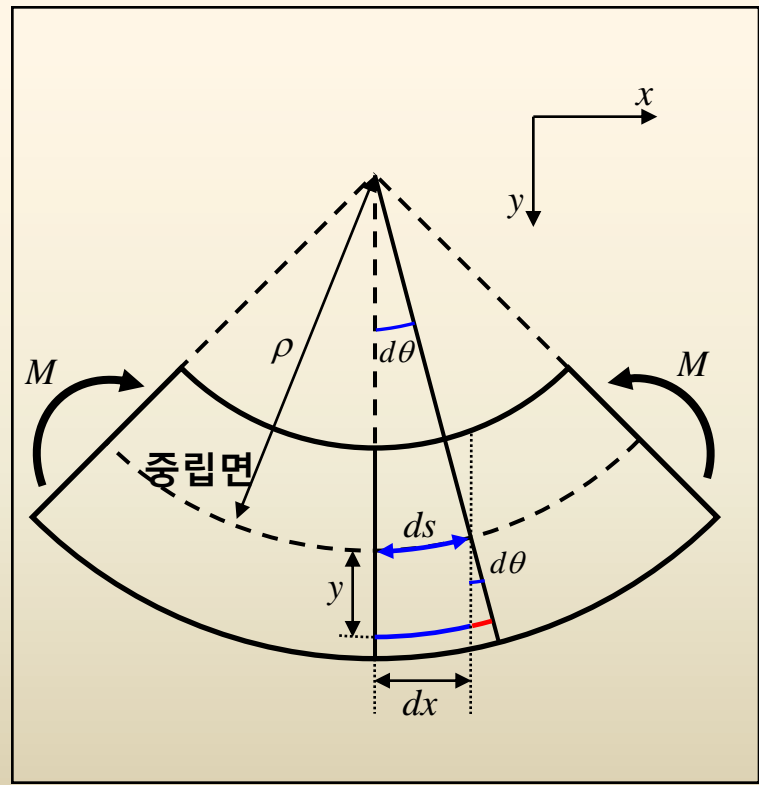
Ex) 탄성선의 미분 방정식

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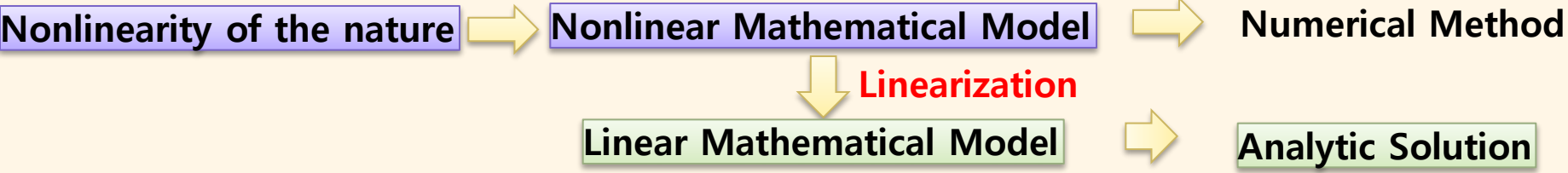
$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

② 중립면에서 y만큼 떨어진 곳의 변형율 (ε)

*ds* : 원래 길이



# Nonlinearity



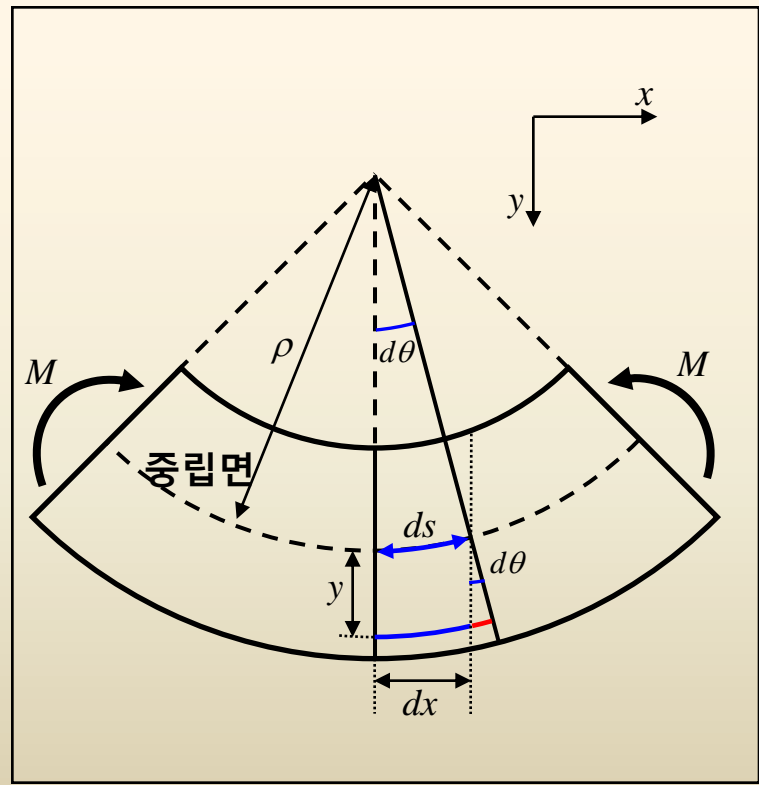
## Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$

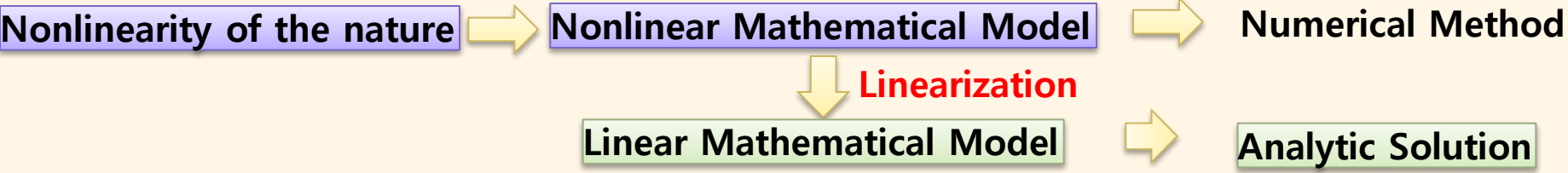
$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

② 중립면에서 y만큼 떨어진 곳의 변형율 (ε)

$ds$  : 원래 길이       $y \cdot d\theta$  : 늘어난 길이



# Nonlinearity



Ex) 탄성선의 미분 방정식

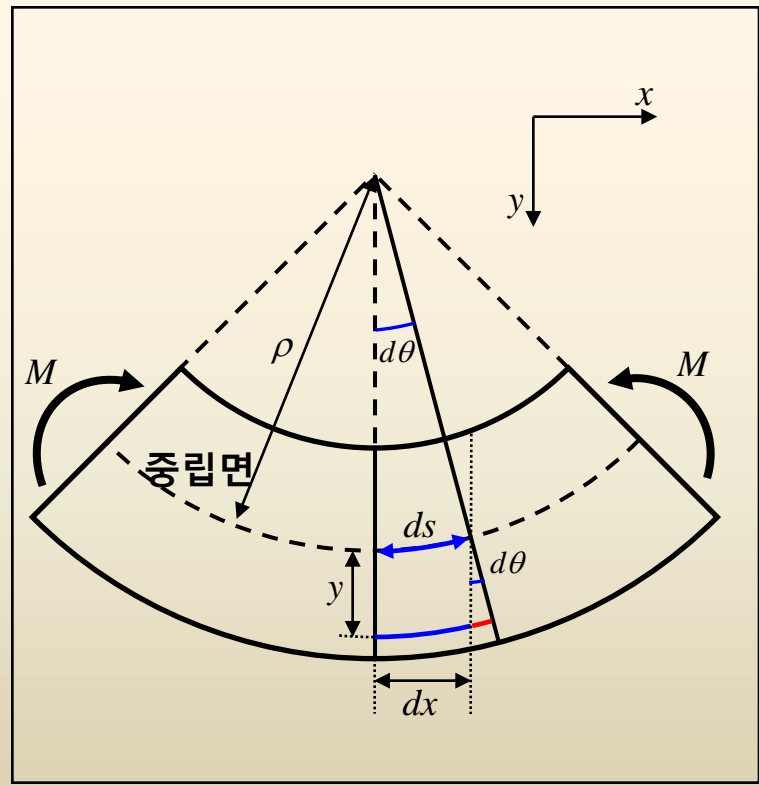
$$\sigma = E\varepsilon$$

$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

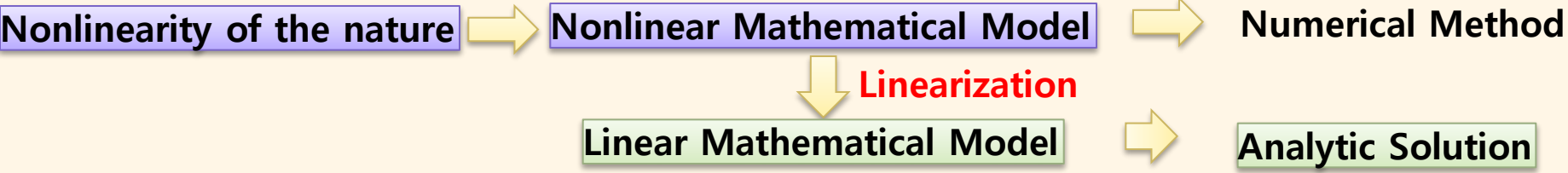
② 중립면에서 y만큼 떨어진 곳의 변형율 (ε)

$ds$  : 원래 길이       $y \cdot d\theta$  : 늘어난 길이

$$\varepsilon = \frac{\text{늘어난길이}}{\text{원래길이}} = \frac{y \cdot d\theta}{ds} = \frac{y}{\rho}$$



# Nonlinearity



Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$

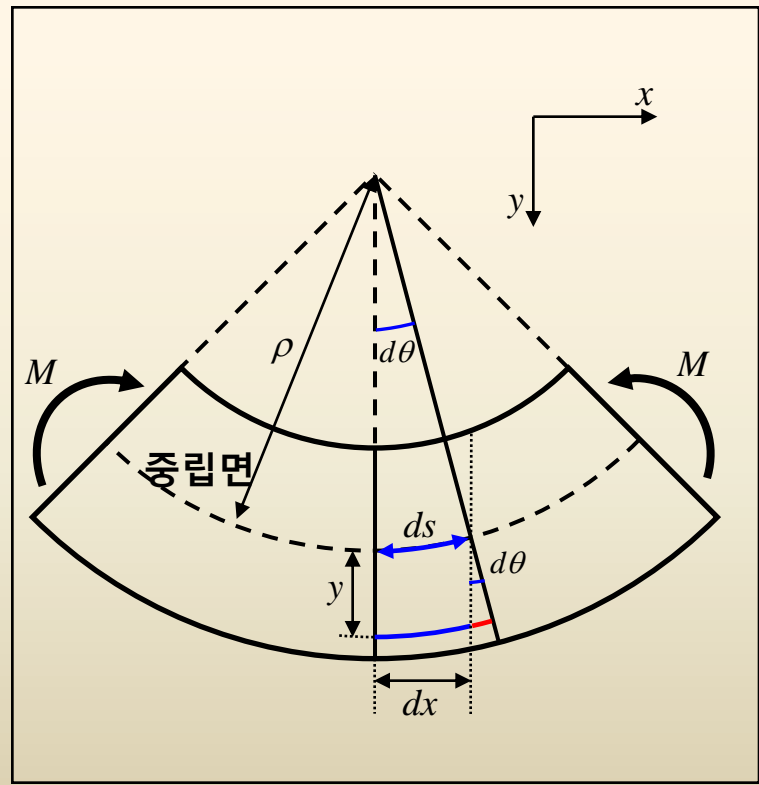
$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

② 중립면에서 y만큼 떨어진 곳의 변형율 (ε)

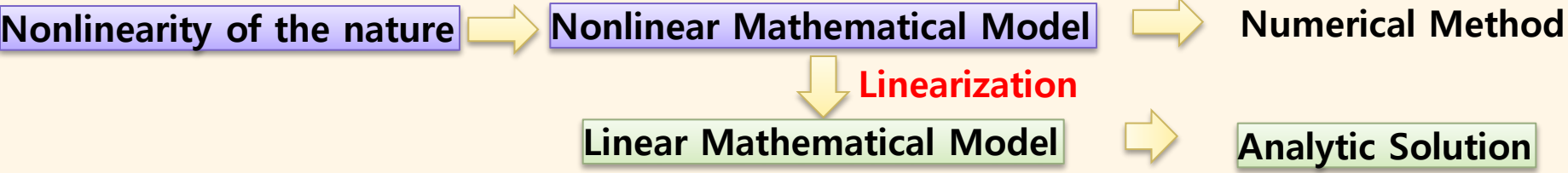
$ds$  : 원래 길이       $y \cdot d\theta$  : 늘어난 길이

$$\varepsilon = \frac{\text{늘어난길이}}{\text{원래길이}} = \frac{y \cdot d\theta}{ds} = \frac{y}{\rho}$$

③ 중립면에서 y만큼 떨어진 곳의 응력(σ)



# Nonlinearity



## Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$

$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

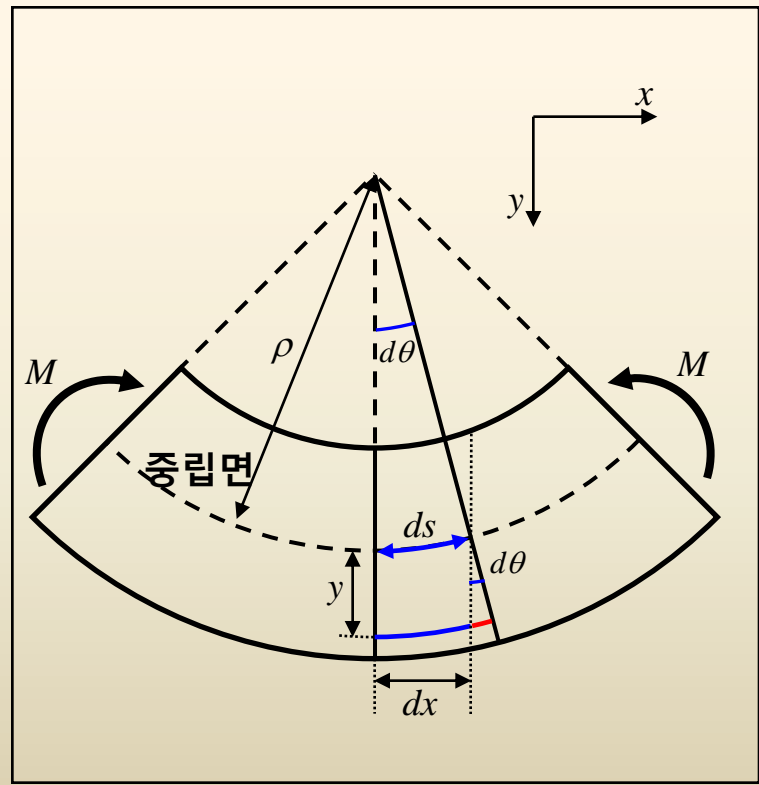
② 중립면에서 y만큼 떨어진 곳의 변형율 (ε)

$ds$  : 원래 길이       $y \cdot d\theta$  : 늘어난 길이

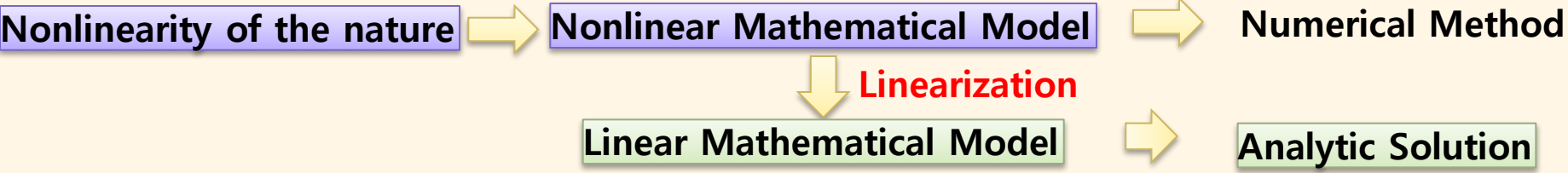
$$\varepsilon = \frac{\text{늘어난길이}}{\text{원래길이}} = \frac{y \cdot d\theta}{ds} = \frac{y}{\rho}$$

③ 중립면에서 y만큼 떨어진 곳의 응력(σ)

$$\sigma = E \cdot \varepsilon = E \cdot \frac{y}{\rho}$$



# Nonlinearity



Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$

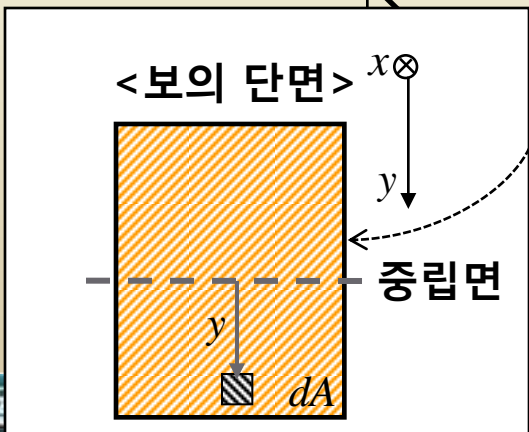
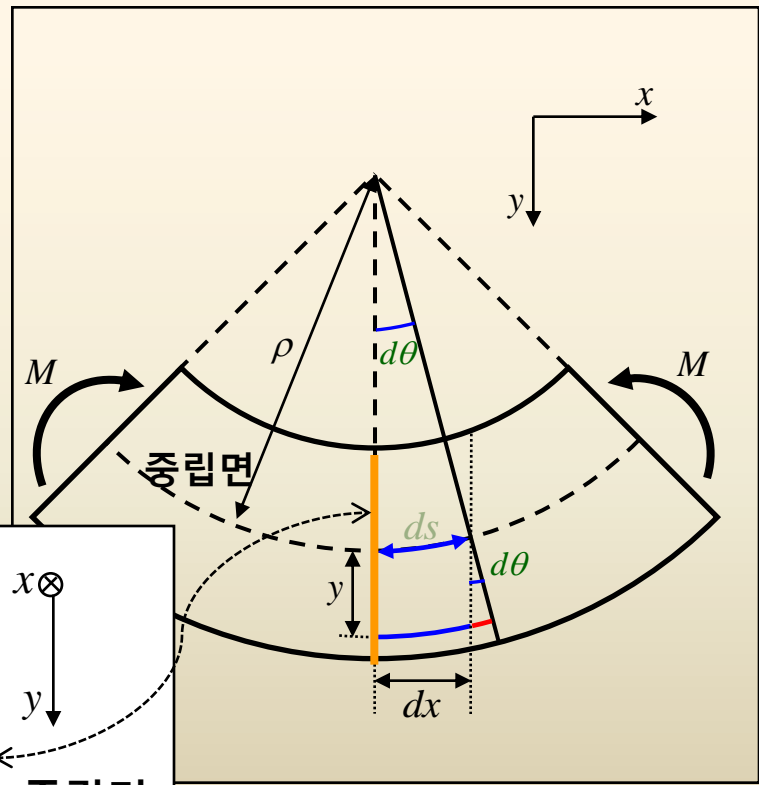
$$\textcircled{1} \rho \cdot d\theta = ds \implies \frac{d\theta}{ds} = \frac{1}{\rho}$$

③ 중립면에서 y만큼 떨어진 곳의 응력( $\sigma$ )

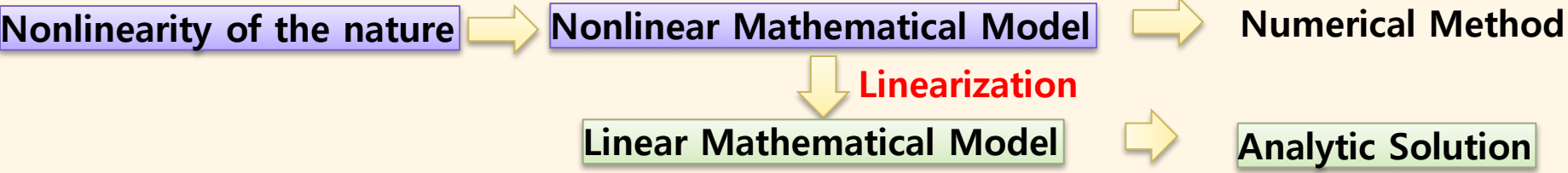
$$\sigma = E \cdot \varepsilon = E \cdot \frac{y}{\rho}$$

④ 미소면적에 작용하는 힘 :

$$dF = \sigma dA = E \cdot \frac{y}{\rho} dA$$



# Nonlinearity



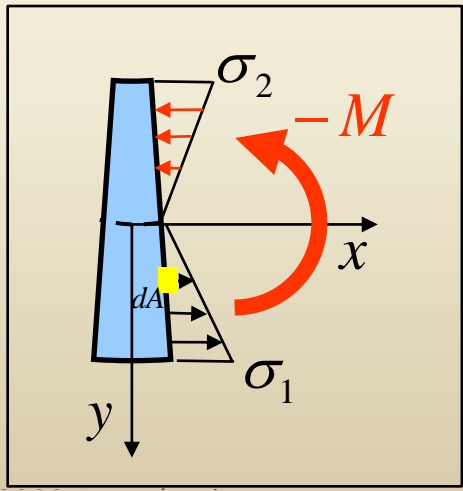
## Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$

$$\textcircled{1} \rho \cdot d\theta = ds \implies \frac{d\theta}{ds} = \frac{1}{\rho}$$

$$\textcircled{4} \text{ 미소면적에 작용하는 힘 : } dF = \sigma dA = E \cdot \frac{y}{\rho} dA$$

⑤ 미소면적에 작용하는 모멘트



• 응력이 양인 곳에서의 모멘트

$$dM = - y \sigma dA$$

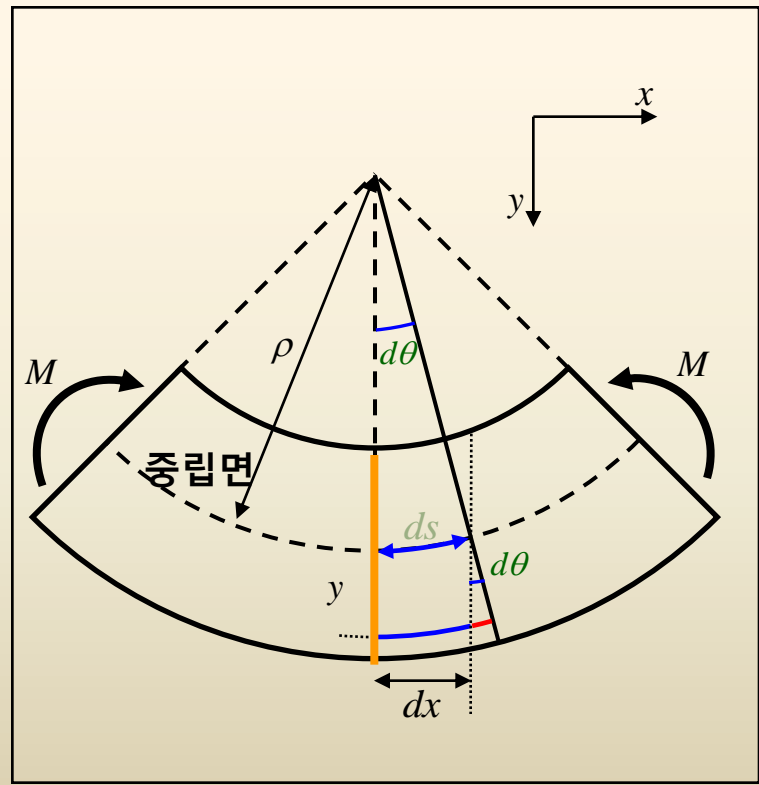
(< 0) (> 0) (> 0) (> 0)

• 응력이 음인 곳에서의 모멘트

$$dM = - y \sigma dA$$

(< 0) (< 0) (< 0) (> 0)

$$\therefore dM = -y\sigma dA$$

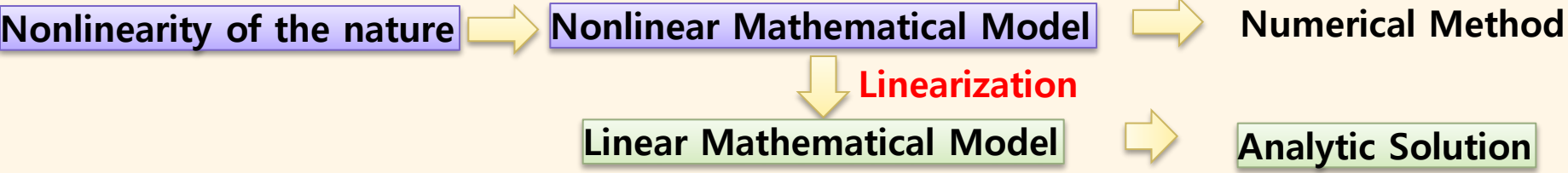


- 상면 '압축', 하면 '인장'
- 선박의 경우 sagging condition





# Nonlinearity



## Ex) 탄성선의 미분 방정식

$$\sigma = E\varepsilon$$

$$\textcircled{1} \rho \cdot d\theta = ds \quad \longrightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

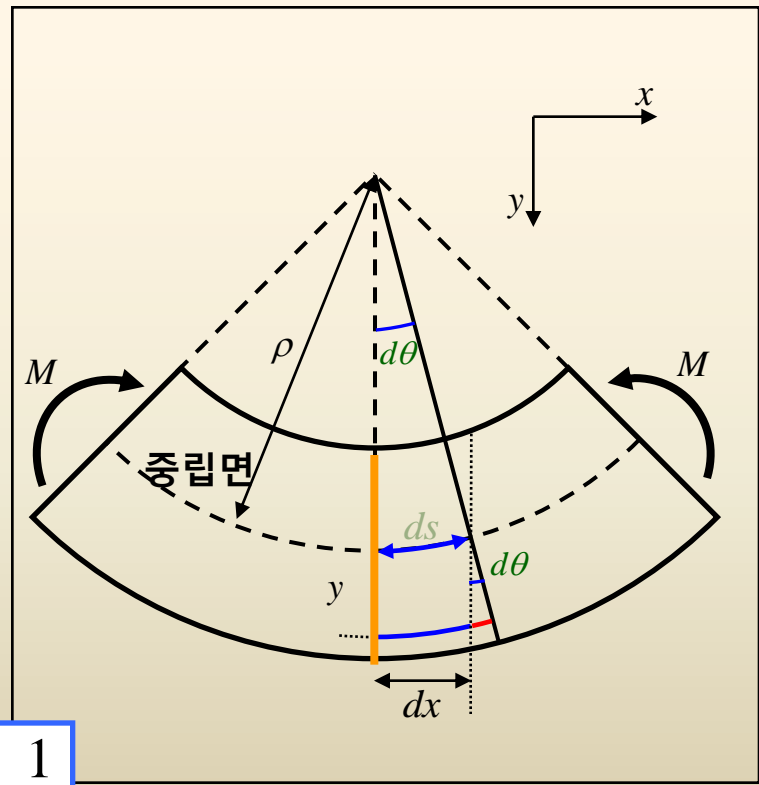
$$\textcircled{4} \text{ 미소면적에 작용하는 힘 : } dF = \sigma dA = E \cdot \frac{y}{\rho} dA$$

$$\textcircled{5} \text{ 미소면적에 작용하는 모멘트 } dM = -y\sigma dA$$

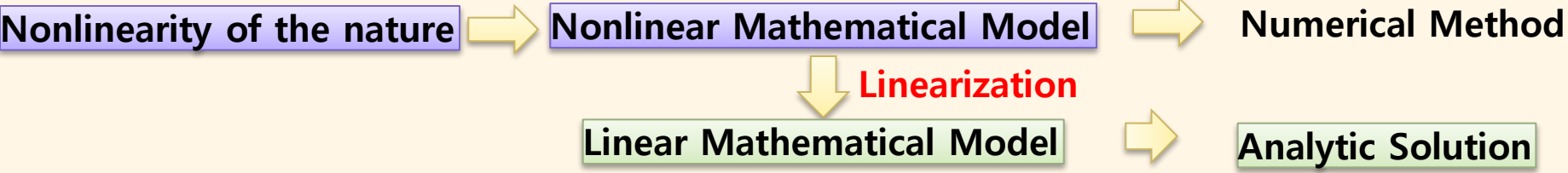
⑥ 단면에 작용하는 모멘트 :

$$\begin{aligned}
 M &= \int_A dM = -\int_A y dF \\
 &= -\int_A y \cdot E \frac{y}{\rho} dA = -\frac{E}{\rho} \int_A y^2 dA
 \end{aligned}$$

Define  $I = \int_A y^2 dA$  then,  $M = -\frac{EI}{\rho}$   $\longrightarrow$   $\frac{M}{EI} = -\frac{1}{\rho}$



# Nonlinearity

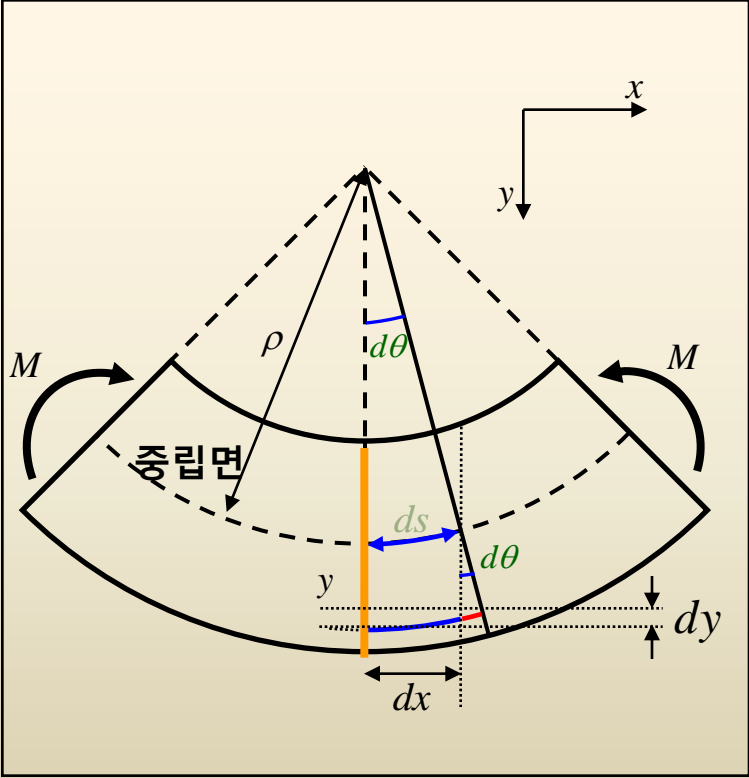


Ex) 탄성선의 미분 방정식

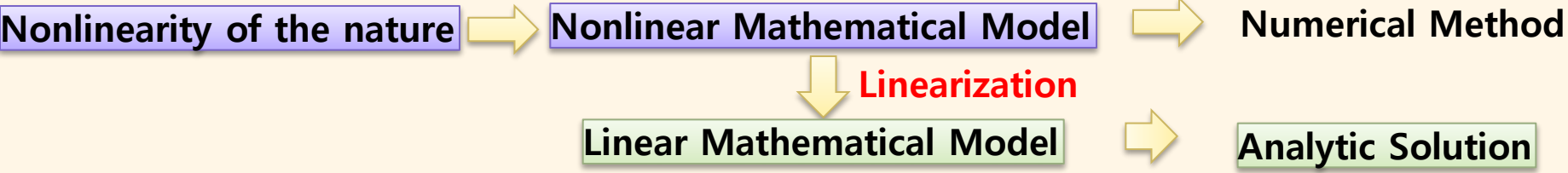
$$\rho \cdot d\theta = ds \quad \Rightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

$$dF = \sigma dA = E \cdot \frac{y}{\rho} dA \quad \Rightarrow \quad \therefore \frac{d\theta}{ds} = -\frac{M}{EI}$$

$$dM = -y\sigma dA \quad \Rightarrow \quad \frac{M}{EI} = -\frac{1}{\rho}$$



# Nonlinearity

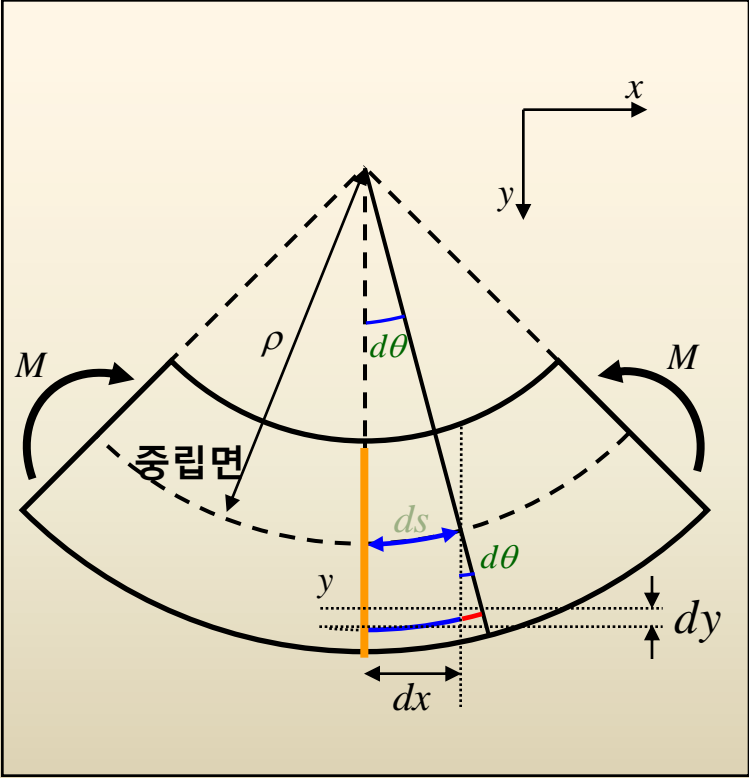


Ex) 탄성선의 미분 방정식

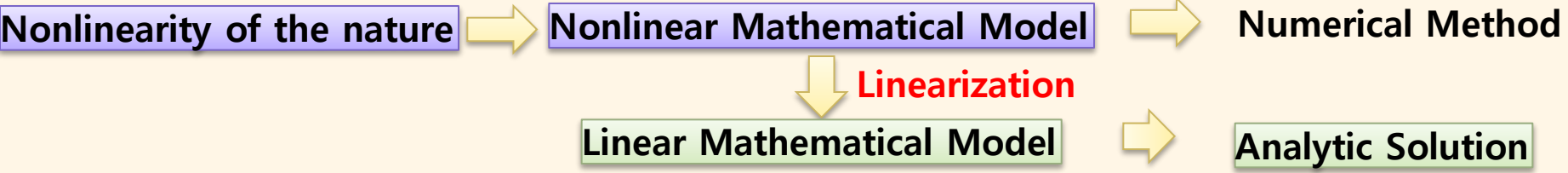
$$\rho \cdot d\theta = ds \quad \rightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

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# Nonlinearity



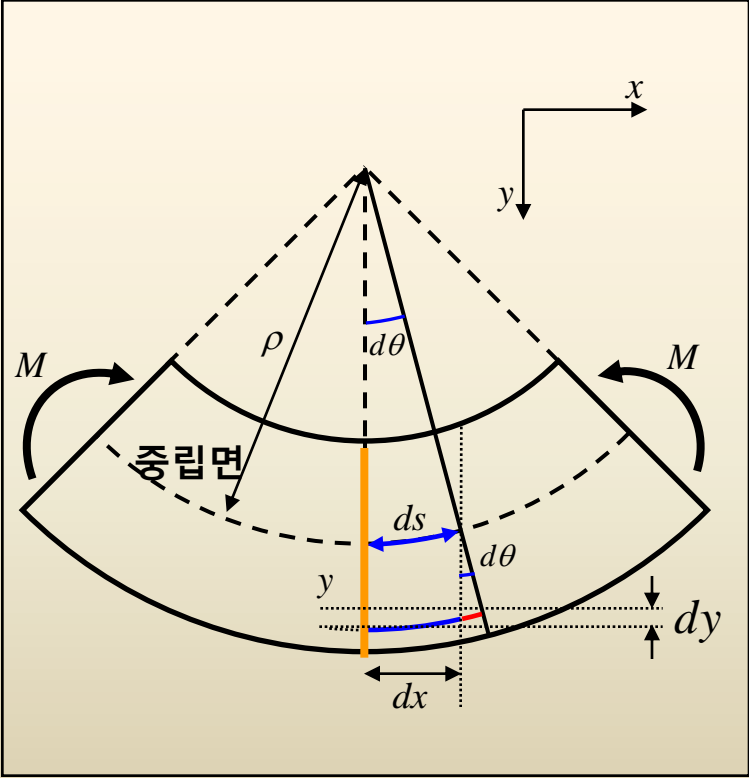
Ex) 탄성선의 미분 방정식

$$\rho \cdot d\theta = ds \quad \Rightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

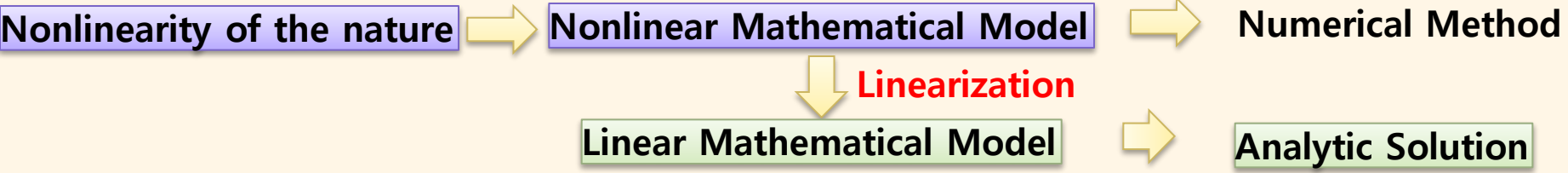
$$dF = \sigma dA = E \cdot \frac{y}{\rho} dA \quad \Rightarrow \quad \therefore \frac{d\theta}{ds} = -\frac{M}{EI}$$

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⑦ Assume that



# Nonlinearity



Ex) 탄성선의 미분 방정식

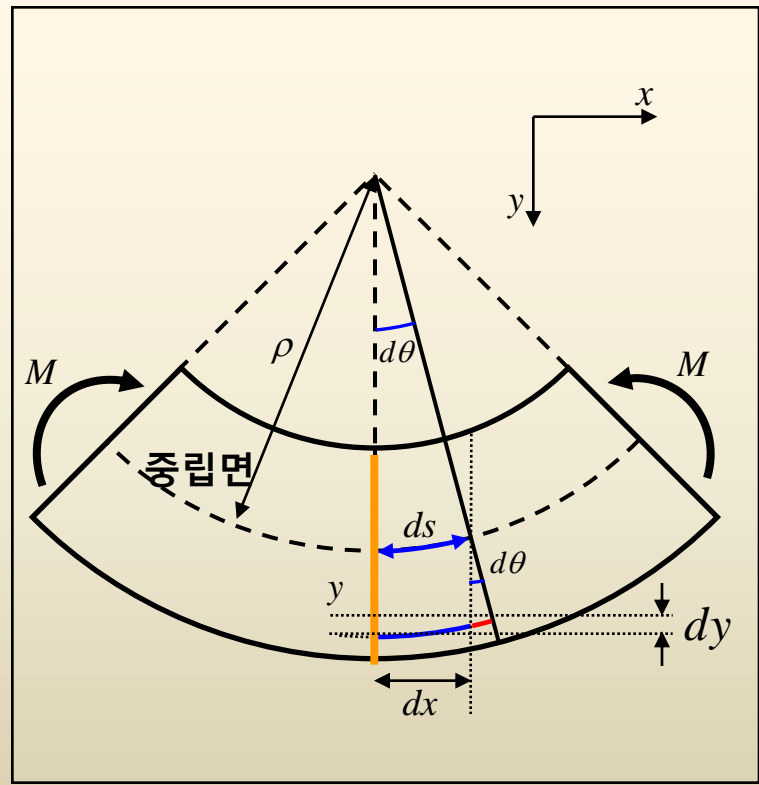
$$\rho \cdot d\theta = ds \quad \Rightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

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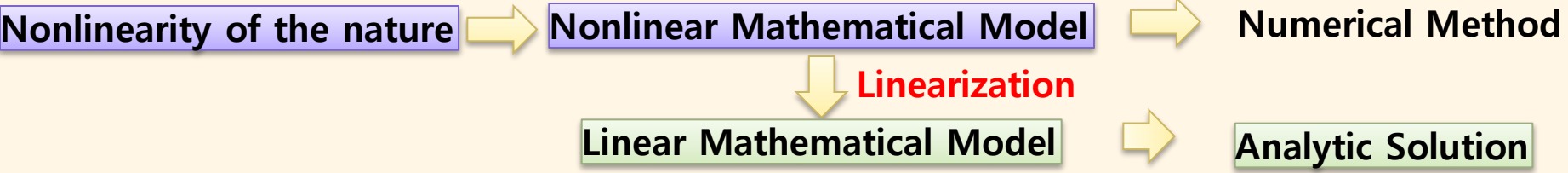
$$dM = -y\sigma dA \quad \Rightarrow \quad \frac{M}{EI} = -\frac{1}{\rho}$$

⑦ Assume that

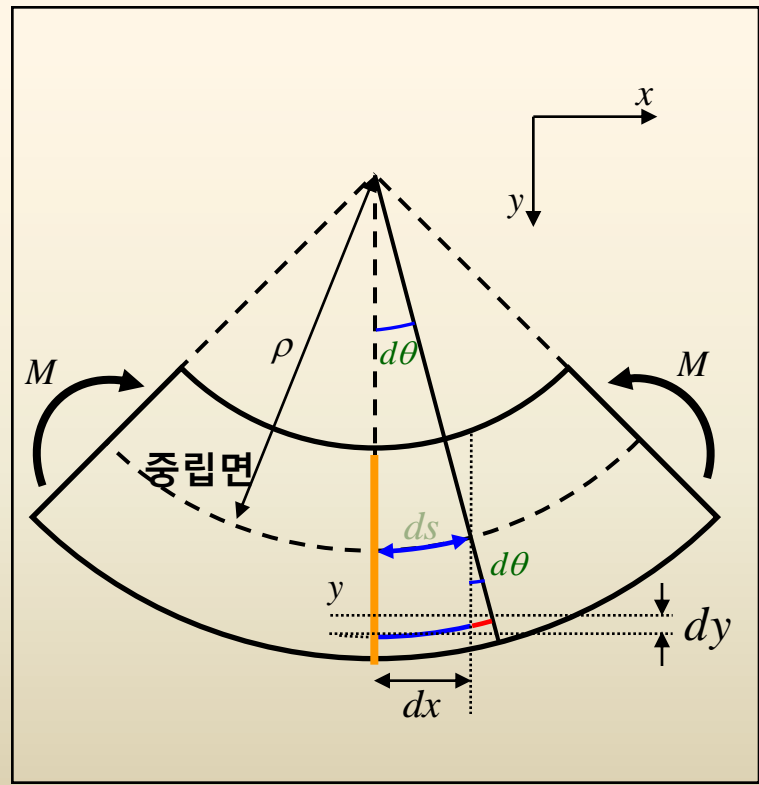
$$ds \approx dx, \quad \theta \approx \tan(\theta) = \frac{dy}{dx}$$



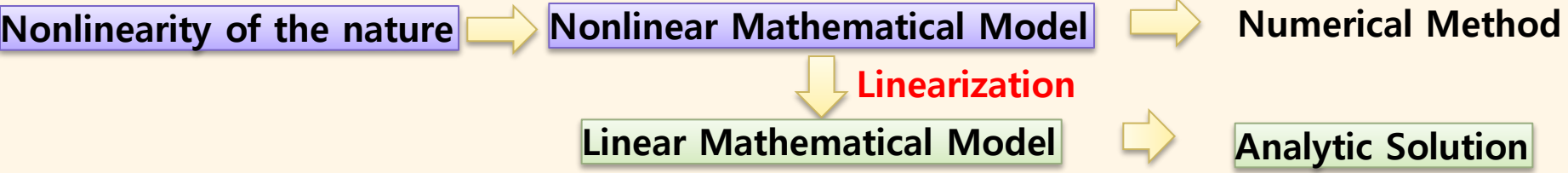
# Nonlinearity



Ex) 탄성선의 미분 방정식

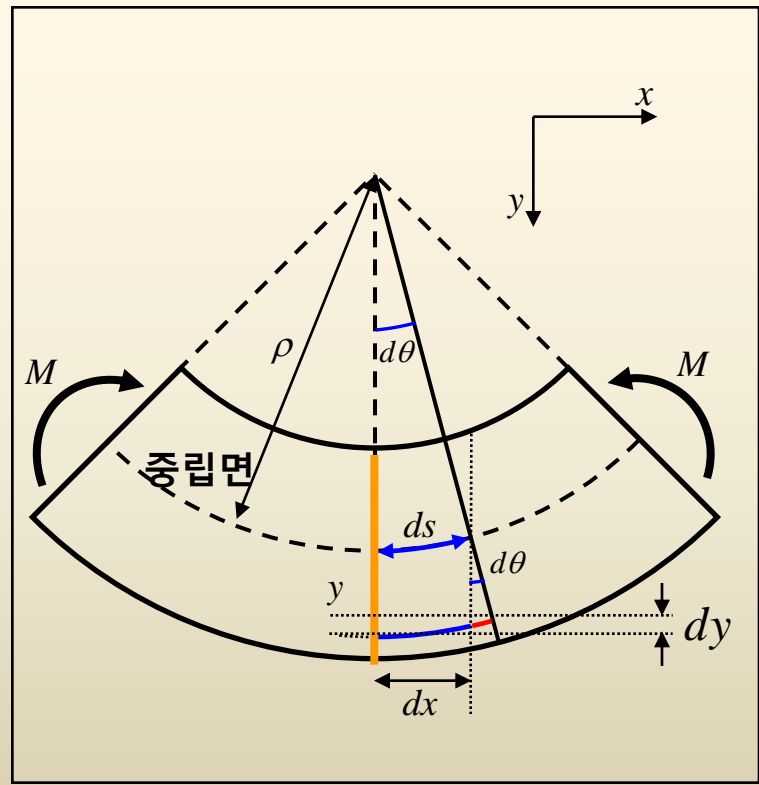


# Nonlinearity

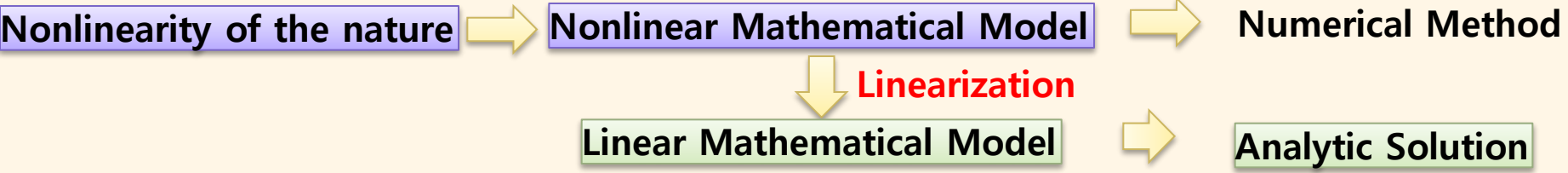


Ex) 탄성선의 미분 방정식

$$\underline{ds \approx dx}, \theta \approx \tan(\theta) = \frac{dy}{dx}$$

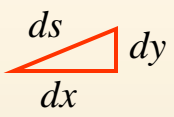


# Nonlinearity

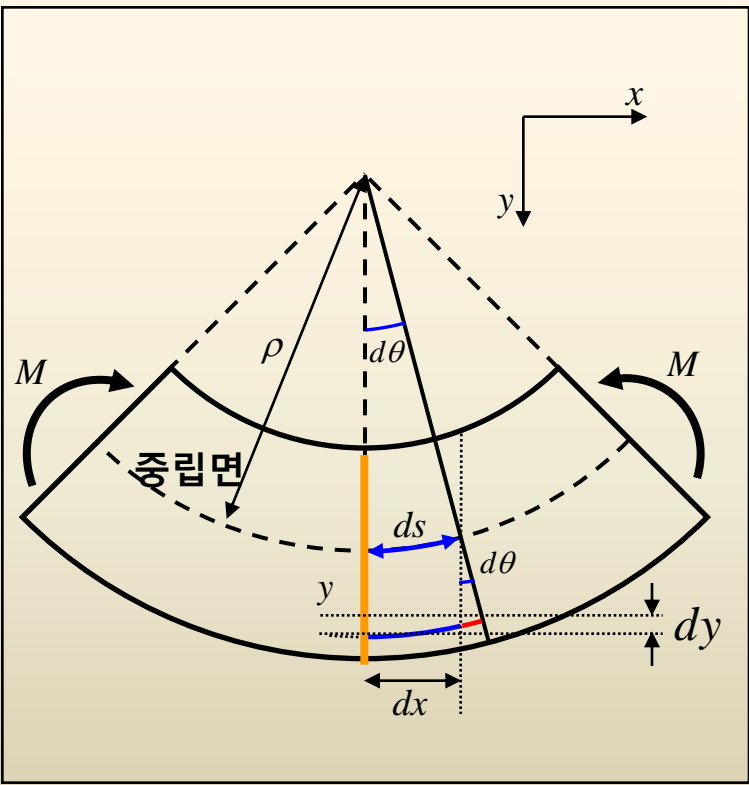


Ex) 탄성선의 미분 방정식

$$ds \approx dx, \theta \approx \tan(\theta) = \frac{dy}{dx}$$

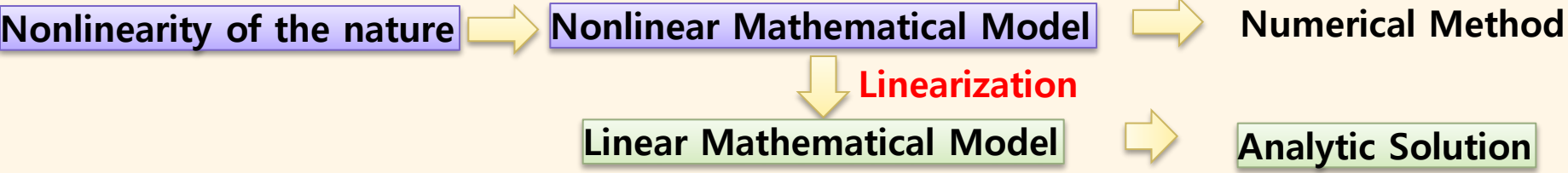


$$ds^2 = dx^2 + dy^2 \rightarrow ds = dx \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$





# Nonlinearity

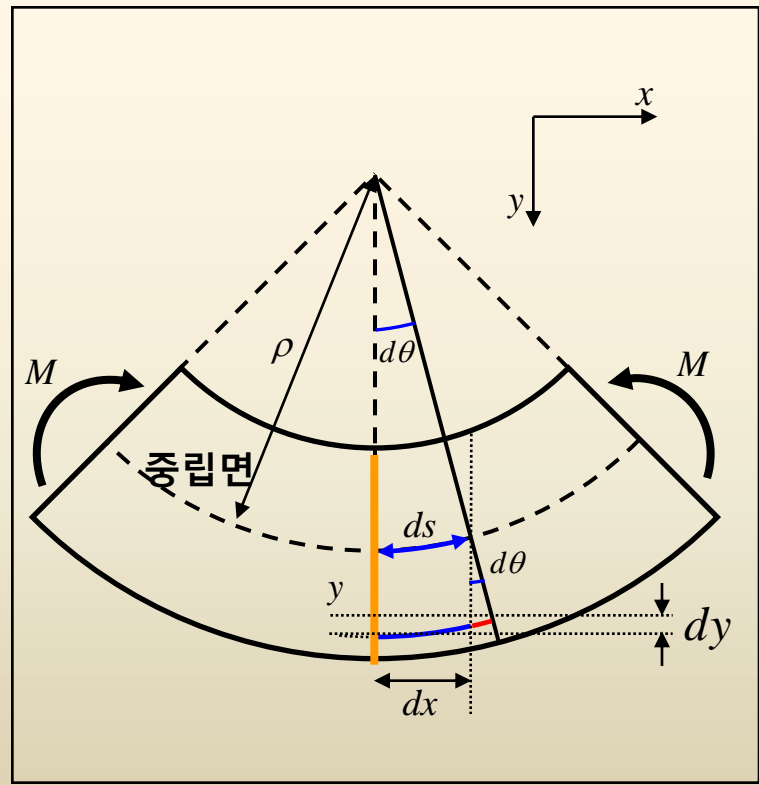


Ex) 탄성선의 미분 방정식

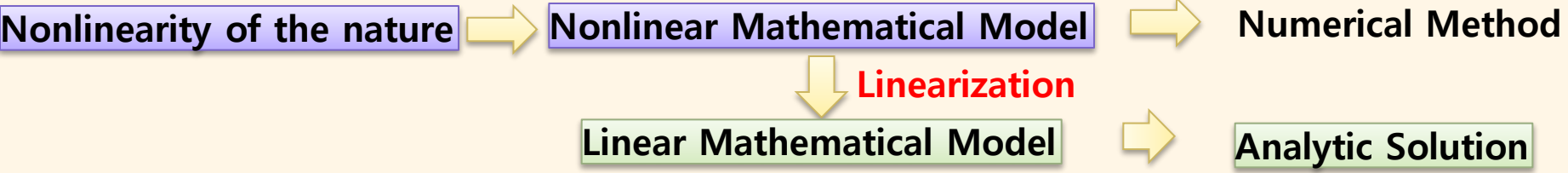
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let,  $z = \left(\frac{dy}{dx}\right)^2$  then,  $\sqrt{1 + \left(\frac{dy}{dx}\right)^2} = \sqrt{1 + z}$



# Nonlinearity



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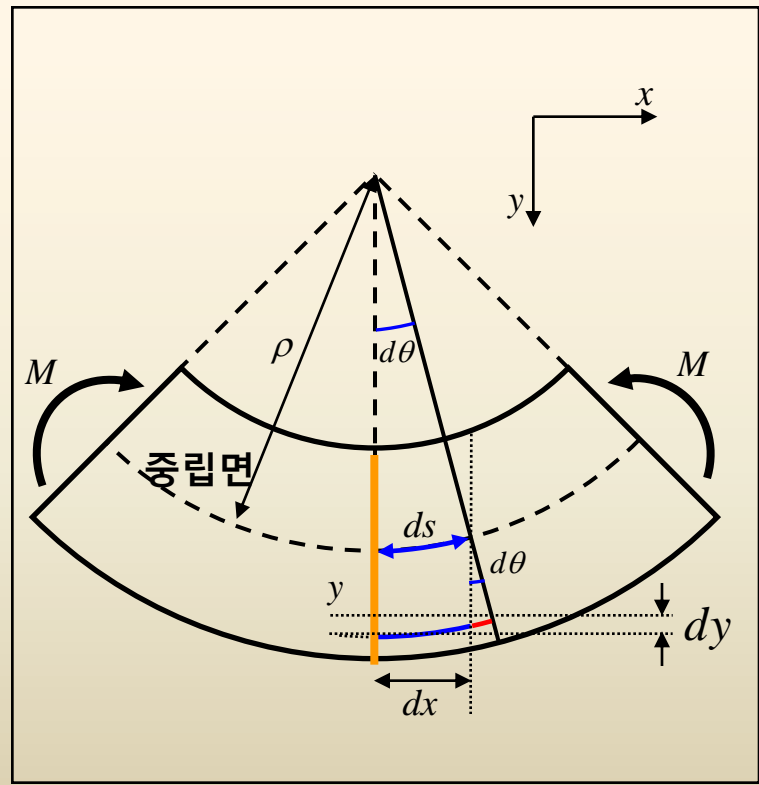
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$$f(z) = \sqrt{1+z}$$

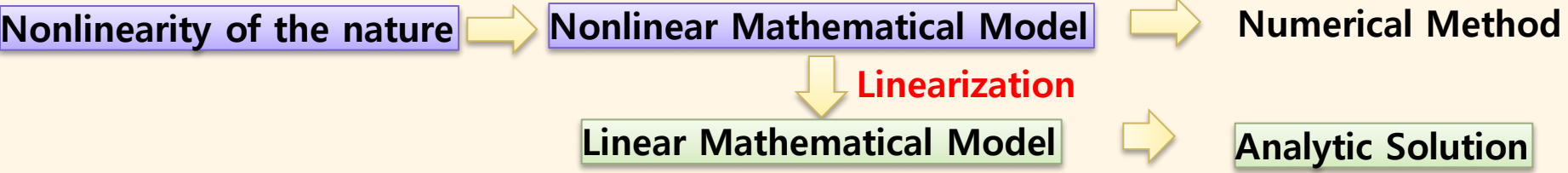
$$f(0) = 1$$

$$f'(0) = \frac{1}{2}(1+z)^{-\frac{1}{2}} \Big|_{z=0} = \frac{1}{2}$$

$$f''(0) = -\frac{1}{4}(1+z)^{-\frac{3}{2}} \Big|_{z=0} = -\frac{1}{4}$$



# Nonlinearity



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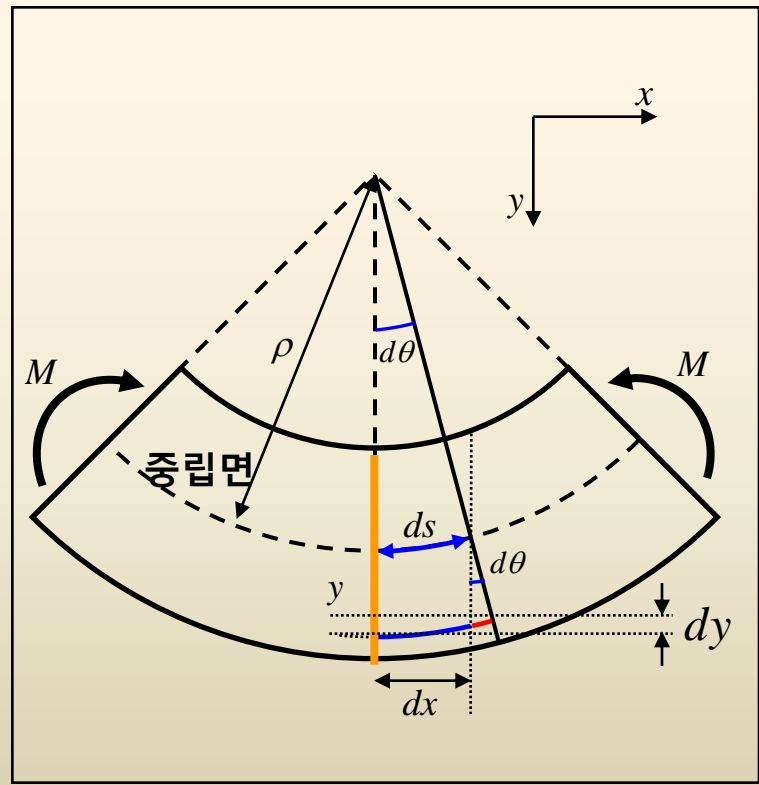
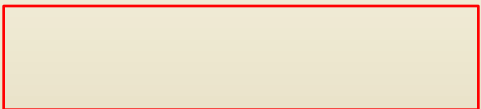
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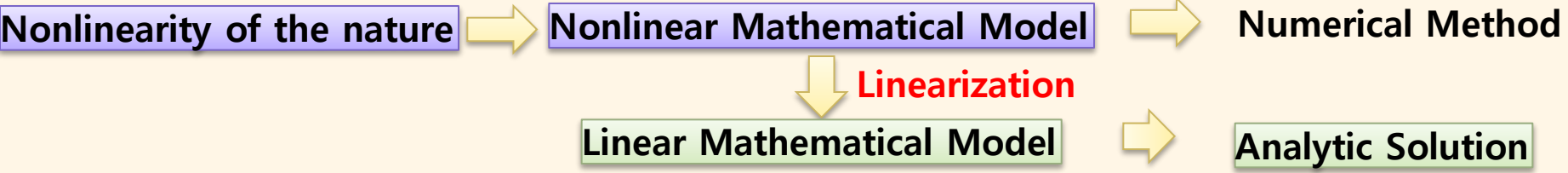
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# Nonlinearity



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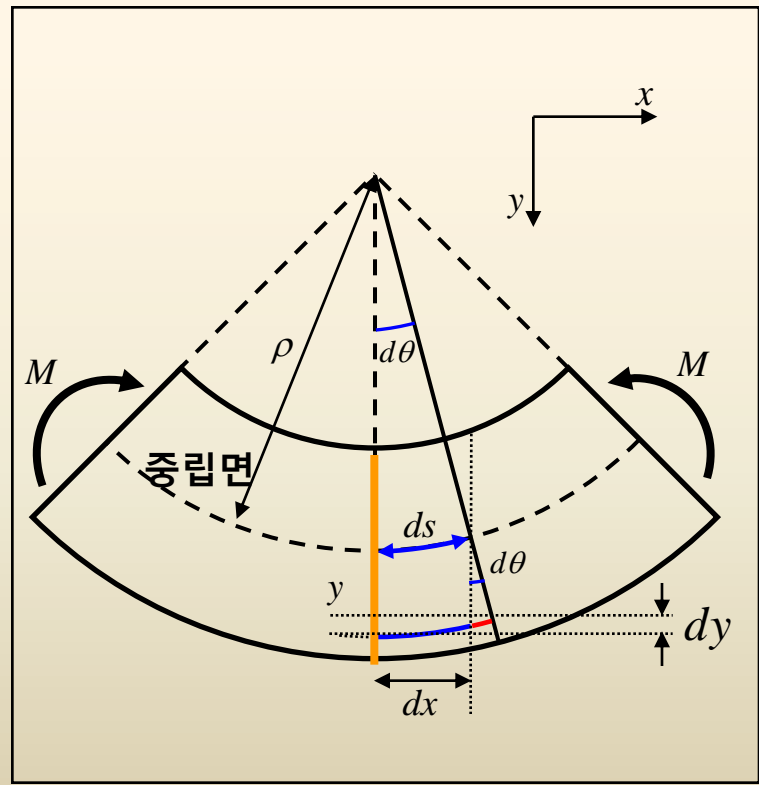
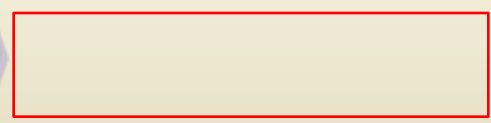
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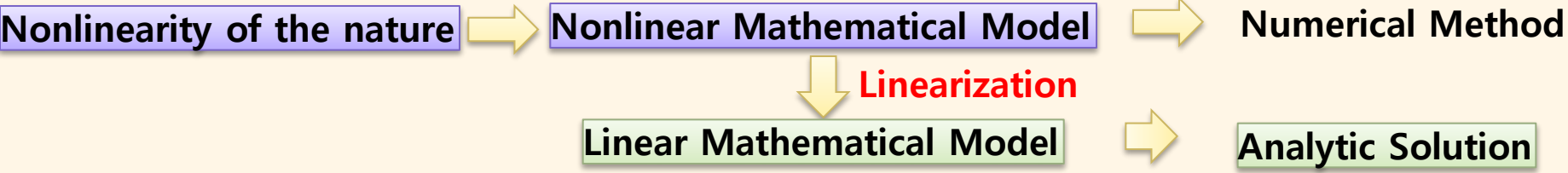
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# Nonlinearity



Ex) 탄성선의 미분 방정식

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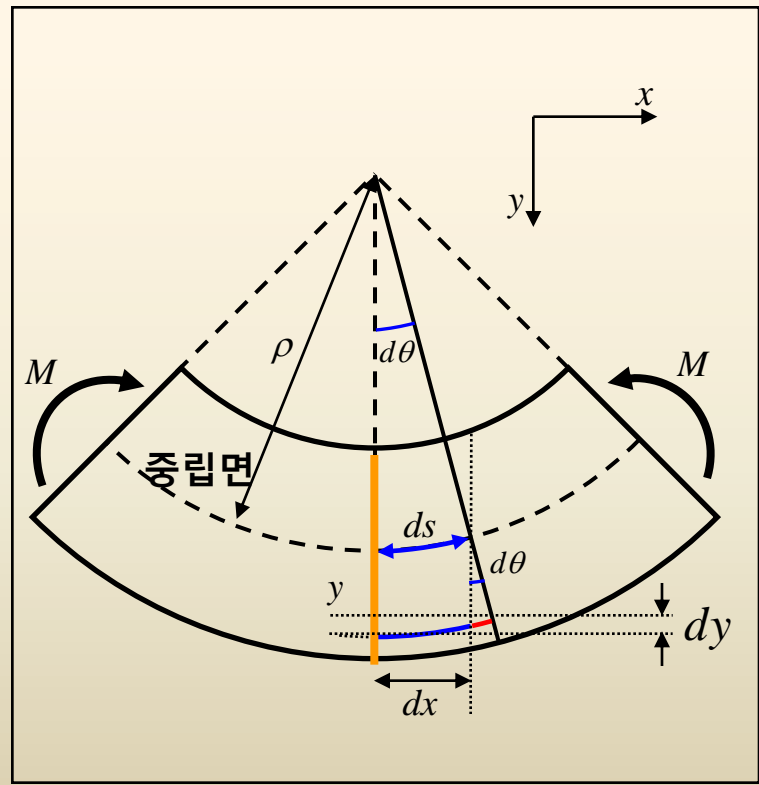
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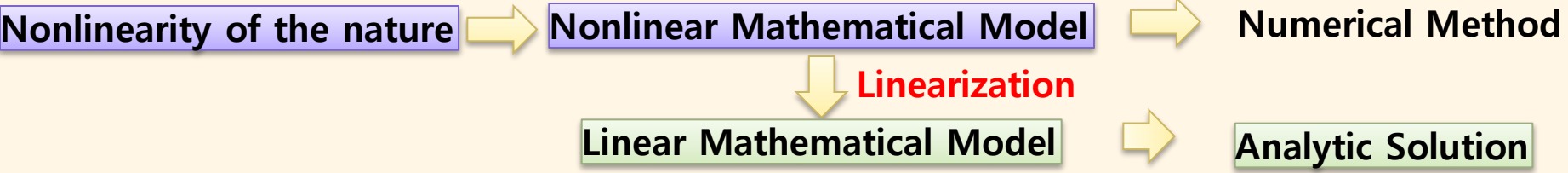
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$$\therefore f(z) = 1 + \frac{1}{2}z + \frac{1}{2}\left(-\frac{1}{4}\right)z^2 + \dots$$



# Nonlinearity



Ex) 탄성선의 미분 방정식

$$ds \approx dx, \theta \approx \tan(\theta) = \frac{dy}{dx}$$

$$ds^2 = dx^2 + dy^2 \rightarrow ds = dx \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

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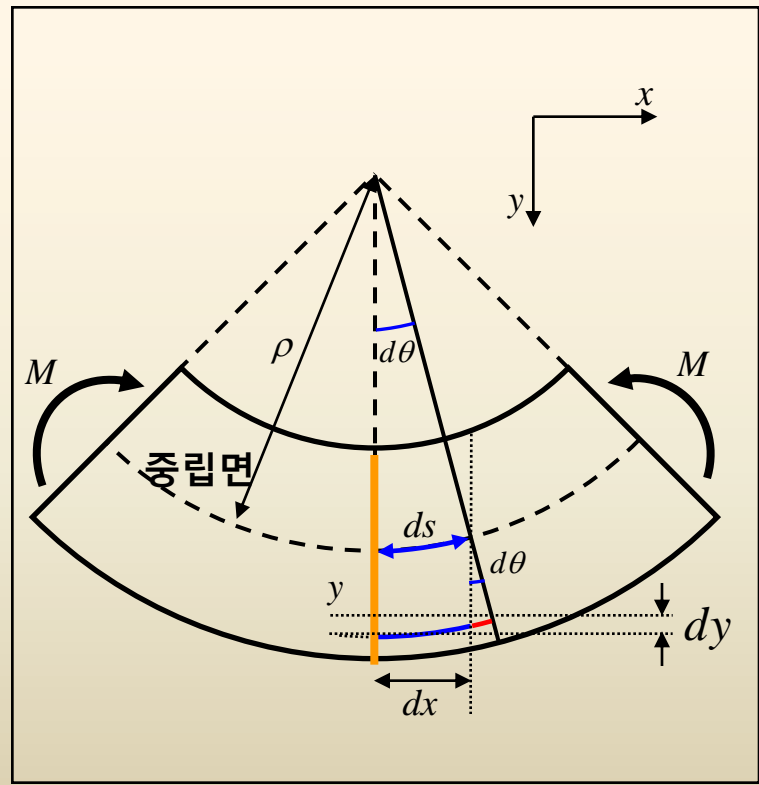
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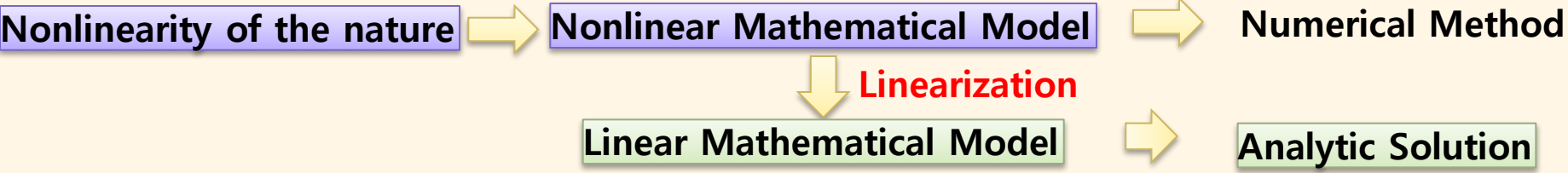
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# Nonlinearity



Ex) 탄성선의 미분 방정식

$$ds \approx dx, \theta \approx \tan(\theta) = \frac{dy}{dx}$$

$\frac{ds}{dx}$   $dy$

$$ds^2 = dx^2 + dy^2 \rightarrow ds = dx \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

let,  $z = \left(\frac{dy}{dx}\right)^2$  then,  $\sqrt{1 + \left(\frac{dy}{dx}\right)^2} = \sqrt{1 + z}$

$$f(z) = \sqrt{1+z}$$

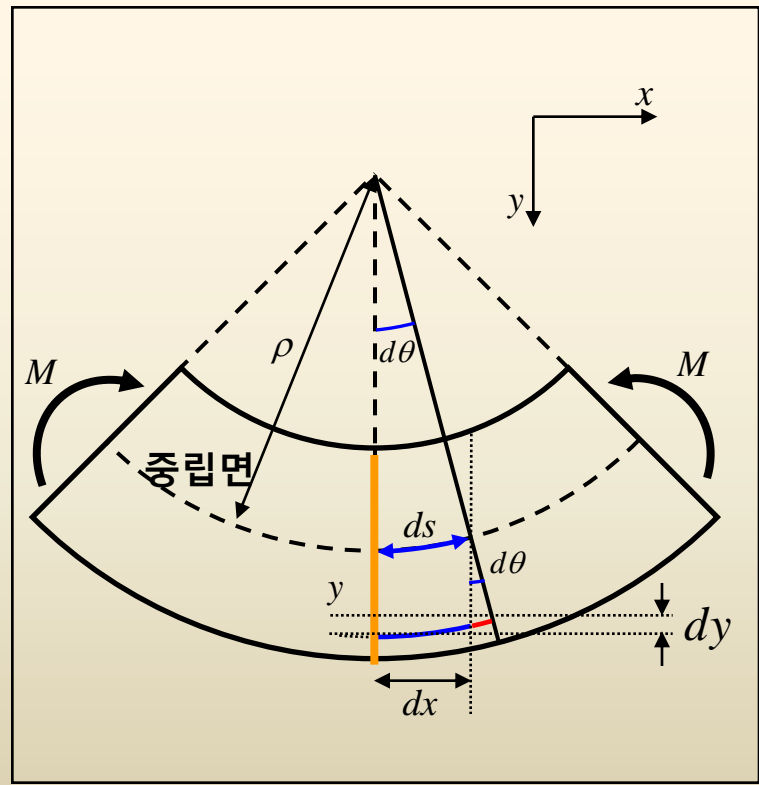
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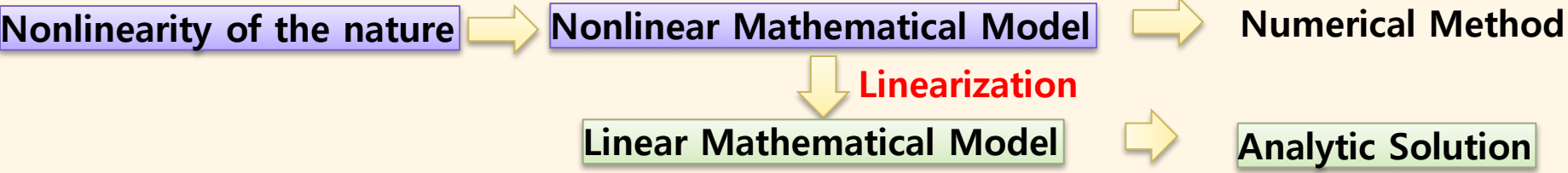
$$f''(0) = -\frac{1}{4}(1+z)^{-\frac{3}{2}} \Big|_{z=0} = -\frac{1}{4}$$

$$\therefore f(z) = 1 + \frac{1}{2}z + \frac{1}{2}\left(-\frac{1}{4}\right)z^2 + \dots$$

if,  $\theta \ll 1$



# Nonlinearity



Ex) 탄성선의 미분 방정식

$$ds \approx dx, \theta \approx \tan(\theta) = \frac{dy}{dx}$$

$$ds^2 = dx^2 + dy^2 \rightarrow ds = dx \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

let,  $z = \left(\frac{dy}{dx}\right)^2$  then,  $\sqrt{1 + \left(\frac{dy}{dx}\right)^2} = \sqrt{1 + z}$

$$f(z) = \sqrt{1+z}$$

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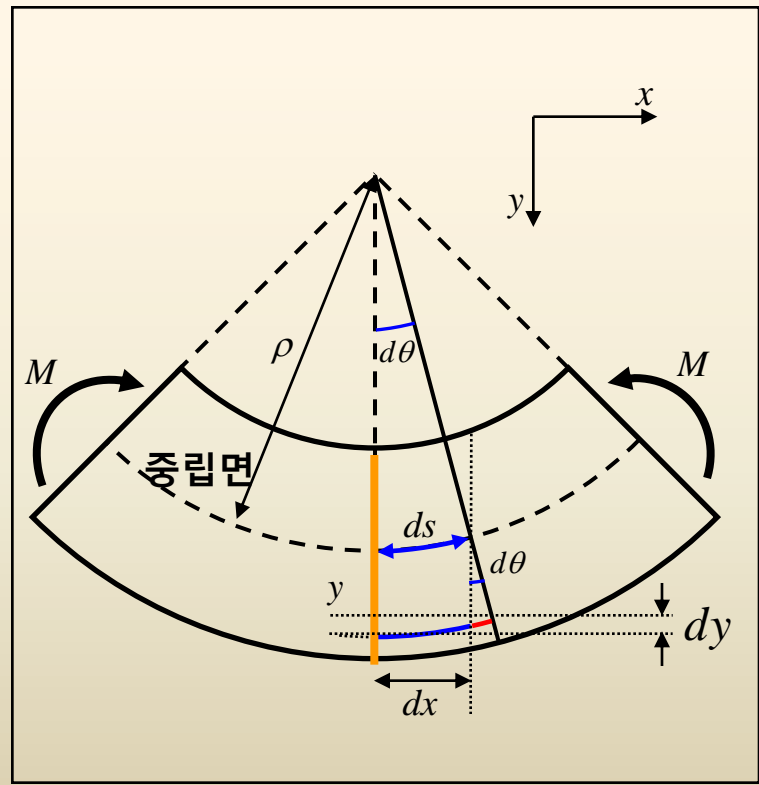
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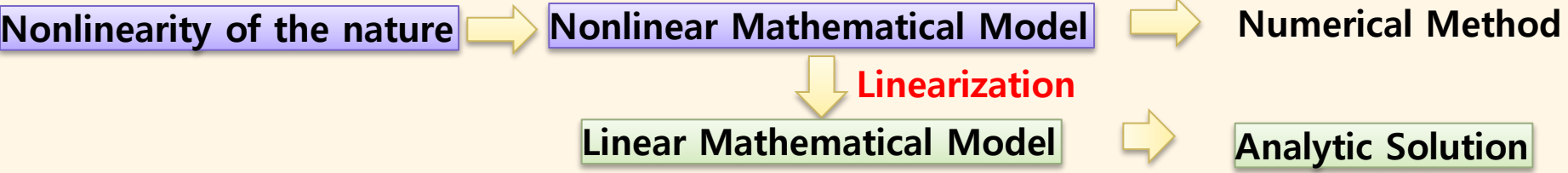
if,  $\theta \ll 1$

$$\therefore f(z) = \sqrt{1+z} \approx 1$$





# Nonlinearity



Ex) 탄성선의 미분 방정식

$$ds \approx dx, \theta \approx \tan(\theta) = \frac{dy}{dx}$$

$$ds^2 = dx^2 + dy^2 \rightarrow ds = dx \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

let,  $z = \left(\frac{dy}{dx}\right)^2$  then,  $\sqrt{1 + \left(\frac{dy}{dx}\right)^2} = \sqrt{1 + z}$

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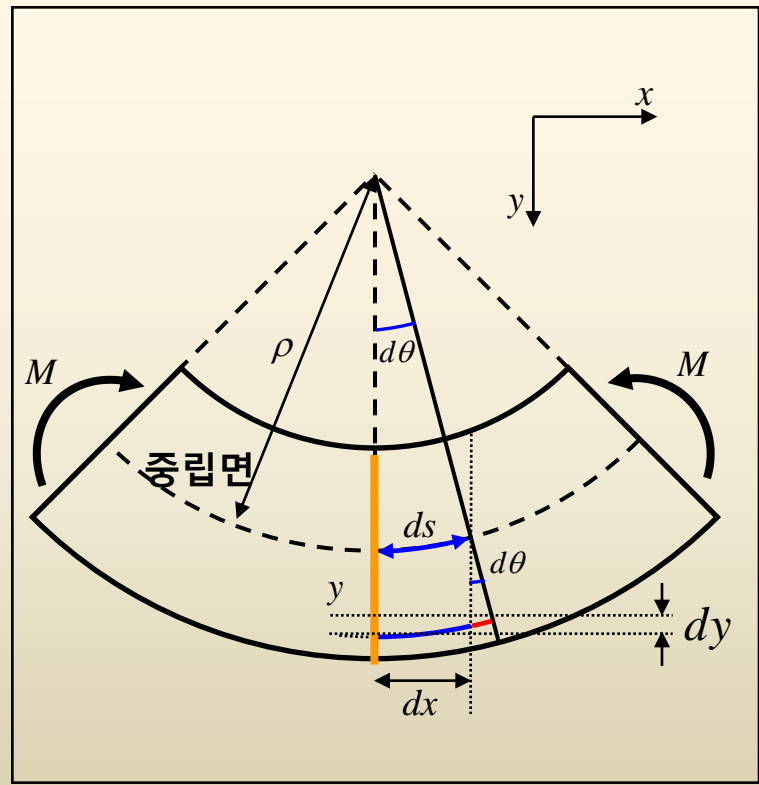
$$f''(0) = -\frac{1}{4}(1+z)^{-\frac{3}{2}} \Big|_{z=0} = -\frac{1}{4}$$

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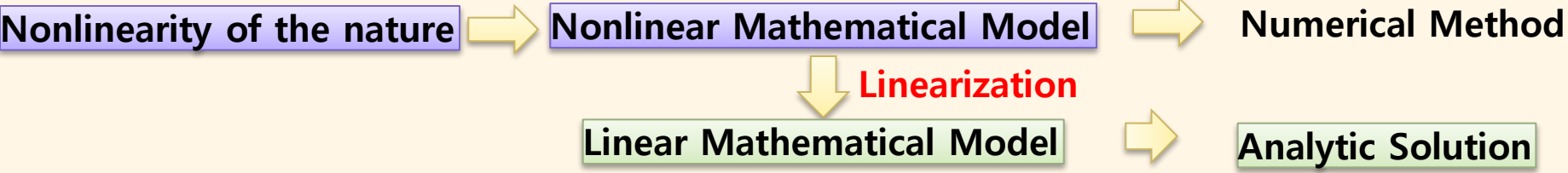
if,  $\theta \ll 1$

$$\therefore f(z) = \sqrt{1+z} \approx 1$$

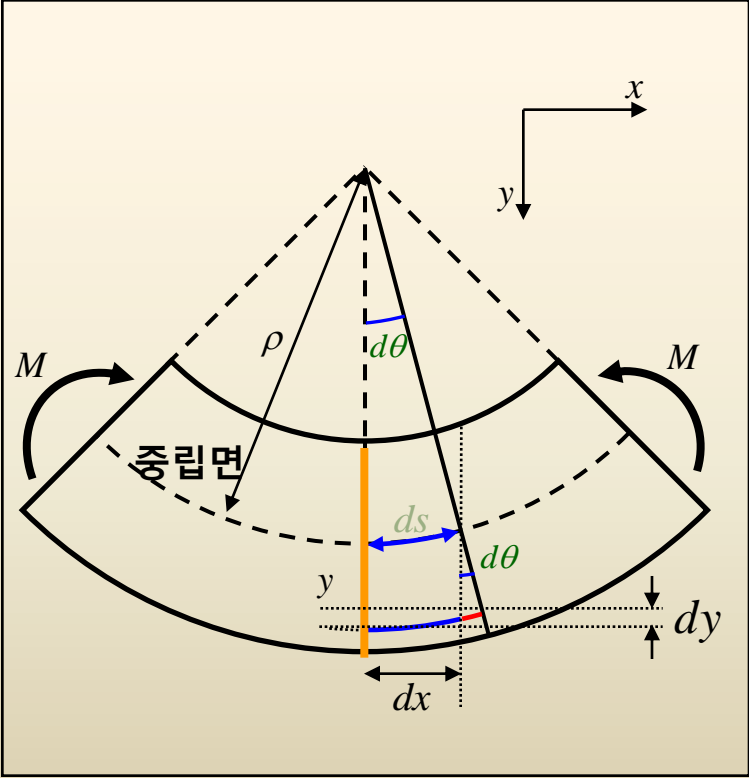
$$\therefore ds \approx dx$$



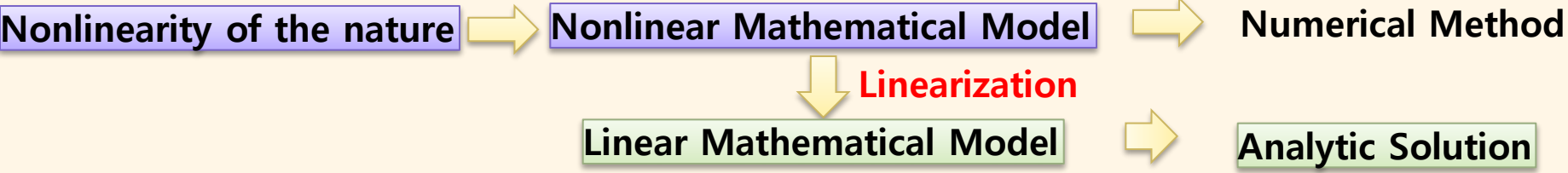
# Nonlinearity



Ex) 탄성선의 미분 방정식

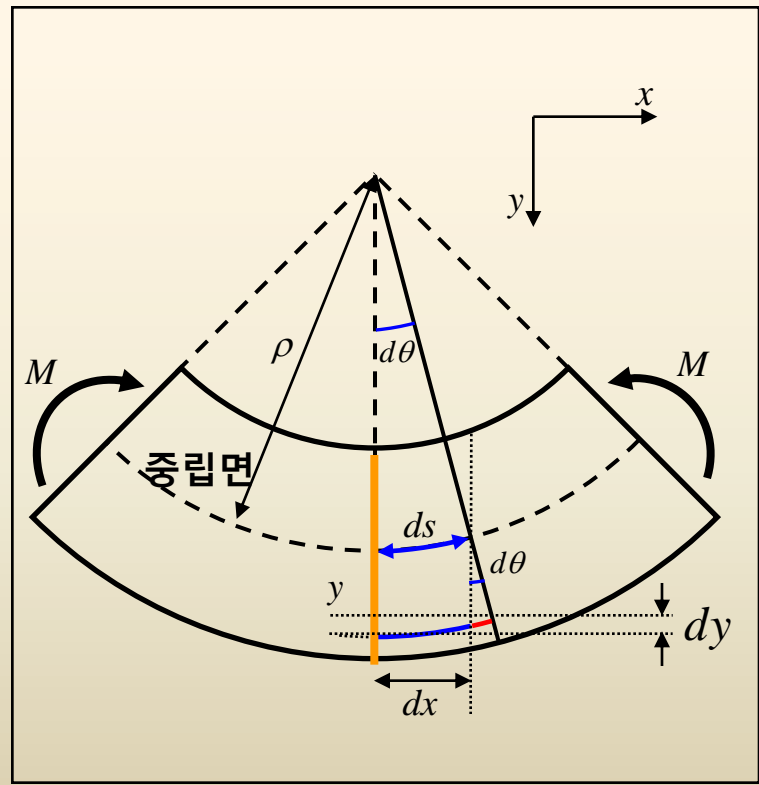


# Nonlinearity

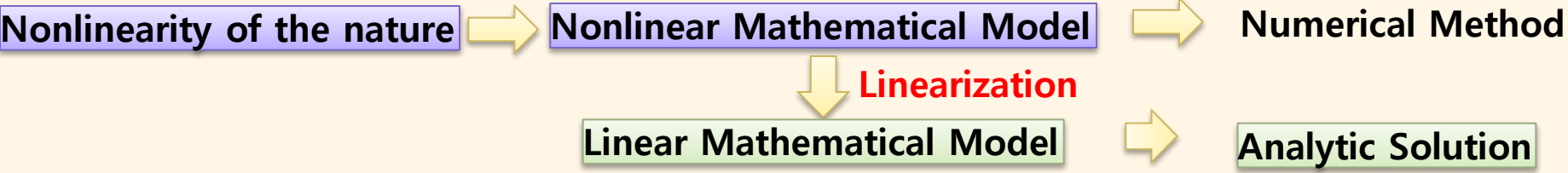


Ex) 탄성선의 미분 방정식

$$ds \approx dx, \quad \theta \approx \tan(\theta) = \frac{dy}{dx}$$

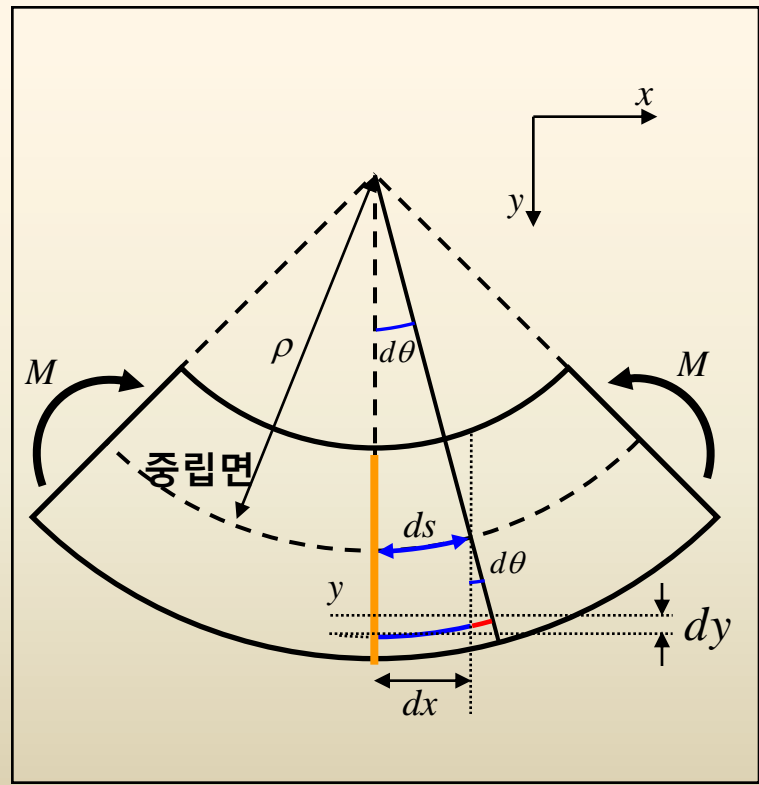
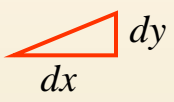


# Nonlinearity

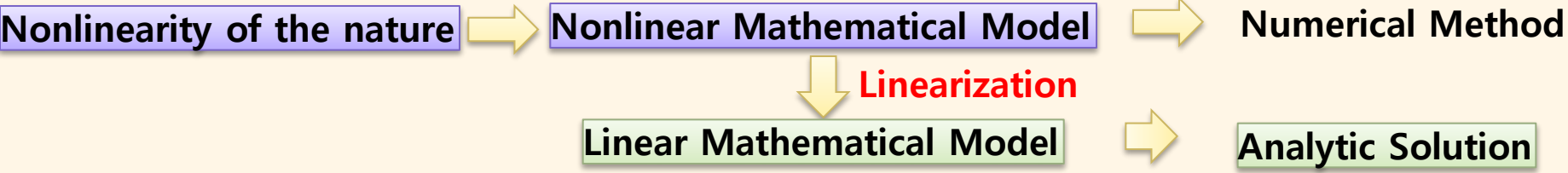


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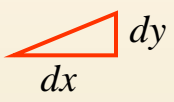


# Nonlinearity

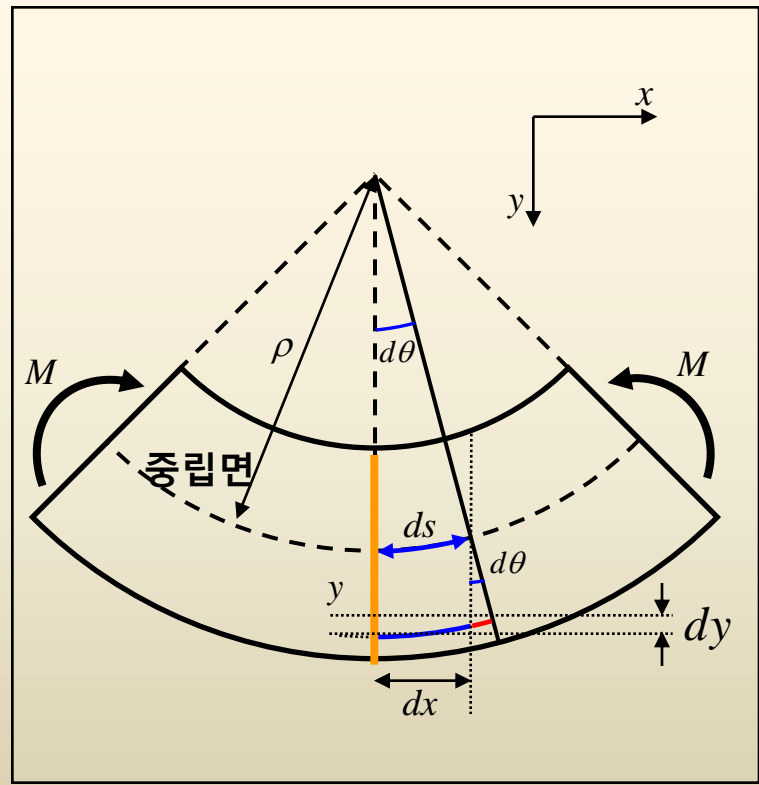


Ex) 탄성선의 미분 방정식

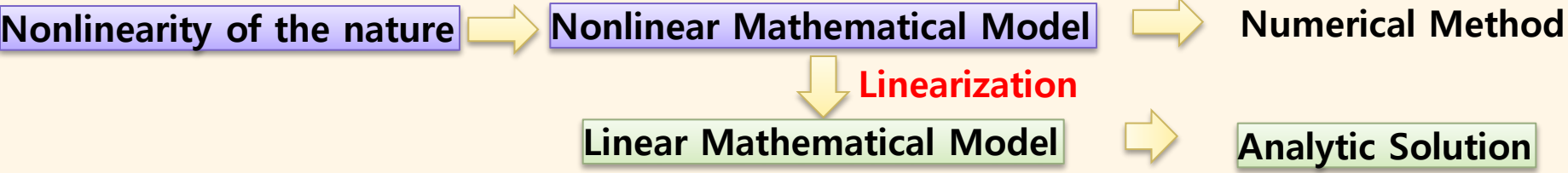
$$ds \approx dx, \quad \theta \approx \tan(\theta) = \frac{dy}{dx}$$



$$\tan \theta = \theta + \frac{\theta^3}{3} + \frac{2\theta^5}{15} + \dots$$



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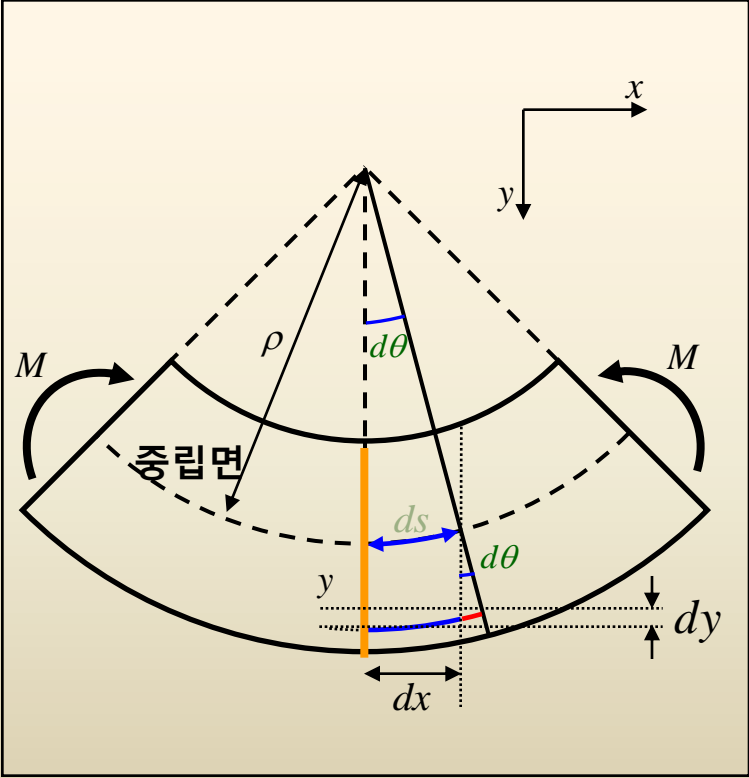


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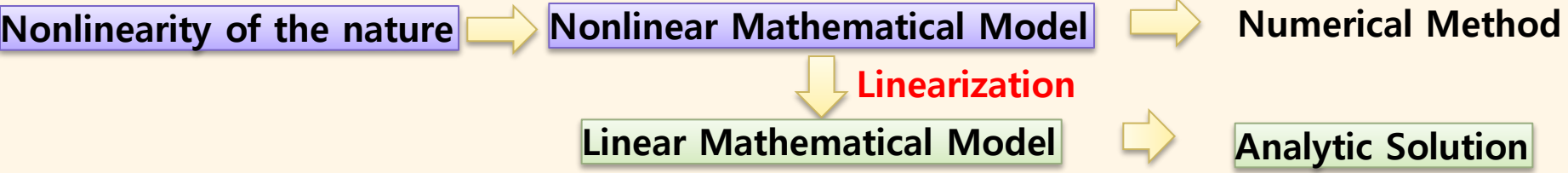
$$\rho \cdot d\theta = ds \quad \Rightarrow \quad \frac{d\theta}{ds} = \frac{1}{\rho}$$

$$dF = \sigma dA = E \cdot \frac{y}{\rho} dA \quad \Rightarrow \quad \therefore \frac{d\theta}{ds} = -\frac{M}{EI}$$

$$dM = -y\sigma dA \quad \Rightarrow \quad \frac{M}{EI} = -\frac{1}{\rho}$$



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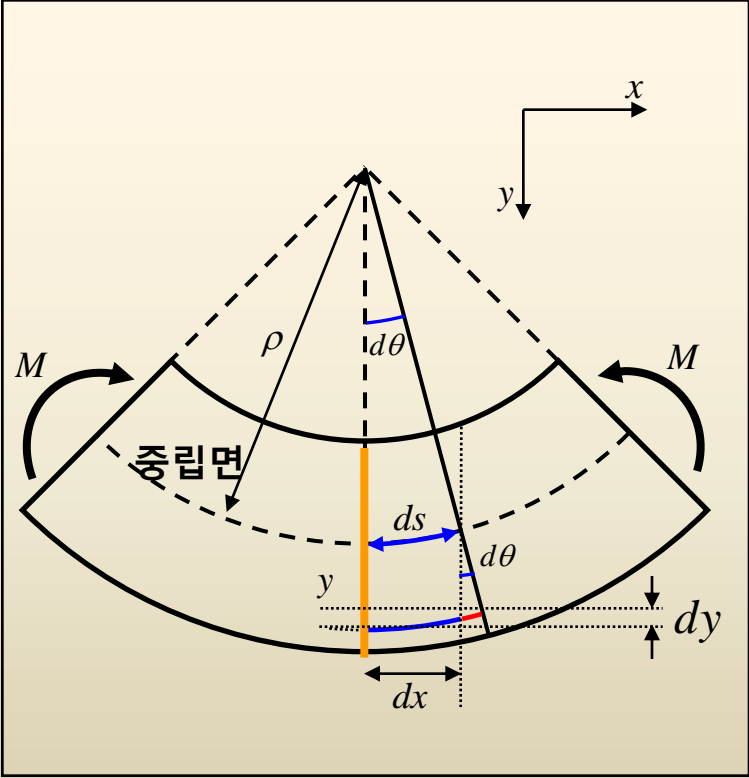
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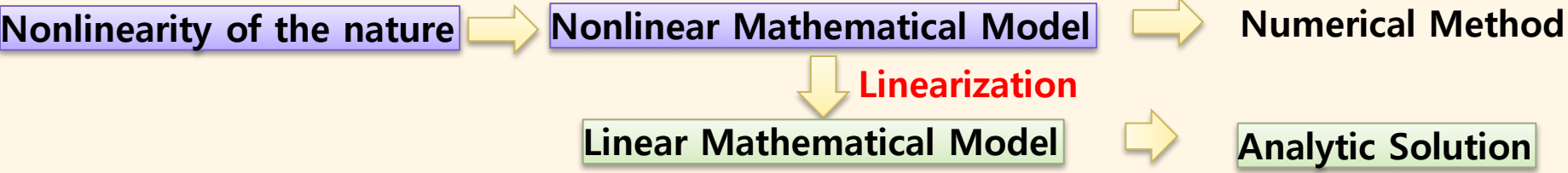
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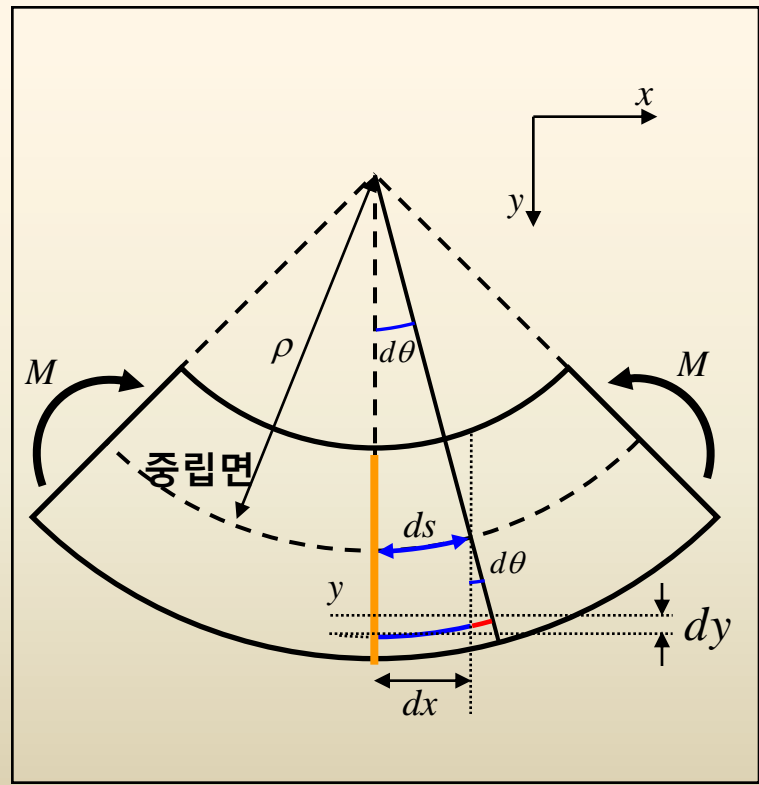
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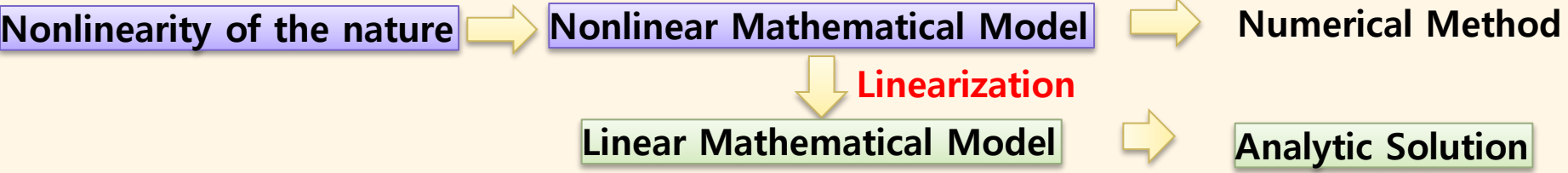
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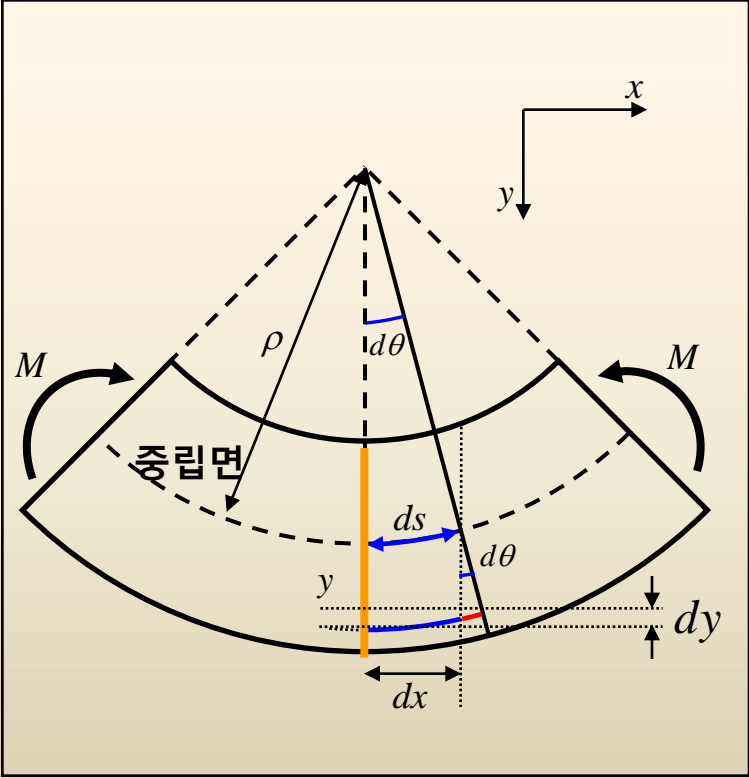
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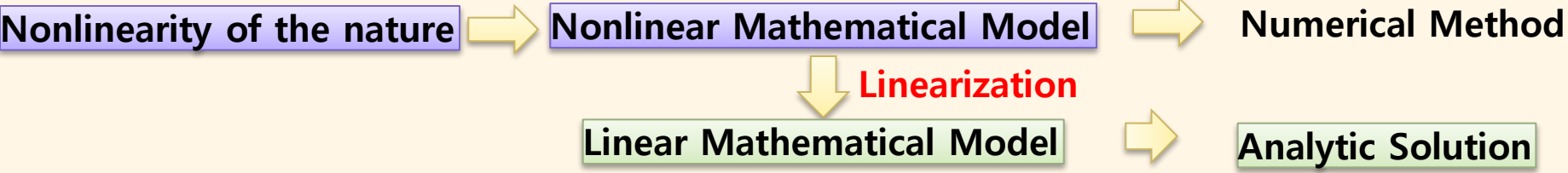
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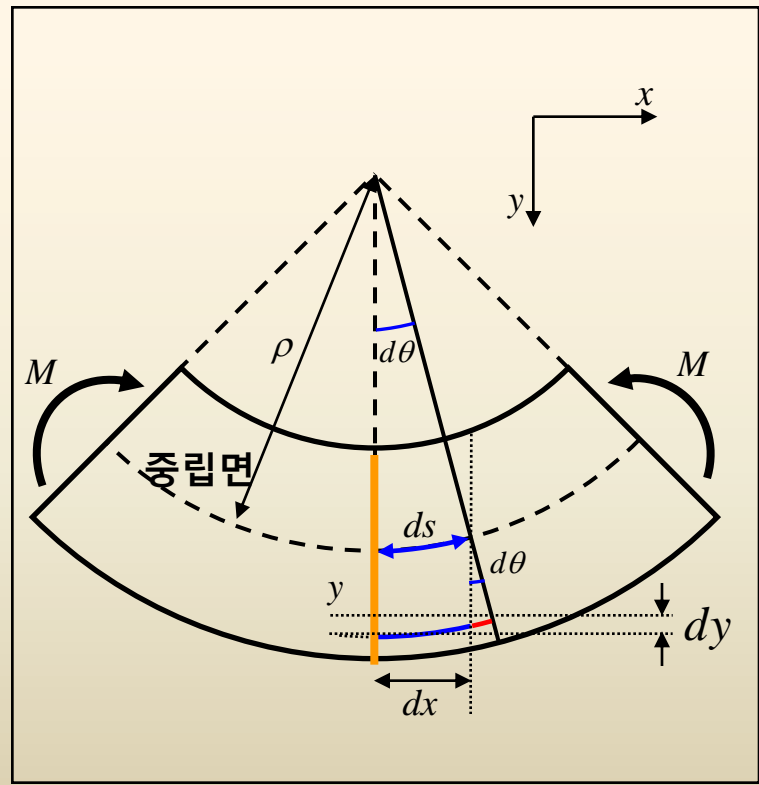
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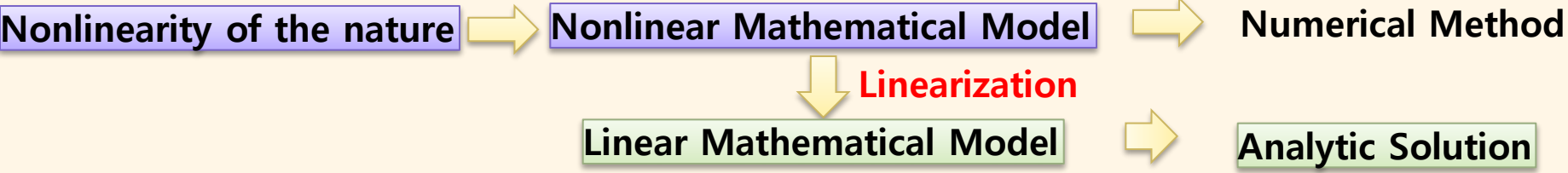
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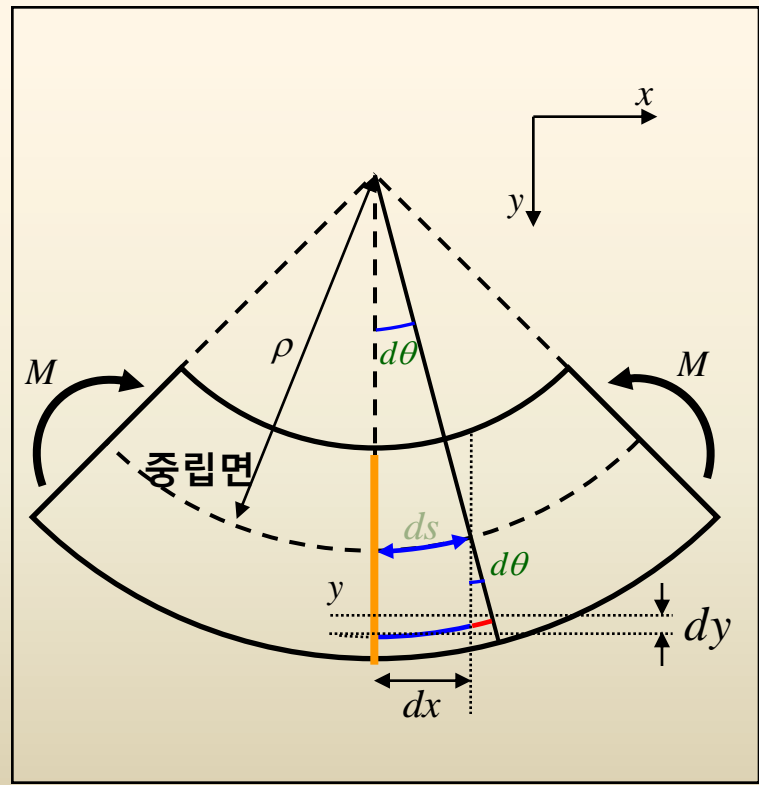
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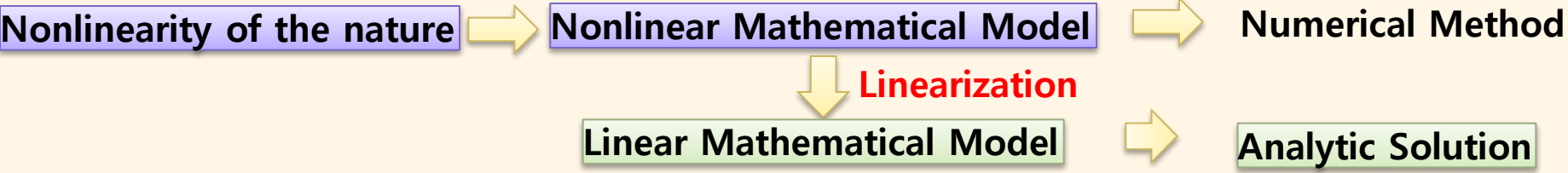
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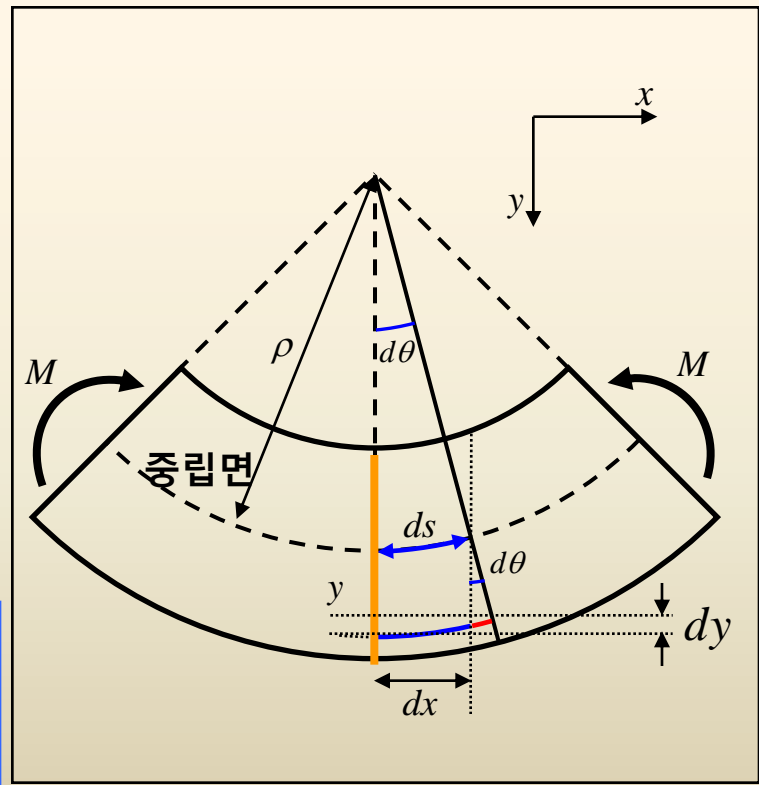
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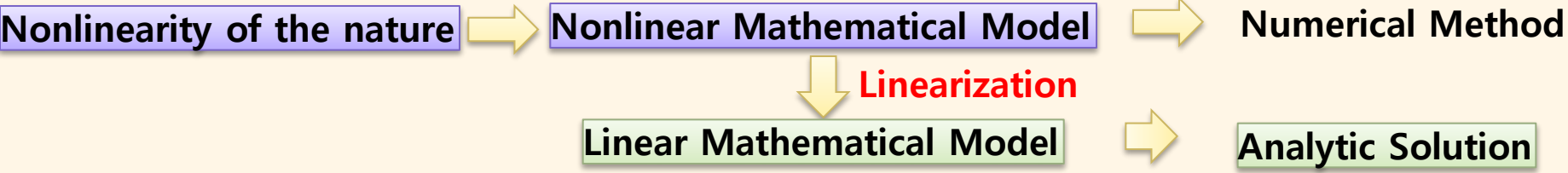
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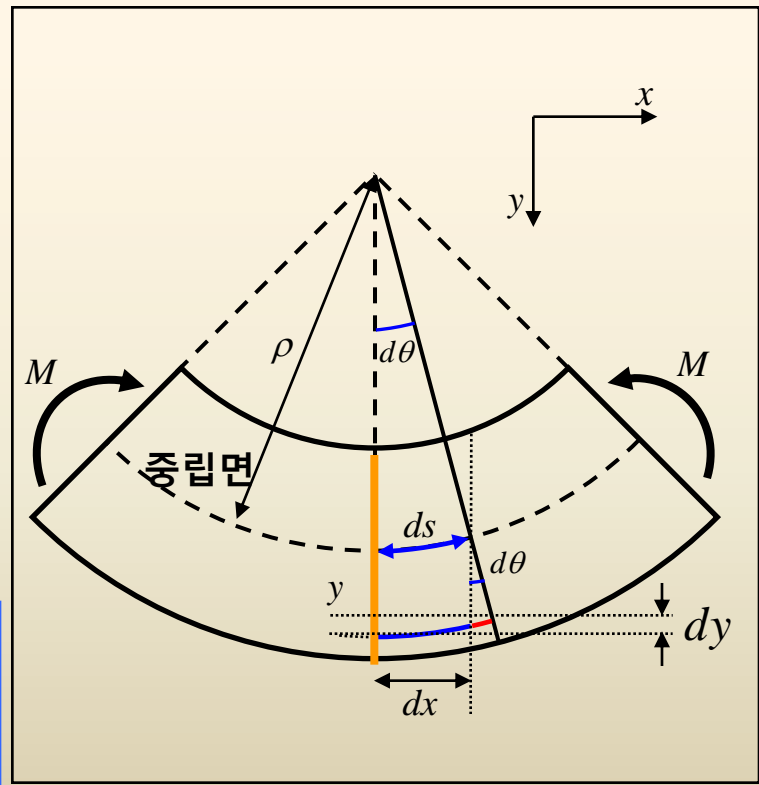
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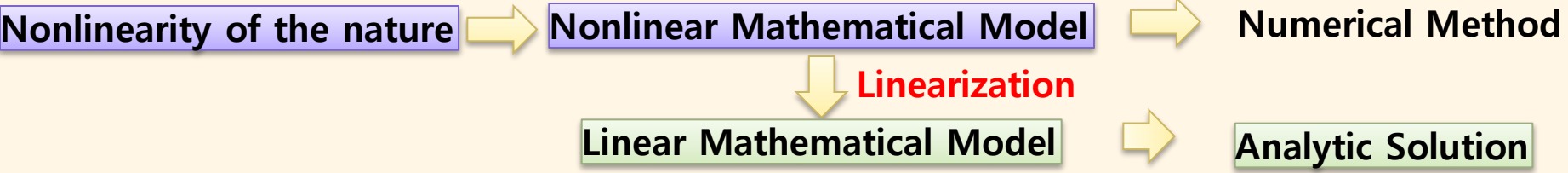
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# Nonlinearity



Ex) 분포하중을 고려한 탄성선의 미분 방정식

$$\frac{d^2 y}{dx^2} = -\frac{M}{EI}$$

y 방향의 합력 :

$$(V + dV) - V + f(x)dx = 0$$

$$\Rightarrow dV + f(x)dx = 0$$

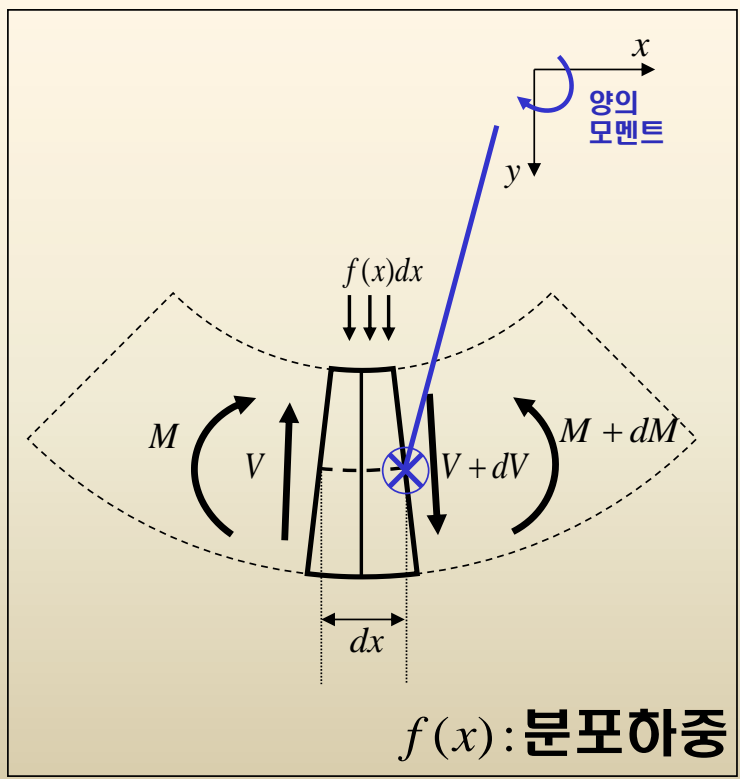
$$\Rightarrow \frac{dV}{dx} = -f(x)$$

모멘트 (파란색 축 기준):

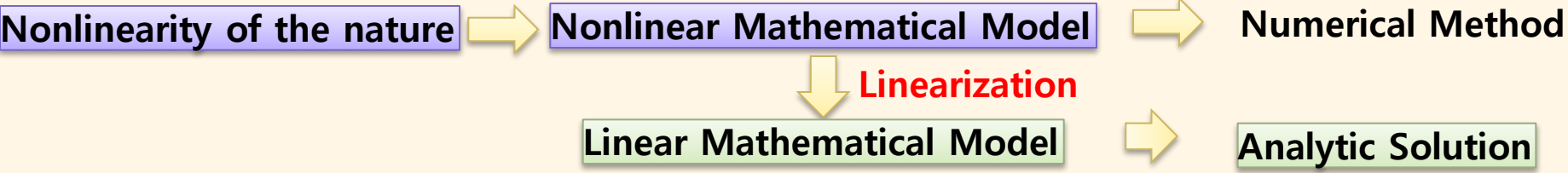
$$-(M + dM) + M + Vdx - f(x)dx \cdot \frac{1}{2}dx = 0$$

$$\Rightarrow dM - Vdx = 0 \quad (\because (dx)^2 \approx 0)$$

$$\Rightarrow \frac{dM}{dx} = V(x)$$



# Nonlinearity



Ex) 분포하중 을 고려한 탄성선의 미분 방정식

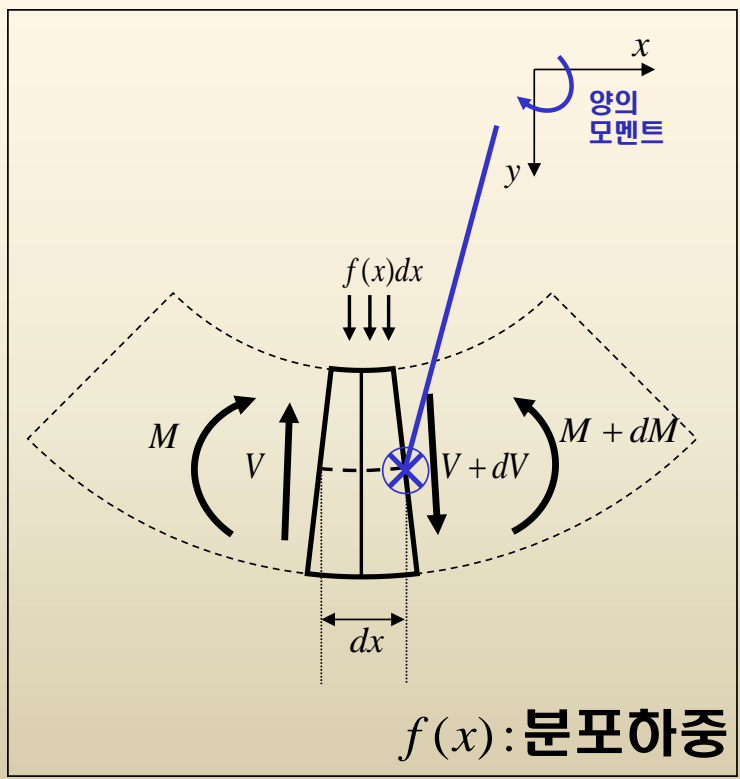
$$\frac{dV}{dx} = -f(x) \quad \frac{dM}{dx} = V(x)$$

$$\frac{d^2 y}{dx^2} = -\frac{M}{EI} \quad : \text{탄성선의 미분방정식}$$

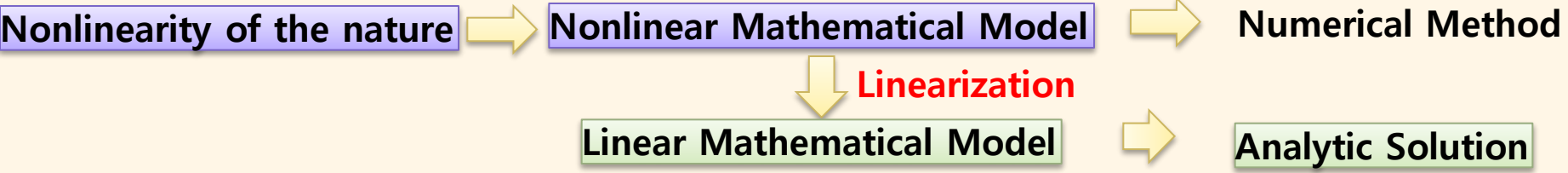
$$\frac{d^3 y}{dx^3} = -\frac{1}{EI} \cdot \frac{dM}{dx} = -\frac{1}{EI} \cdot V(x)$$

$$\frac{d^4 y}{dx^4} = -\frac{1}{EI} \cdot \frac{dV}{dx} = \frac{1}{EI} \cdot f(x)$$

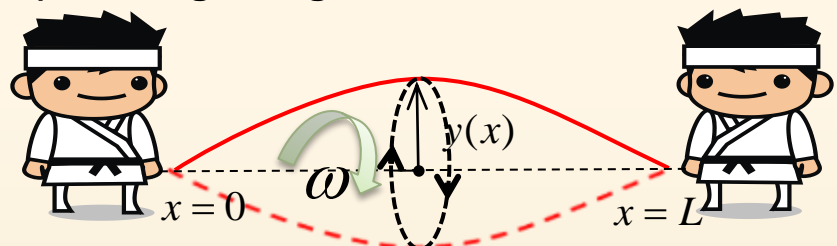
$$\therefore EI \frac{d^4 y}{dx^4} = f(x)$$



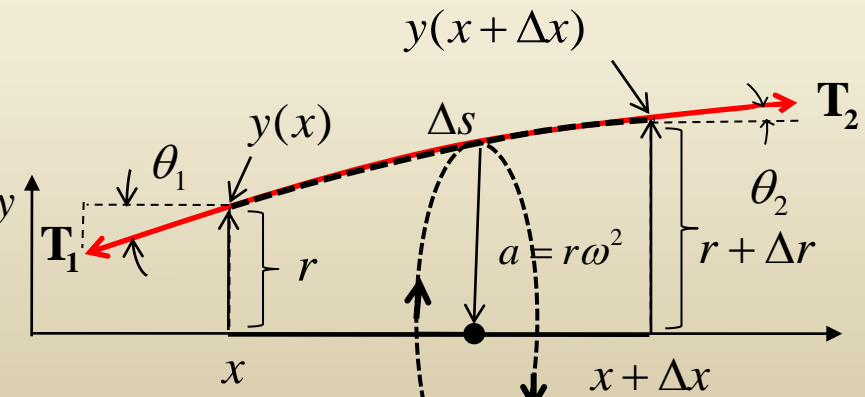
# Nonlinearity



## Ex) Rotating String



$\rho$  : string density  
 $\omega$  : string angular velocity  
 $T$  : magnitude of tension



$$\sum F_x = T_1 \cos \theta_1 - T_2 \cos \theta_2 = 0$$

$$T_1 \cos \theta_1 = T_2 \cos \theta_2 = T$$

$$\sum F_y = T_2 \sin \theta_2 - T_1 \sin \theta_1$$

$$= T \frac{\sin \theta_2}{\cos \theta_2} - T \frac{\sin \theta_1}{\cos \theta_1} \because T_1 \cos \theta_1 = T_2 \cos \theta_2 = T$$

$$= T \tan \theta_2 - T \tan \theta_1$$

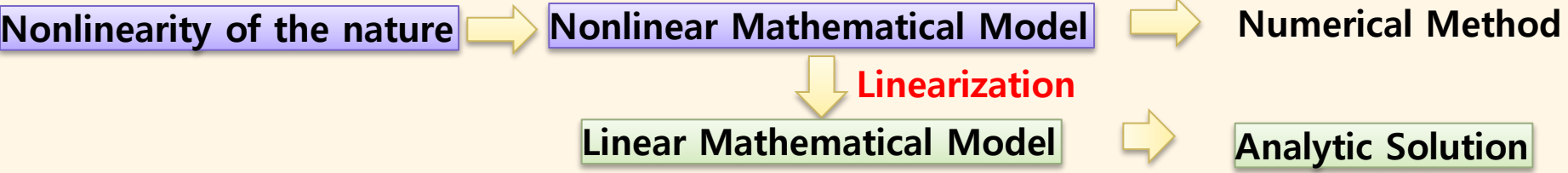
$$= T [y'(x + \Delta x) - y'(x)]$$

$$\because \tan \theta_1 = \left. \frac{dy}{dx} \right|_x, \tan \theta_2 = \left. \frac{dy}{dx} \right|_{x+\Delta x}$$

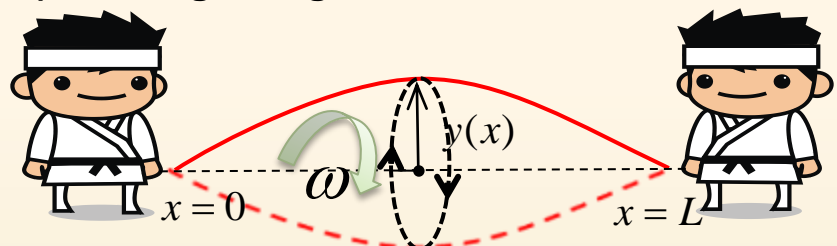




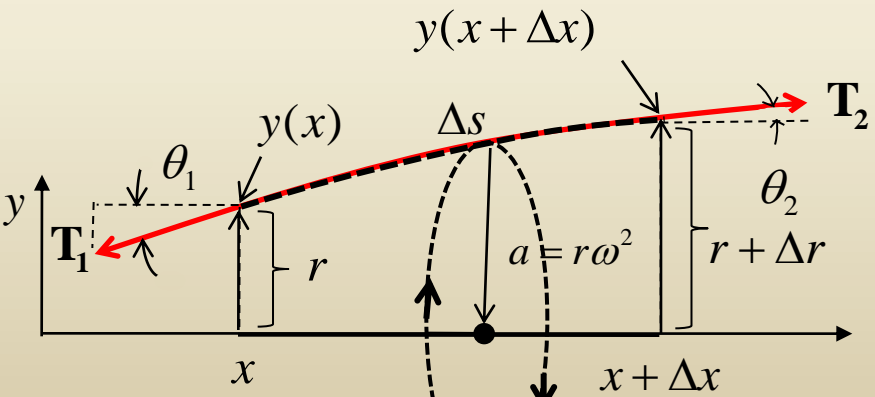
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$$\sum F_y = T[y'(x + \Delta x) - y'(x)]$$

assum.:  $\Delta x \ll 1$  linearization

Mass:  $m = \rho \Delta s \approx \rho \Delta x$

Centripetal acceleration:  $a = -r\omega^2$

When  $\Delta x$  is small,

$$r + \Delta r = r + r' \Delta x + \dots = y + y' \Delta x + \dots$$

linearization

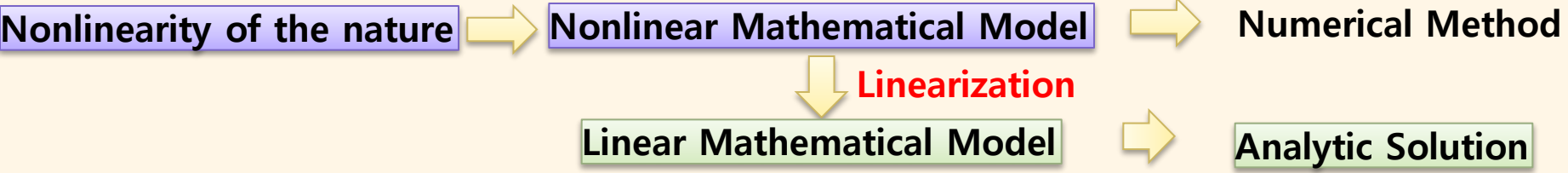
$$r + \Delta r \approx r = y, a = -r\omega^2 = -y\omega^2$$

$$\therefore \sum F_y = ma \approx -(\rho \Delta x) y \omega^2$$

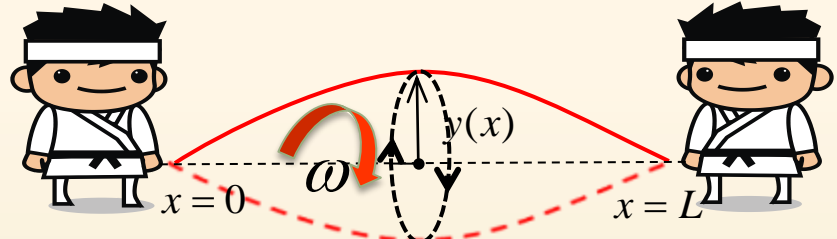
Acceleration point in the direction opposite to the positive y direction



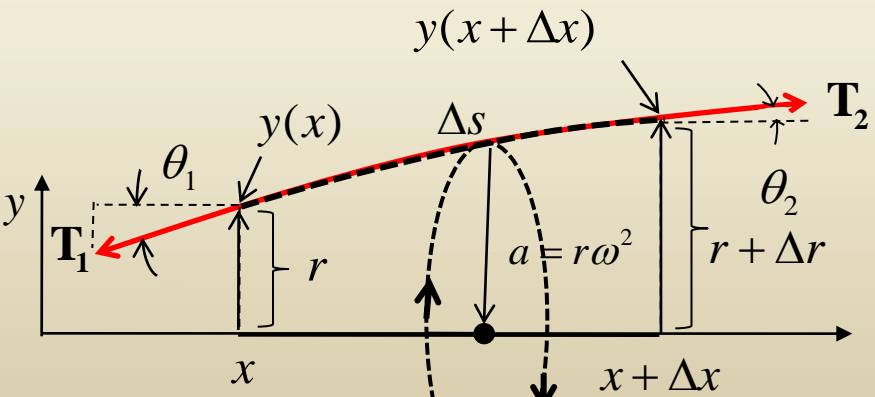
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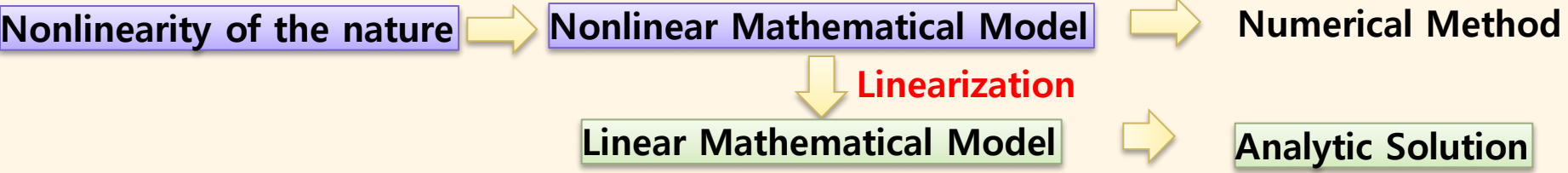
$$T \frac{y'(x + \Delta x) - y'(x)}{\Delta x} + \rho \omega^2 y = 0$$

$$\frac{y'(x + \Delta x) - y'(x)}{\Delta x} \approx \frac{d^2 y}{dx^2}$$

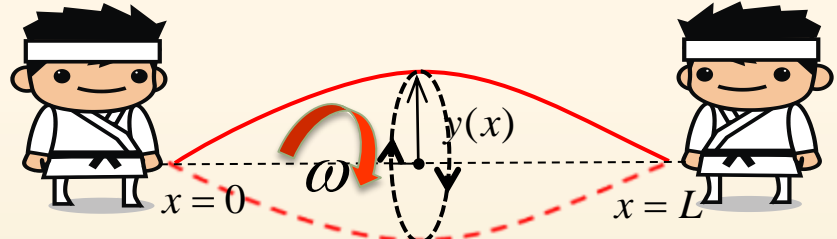
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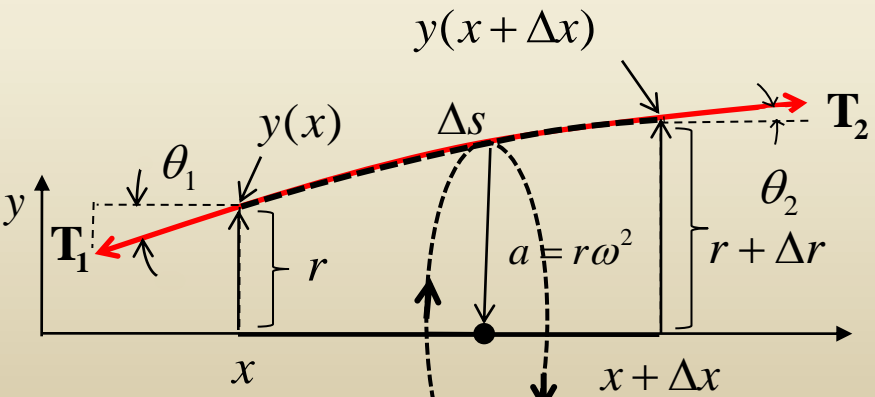
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$$\sum F_y = T[y'(x + \Delta x) - y'(x)] \quad , ma \approx -(\rho \Delta x) y \omega^2$$

$$\therefore T \frac{d^2 y}{dx^2} + \rho \omega^2 y = 0$$



What if ..

$$r + \Delta r = r + r' \Delta x + \dots = y + y' \Delta x + \dots$$

then,  $a = -(r + \Delta r) \omega^2 = -(y + y' \Delta x) \omega^2$

$$\therefore T[y'(x + \Delta x) - y'(x)] = -(\rho \Delta x)(y + y' \Delta x) \omega^2$$

$$\Rightarrow T \frac{d^2 y}{dx^2} + \rho \omega^2 \Delta x y' + \rho \omega^2 y = 0$$

Not a form of  $\frac{dy}{dx}$  or polynomial of  $x$

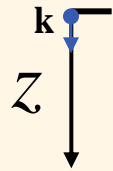
$\Delta x y' \approx 0 \because \Delta x \ll 1, \Delta s \approx \Delta x$  means  $y' (= dy/dx)$  is small too

$$\therefore T \frac{d^2 y}{dx^2} + \rho \omega^2 y = 0$$



# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2z}{dt^2}$

①

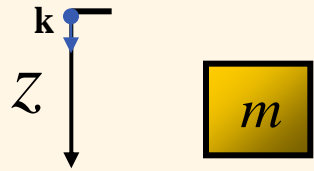


②



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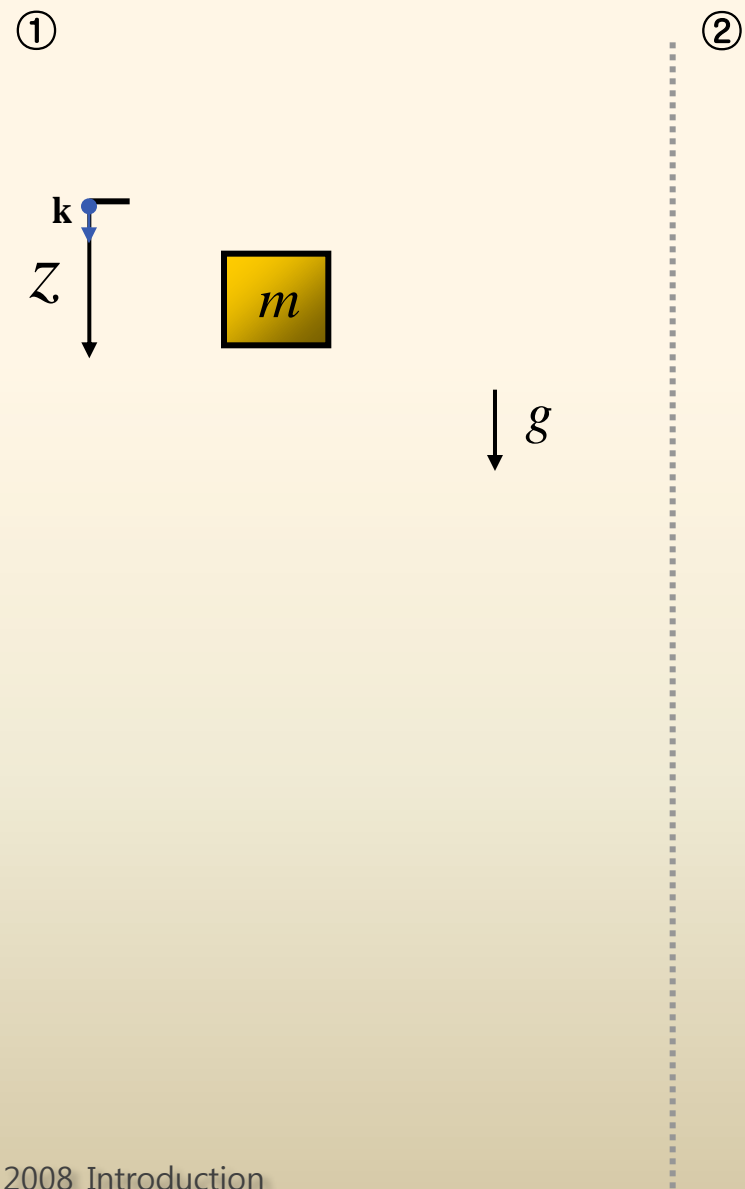
①



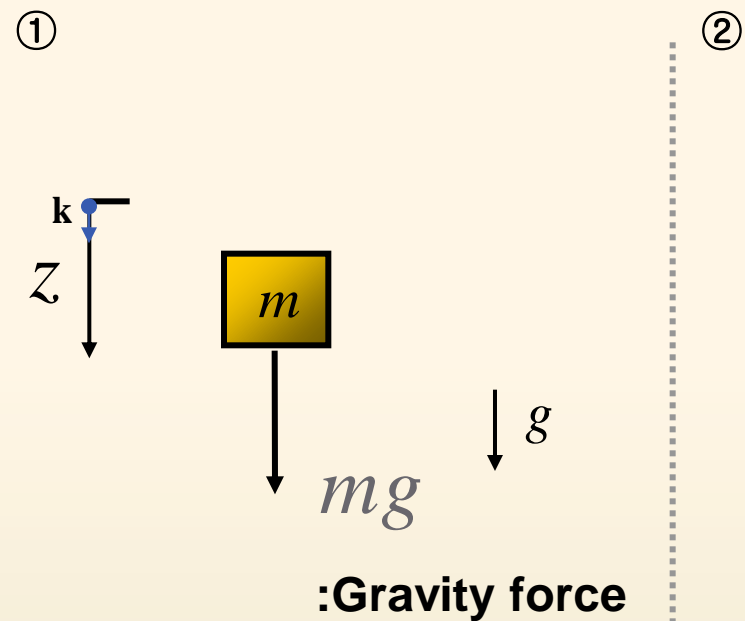
②



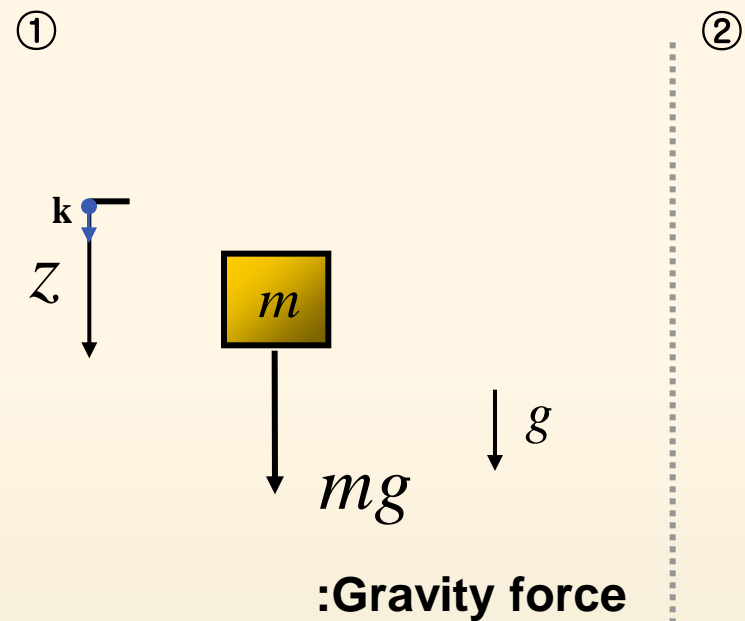
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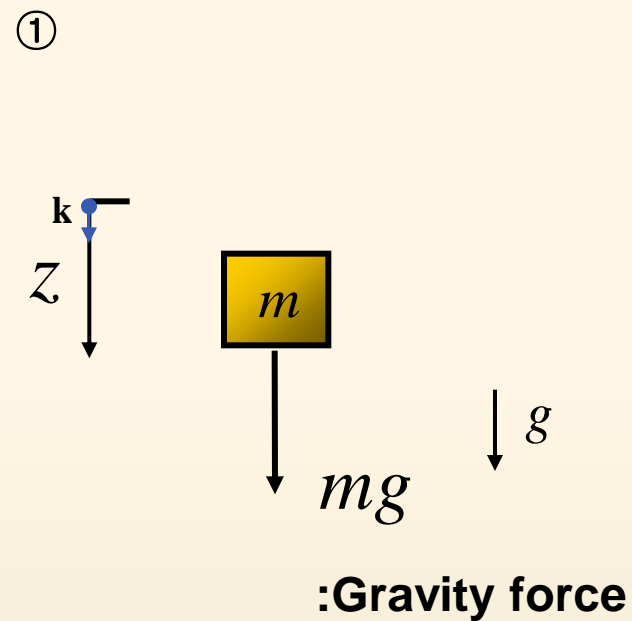
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$$mz'' = \mathbf{F}$$





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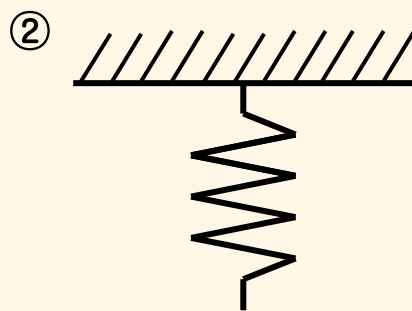
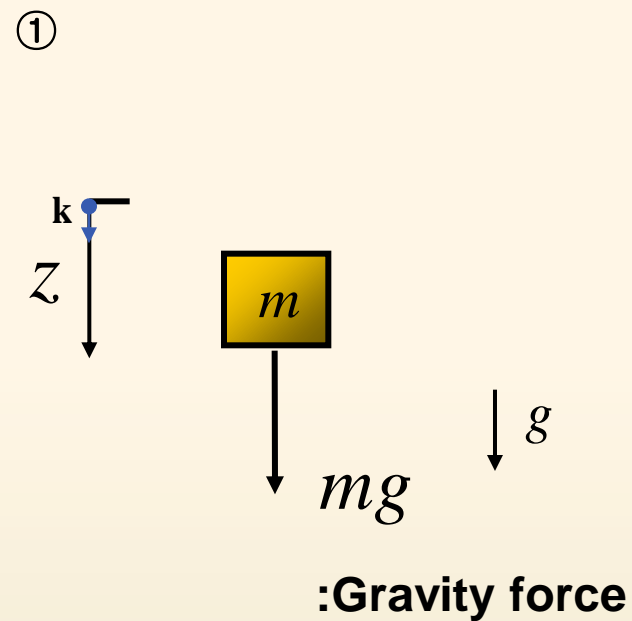


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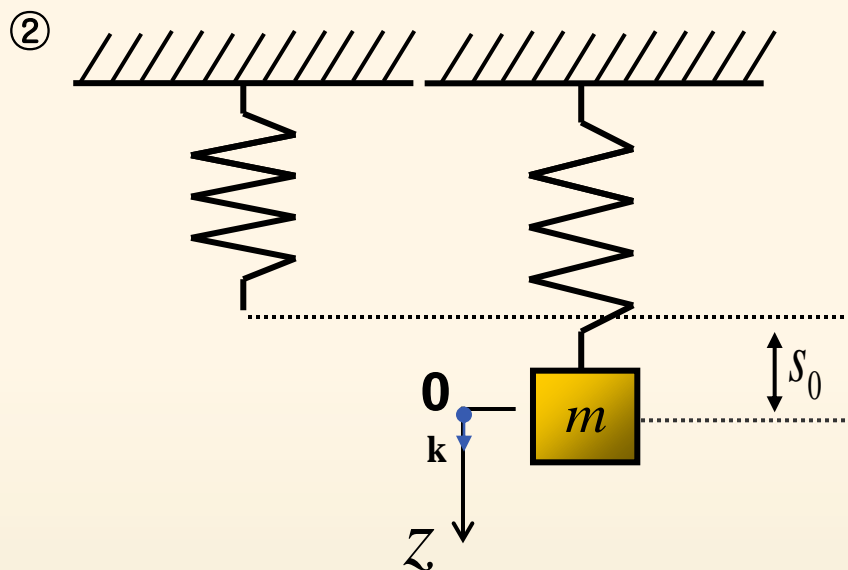
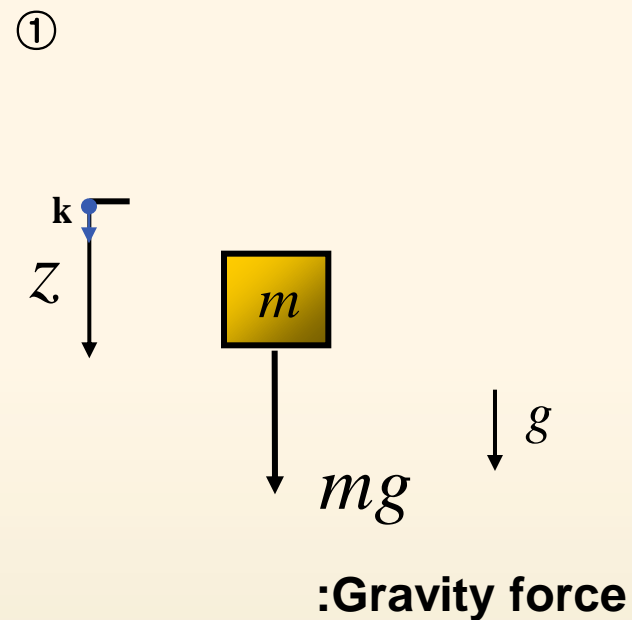


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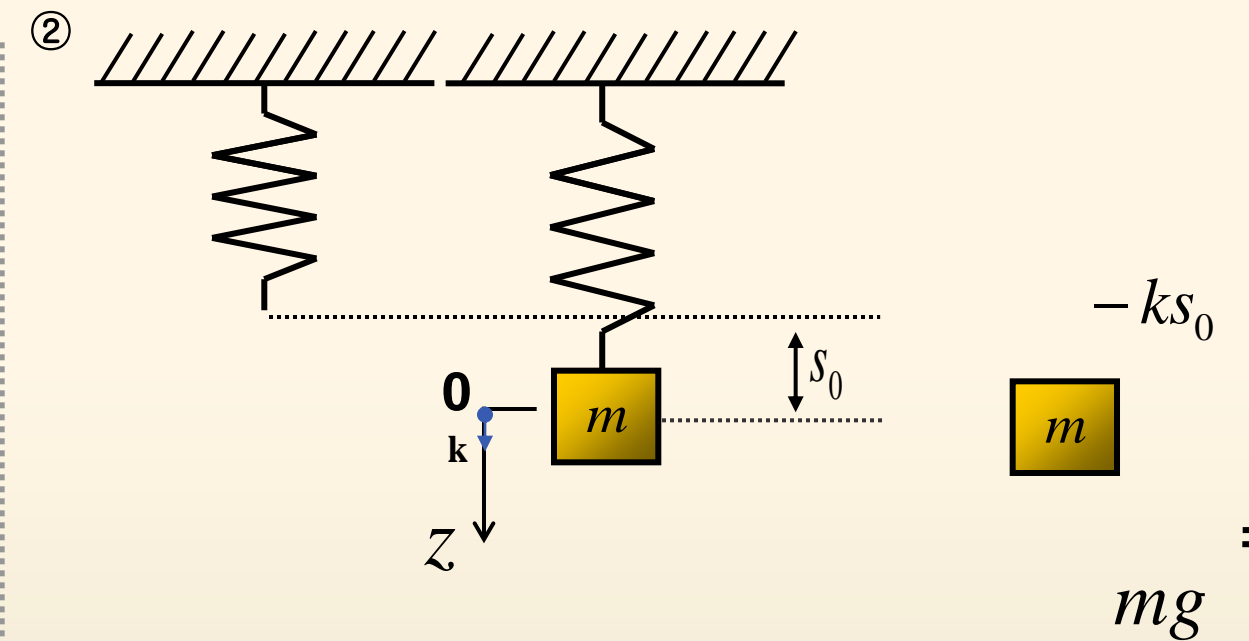
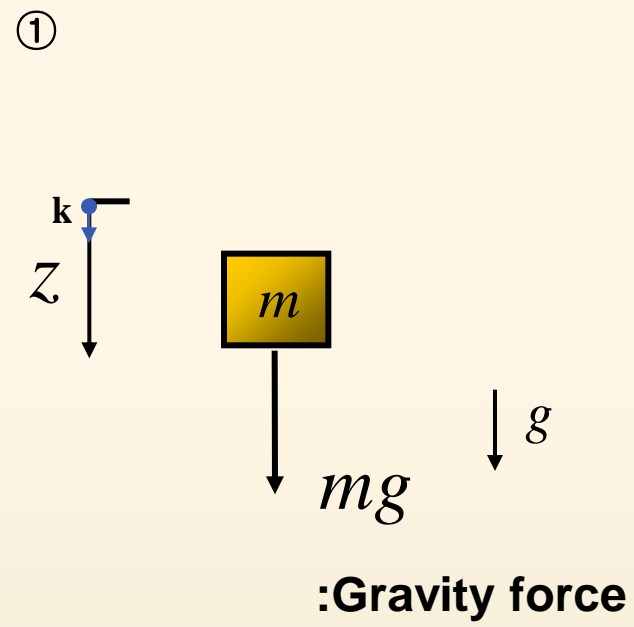
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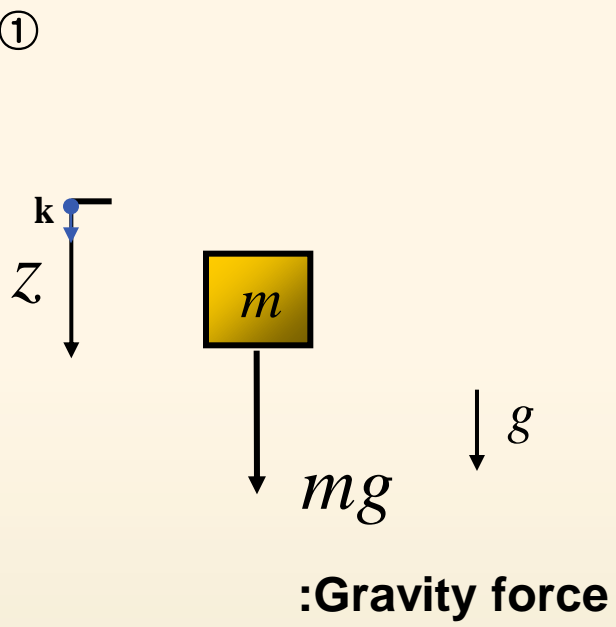


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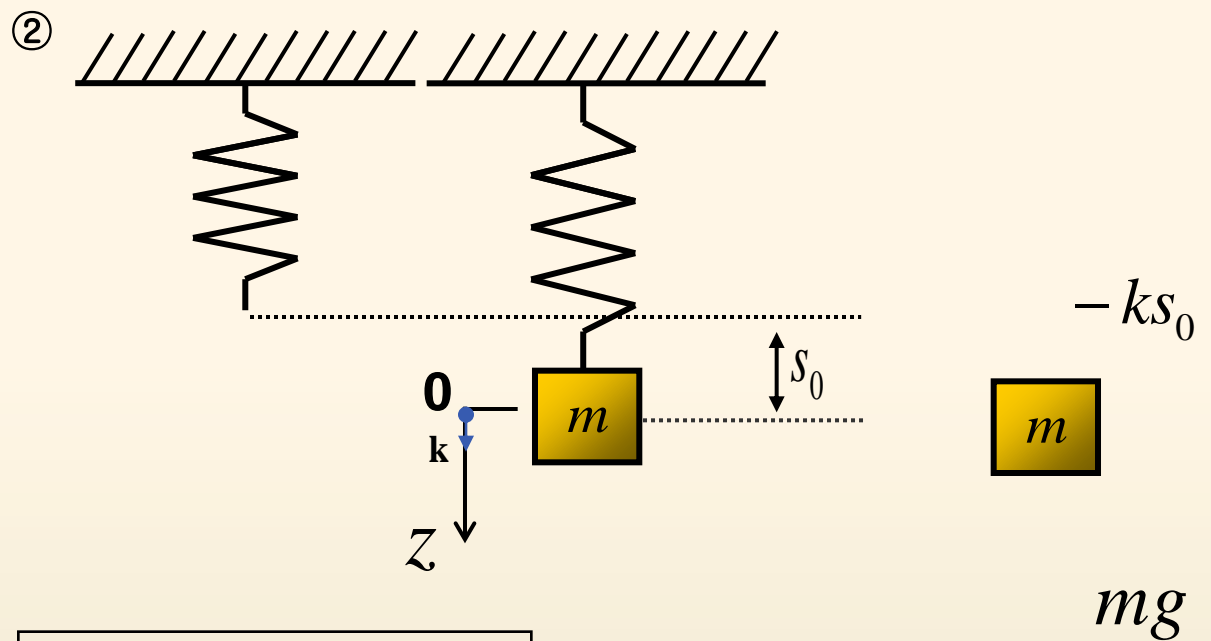
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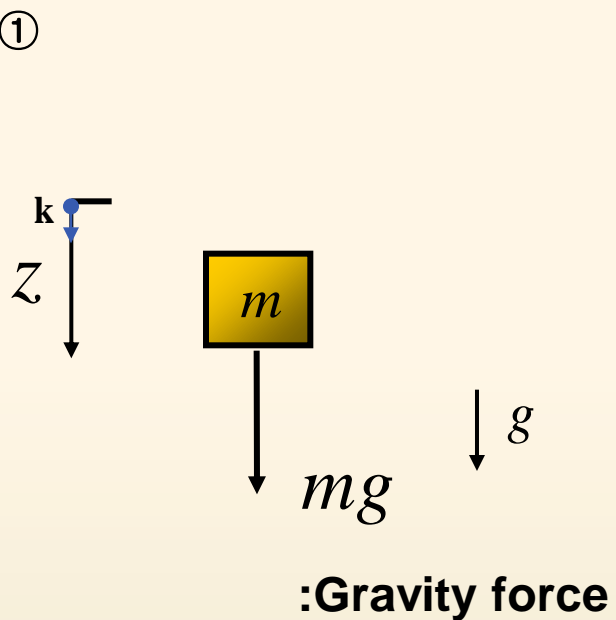


Nonlinearity of spring

$$\mathbf{F}(z) = -kz - k_1z^3$$



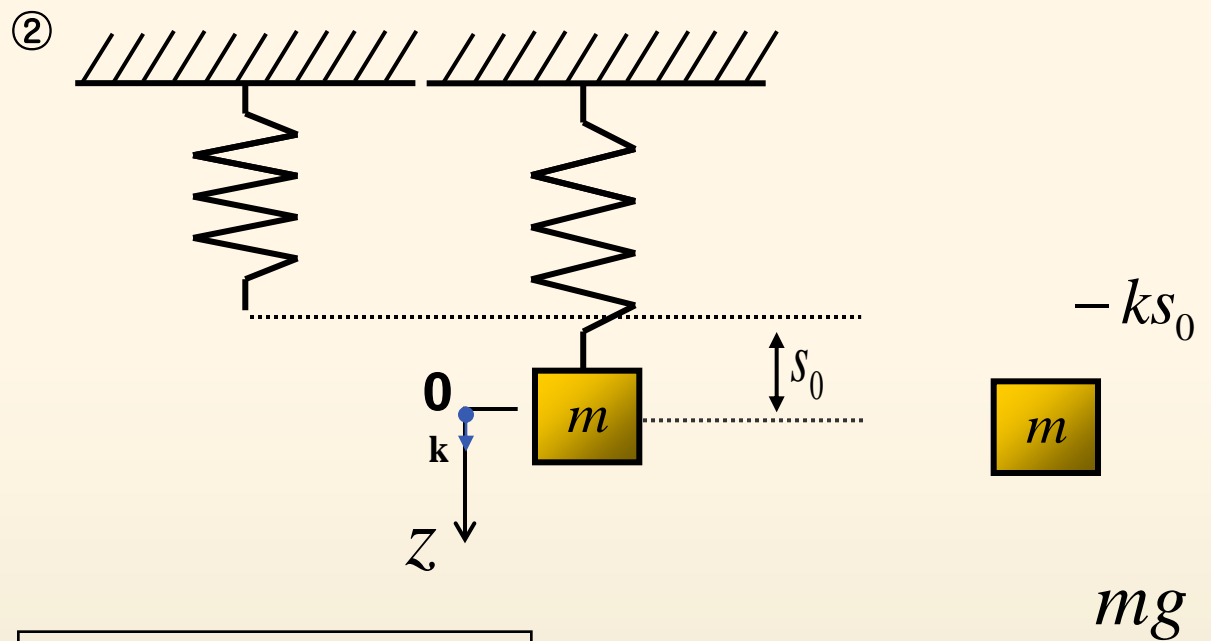
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By Newton's 2<sup>nd</sup> law,

$$m\mathbf{z}'' = \mathbf{F}$$

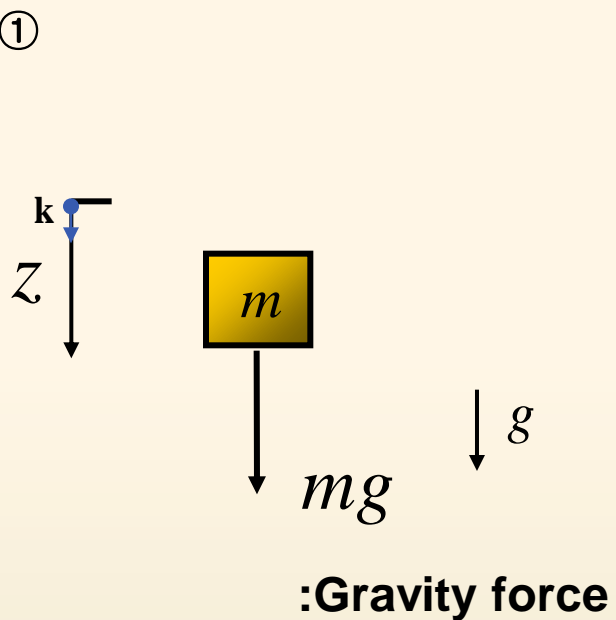
$$= mg\mathbf{k}$$



Nonlinearity of spring  
 $\mathbf{F}(z) = -kz - k_1z^3$   
 linearize  
 Hooke's law  
 $F \propto z$   
 $\mathbf{F}_{spring} = -kz$   
 $k$  : spring constant

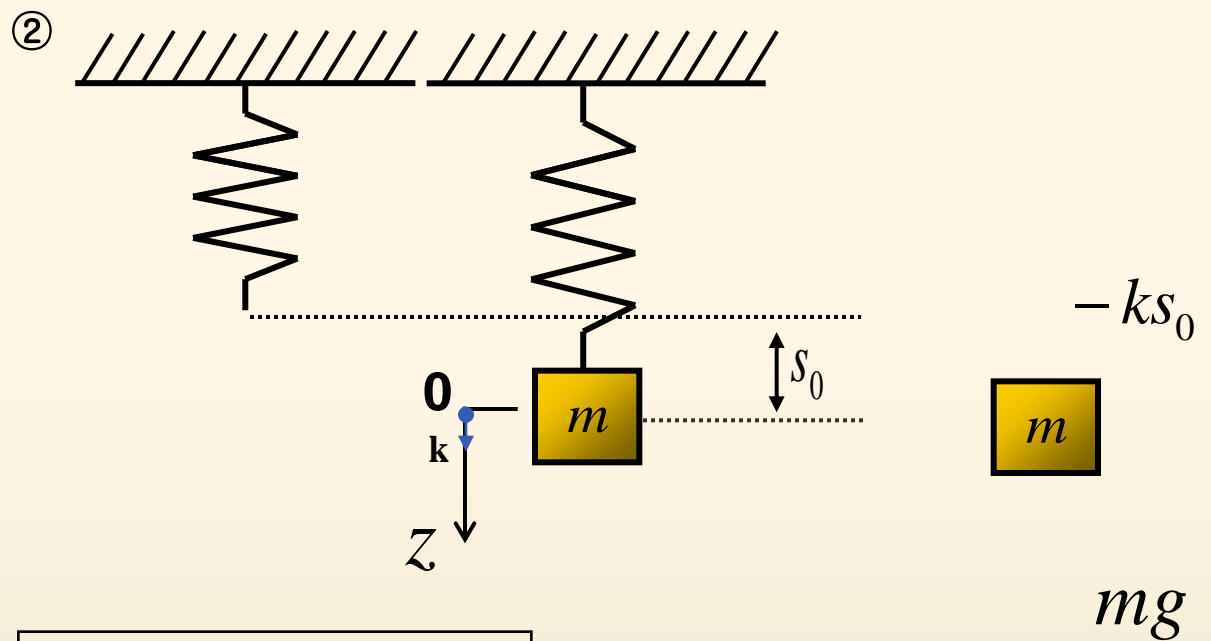


# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



By Newton's 2<sup>nd</sup> law,

$$mz'' = \mathbf{F} = mg\mathbf{k}$$

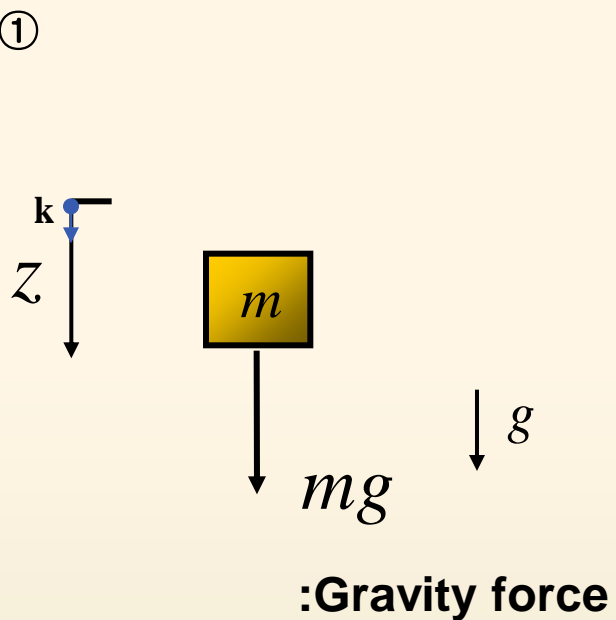


Nonlinearity of spring  
 $\mathbf{F}(z) = \ominus kz \ominus k_1 z^3$   
 linearize  
 Hooke's law  
 $F \propto z$   
 $\mathbf{F}_{spring} = \ominus kz$   
 $k$  : spring constant

○ opposite to the direction of displacement

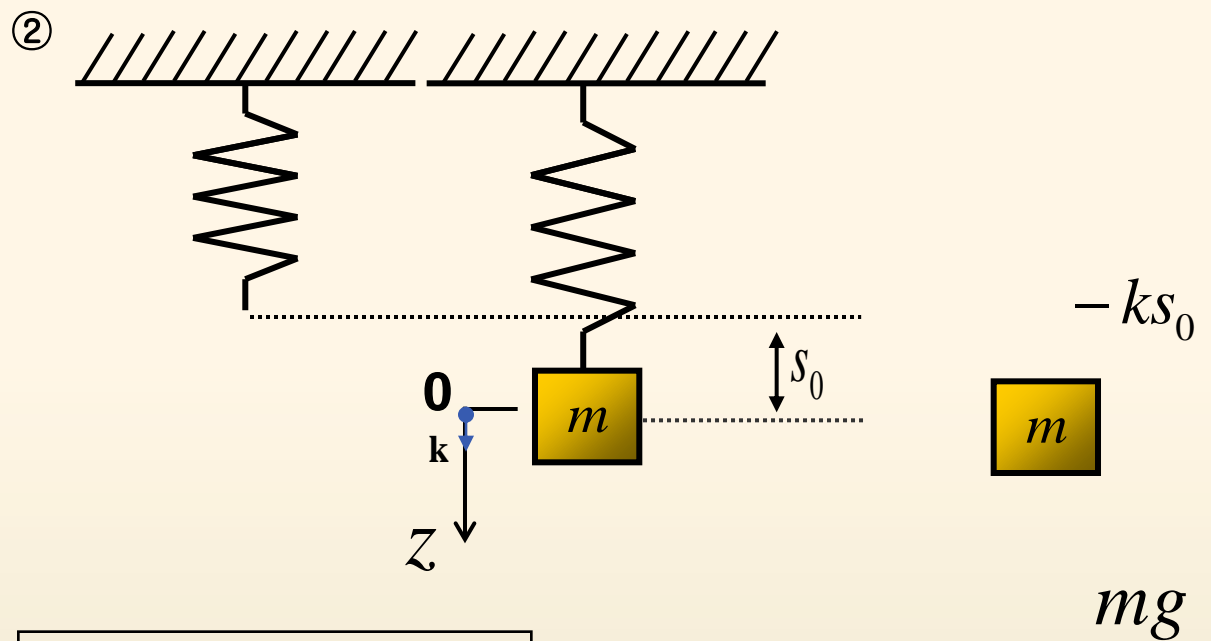


# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



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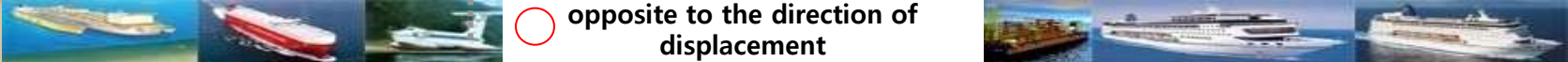
$$mz'' = \mathbf{F} = mg\mathbf{k}$$



Nonlinearity of spring  
 $\mathbf{F}(z) = \ominus kz \ominus k_1 z^3$   
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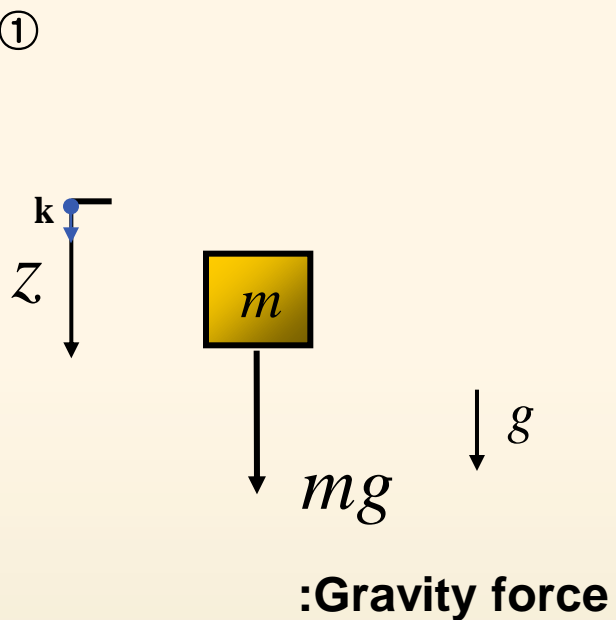
$$mz'' = \mathbf{F}$$

○ opposite to the direction of displacement



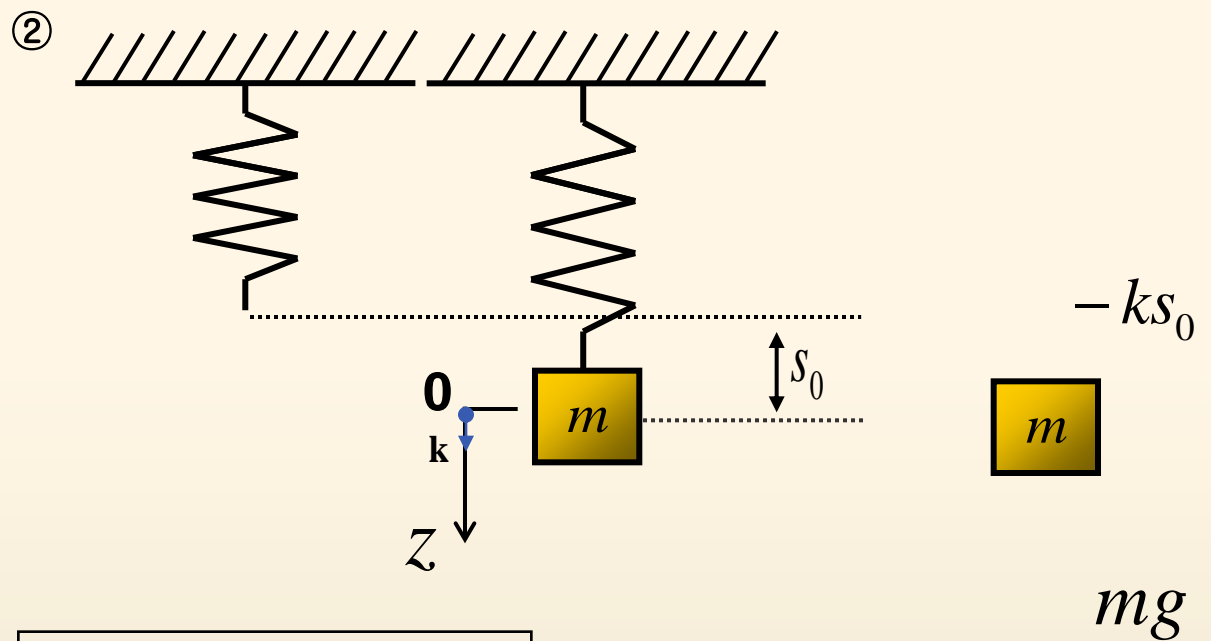


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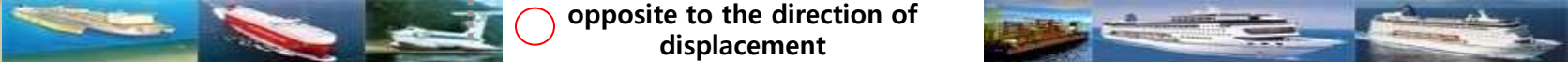
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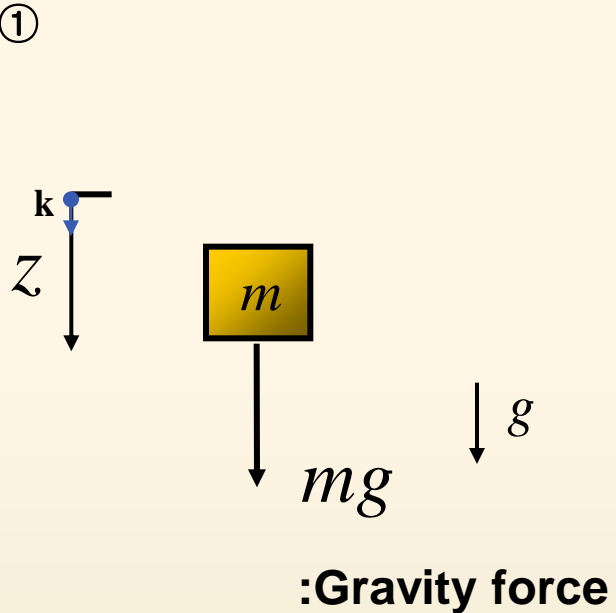
Nonlinearity of spring  
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$$mz'' = \mathbf{F} = mg\mathbf{k} - ks_0\mathbf{k}$$

○ opposite to the direction of displacement



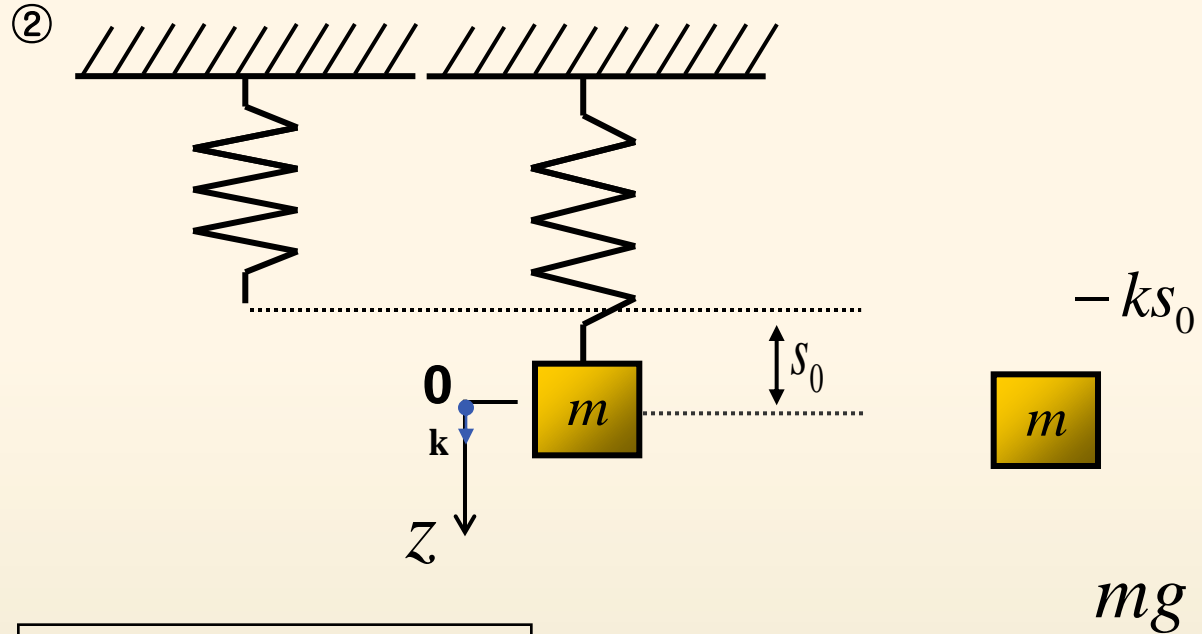
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By Newton's 2<sup>nd</sup> law,

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$$= mg\mathbf{k}$$



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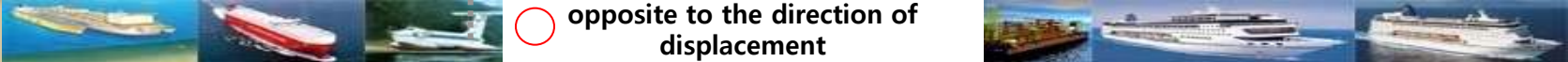
$$mz'' = \mathbf{F}$$

$$= mg\mathbf{k} - ks_0\mathbf{k}$$

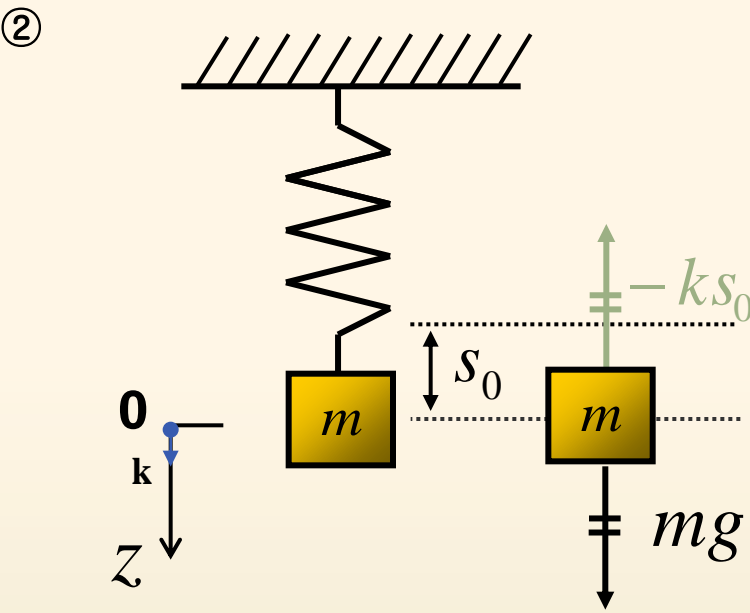
$$= 0 \quad (\because z'' = 0)$$

: static equilibrium

○ opposite to the direction of displacement



# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2z}{dt^2}$

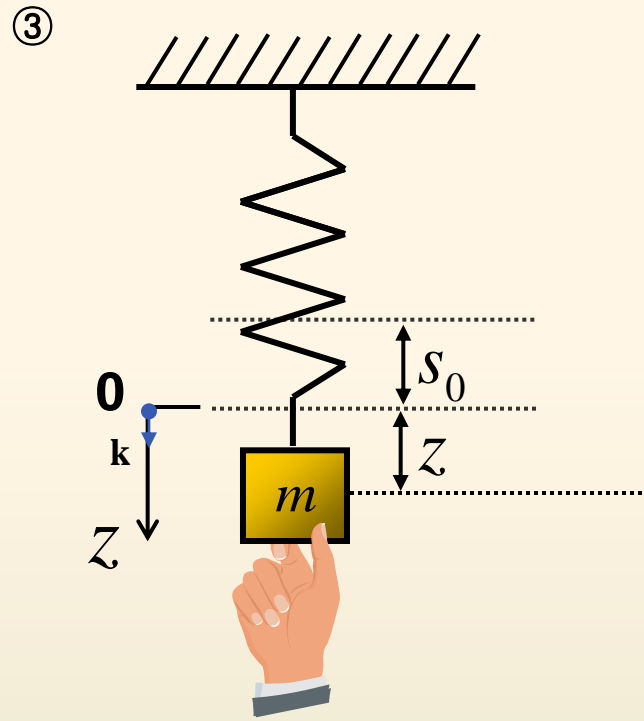
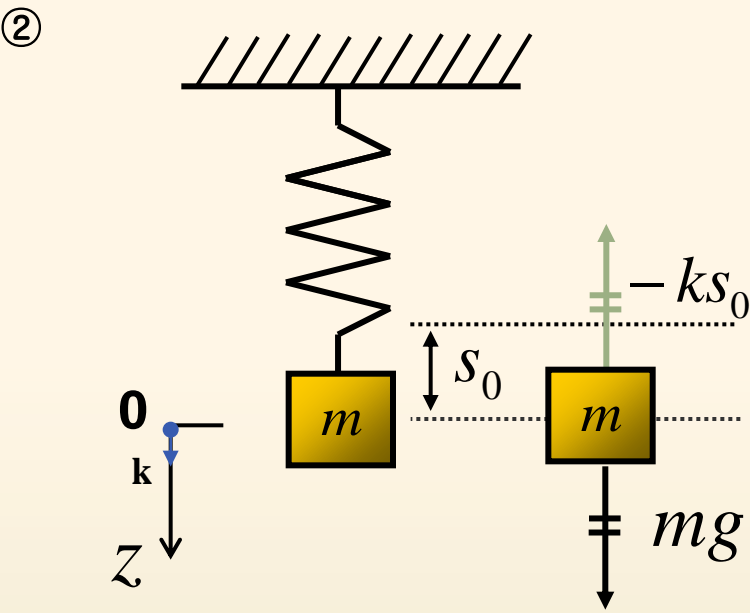


③

$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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 &= 0 \quad (\because z'' = 0) \\
 &\text{: static equilibrium}
 \end{aligned}$$



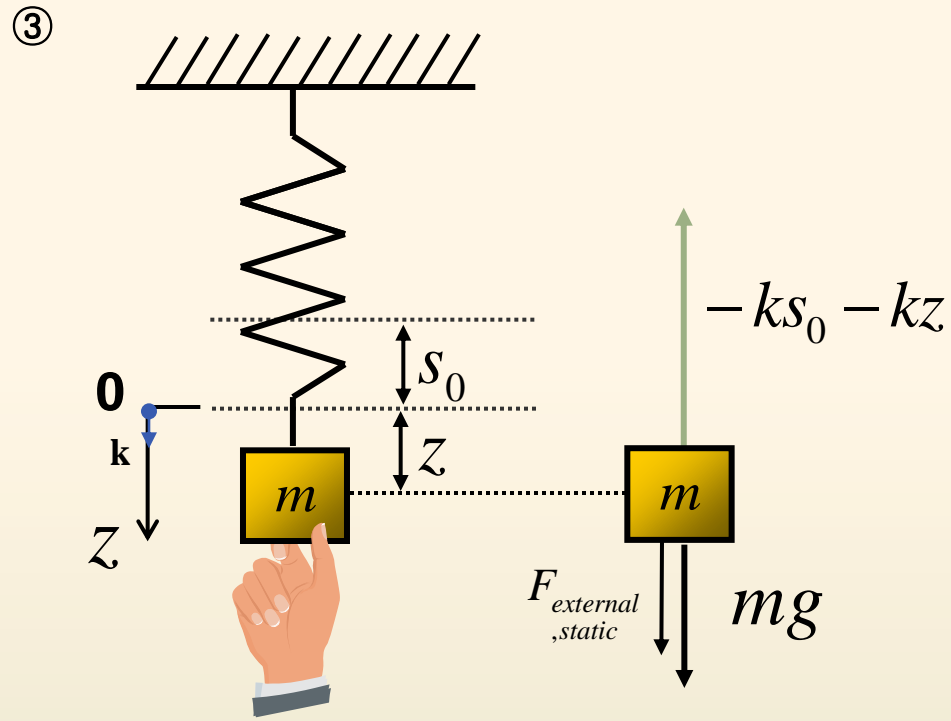
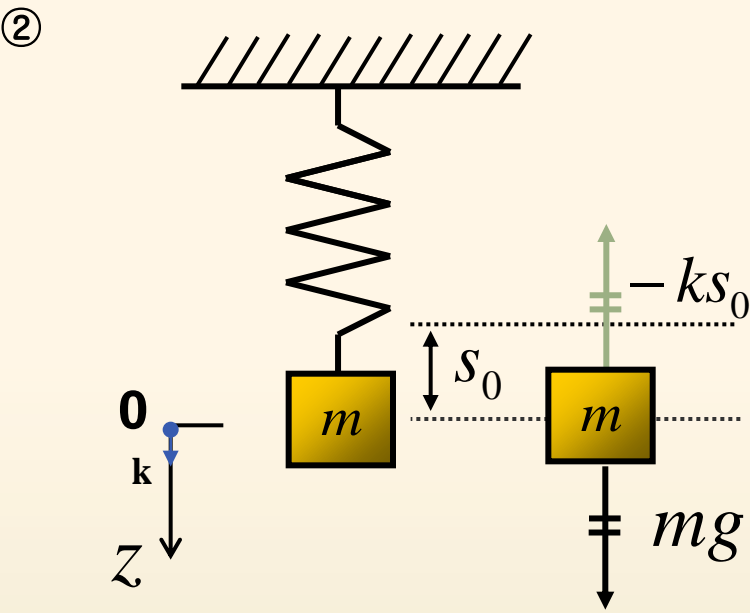
# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



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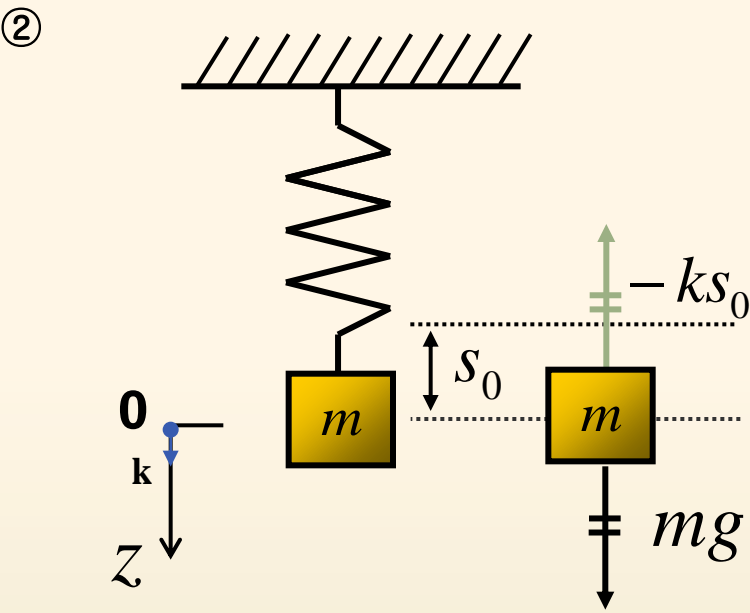
# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2z}{dt^2}$



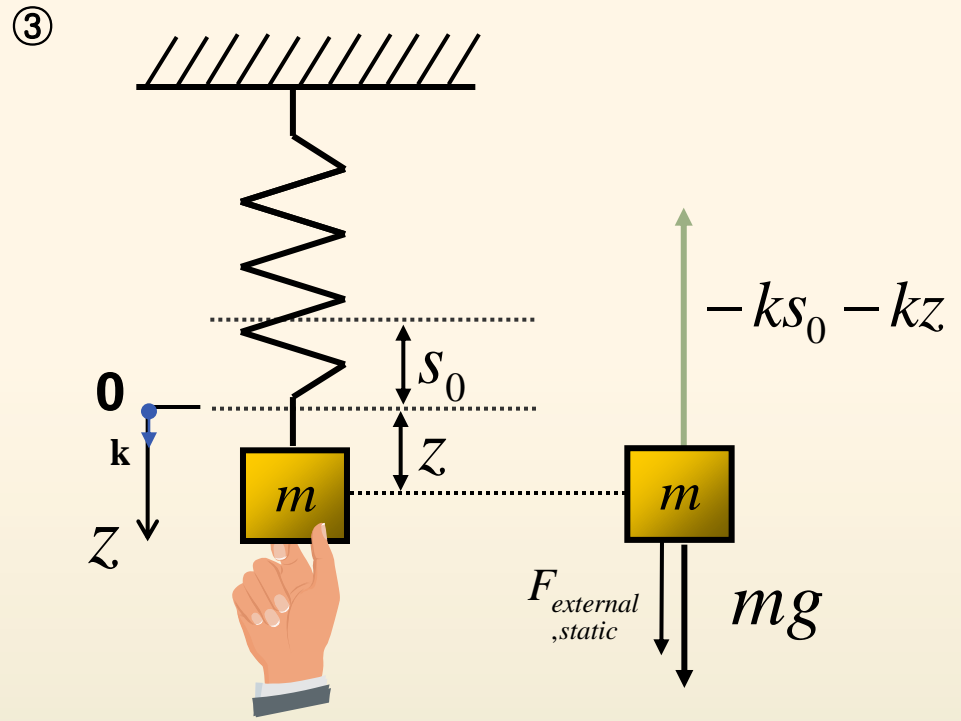
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# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



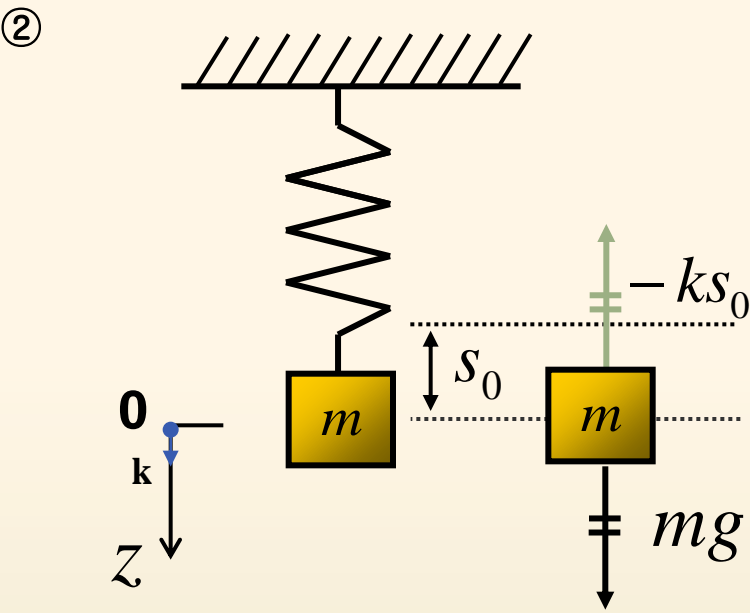
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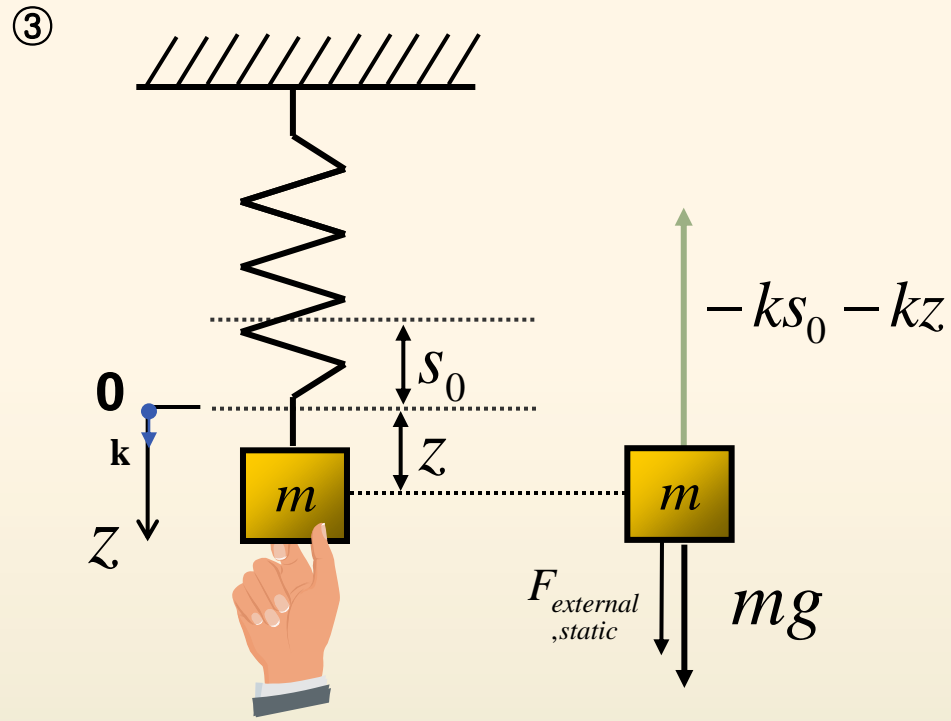
$$m\mathbf{z}'' = \mathbf{F}$$



# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2 z}{dt^2}$



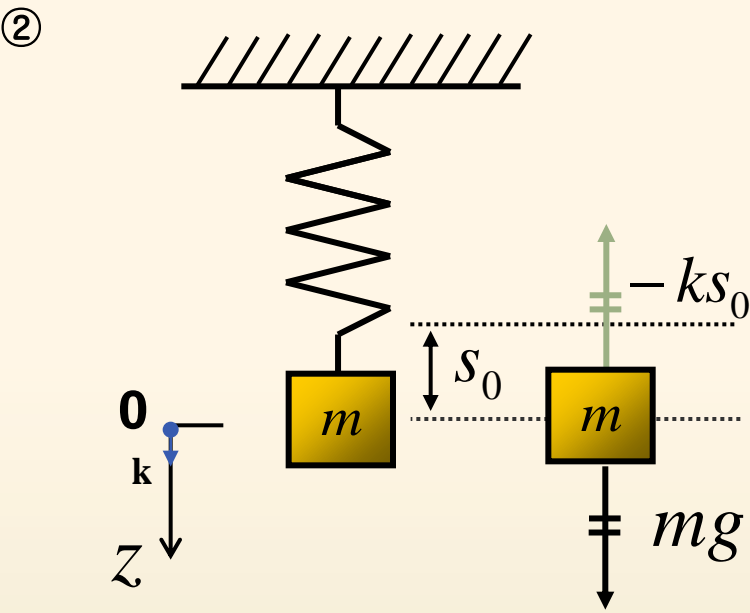
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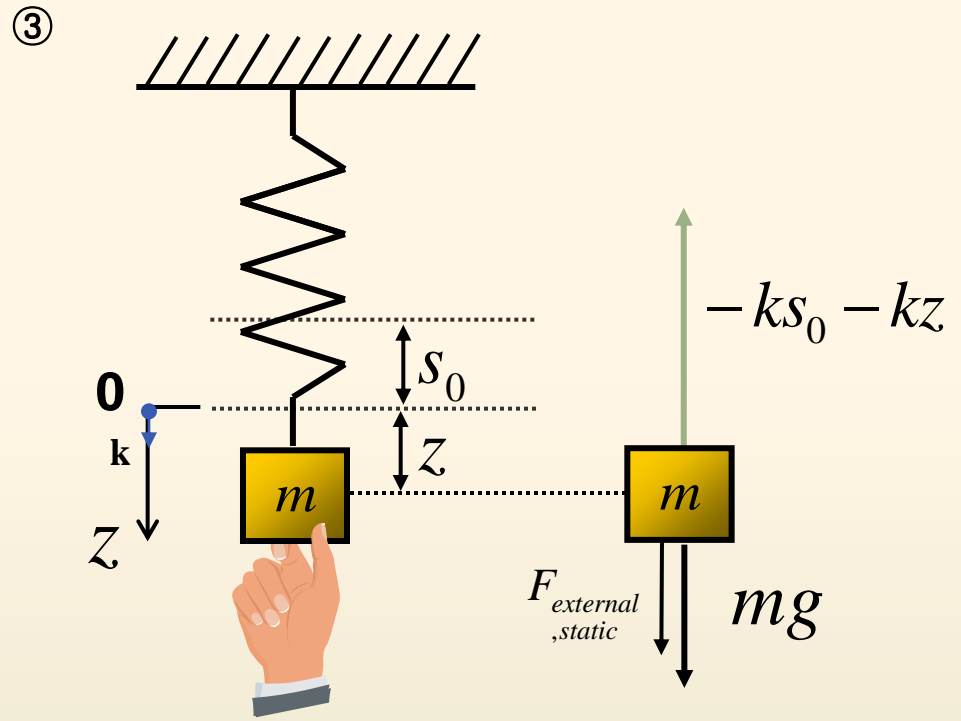
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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 \end{aligned}$$



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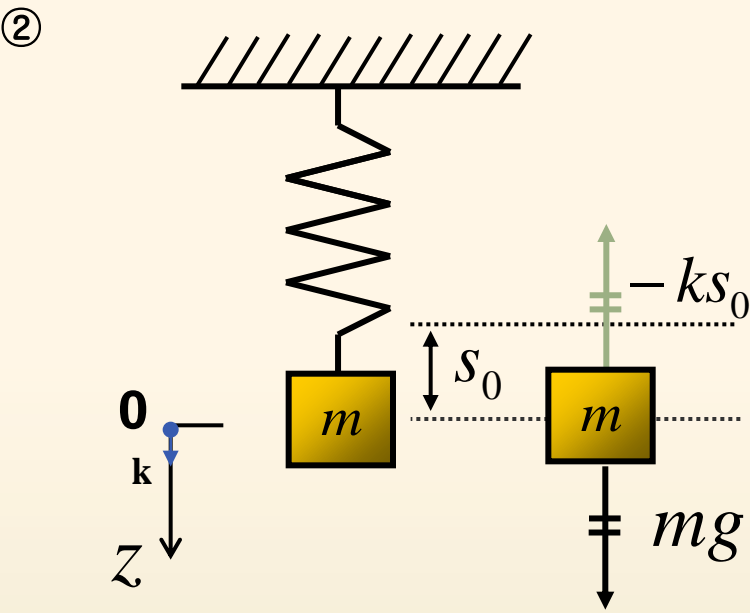


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 &= -kz\mathbf{k} + \mathbf{F}_{external,static}
 \end{aligned}$$

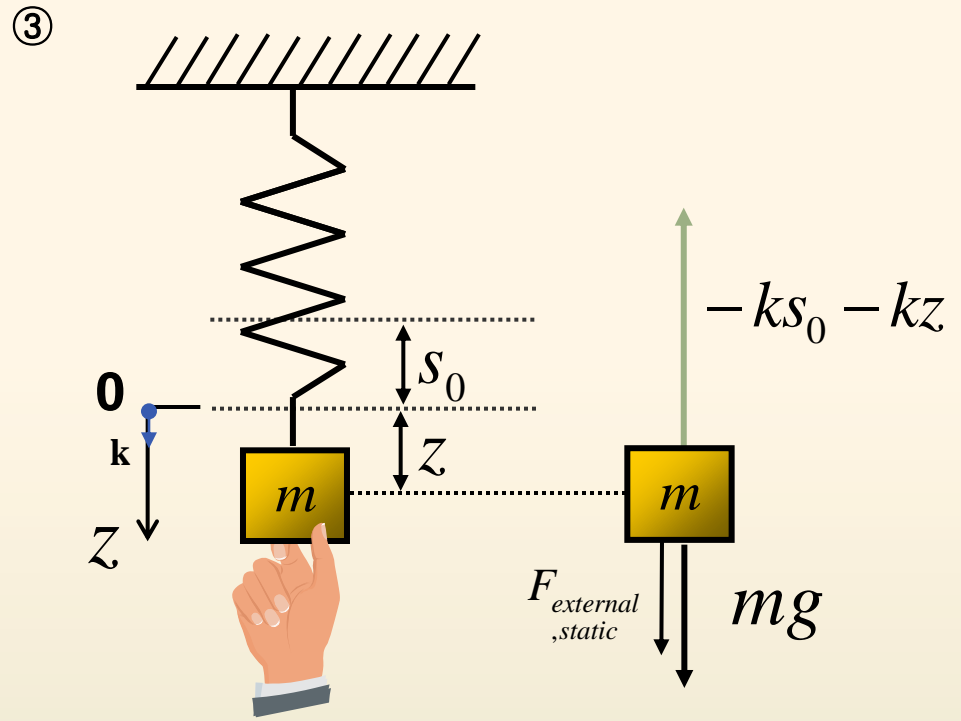




# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2z}{dt^2}$



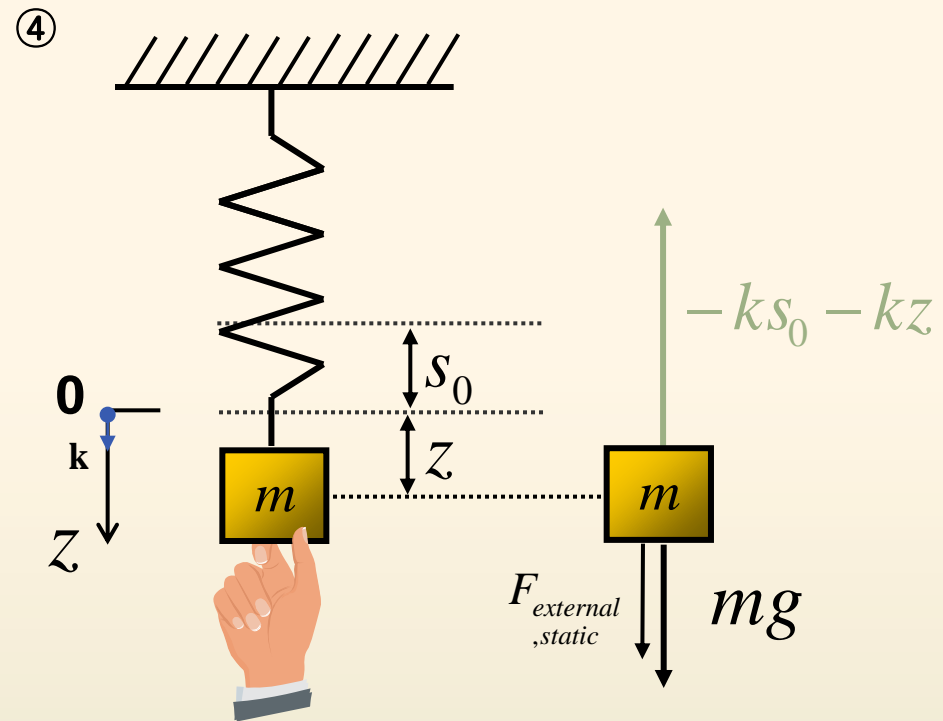
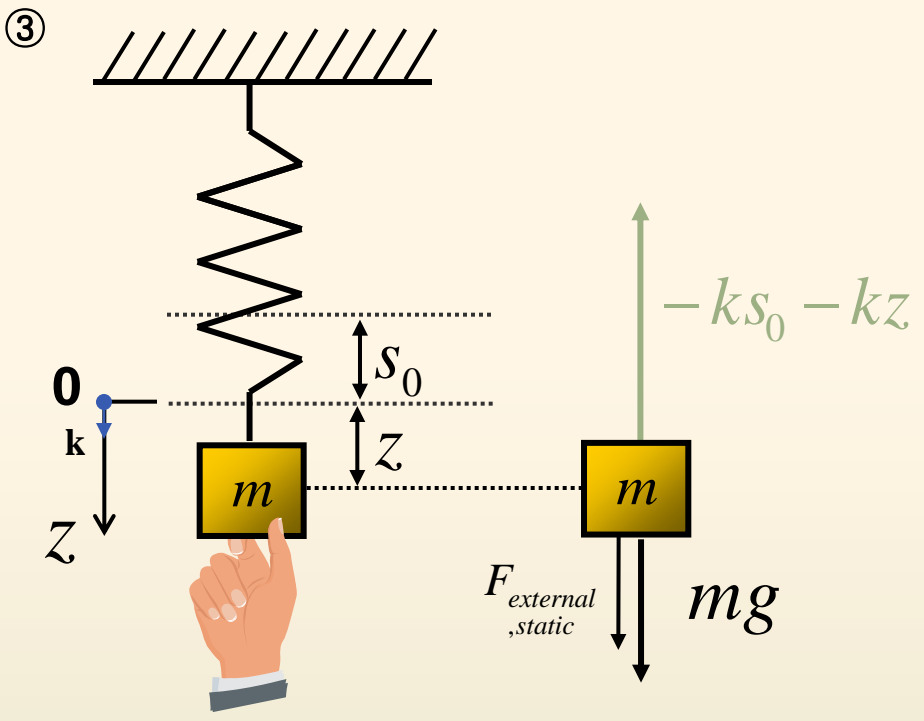
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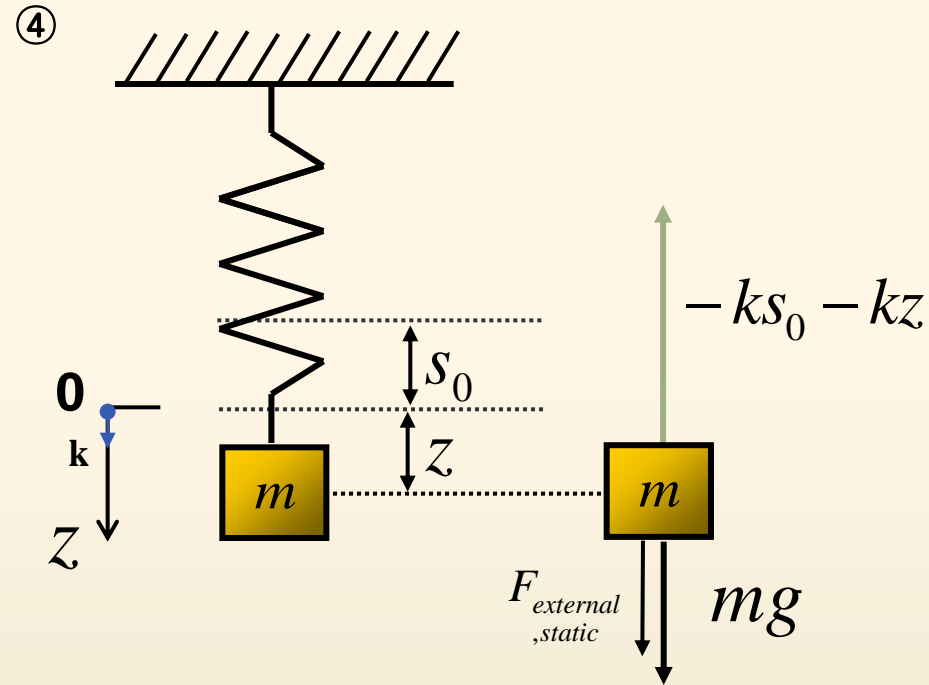
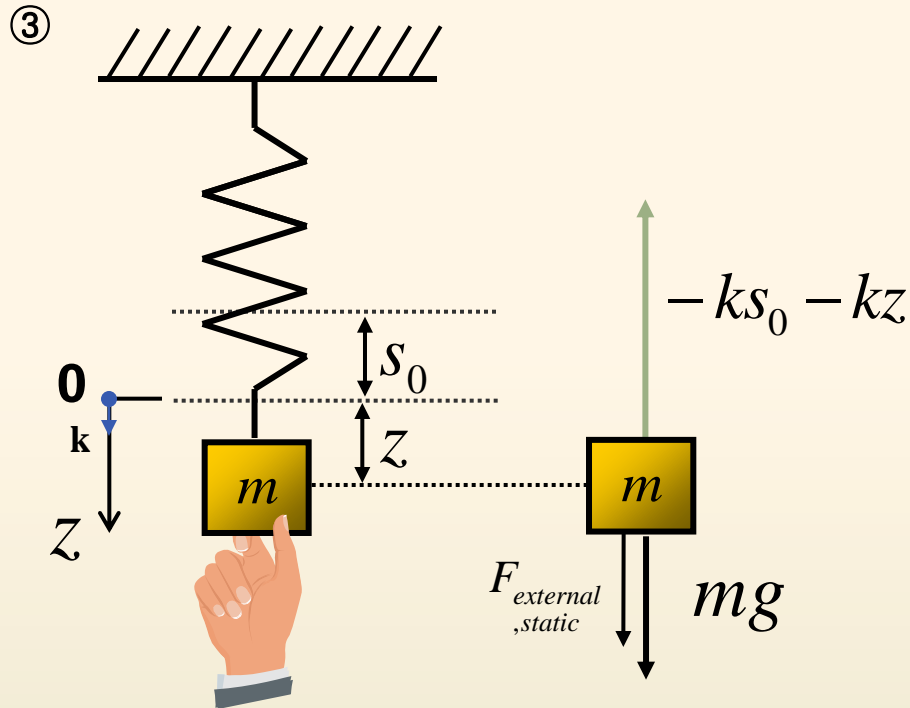


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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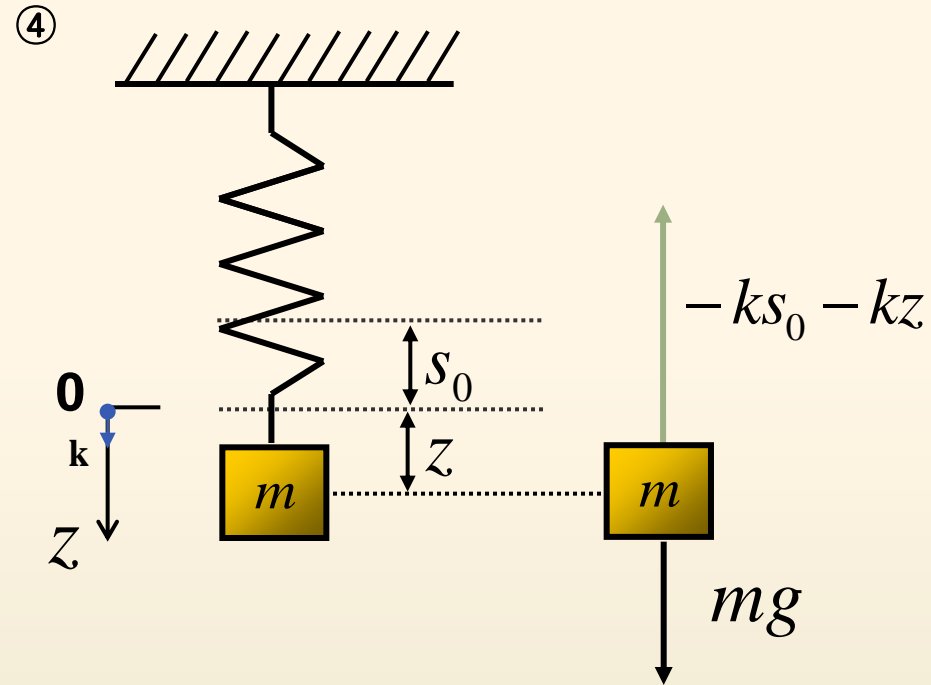
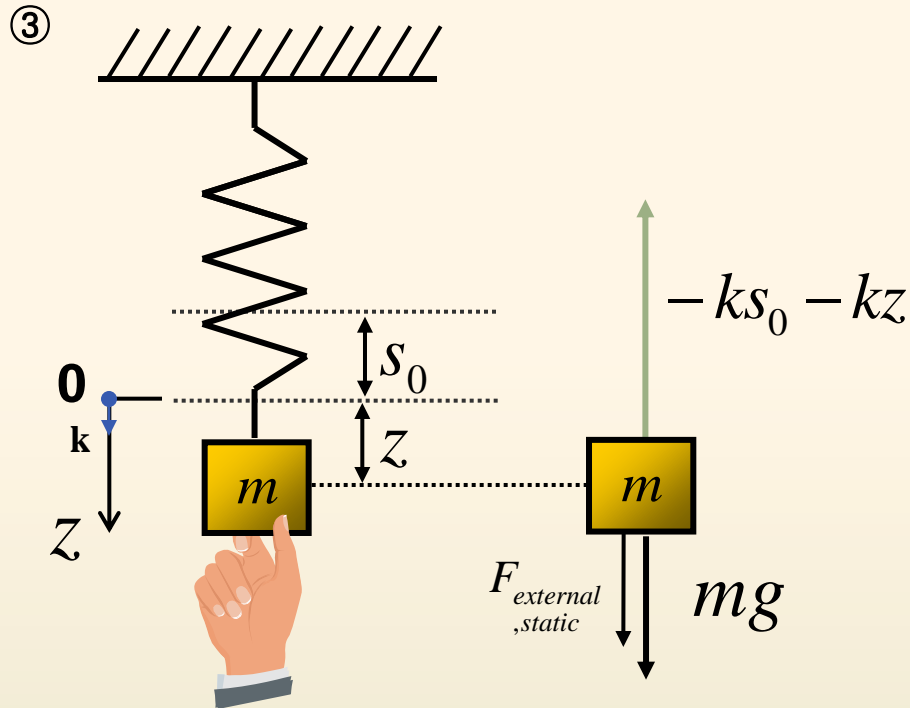


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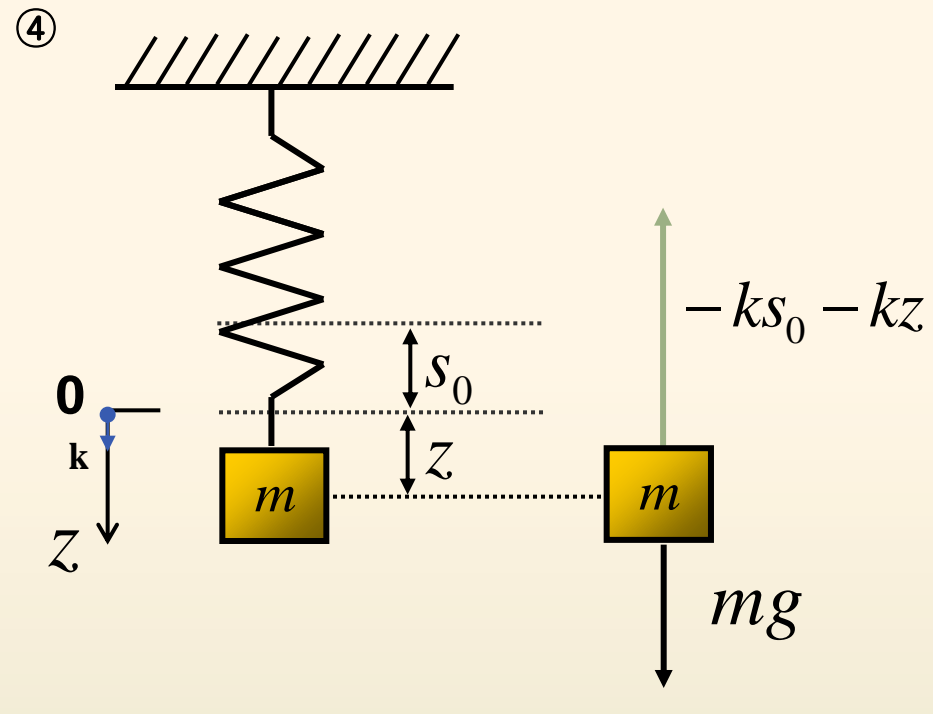
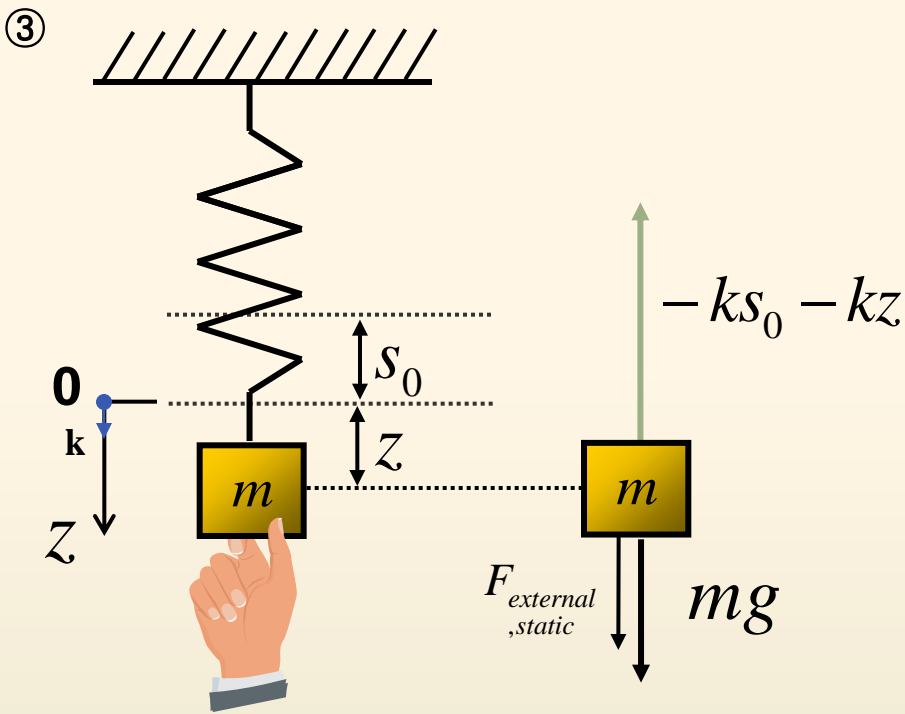


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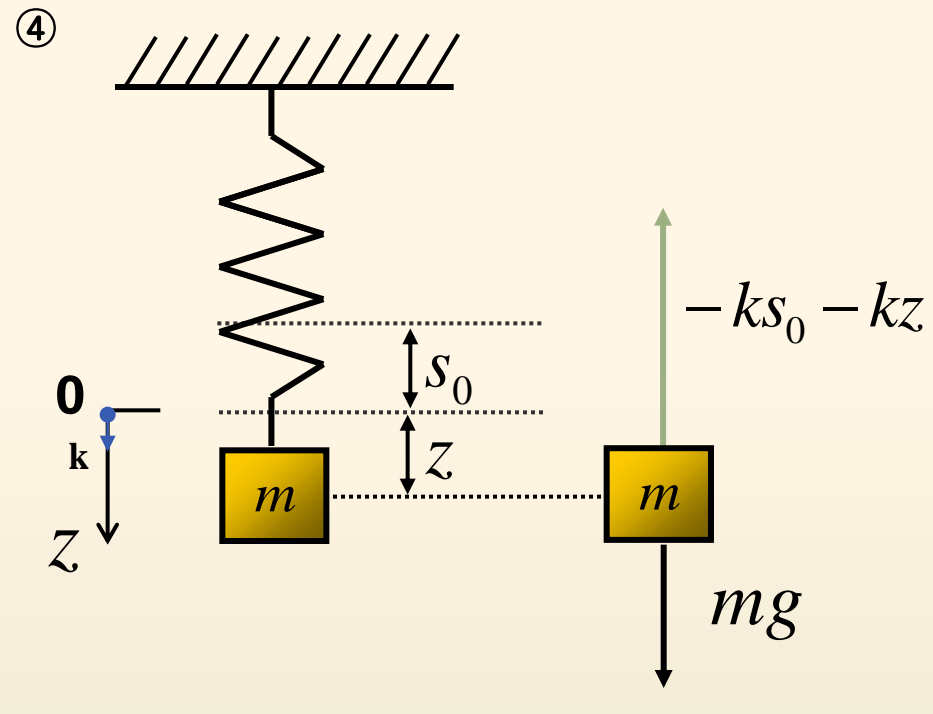
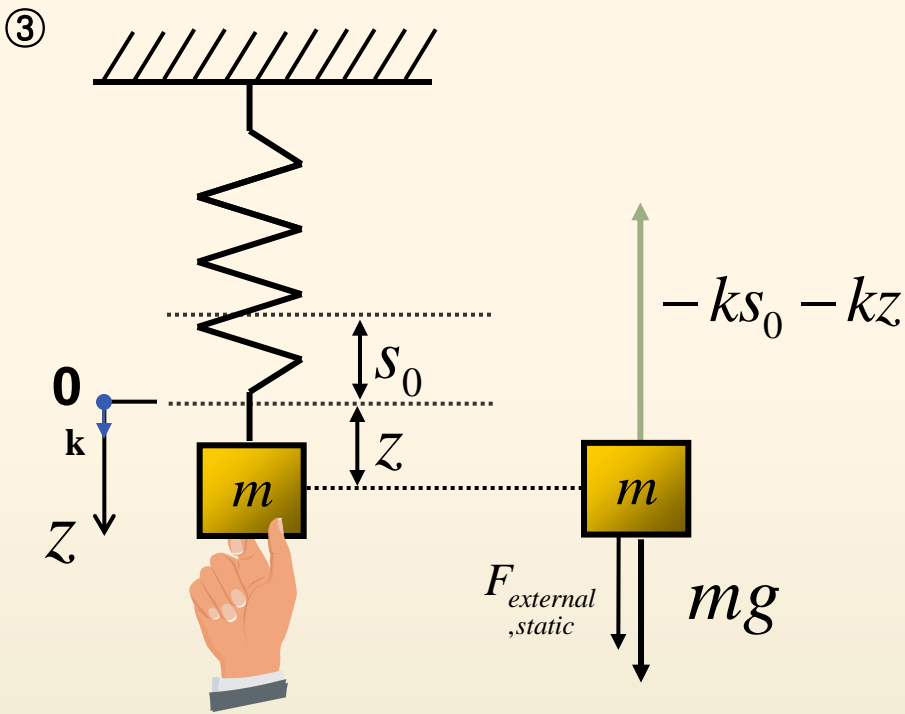
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 \end{aligned}$$

$m\mathbf{z}'' + k\mathbf{z} = 0$  
 Physical Phenomenon  
 Mathematical Equation  
 Oscillation by the restoring force



# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2z}{dt^2}$



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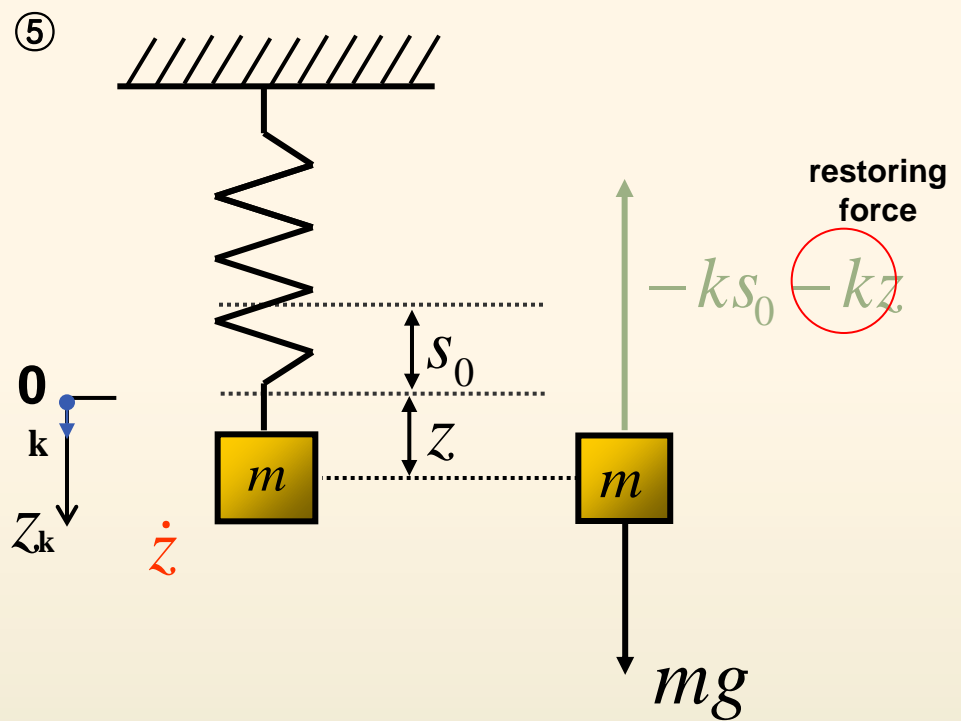
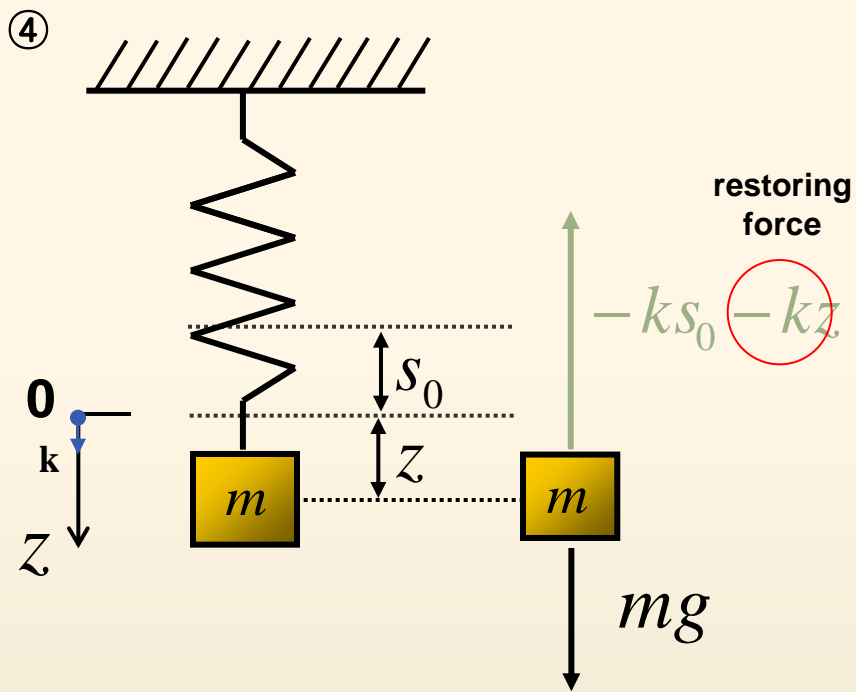
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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 &= -kz\mathbf{k} \quad \text{restoring force}
 \end{aligned}$$

$m\mathbf{z}'' + k\mathbf{z} = 0$  Oscillation by the restoring force

Physical Phenomenon ↔ Mathematical Equation



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



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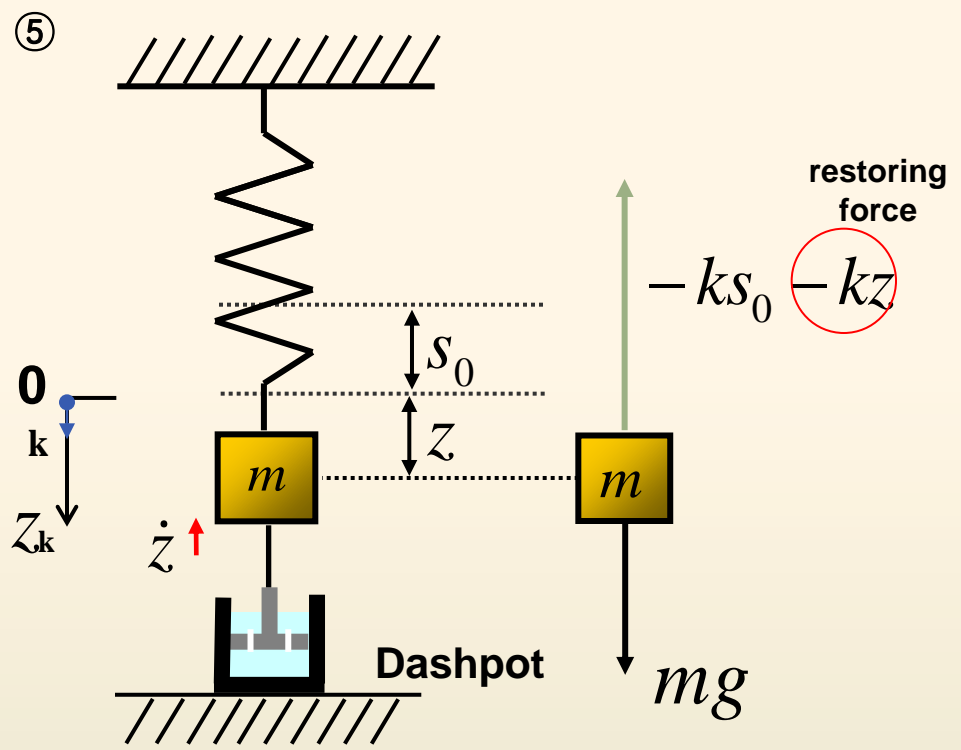
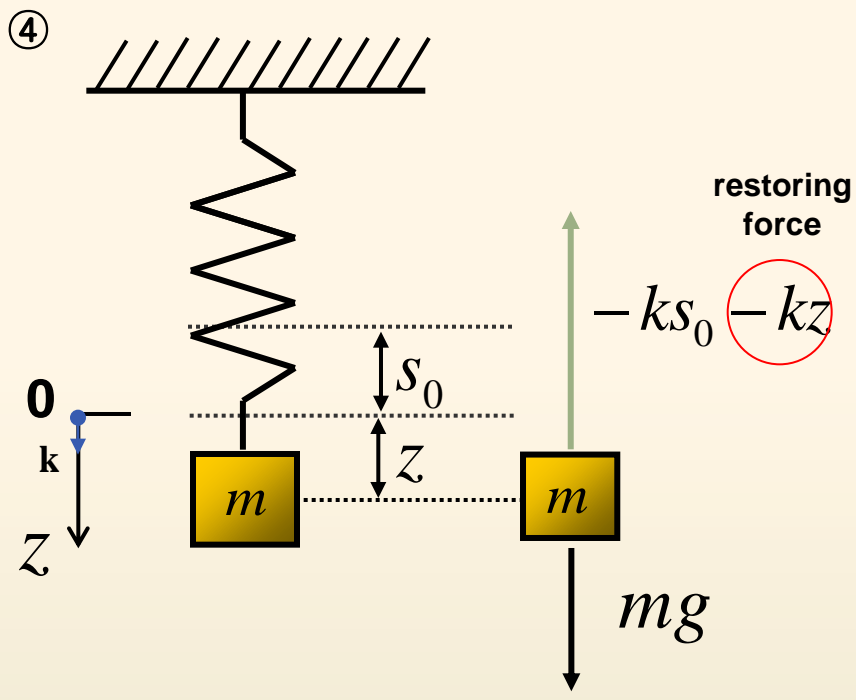
Physical Phenomenon  
 Mathematical Equation

$$m\mathbf{z}'' + kz = 0$$

oscillation by the restoring force



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



$$\begin{aligned}
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Physical Phenomenon  
 Mathematical Equation

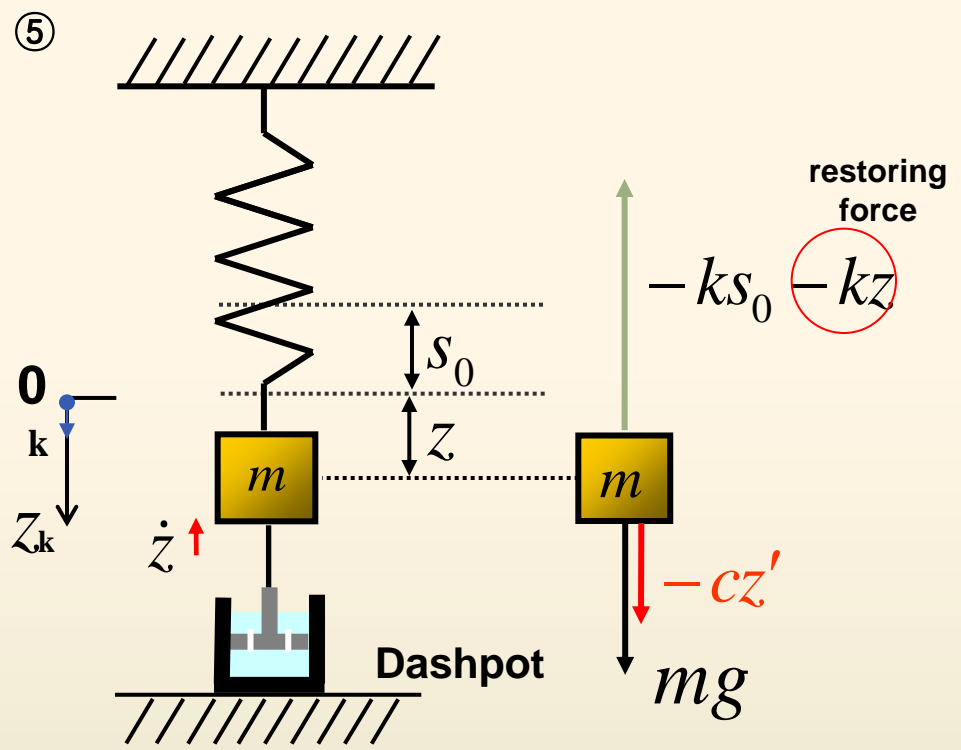
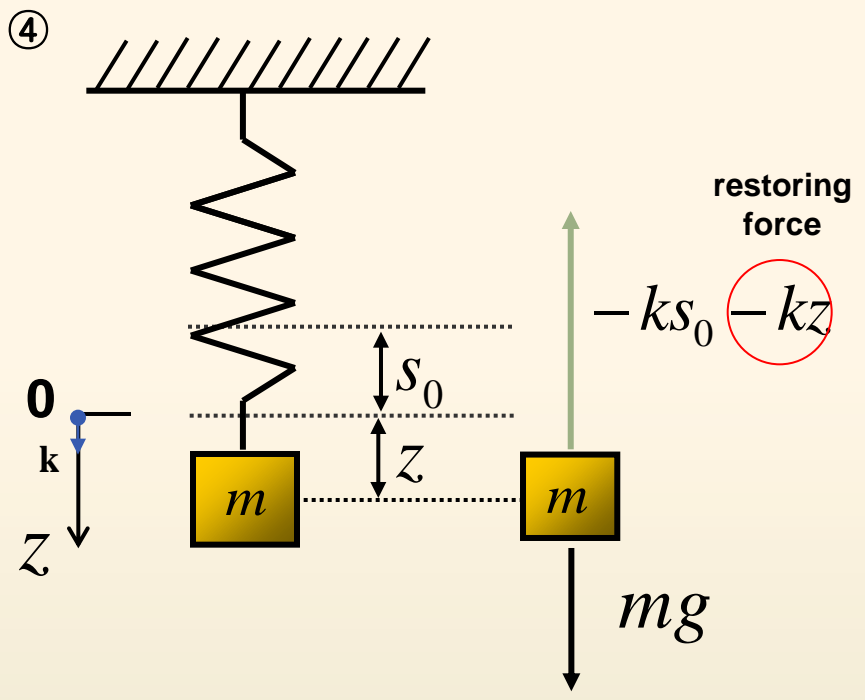
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Oscillation by the restoring force





# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



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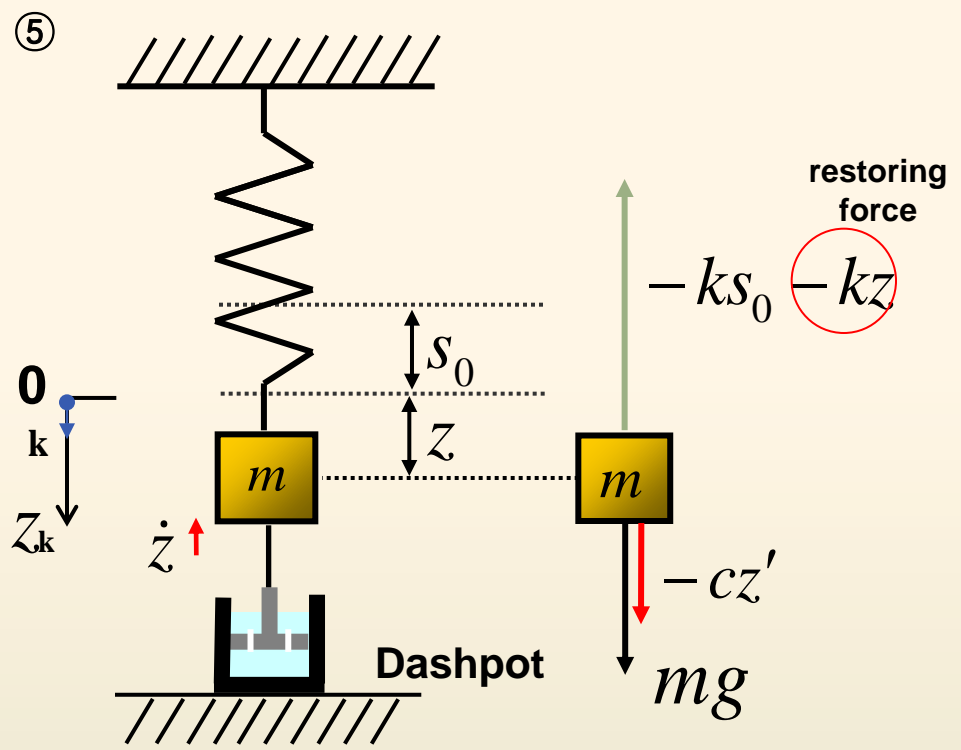
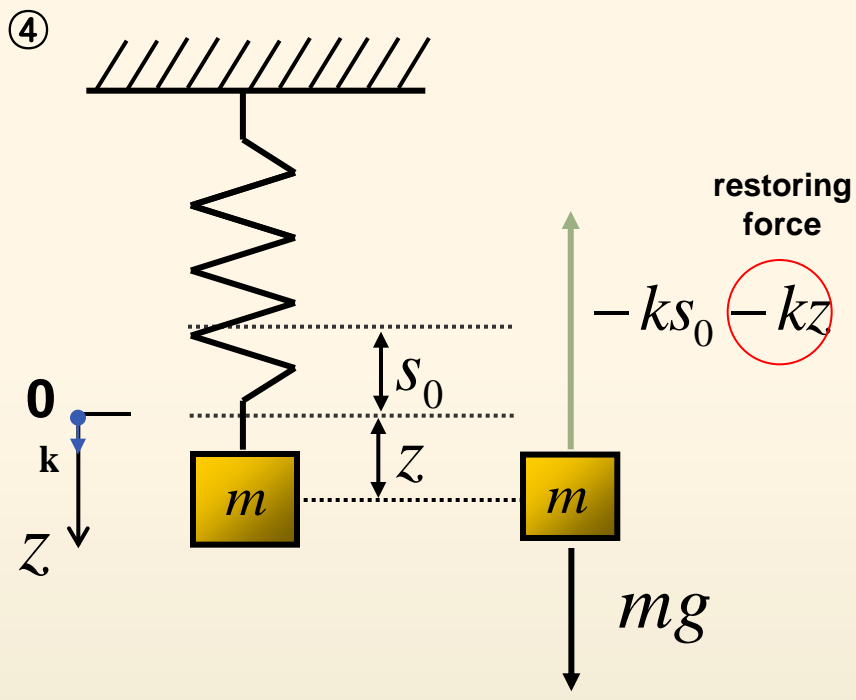
Physical Phenomenon  
 Mathematical Equation

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Oscillation by the restoring force



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 \end{aligned}$$

$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} - cz'\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

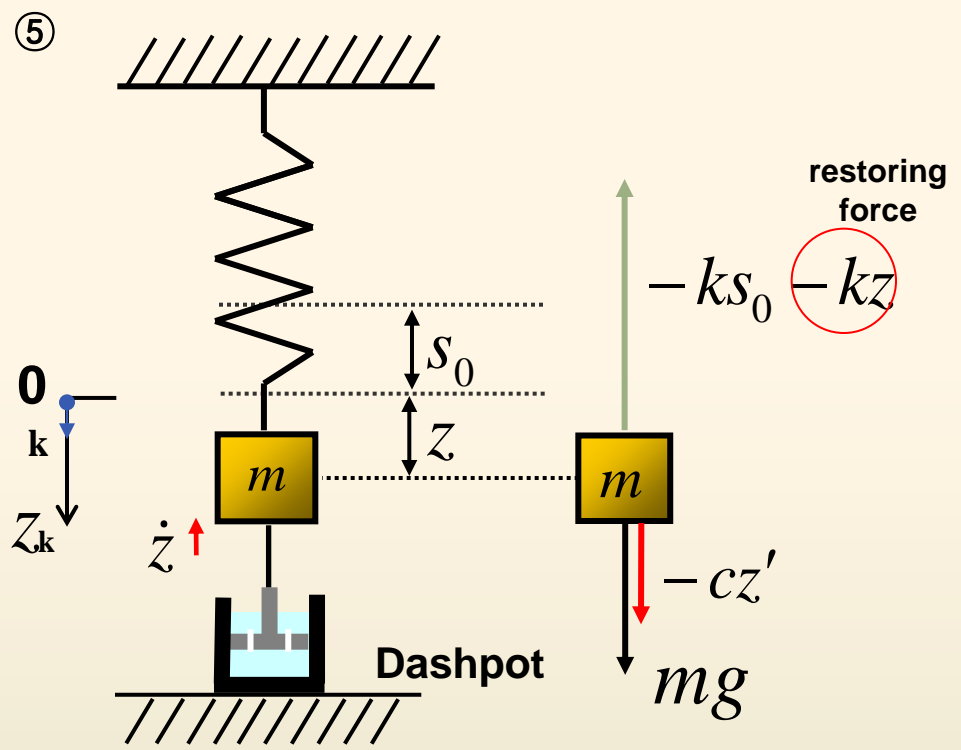
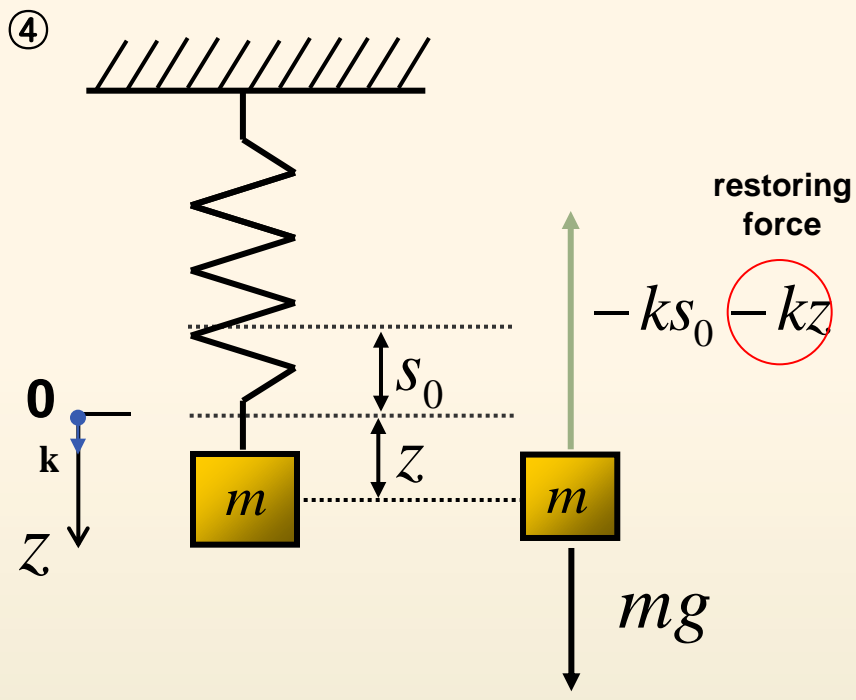
Physical Phenomenon  
 Mathematical Equation

$$m\mathbf{z}'' + kz = 0$$

Oscillation by the restoring force



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



$$\begin{aligned}
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 \end{aligned}$$

Physical Phenomenon  
 Mathematical Equation

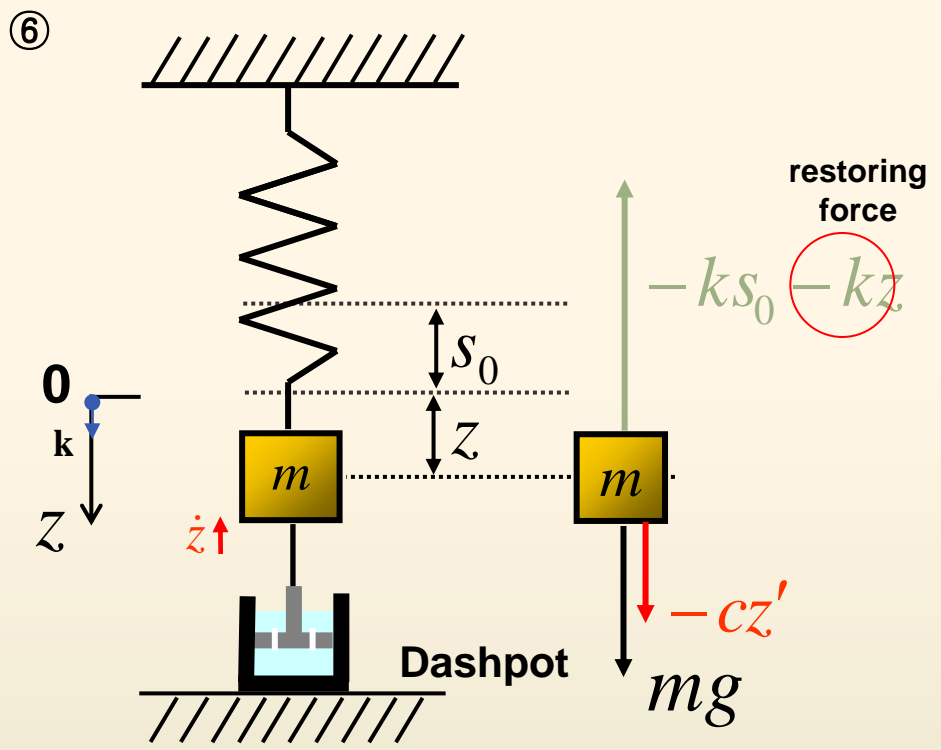
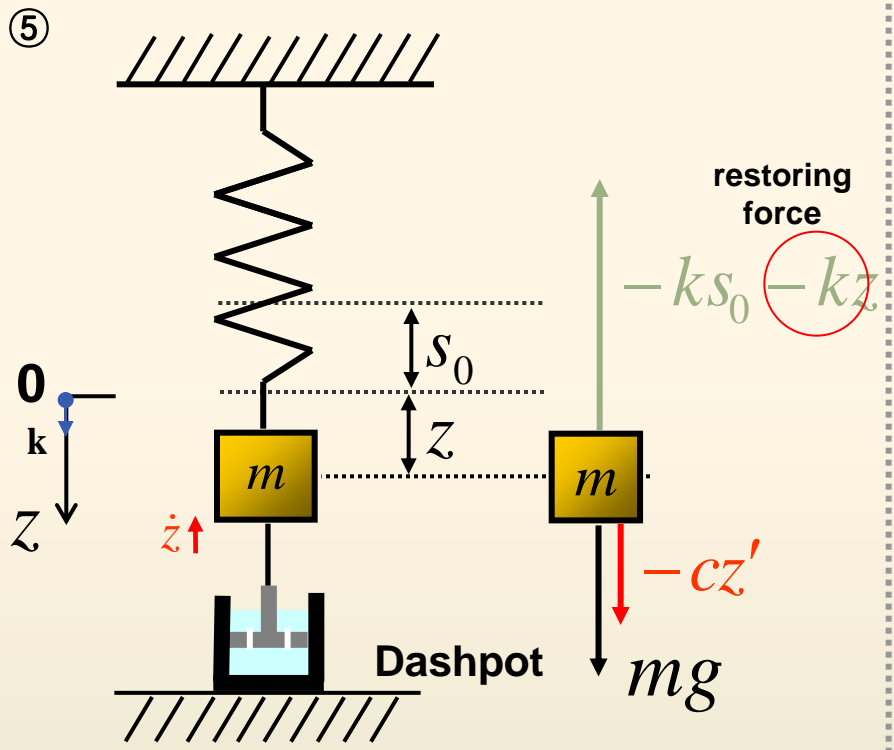
$$m\mathbf{z}'' + kz = 0$$

oscillation by the restoring force

$$m\mathbf{z}'' + cz' + kz = 0$$



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



$$mz'' = F$$

$$= mgk - ks_0k - kz k - cz'k$$

$$= -kz k - cz'k$$

$$mz'' = F$$

$$= mgk - ks_0k - kz k - cz'k$$

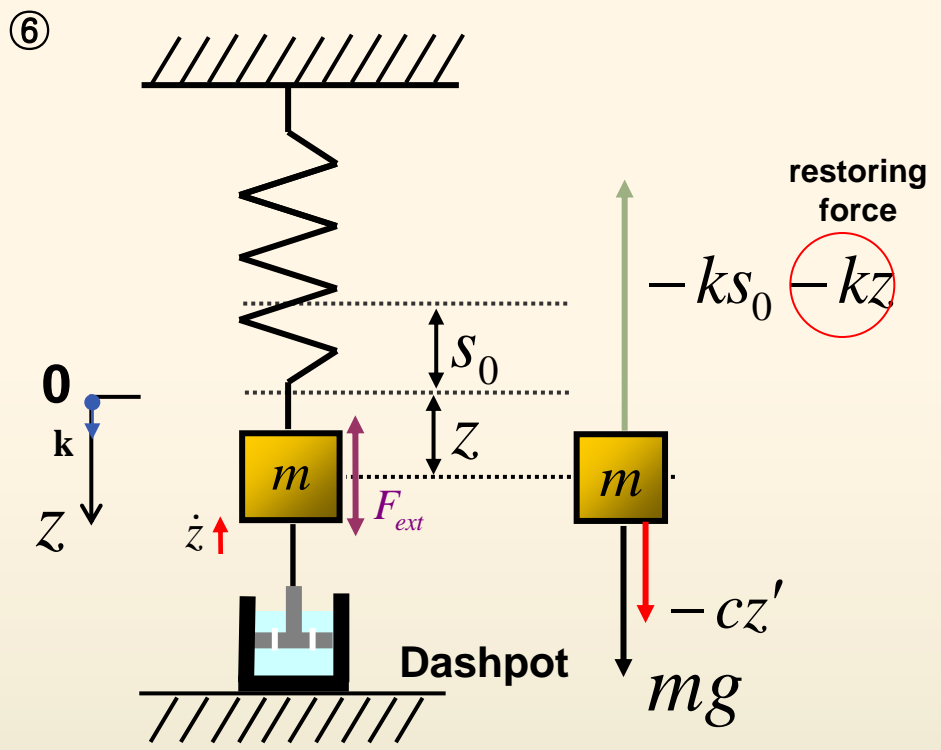
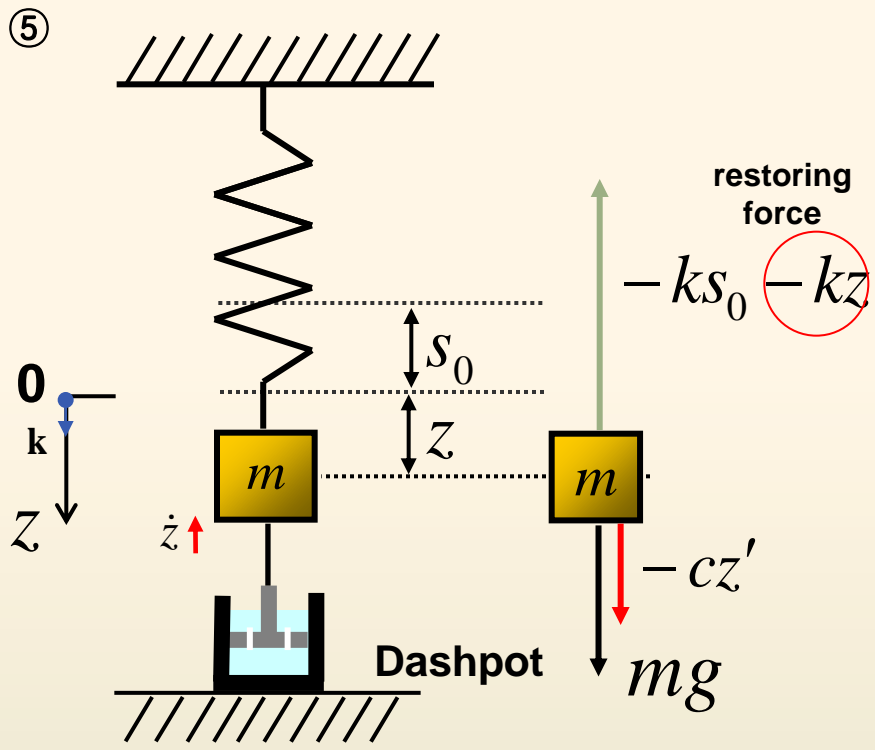
$$= -kz k - cz'k$$

Physical Phenomenon  
 Mathematical Equation

$$mz'' + cz' + kz = 0$$



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



$$mz'' = F$$

$$= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} - cz'\mathbf{k}$$

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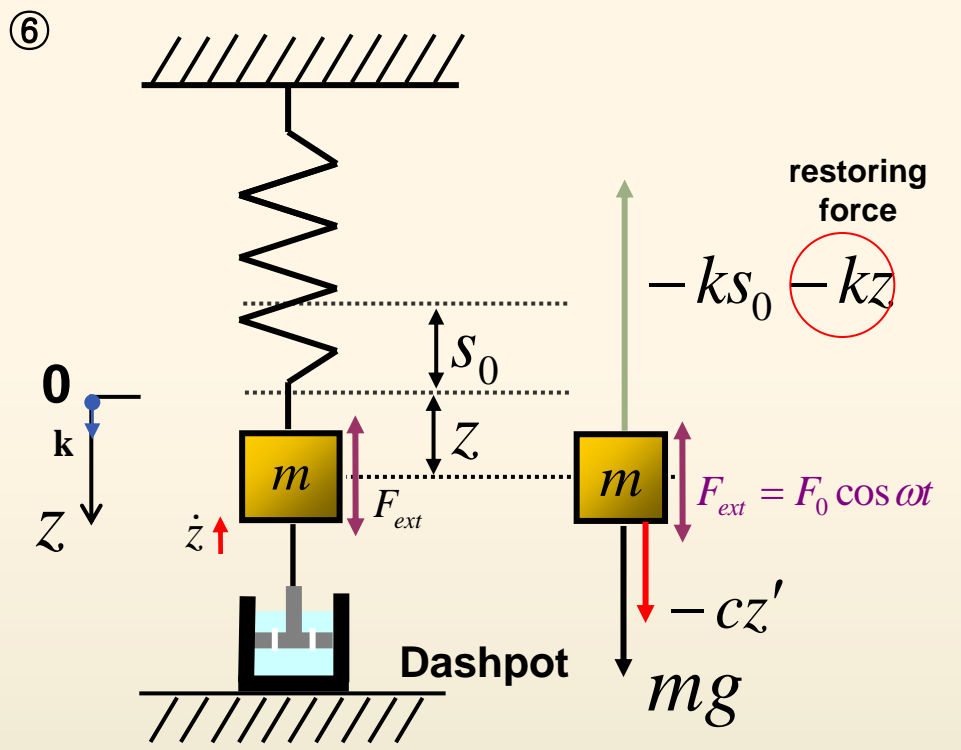
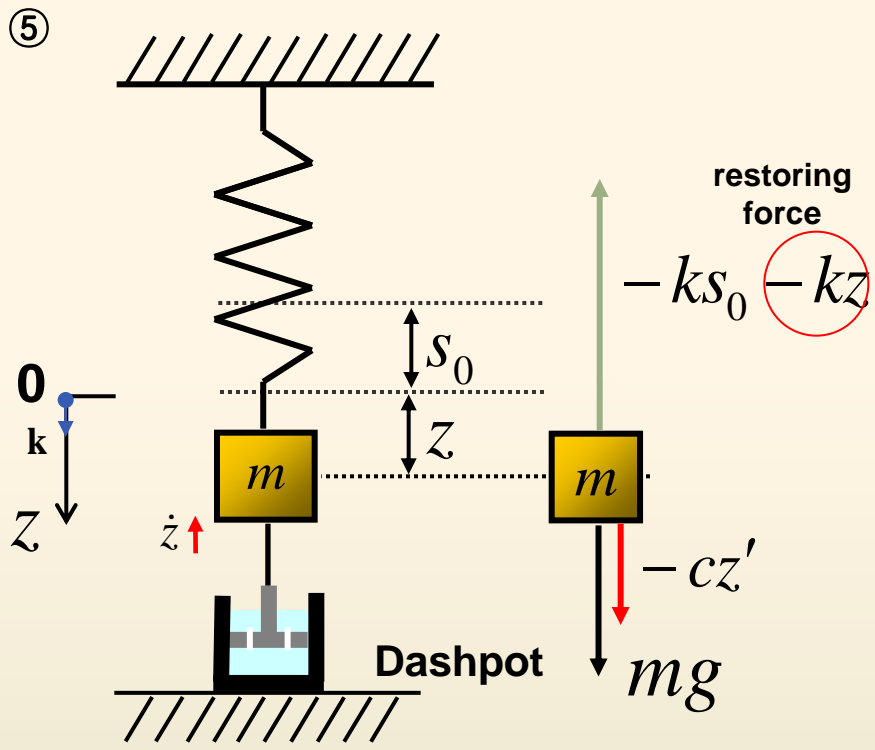
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 Mathematical Equation

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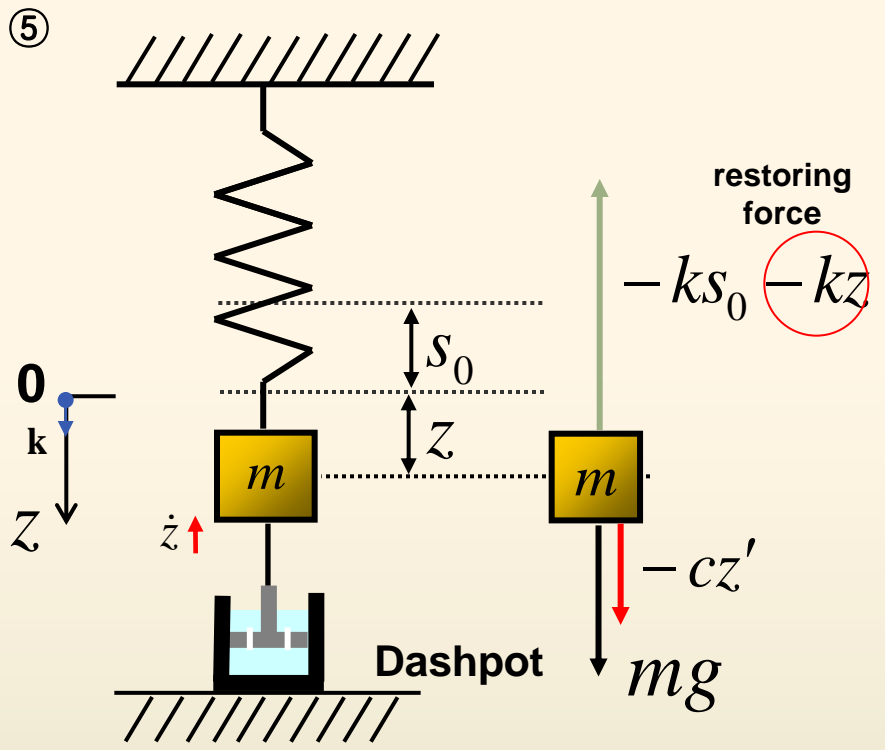
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Physical Phenomenon  
 Mathematical Equation

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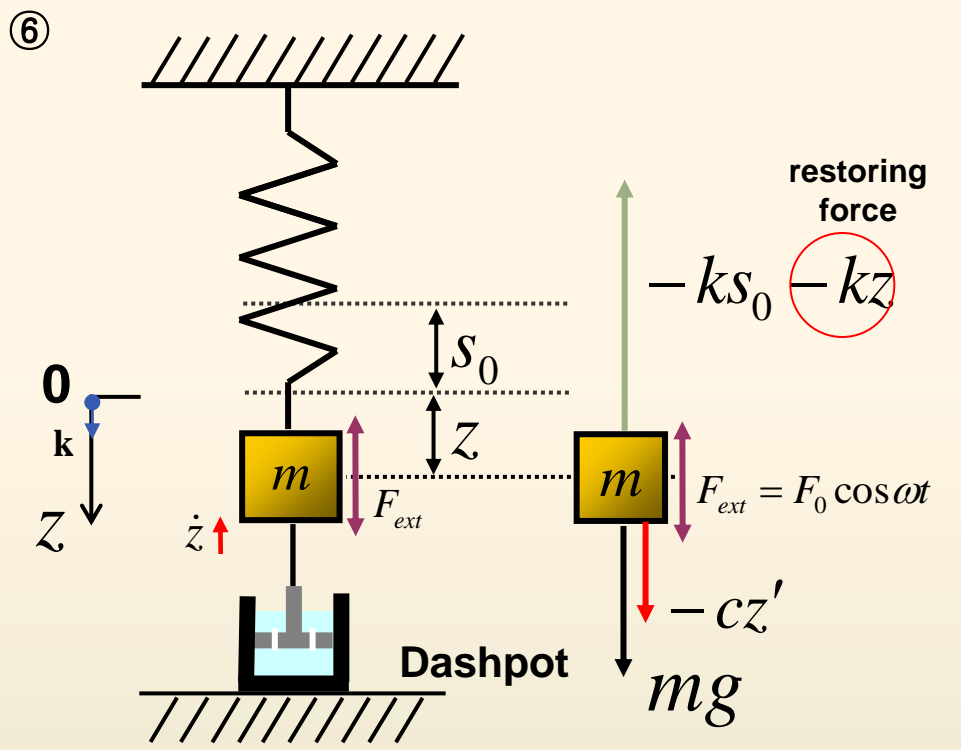
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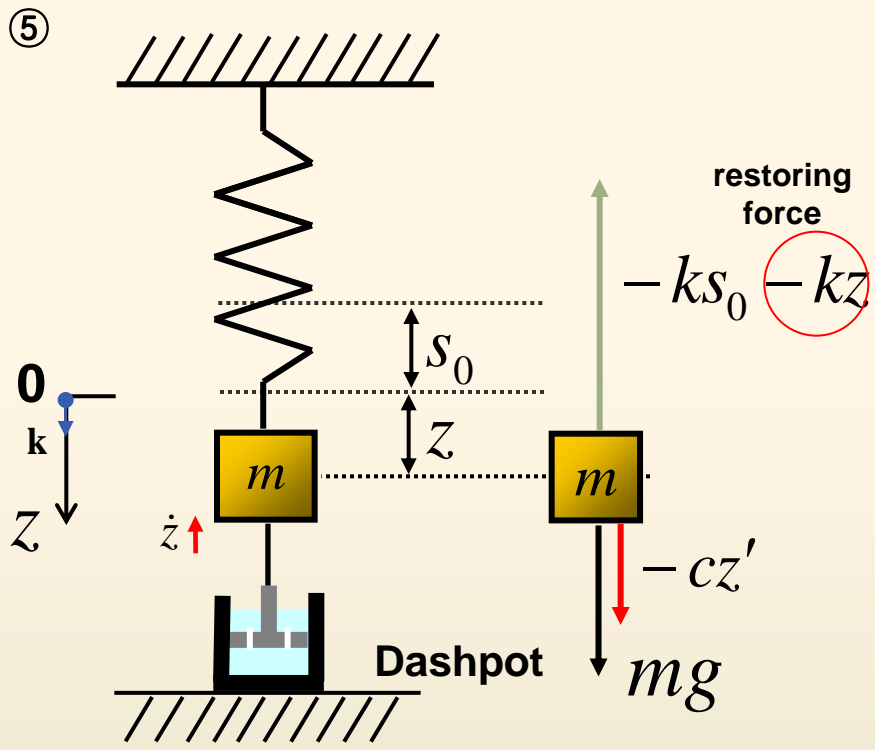
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Physical Phenomenon  
 Mathematical Equation

$$mz'' + cz' + kz = 0$$



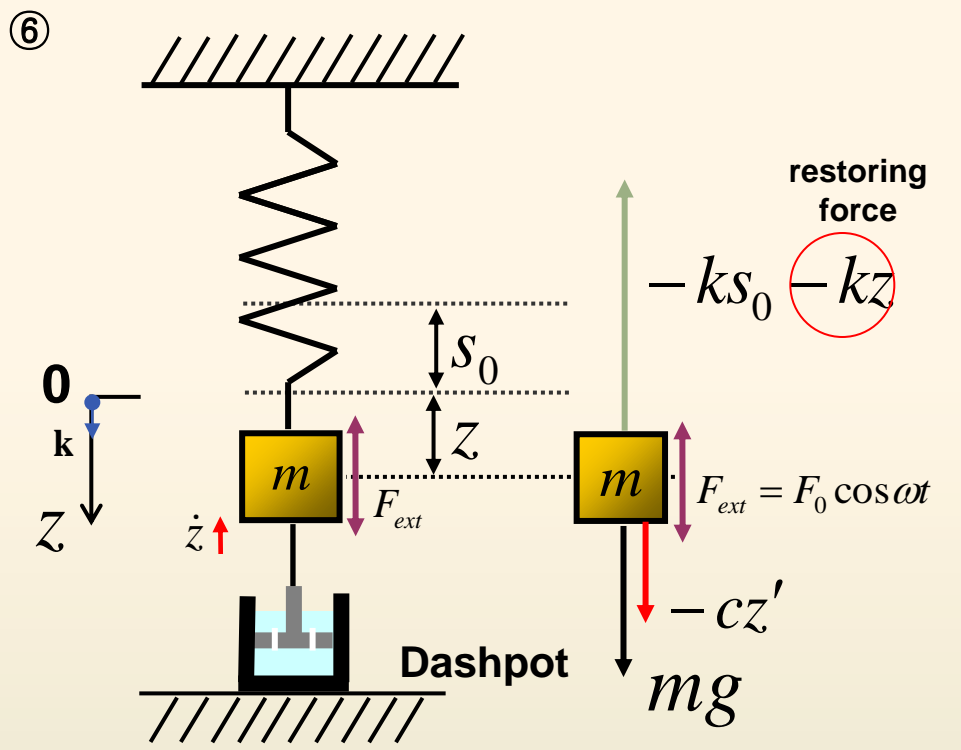
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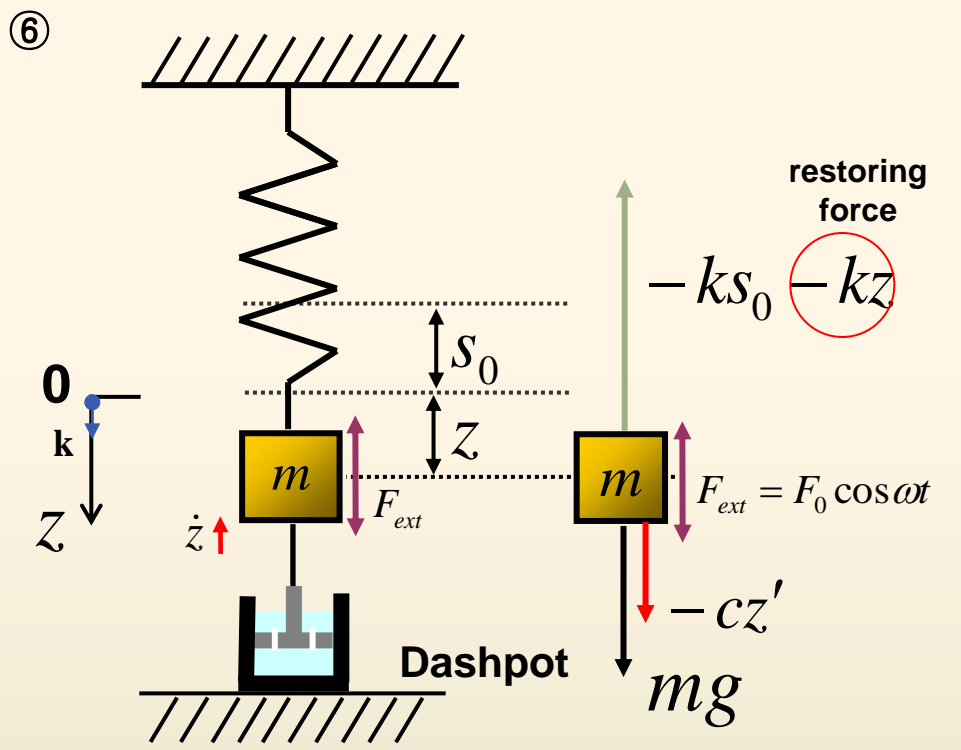
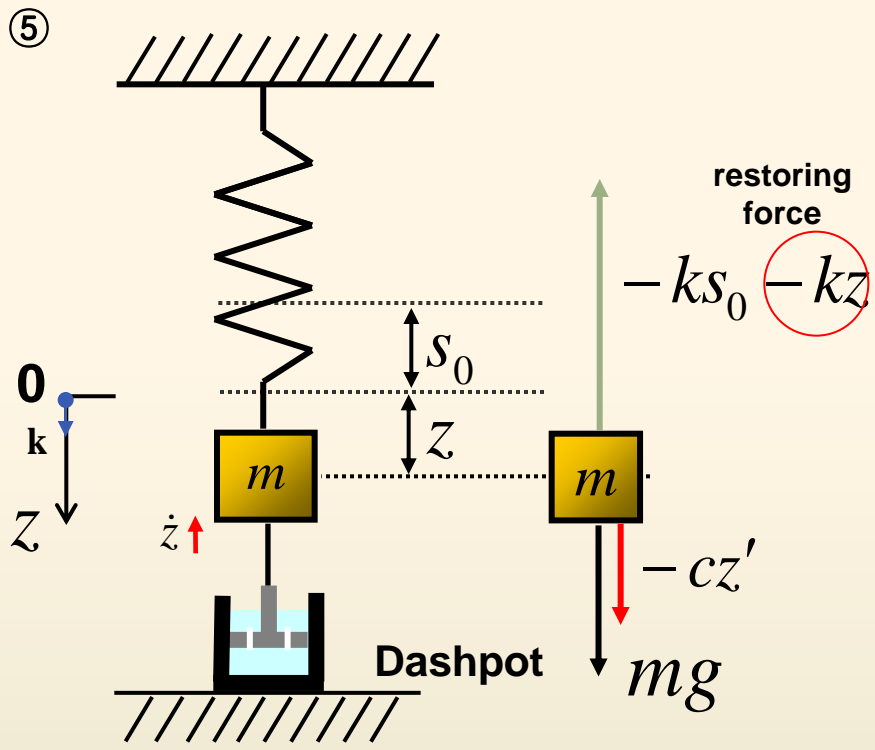
Physical Phenomenon  
 Mathematical Equation

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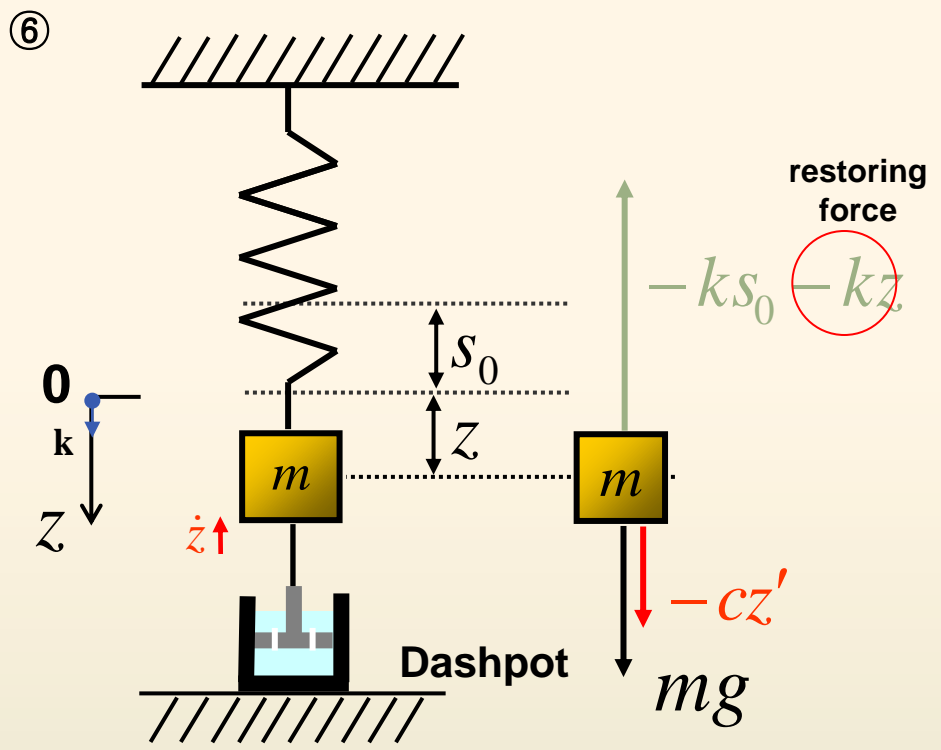
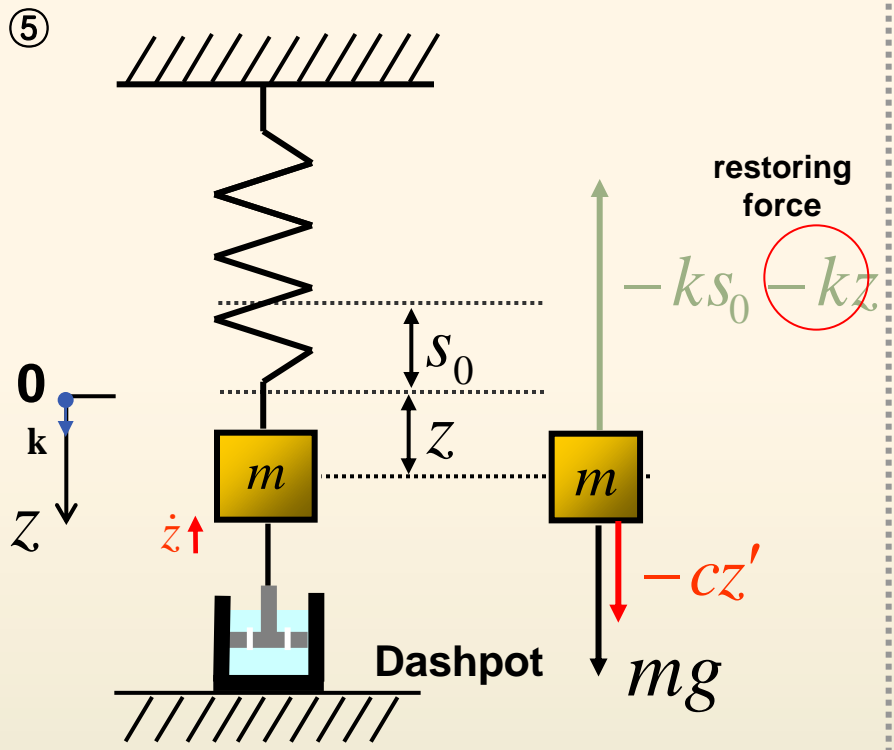
Physical Phenomenon  
 Mathematical Equation

$$mz'' + cz' + kz = 0$$

$$mz'' + cz' + kz = F_0 \cos \omega t$$



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



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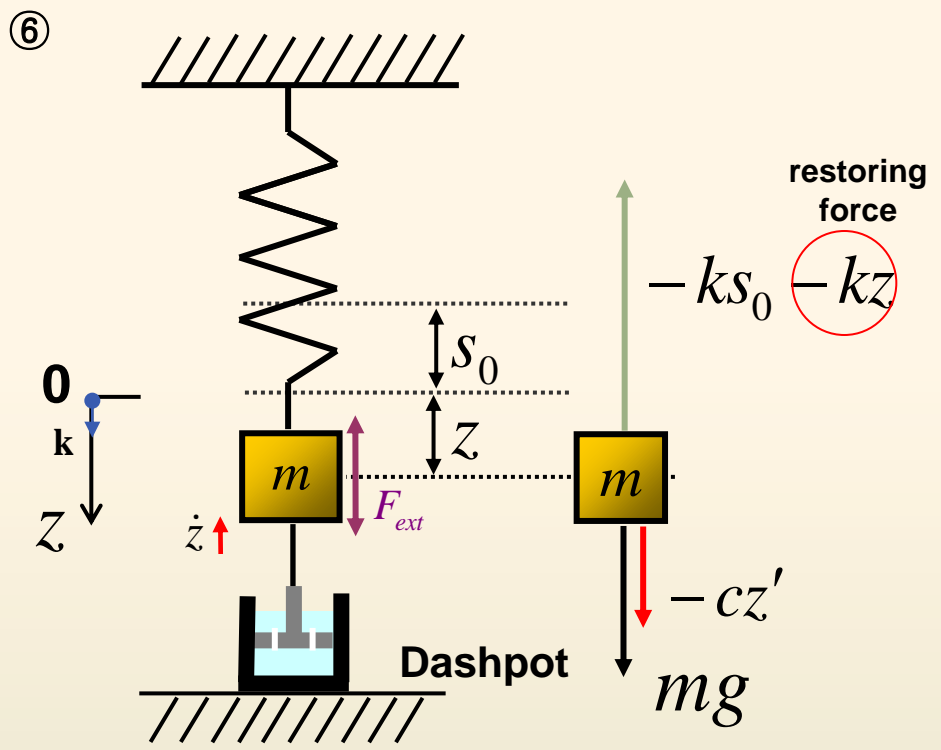
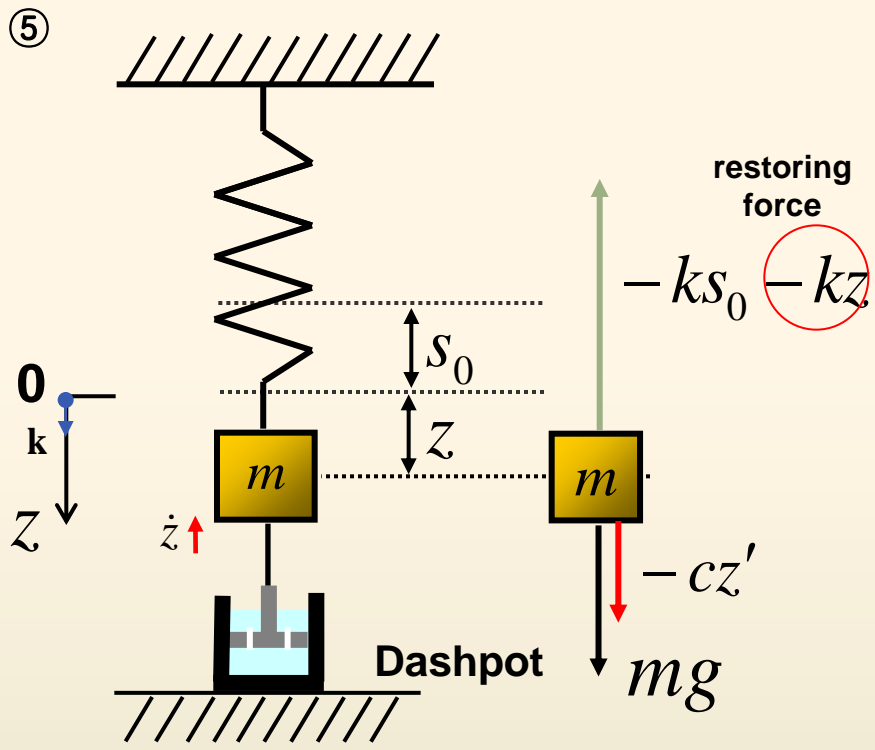
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 Mathematical Equation

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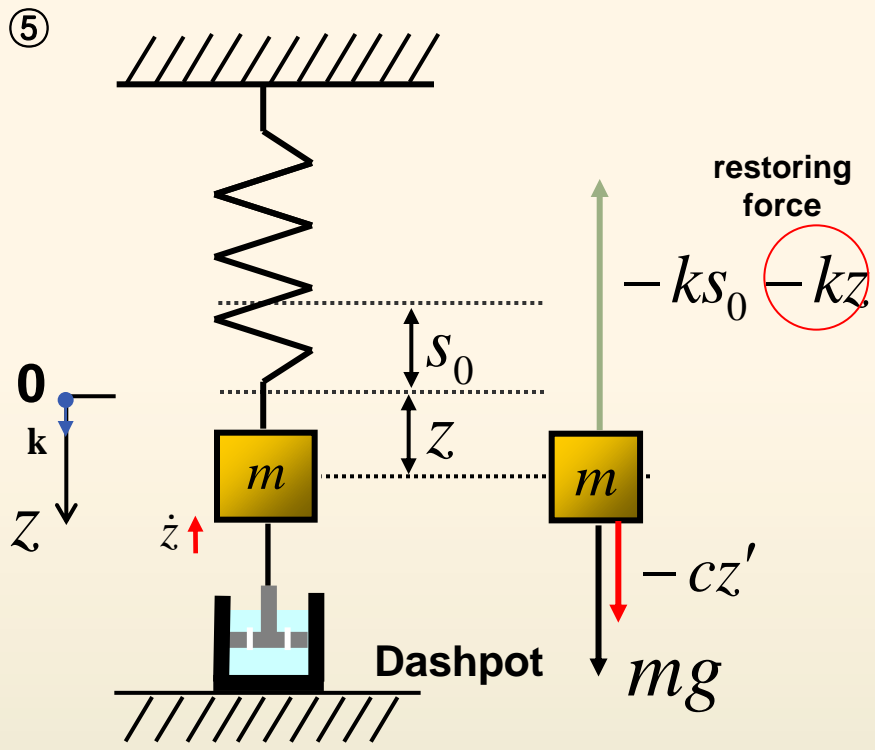
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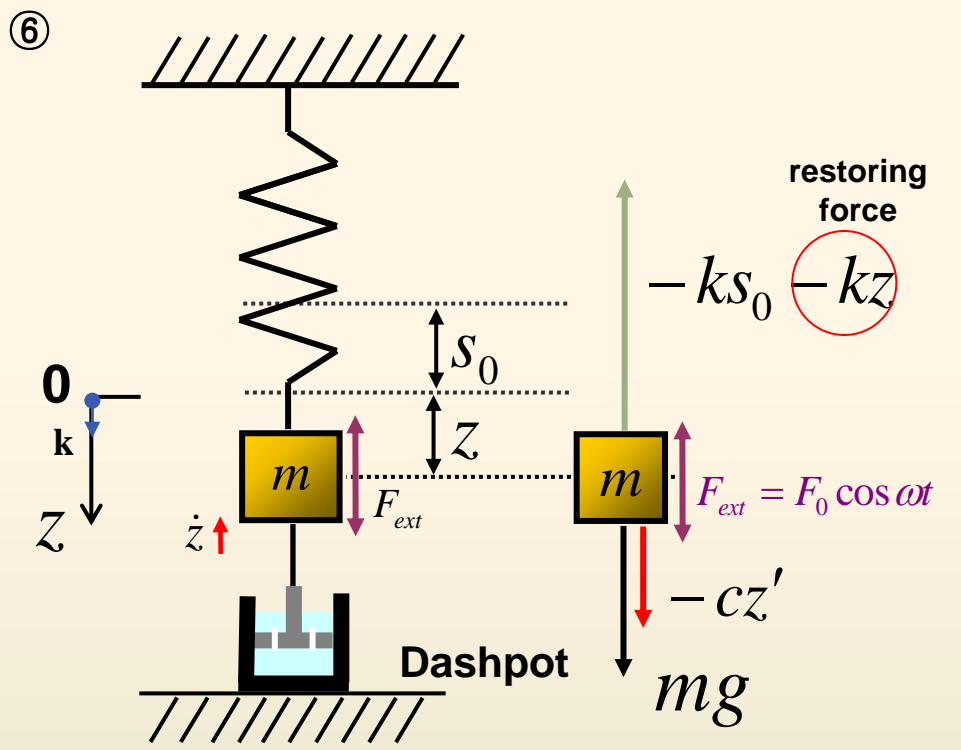
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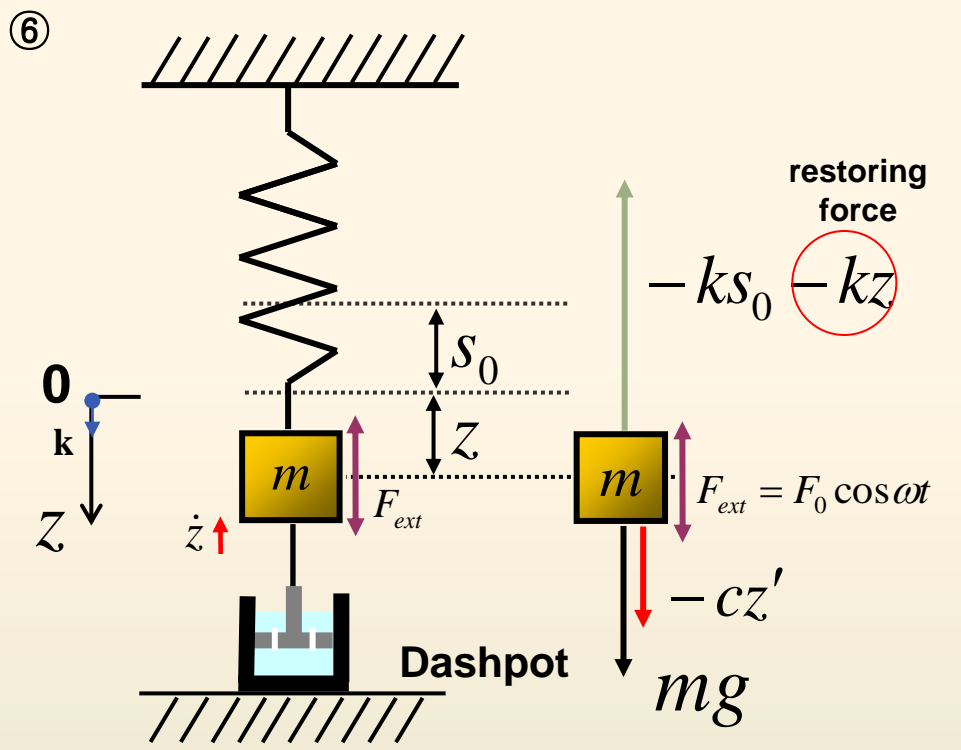
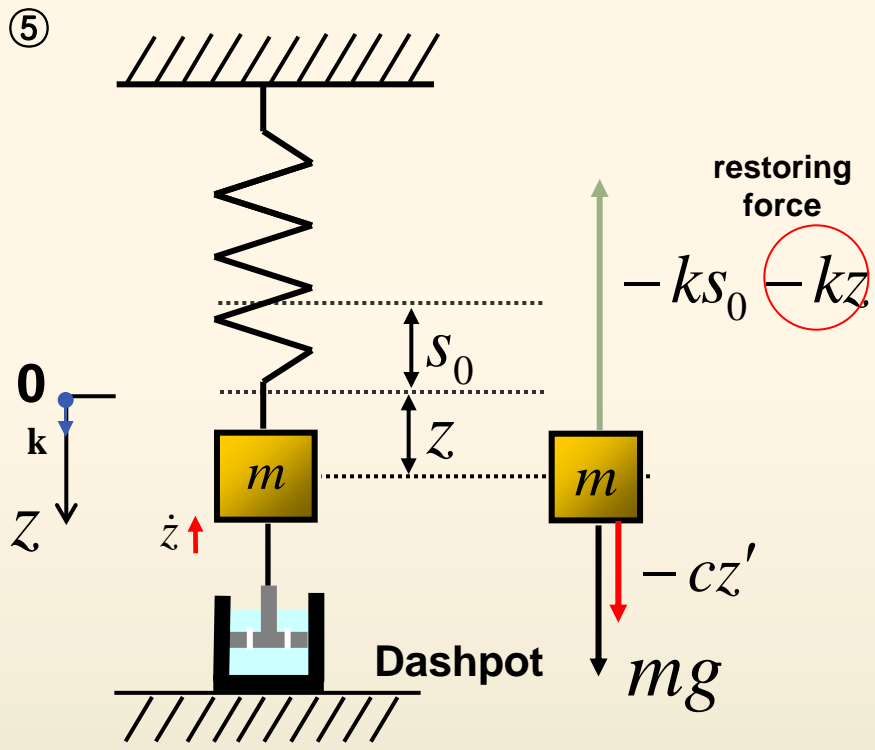
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Physical Phenomenon  
 Mathematical Equation

$$mz'' + cz' + kz = 0$$



# Spring/Mass Systems: Driven Motion $z = z(t), z'' = \frac{d^2z}{dt^2}$



$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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 &= -k\mathbf{z}\mathbf{k} - c\mathbf{z}'\mathbf{k}
 \end{aligned}$$

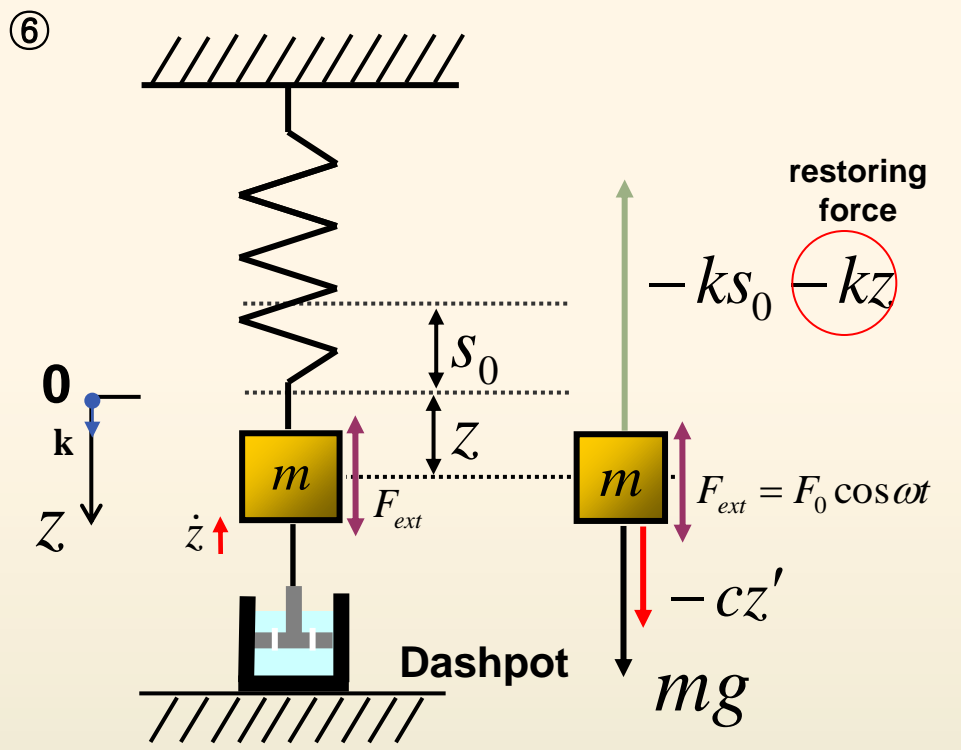
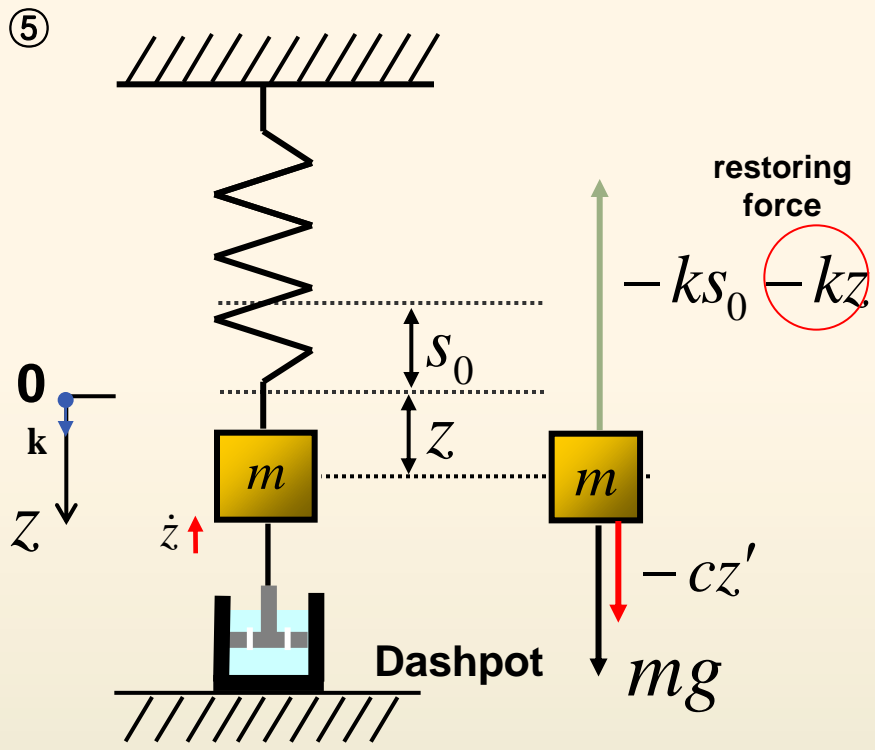
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 &= -k\mathbf{z}\mathbf{k} - c\mathbf{z}'\mathbf{k}
 \end{aligned}$$

Physical Phenomenon  
 Mathematical Equation

$$m\mathbf{z}'' + c\mathbf{z}' + k\mathbf{z} = 0$$



# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2 z}{dt^2}$



$$mz'' = F$$

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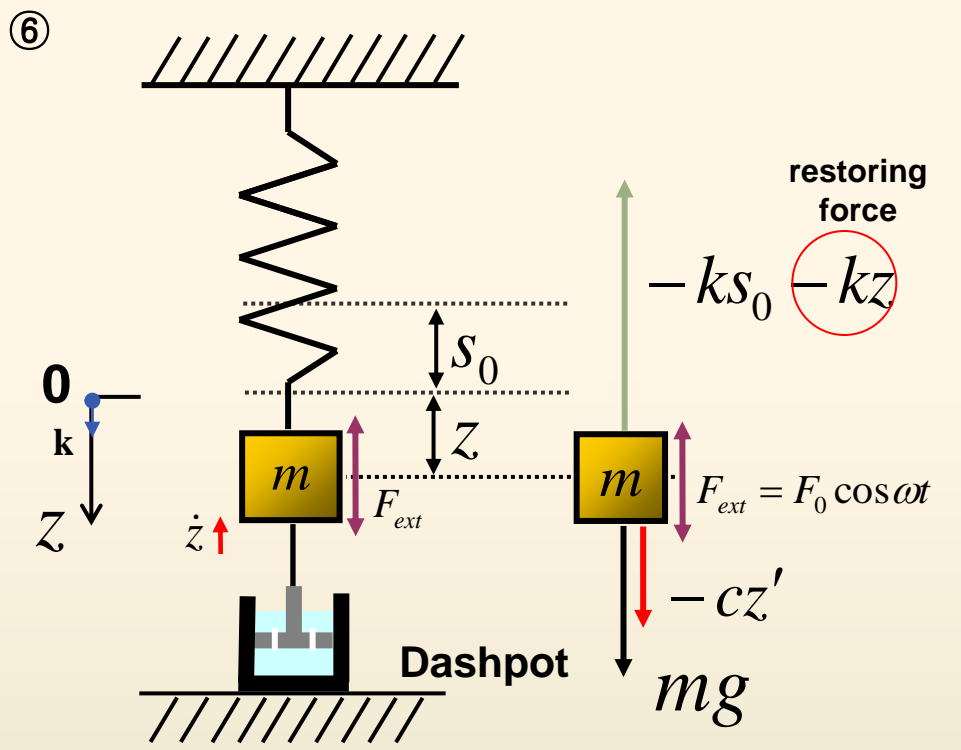
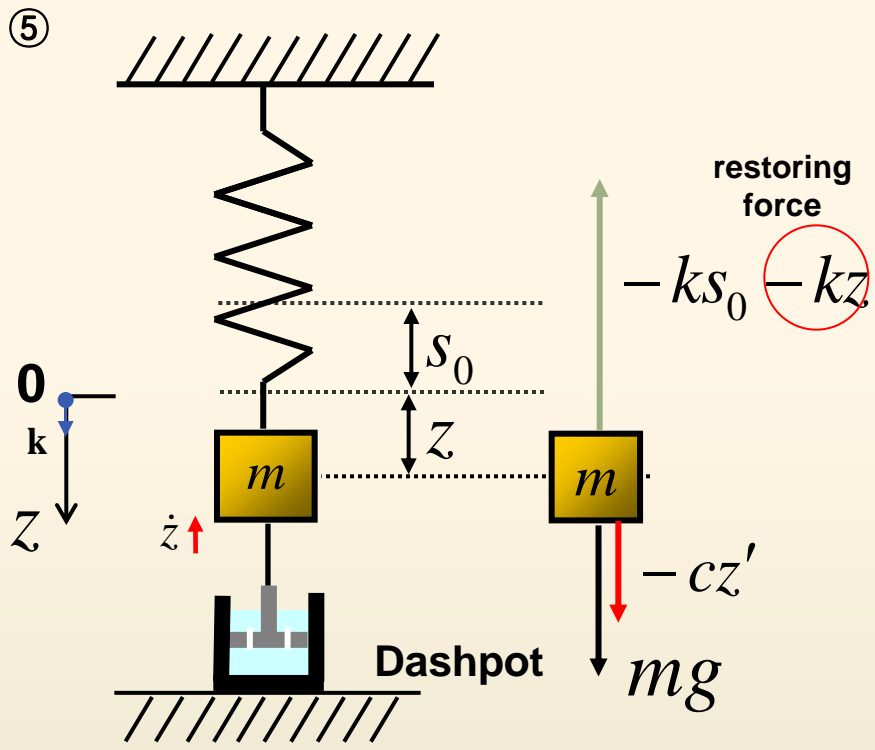
$$= -kz\mathbf{k} - cz'\mathbf{k} + F_0 \cos \omega t$$

Physical Phenomenon  
 Mathematical Equation

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# Spring/Mass Systems: Driven Motion $z = z(t)$ , $z'' = \frac{d^2 z}{dt^2}$



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 \end{aligned}$$

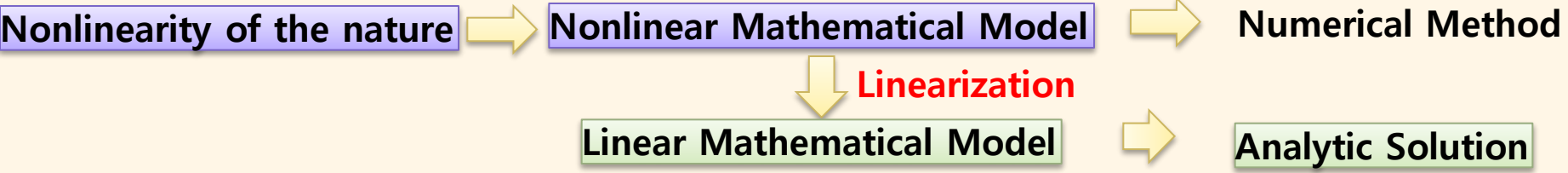
Physical Phenomenon  
 Mathematical Equation

$$m\mathbf{z}'' + c\mathbf{z}' + k\mathbf{z} = 0$$

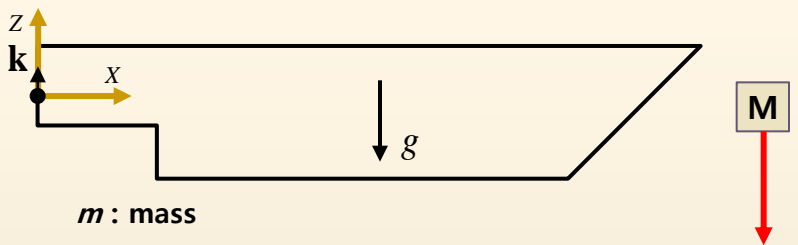
$$m\mathbf{z}'' + c\mathbf{z}' + k\mathbf{z} = \mathbf{F}_0 \cos \omega t$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 1



$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Mass-Spring-Damper system

Diagram of a mass-spring-damper system. A mass  $m$  is suspended from a fixed point by a spring with constant  $k$ . A coordinate  $z$  is defined pointing downwards. Gravity  $g$  is shown acting downwards. The force  $mg$  is shown acting on the mass.

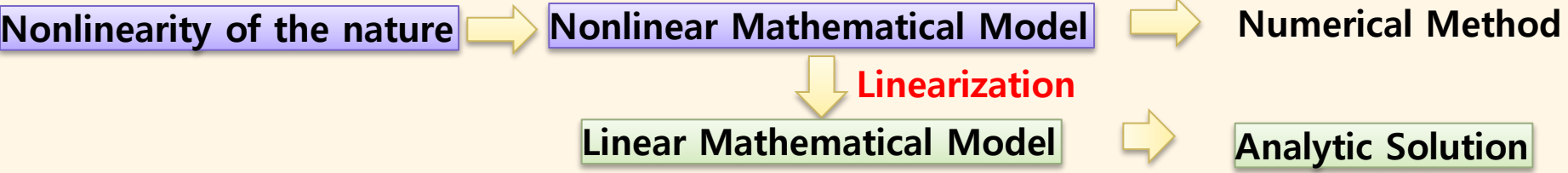
①

By Newton's 2<sup>nd</sup> law,

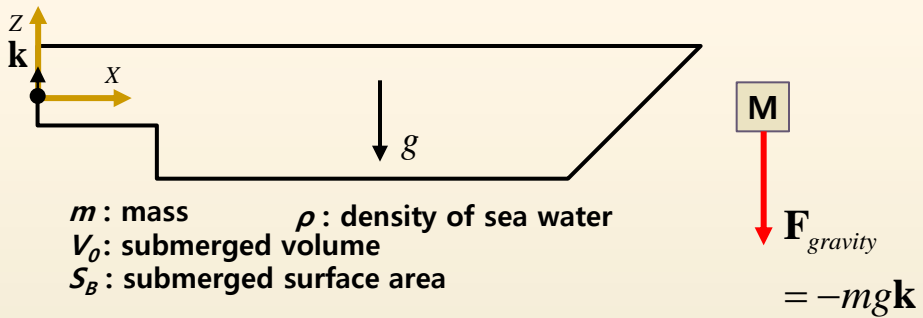
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k}
 \end{aligned}$$




# Nonlinearity



## Ex) Heave Motion of a Ship – step 2



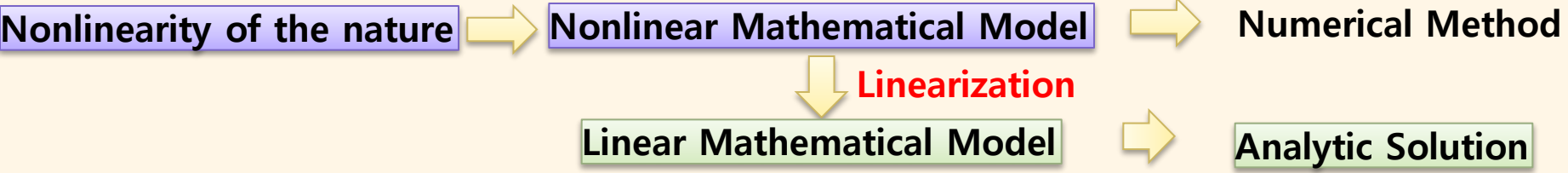
$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Mass-Spring-Damper system

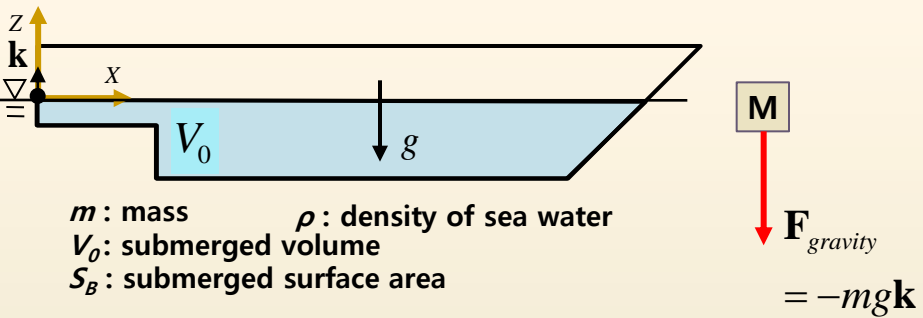
$mz'' = \mathbf{F}$   
 $= mg\mathbf{k} - ks_0\mathbf{k}$   
 $= 0 \quad (\because z'' = 0)$   
 : static equilibrium



# Nonlinearity



## Ex) Heave Motion of a Ship – step 2



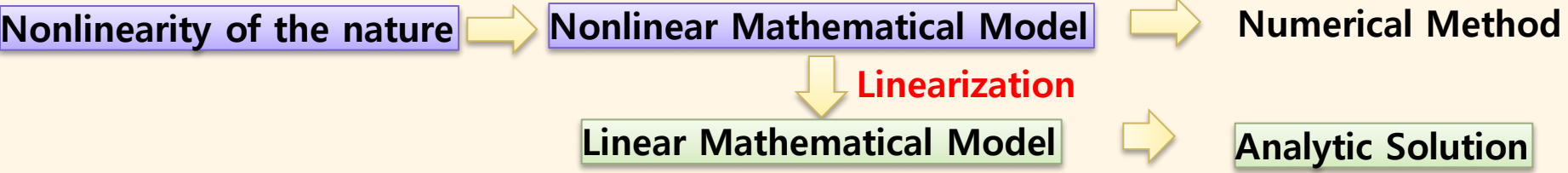
$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
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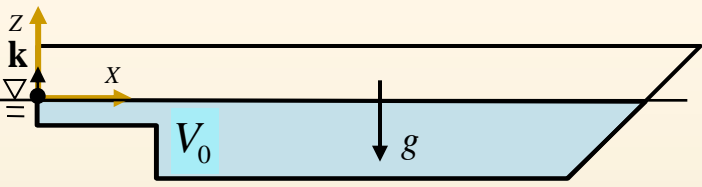
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# Nonlinearity



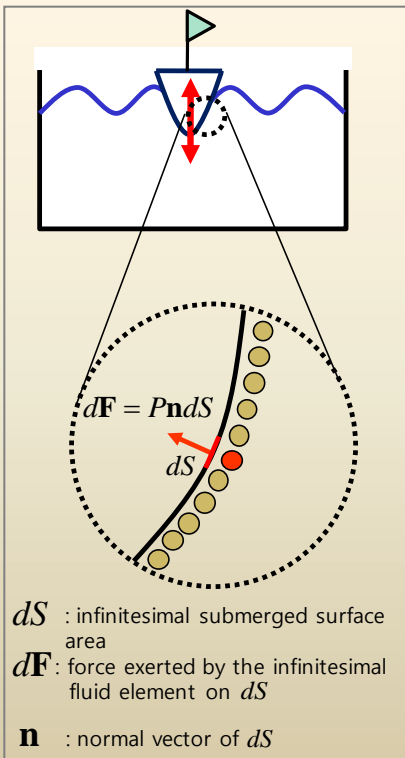
## Ex) Heave Motion of a Ship – step 2



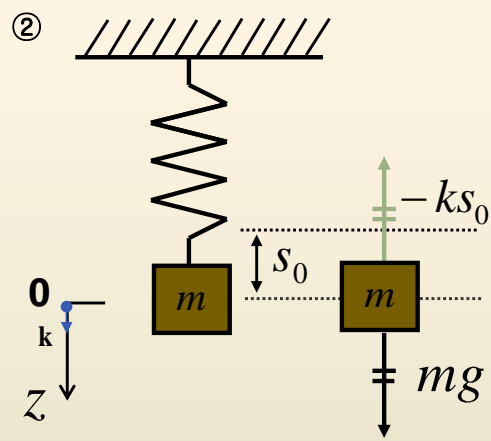
$m$  : mass  
 $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area

$$\begin{aligned}
 & \mathbf{M} \\
 & \downarrow \mathbf{F}_{gravity} \\
 & = -mg\mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
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 \end{aligned}$$



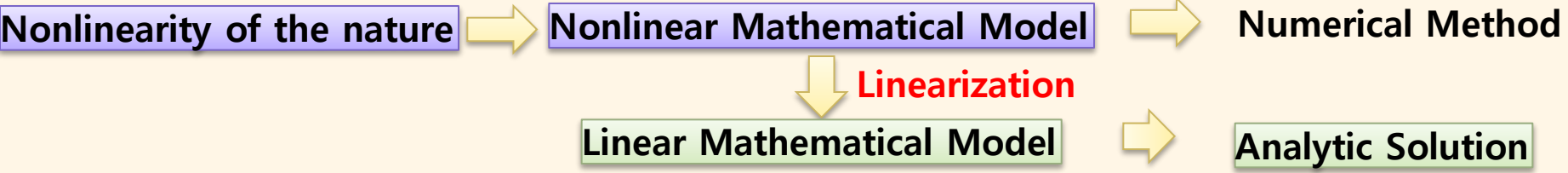
### ✓ Mass-Spring-Damper system



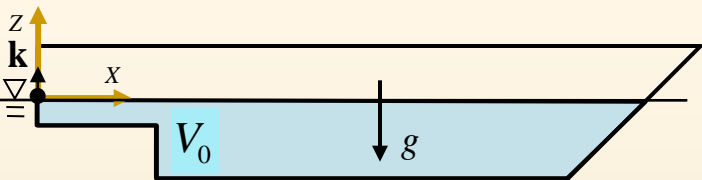
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# Nonlinearity



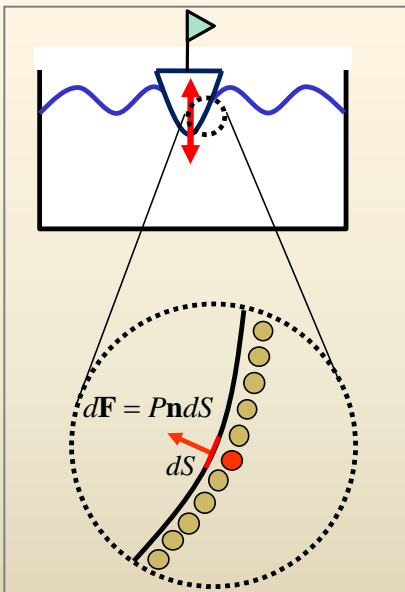
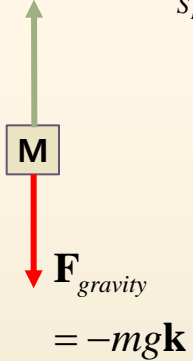
## Ex) Heave Motion of a Ship – step 2



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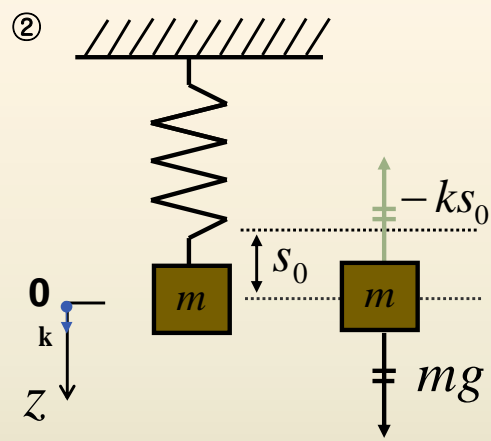
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS = \rho g V_0 \mathbf{k}$$



$dS$  : infinitesimal submerged surface area  
 $d\mathbf{F}$  : force exerted by the infinitesimal fluid element on  $dS$   
 $\mathbf{n}$  : normal vector of  $dS$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

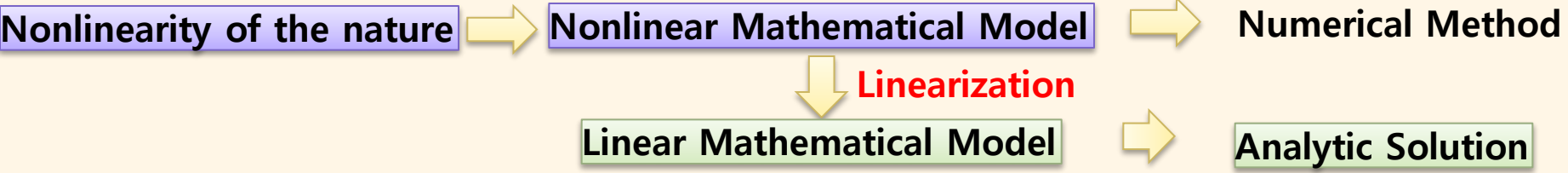
✓ Mass-Spring-Damper system



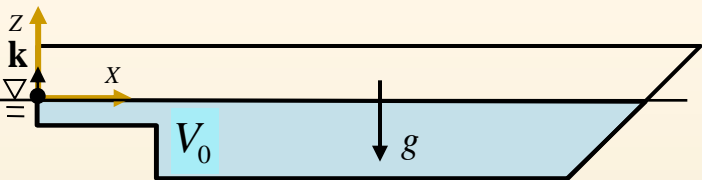
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# Nonlinearity



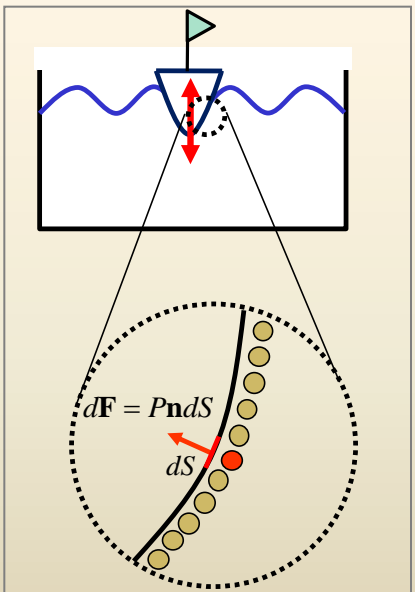
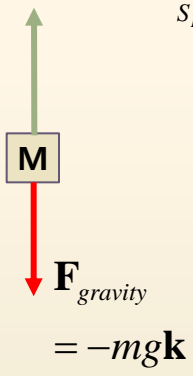
## Ex) Heave Motion of a Ship – step 2



$m$  : mass       $\rho$  : density of sea water  
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 $S_B$  : submerged surface area

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 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

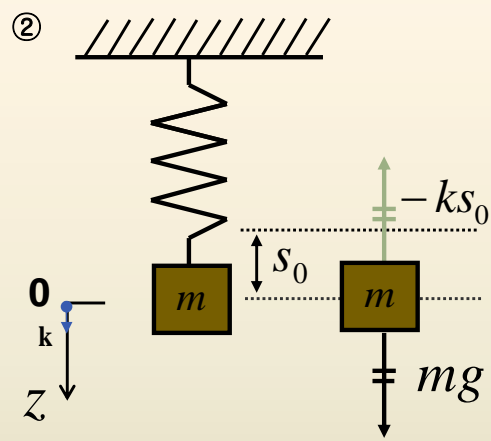
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS = \rho g V_0 \mathbf{k}$$



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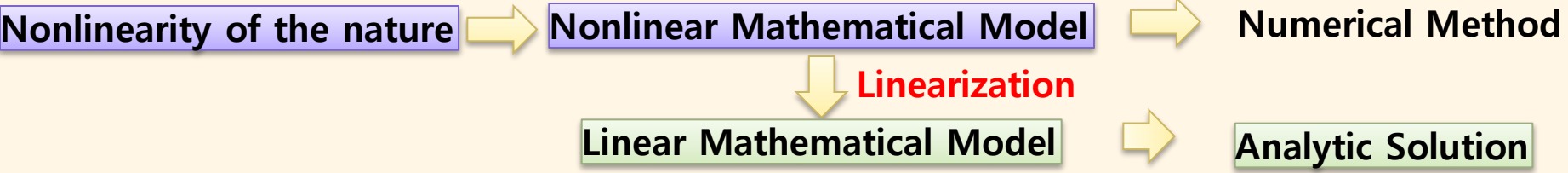
✓ Mass-Spring-Damper system



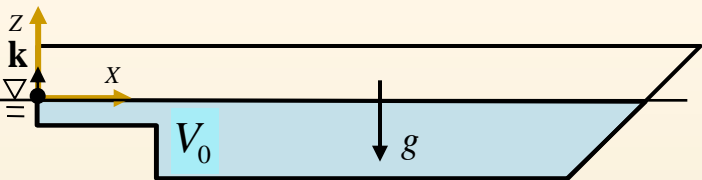
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# Nonlinearity



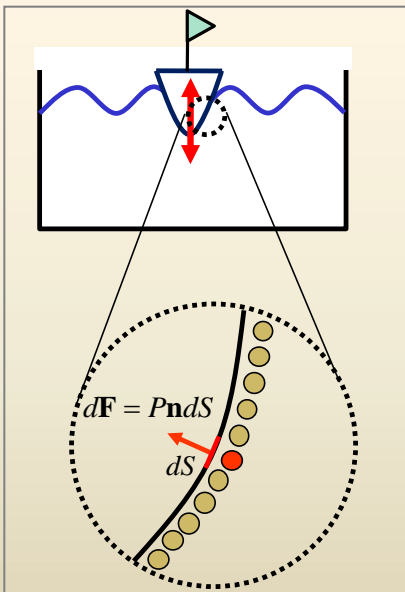
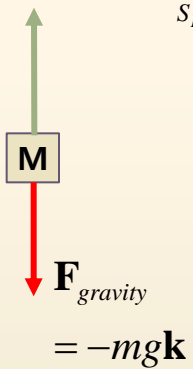
## Ex) Heave Motion of a Ship – step 2



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area

$$\begin{aligned}
 m\ddot{z} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k}
 \end{aligned}$$

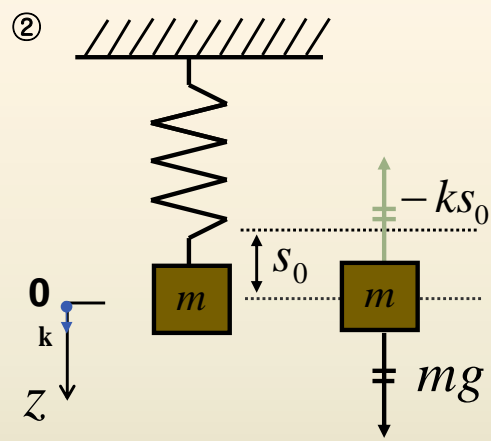
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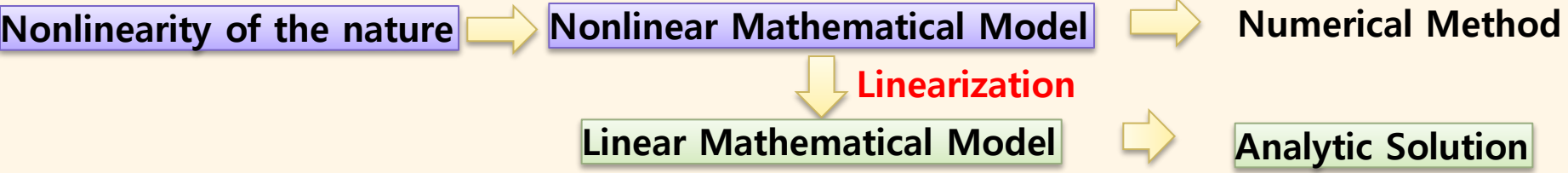
✓ Mass-Spring-Damper system



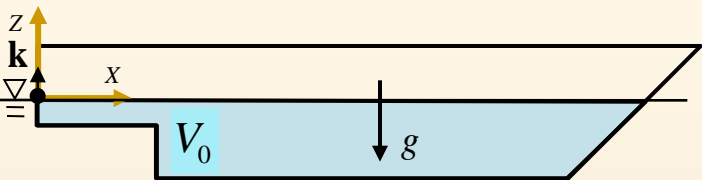
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} \\
 &= 0 \quad (\because z'' = 0) \\
 &: \text{static equilibrium}
 \end{aligned}$$



# Nonlinearity



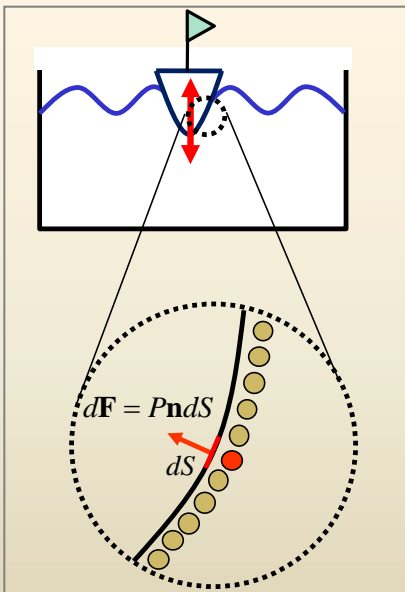
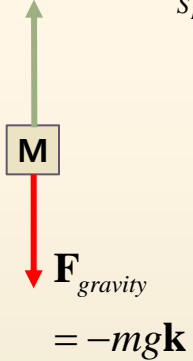
## Ex) Heave Motion of a Ship – step 2



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area

$$\begin{aligned}
 m\ddot{z} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} \\
 &= 0 \quad (\because \ddot{z} = 0) \quad : \text{static equilibrium}
 \end{aligned}$$

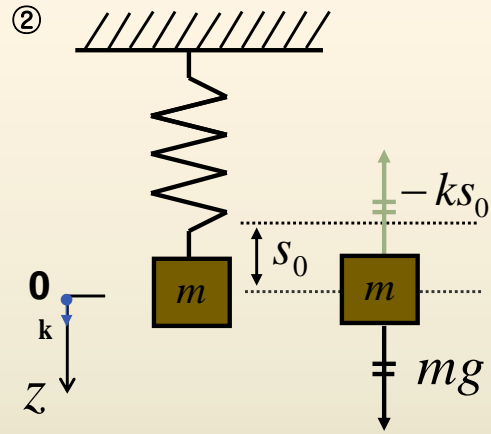
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS = \rho g V_0 \mathbf{k}$$



$dS$  : infinitesimal submerged surface area  
 $d\mathbf{F}$  : force exerted by the infinitesimal fluid element on  $dS$   
 $\mathbf{n}$  : normal vector of  $dS$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

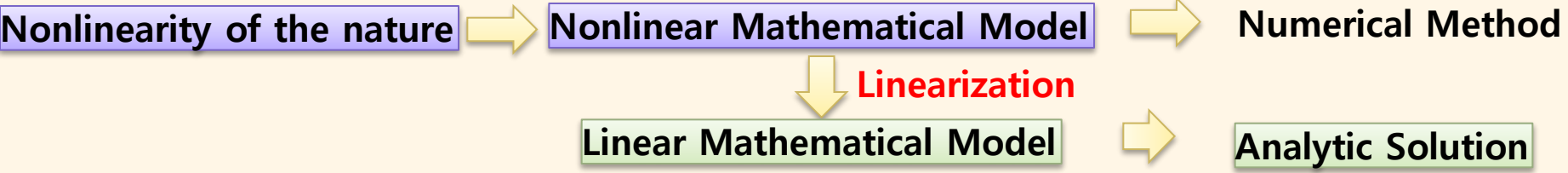
✓ Mass-Spring-Damper system



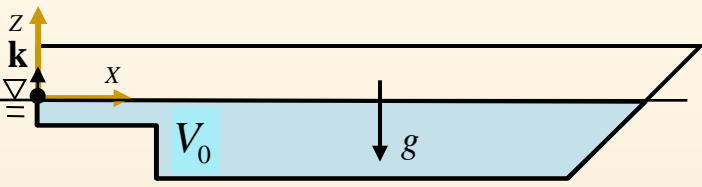
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0 \mathbf{k} \\
 &= 0 \quad (\because z'' = 0) \\
 &: \text{static equilibrium}
 \end{aligned}$$



# Nonlinearity



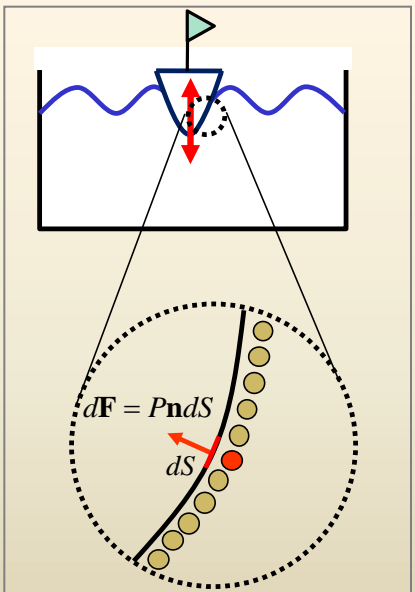
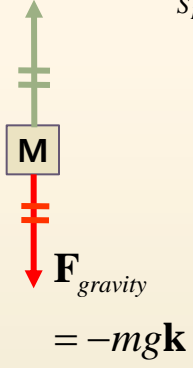
## Ex) Heave Motion of a Ship – step 2



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area

$$\begin{aligned}
 m\ddot{z} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} \\
 &= 0 \quad (\because \ddot{z} = 0) \quad : \text{static equilibrium}
 \end{aligned}$$

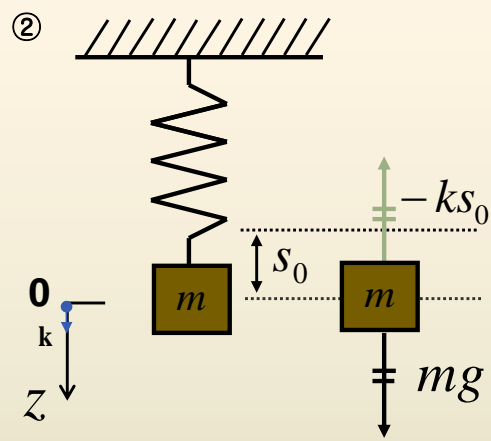
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS = \rho g V_0 \mathbf{k}$$



$dS$  : infinitesimal submerged surface area  
 $d\mathbf{F}$  : force exerted by the infinitesimal fluid element on  $dS$   
 $\mathbf{n}$  : normal vector of  $dS$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

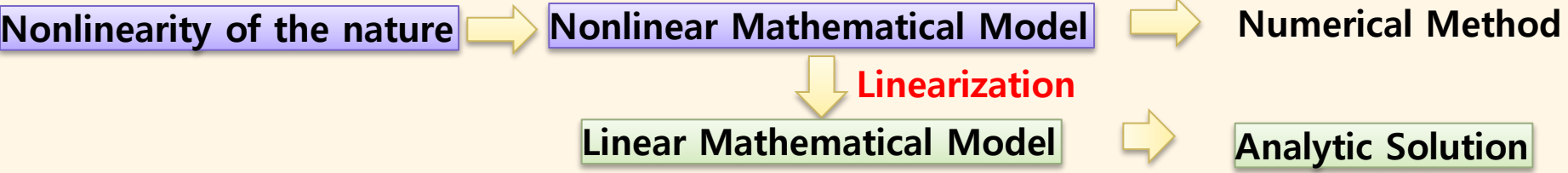


$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0 \mathbf{k} \\
 &= 0 \quad (\because z'' = 0) \\
 &: \text{static equilibrium}
 \end{aligned}$$

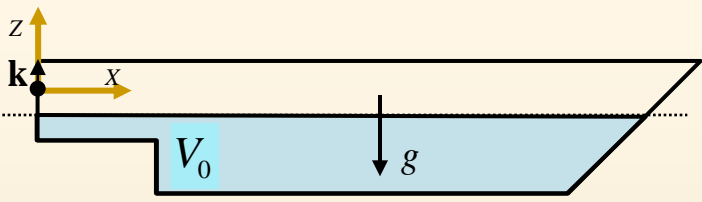




# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $Awp$  : waterplane area

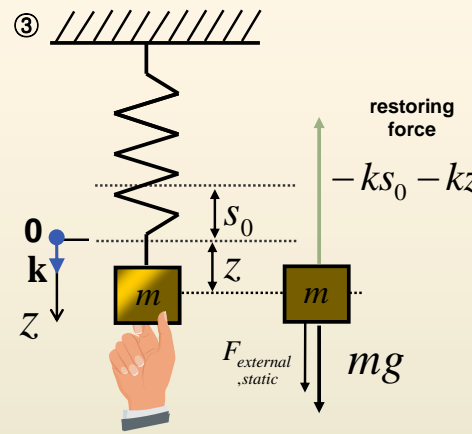
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS$$

$$\mathbf{F}_{gravity} = -mg\mathbf{k}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

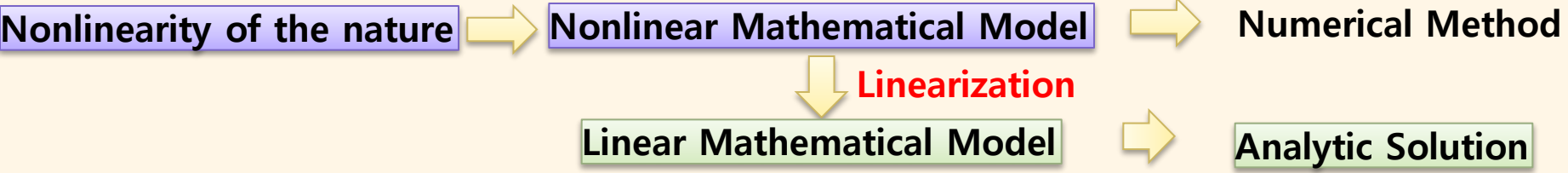
### ✓ Mass-Spring-Damper system



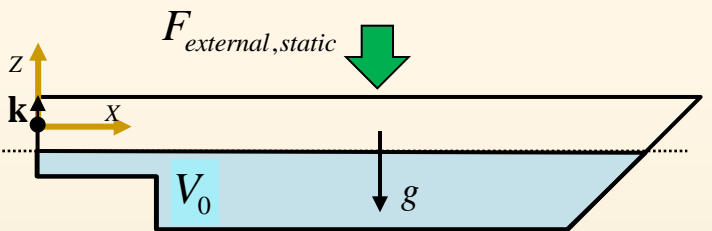
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $Awp$  : waterplane area

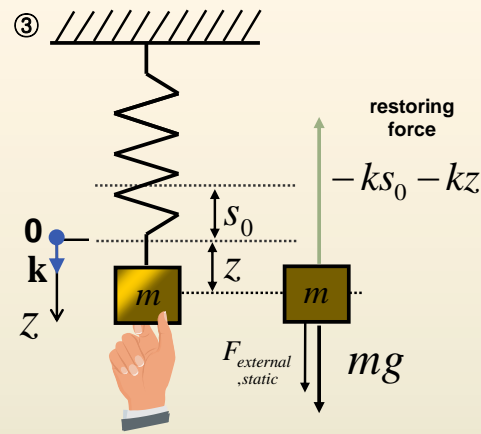
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS$$

$$\mathbf{F}_{gravity} = -mg\mathbf{k}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

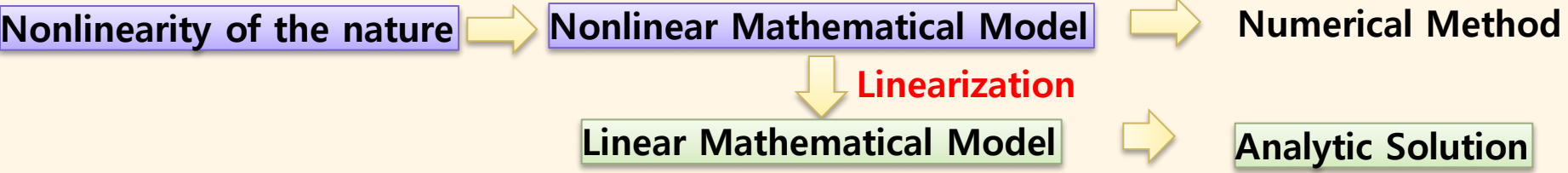
### ✓ Mass-Spring-Damper system



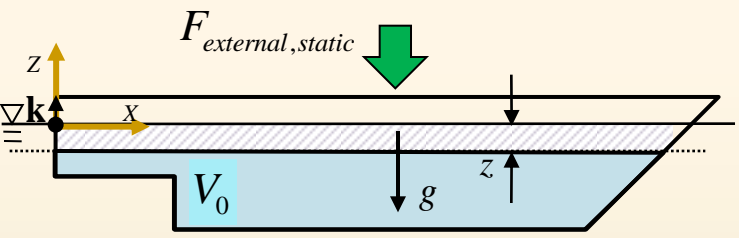
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $Awp$  : waterplane area

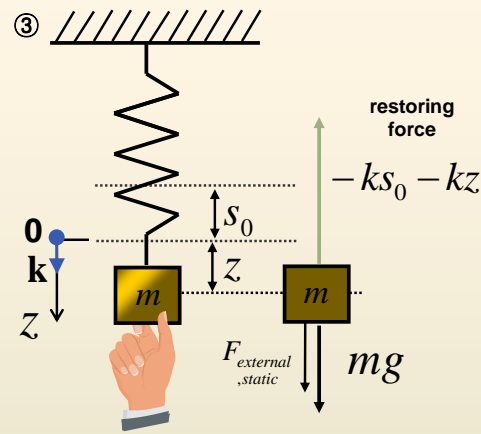
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS$$

$$\mathbf{F}_{gravity} = -mg\mathbf{k}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

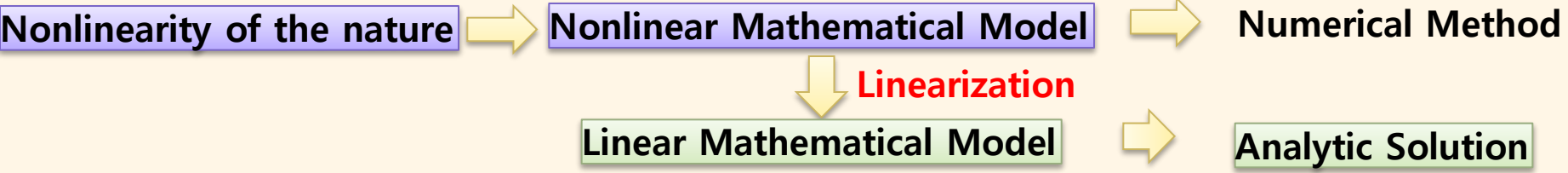
### ✓ Mass-Spring-Damper system



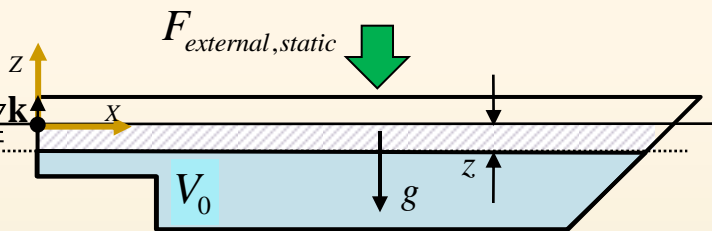
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



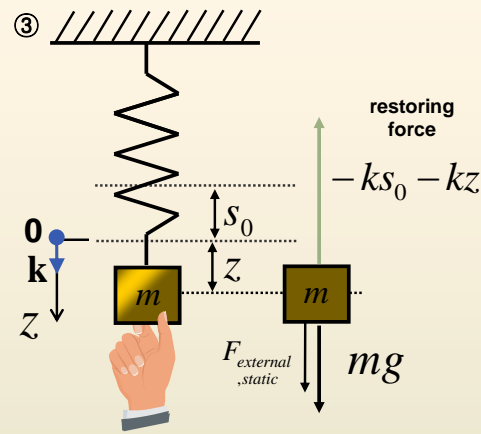
$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $Awp$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

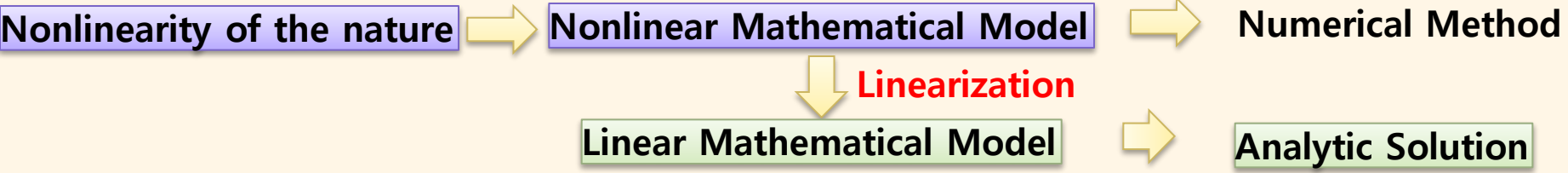
### ✓ Mass-Spring-Damper system



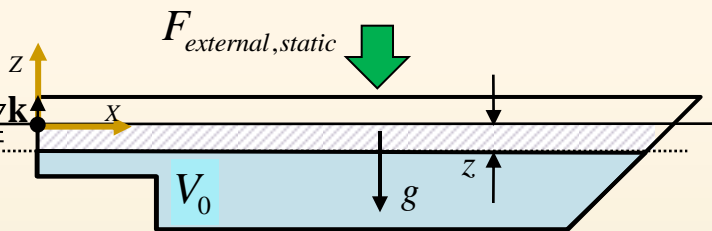
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity

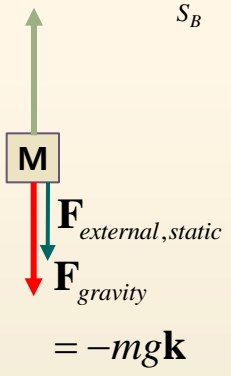


## Ex) Heave Motion of a Ship – step 3



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $Awp$  : waterplane area

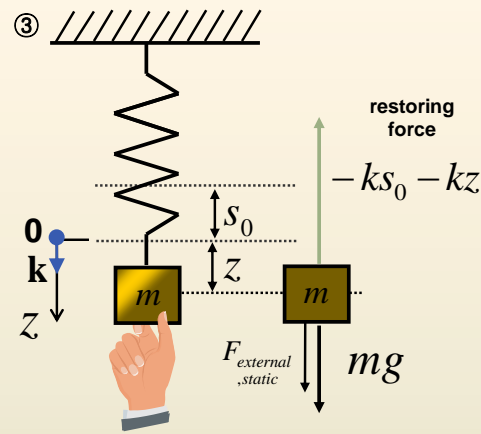
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS$$



$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

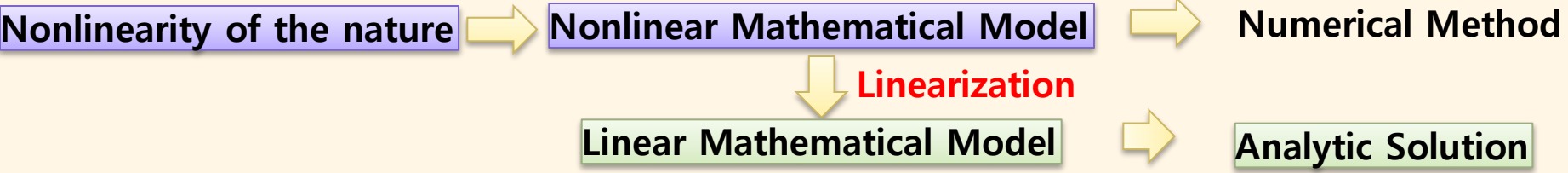
### ✓ Mass-Spring-Damper system



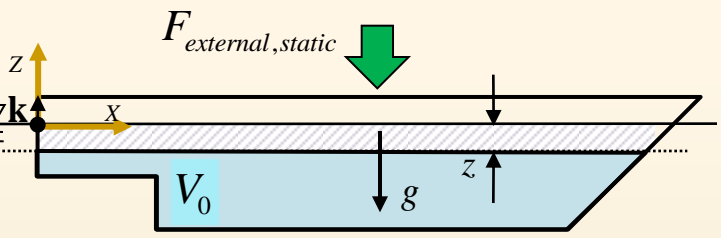
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $Awp$  : waterplane area

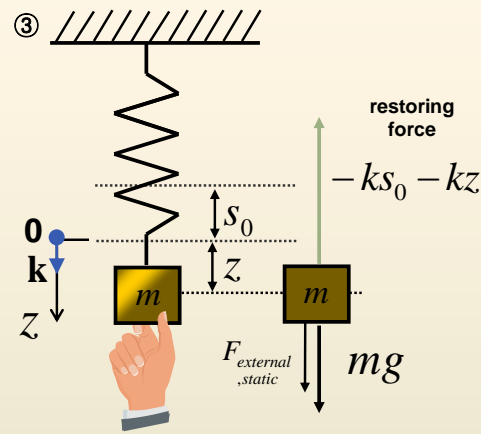
$$\mathbf{F}_{static} = \iint_{S_B} P_{static} \mathbf{n} dS$$

$$\begin{aligned}
 & \mathbf{F}_{external,static} \\
 & \mathbf{F}_{gravity} \\
 & = -mg\mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

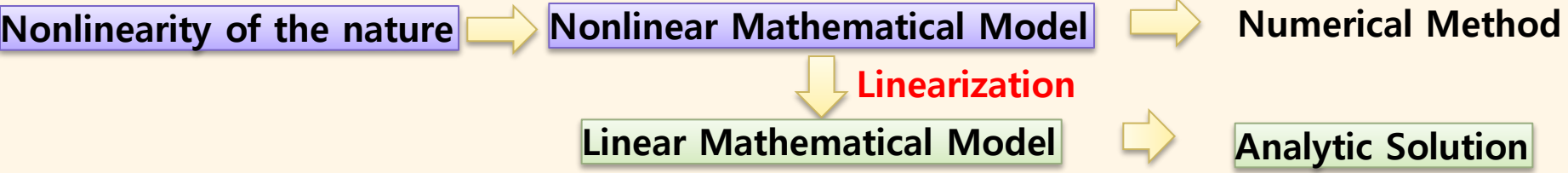
### ✓ Mass-Spring-Damper system



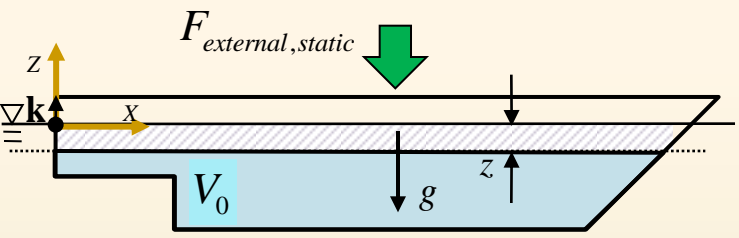
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



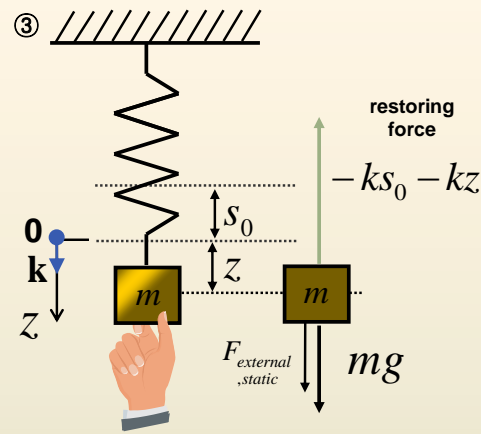
$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $Awp$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 &\text{additional bouyancy caused by additional displacement } z \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

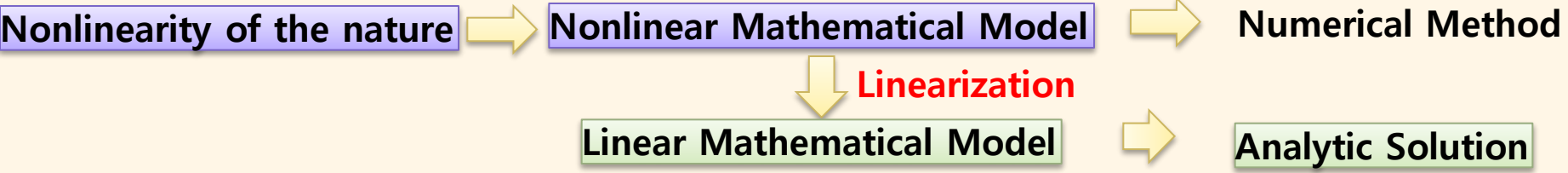
### ✓ Mass-Spring-Damper system



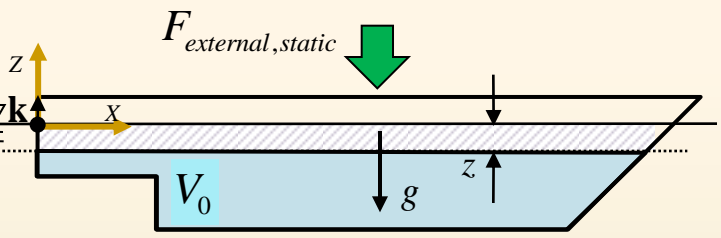
$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



- $m$ : mass
- $\rho$ : density of sea water
- $V_0$ : submerged volume
- $S_B$ : submerged surface area
- $Awp$ : waterplane area

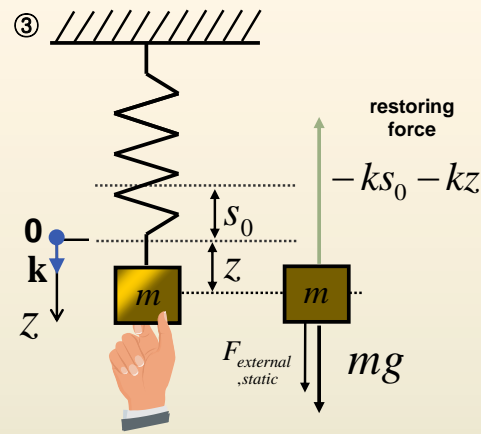
$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 &\text{additional bouyancy caused by additional displacement } z \\
 \mathbf{F}_{external,static} &= -mg\mathbf{k}
 \end{aligned}$$

if, z is small

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

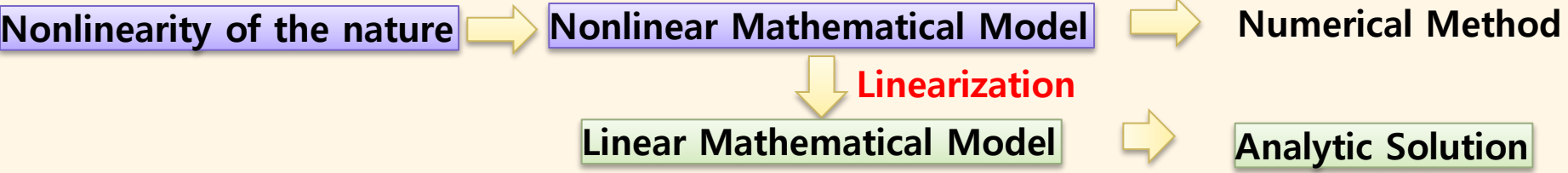


$$\begin{aligned}
 mz'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$

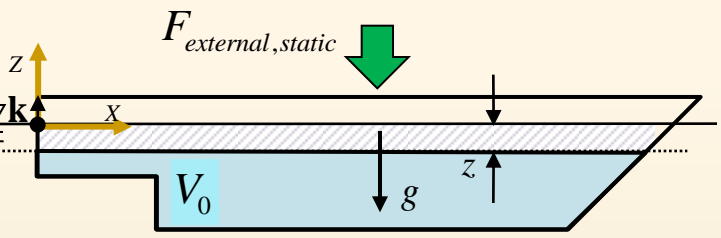




# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ buoyancy} \\
 \mathbf{F}_{external,static} &= -mg\mathbf{k}
 \end{aligned}$$

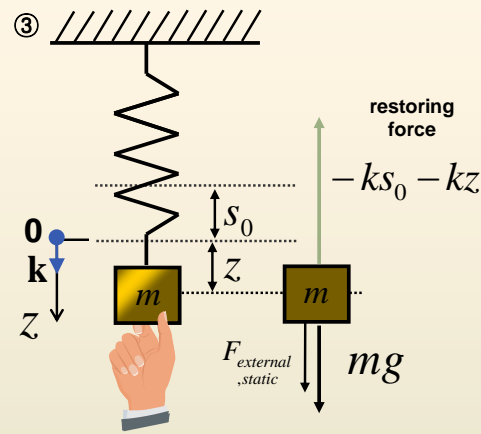
additional buoyancy caused by additional displacement  $z$

if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ buoyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 &, k = \rho g A_{WP}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

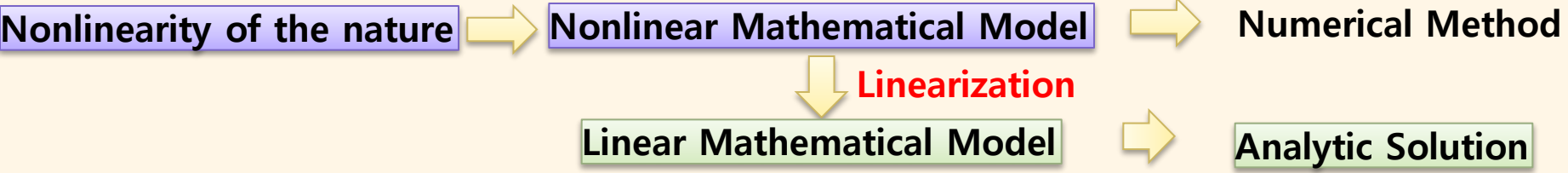
✓ Mass-Spring-Damper system



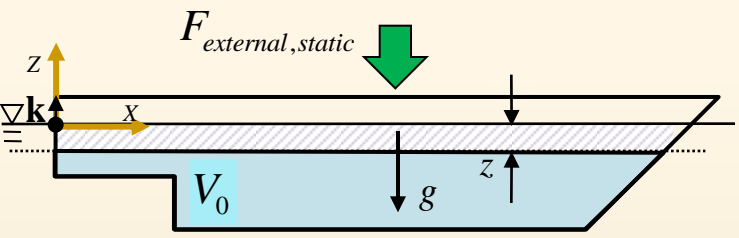
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ buoyancy} \\
 \mathbf{F}_{external,static} &= -mg\mathbf{k}
 \end{aligned}$$

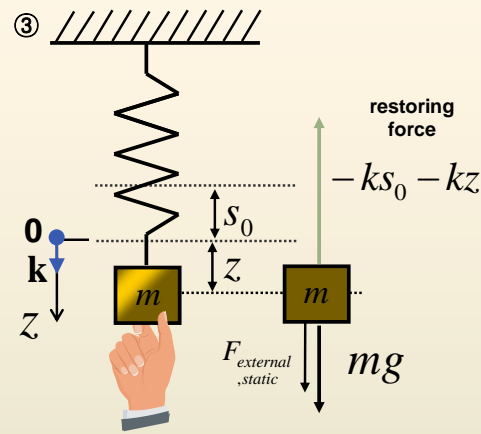
additional buoyancy caused by additional displacement  $\mathbf{z}$

if,  $\mathbf{z}$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ buoyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

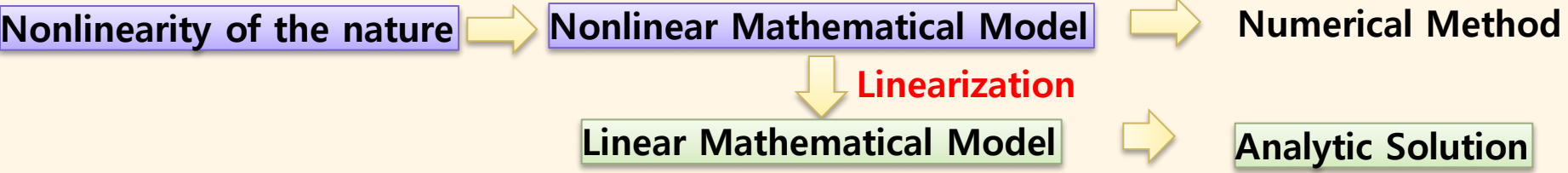
### ✓ Mass-Spring-Damper system



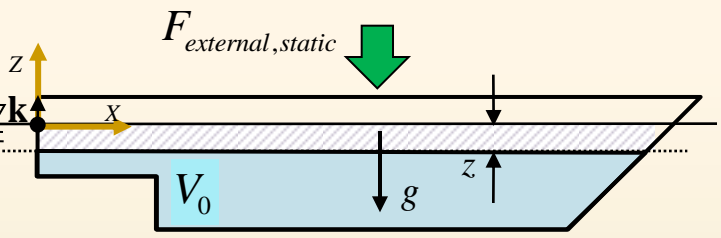
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

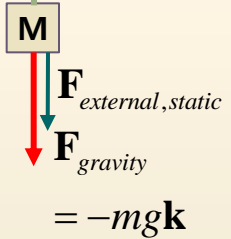
$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ buoyancy}
 \end{aligned}$$

additional buoyancy caused by additional displacement  $z$

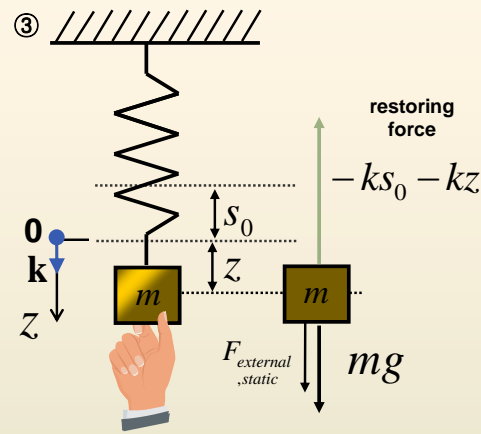
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ buoyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$



✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

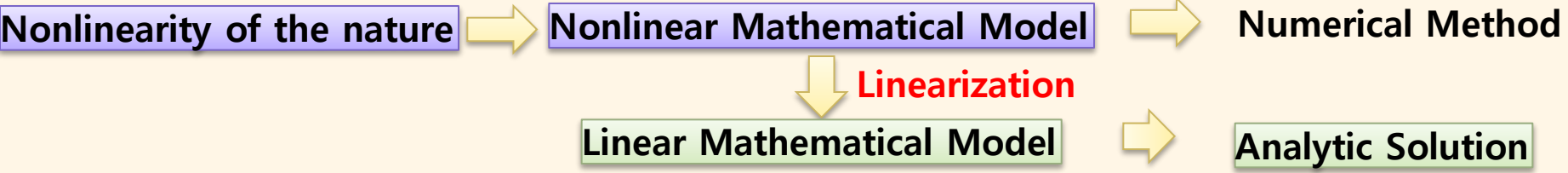
✓ Mass-Spring-Damper system



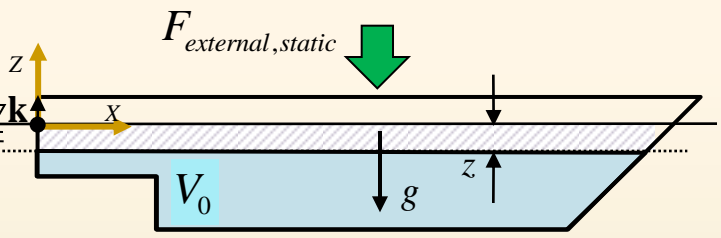
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ buoyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

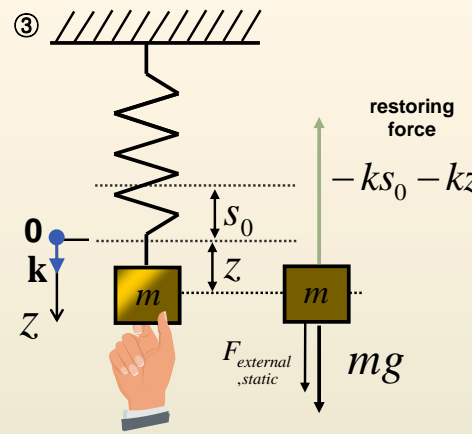
additional buoyancy caused by additional displacement  $\mathbf{z}$

if,  $\mathbf{z}$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ buoyancy} &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z} \\
 &, k = \rho g A_{wp}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

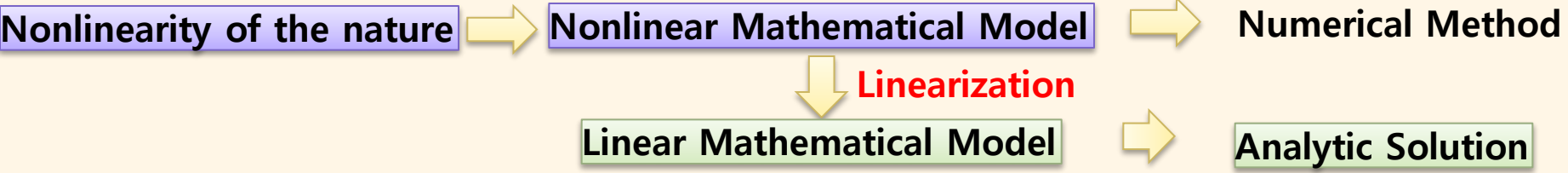
### ✓ Mass-Spring-Damper system



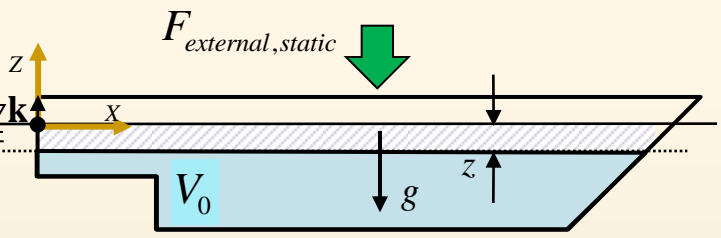
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}
 \end{aligned}$$

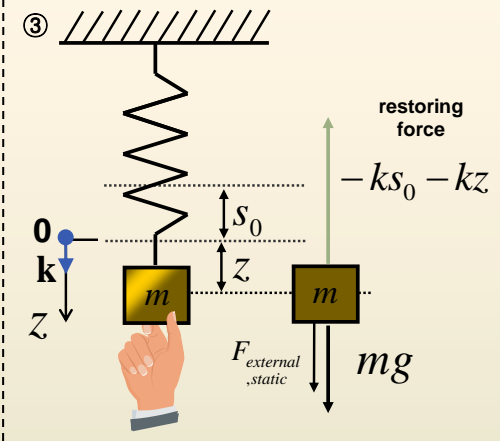
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ buoyancy}
 \end{aligned}$$

additional buoyancy caused by additional displacement  $z$

if,  $z$  is small  
 $\mathbf{F}_{additional\ buoyancy}$   
 $= -\rho g A_{WP} \mathbf{z}$   
 $= -k\mathbf{z}$   
 $, k = \rho g A_{WP}$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

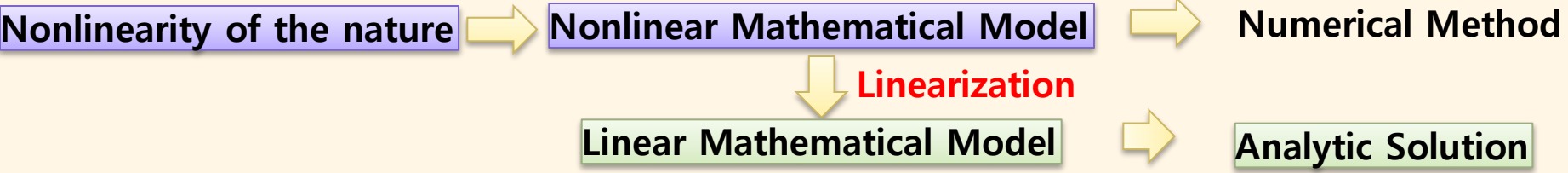
### ✓ Mass-Spring-Damper system



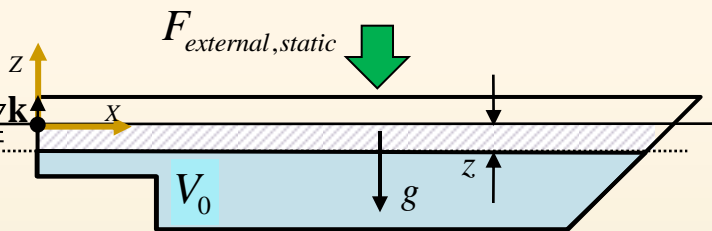
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 3



- $m$  : mass
- $\rho$  : density of sea water
- $V_0$  : submerged volume
- $S_B$  : submerged surface area
- $A_{wp}$  : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

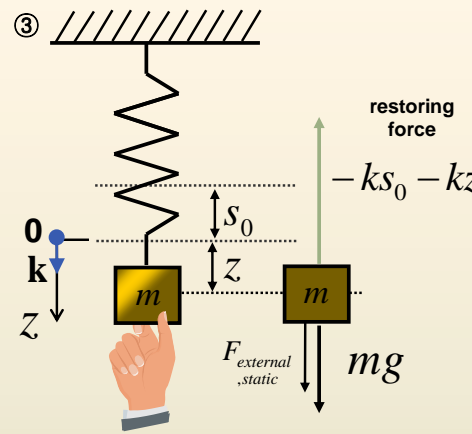
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ buoyancy} \\
 &\text{additional buoyancy caused by additional displacement } z \\
 \mathbf{F}_{external,static} &= -mg\mathbf{k}
 \end{aligned}$$

if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ buoyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

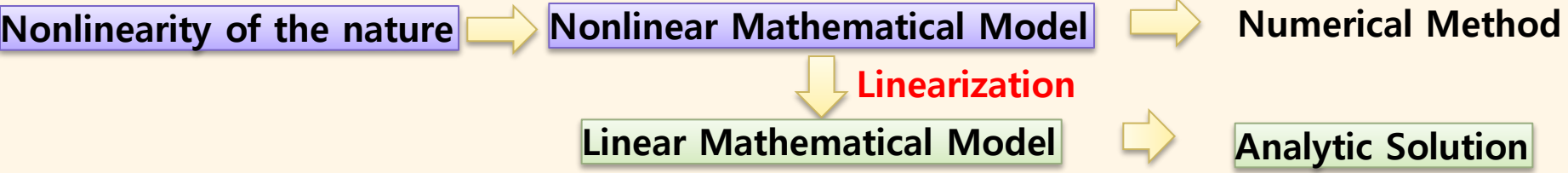
✓ Mass-Spring-Damper system



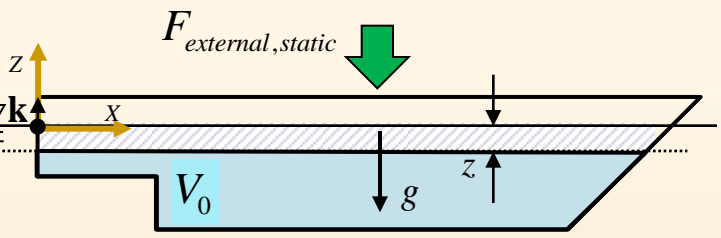
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= 0 \quad (\because z'' = 0)
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $z$

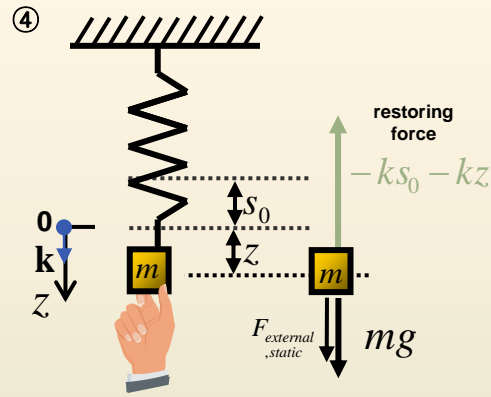
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{WP} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

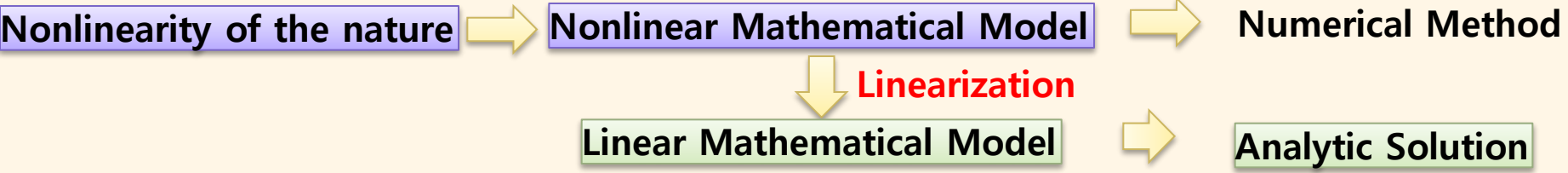
✓ Mass-Spring-Damper system



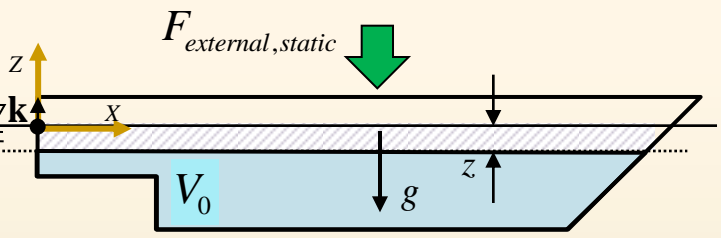
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - k\mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $z$

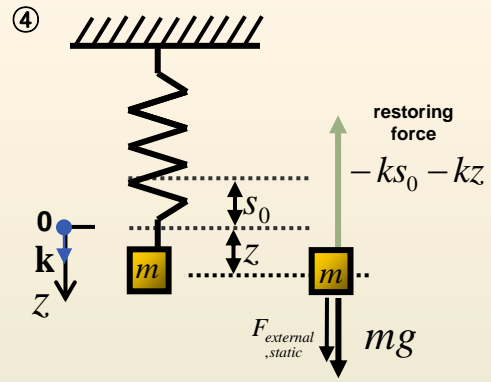
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{WP} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

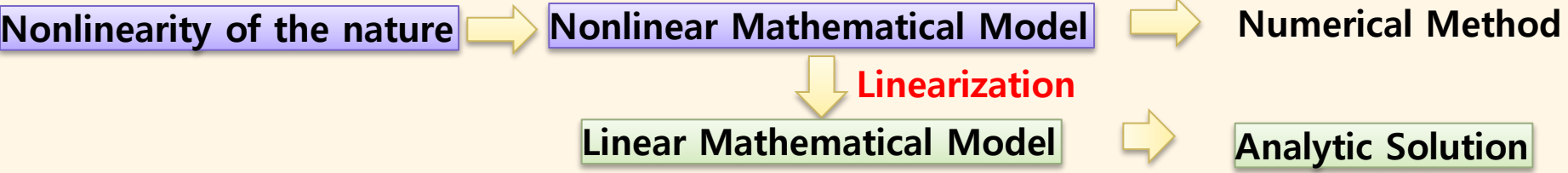


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static}
 \end{aligned}$$

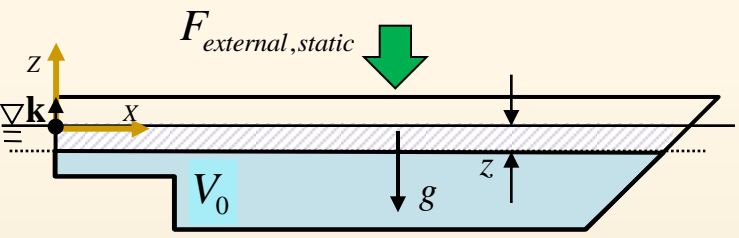




# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $z$

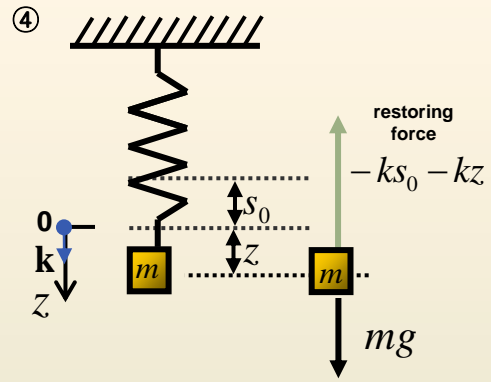
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{wp}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{wp} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

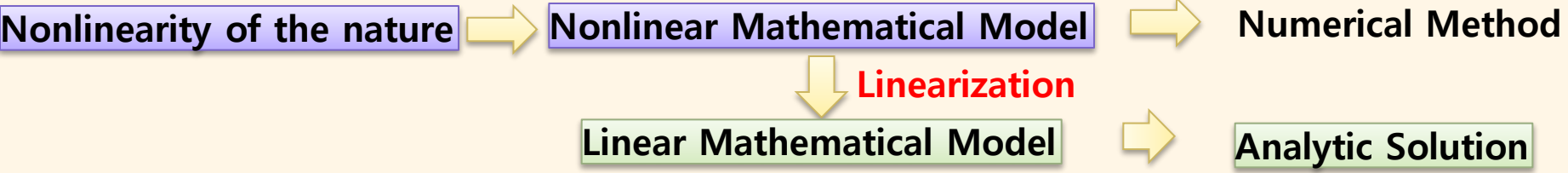
✓ Mass-Spring-Damper system



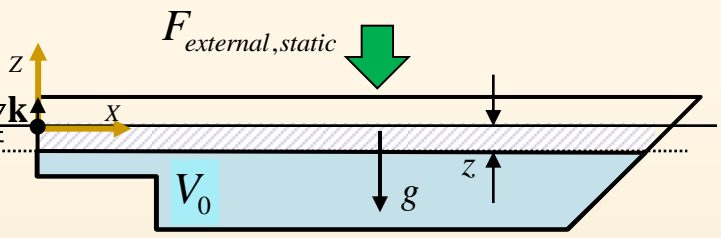
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} + \mathbf{F}_{external,static} \\
 &= -kz\mathbf{k} + \mathbf{F}_{external,static}
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $z$

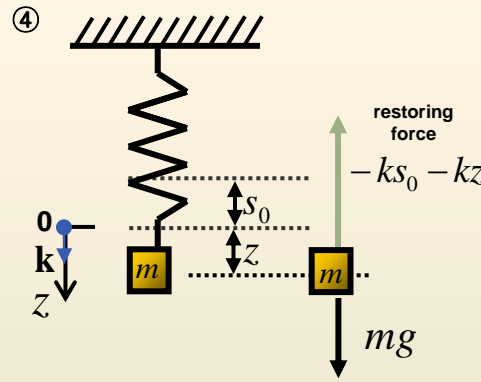
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{WP} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

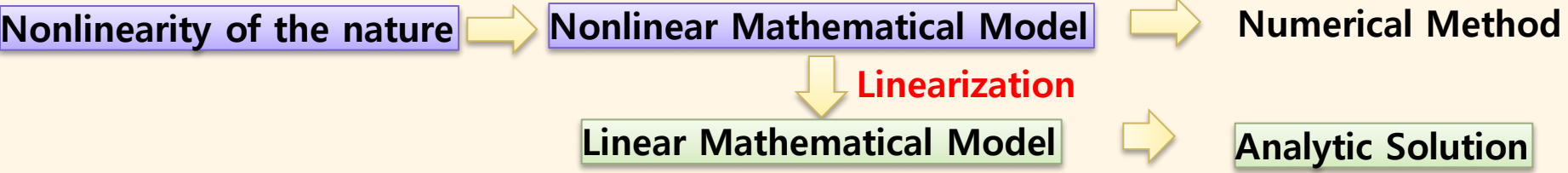
✓ Mass-Spring-Damper system



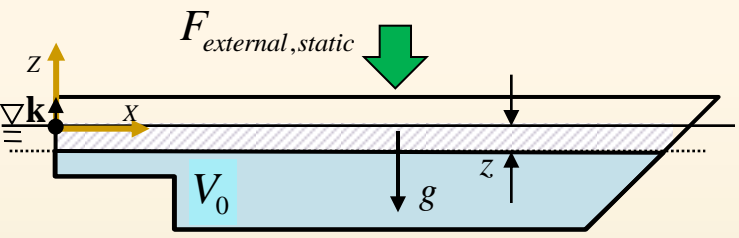
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $z$

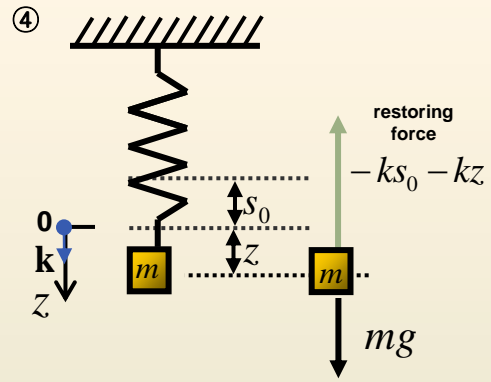
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{WP} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

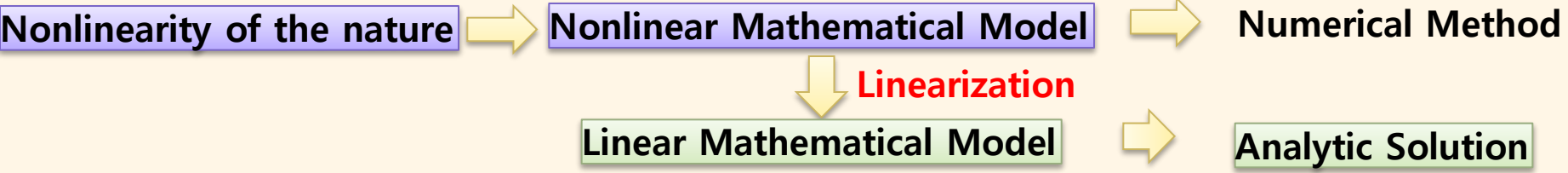


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

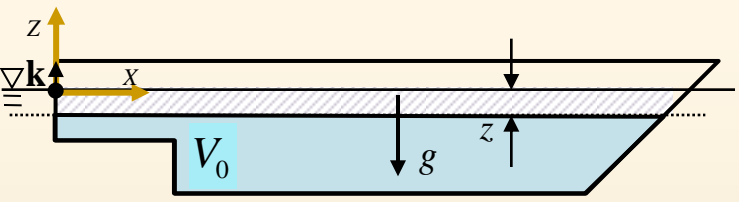
$$m\mathbf{z}'' + k\mathbf{z} = 0 \quad \text{Oscillation by the restoring force}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional buoyancy caused by additional displacement  $z$

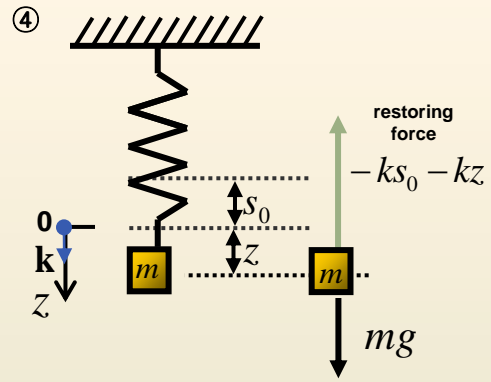
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{WP} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system



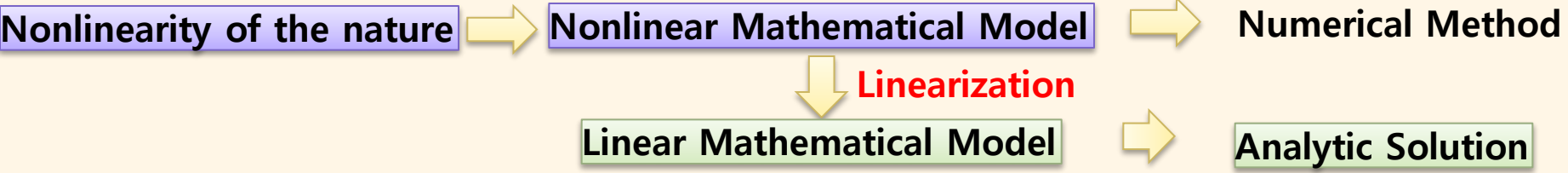
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

$$m\mathbf{z}'' + k\mathbf{z} = 0$$

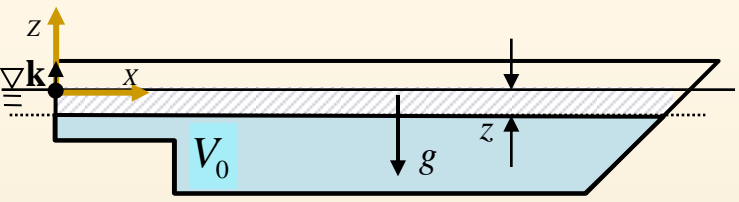
Oscillation by the restoring force



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $z$

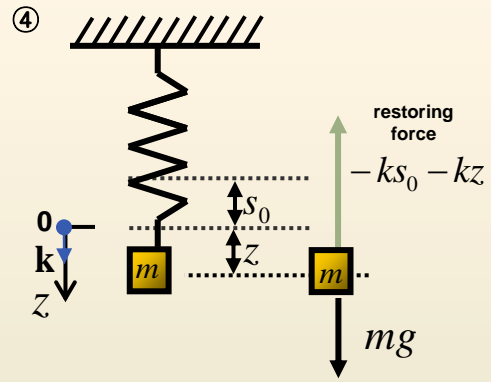
if,  $z$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{WP} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{WP}
 \end{aligned}$$

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{external,static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -\rho g A_{wp} \mathbf{z} + \mathbf{F}_{external,static} \\
 &= -k\mathbf{z} + \mathbf{F}_{external,static}, k = \rho g A_{WP} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

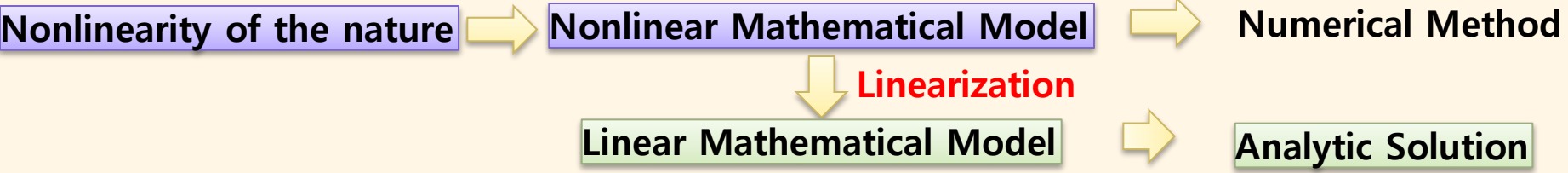


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

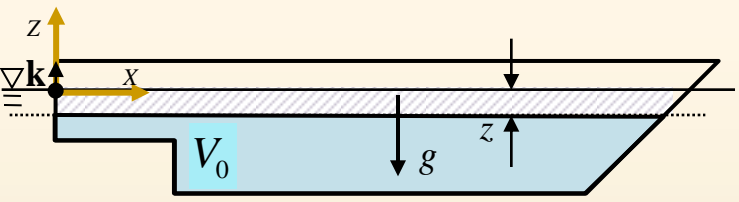
$$m\mathbf{z}'' + k\mathbf{z} = 0 \quad \text{Oscillation by the restoring force}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z} \quad , k = \rho g A_{wp} \\
 &= 0 \quad (\because \ddot{\mathbf{z}} = 0)
 \end{aligned}$$

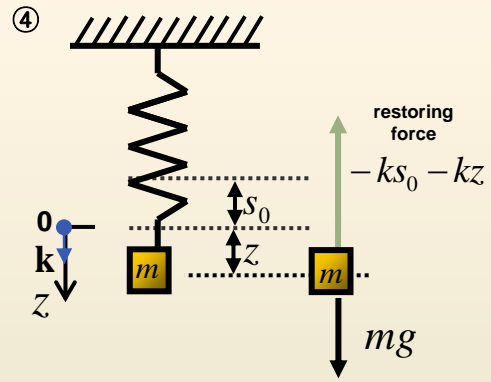
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional buoyancy caused by additional displacement  $\mathbf{z}$

if,  $\mathbf{z}$  is small  
 $\mathbf{F}_{additional\ bouyancy}$   
 $= -\rho g A_{wp} \mathbf{z}$   
 $= -k\mathbf{z}$   
 $, k = \rho g A_{wp}$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system



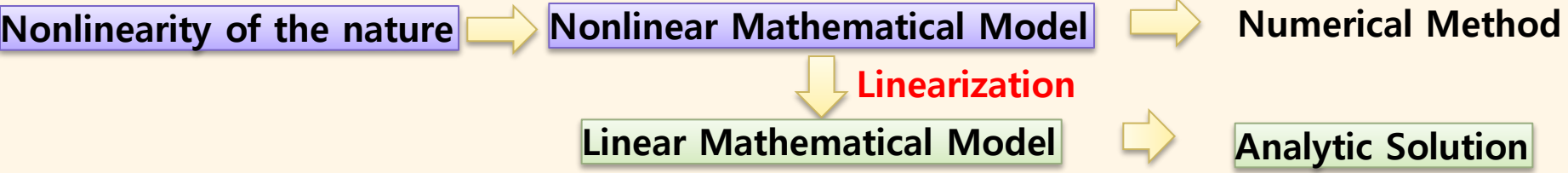
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

$$m\mathbf{z}'' + k\mathbf{z} = 0$$

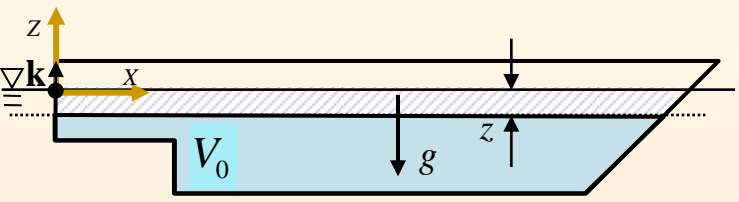
Oscillation by the restoring force



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z} \quad , k = \rho g A_{wp}
 \end{aligned}$$

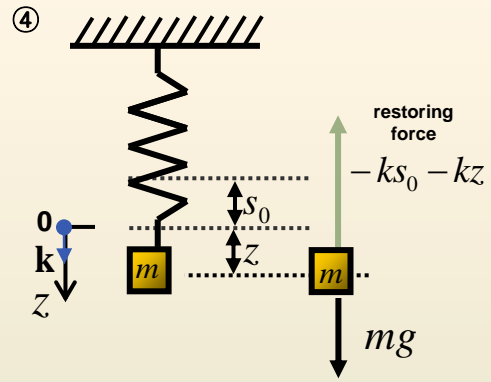
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional buoyancy caused by additional displacement  $\mathbf{z}$

if,  $\mathbf{z}$  is small  
 $\mathbf{F}_{additional\ bouyancy}$   
 $= -\rho g A_{wp} \mathbf{z}$   
 $= -k\mathbf{z}$   
 $, k = \rho g A_{wp}$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system



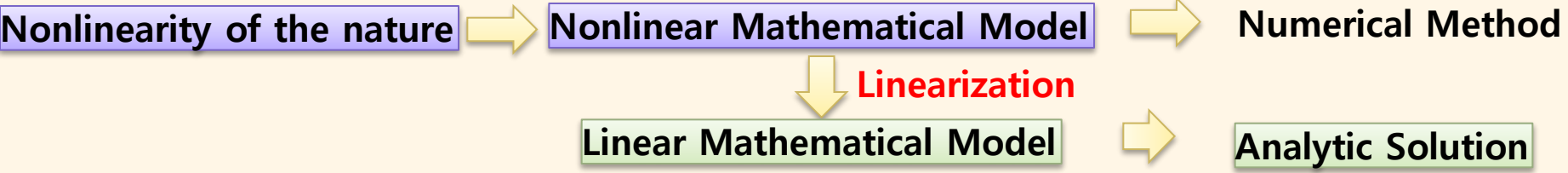
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

$$m\mathbf{z}'' + k\mathbf{z} = 0$$

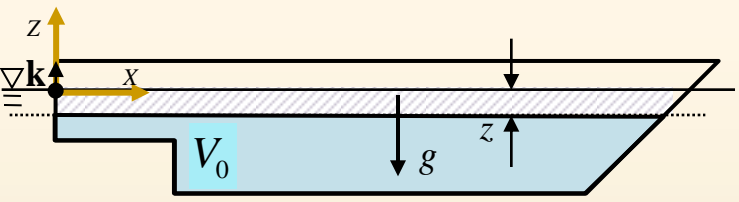
Oscillation by the restoring force



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z} \quad , k = \rho g A_{wp}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} + \mathbf{F}_{additional\ bouyancy} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

additional bouyancy caused by additional displacement  $\mathbf{z}$

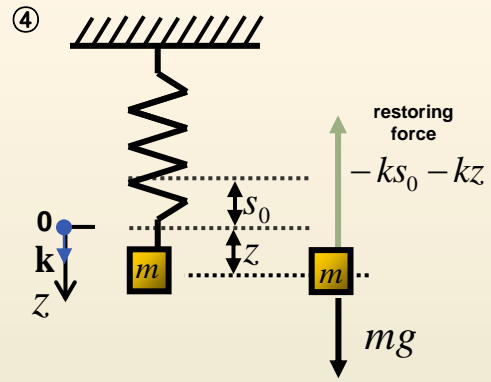
if,  $\mathbf{z}$  is small

$$\begin{aligned}
 \mathbf{F}_{additional\ bouyancy} &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z} \\
 , k &= \rho g A_{wp}
 \end{aligned}$$

**Linearized Restoring Force**

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system



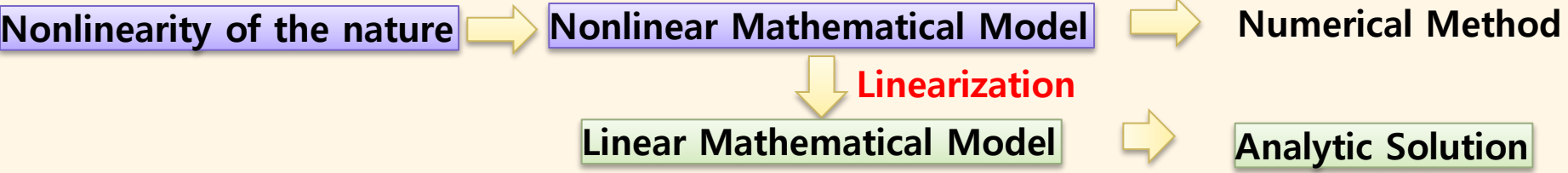
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} \\
 &= -kz\mathbf{k}
 \end{aligned}$$

$$m\mathbf{z}'' + k\mathbf{z} = 0 \quad \text{Oscillation by the restoring force}$$

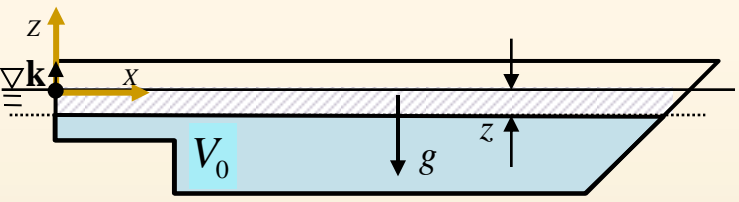




# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

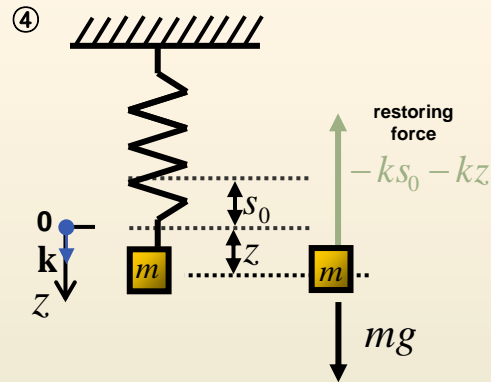
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k \mathbf{z}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

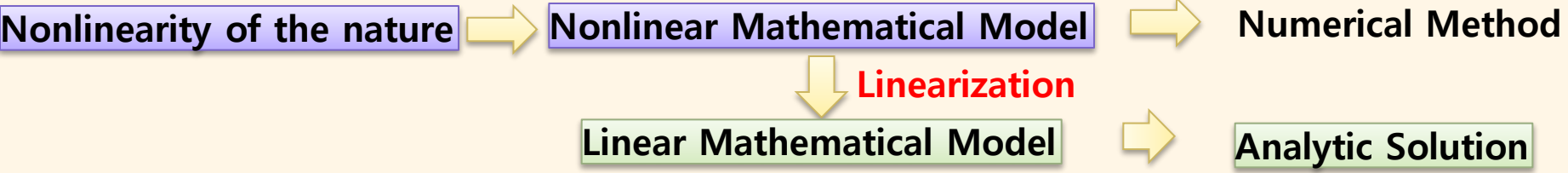


$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} \\
 &= -k z \mathbf{k}
 \end{aligned}$$

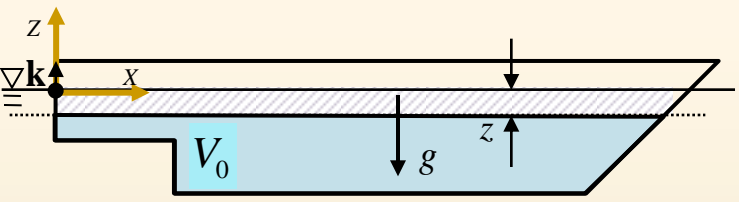
$$m \mathbf{z}'' + k \mathbf{z} = 0 \quad \text{Oscillation by the restoring force}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4




$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z}
 \end{aligned}$$

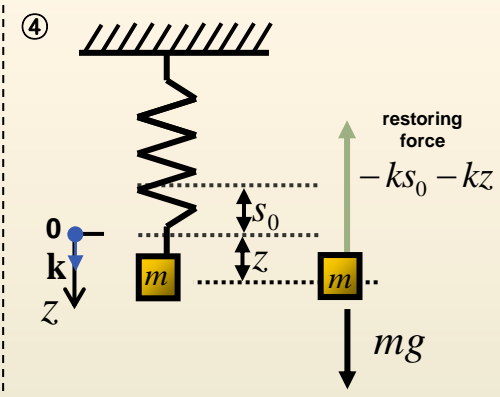
$$\begin{aligned}
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k \mathbf{z}
 \end{aligned}$$

 Ship will oscillate forever?

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

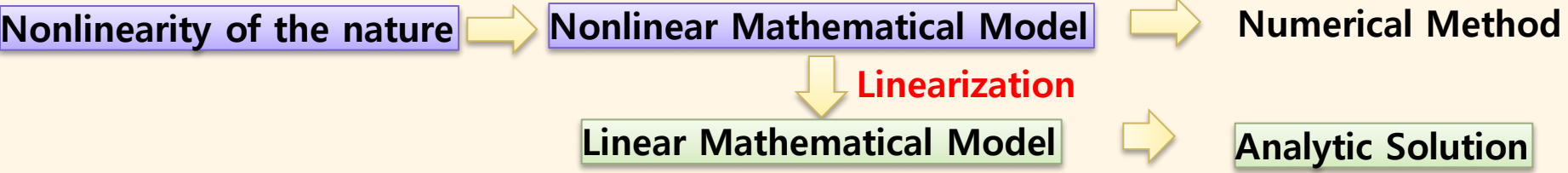


$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} \\
 &= -k z \mathbf{k}
 \end{aligned}$$

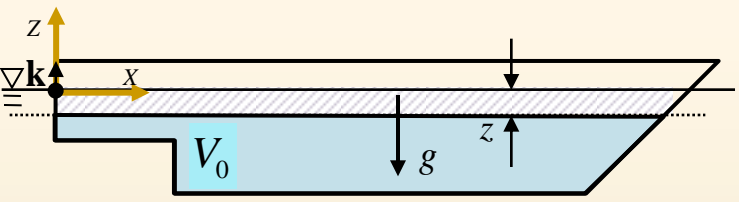
$$m \mathbf{z}'' + k z = 0 \quad \text{Oscillation by the restoring force}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k \mathbf{z}
 \end{aligned}$$

Ship will oscillate forever?

Energy is dissipated by radiation wave →

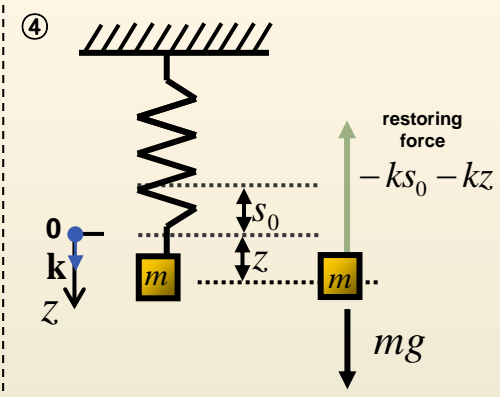
정수 중 선박의 강제 운동에 의해 발생한 힘

Radiation Force

$$\mathbf{F}_{radiation} = \iint_{S_B} P_{radiation} \mathbf{n} dS$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

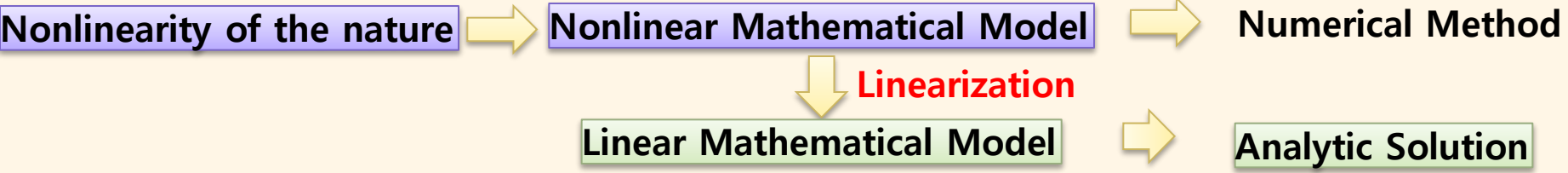


$$\begin{aligned}
 m z'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} \\
 &= -k z \mathbf{k}
 \end{aligned}$$

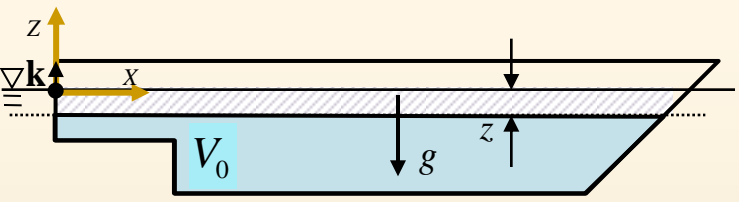
$$m z'' + k z = 0 \quad \text{Oscillation by the restoring force}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 4



- $m$  : mass
- $\rho$  : density of sea water
- $V_0$  : submerged volume
- $S_B$  : submerged surface area
- $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z}
 \end{aligned}$$

$\mathbf{M}$   
 $\mathbf{F}_{gravity} = -m g \mathbf{k}$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k \mathbf{z}
 \end{aligned}$$

Ship will oscillate forever?

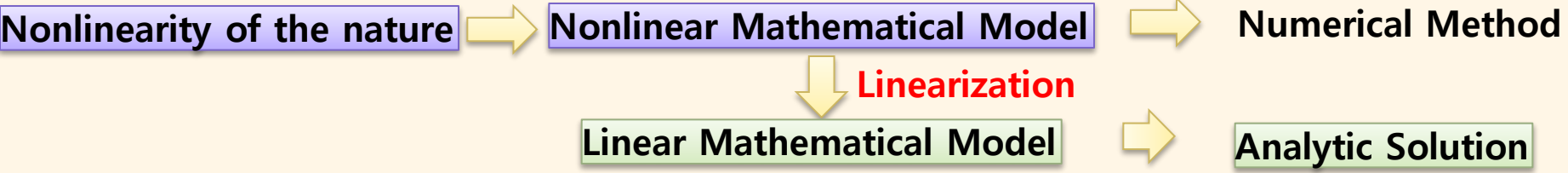
Energy is dissipated by radiation wave →

정수 중 선박의 강제 운동에 의해 발생한 힘

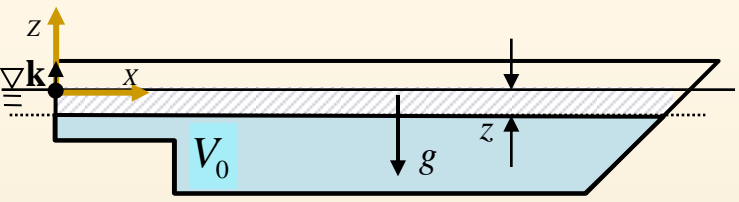
Radiation Force

$$\mathbf{F}_{radiation} = \iint_{S_B} P_{radiation} \mathbf{n} dS$$


# Nonlinearity



## Ex) Heave Motion of a Ship – step 5



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

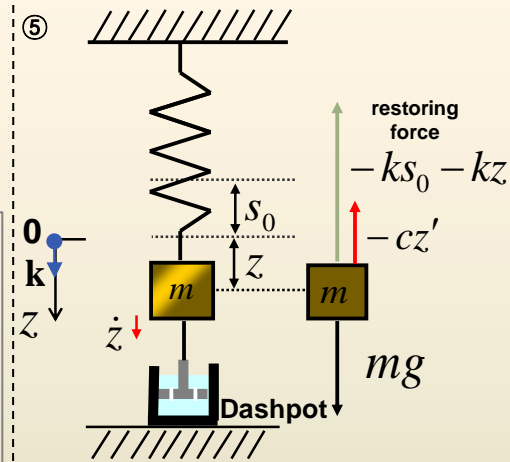
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k \mathbf{z}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

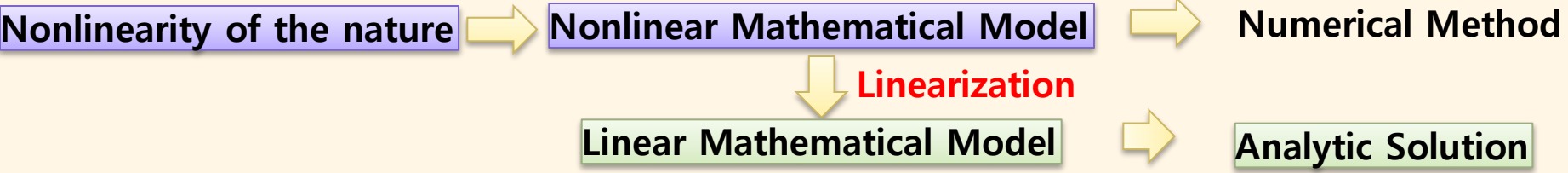
✓ Mass-Spring-Damper system



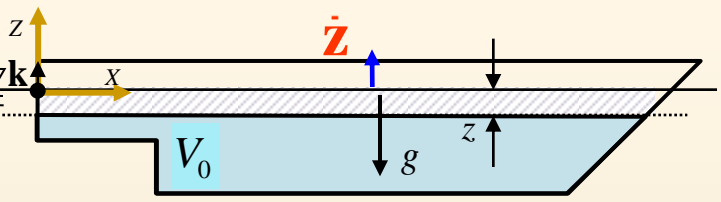
$$\begin{aligned}
 m z'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} \\
 &= -k z \mathbf{k} - c z' \mathbf{k}
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 5

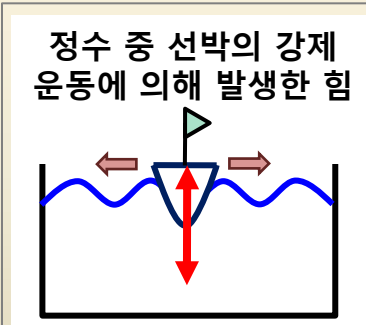


$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k\mathbf{z}
 \end{aligned}$$

$$\mathbf{F}_{gravity} = -mg\mathbf{k}$$

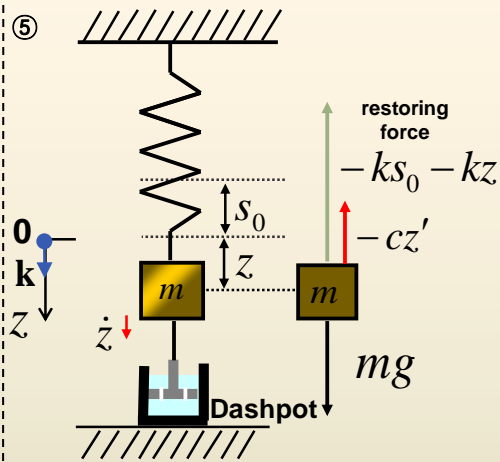


$$\begin{aligned}
 \mathbf{F}_{radiation} &= \iint_{S_B} P_{radiation} \mathbf{n} dS \\
 &= -c\dot{\mathbf{z}}
 \end{aligned}$$

opposite to velocity

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

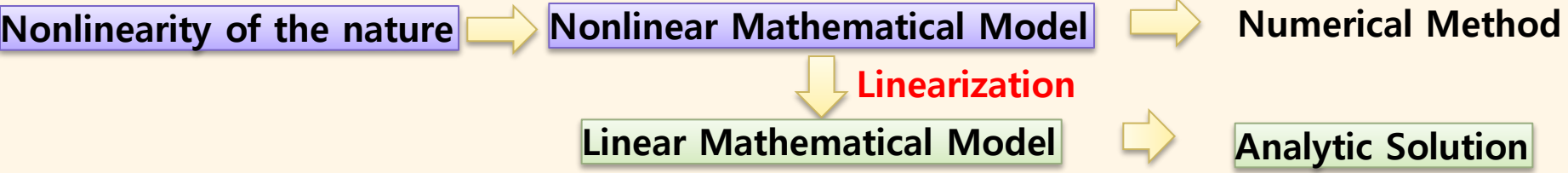
✓ Mass-Spring-Damper system



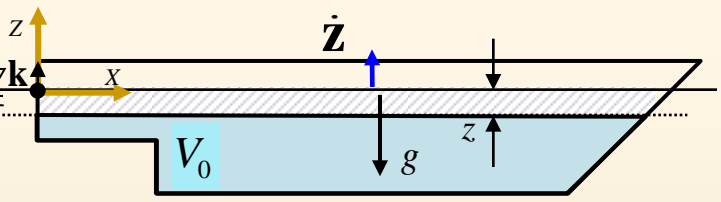
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} - c\dot{\mathbf{z}}\mathbf{k} \\
 &= -kz\mathbf{k} - c\dot{\mathbf{z}}\mathbf{k}
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 5



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

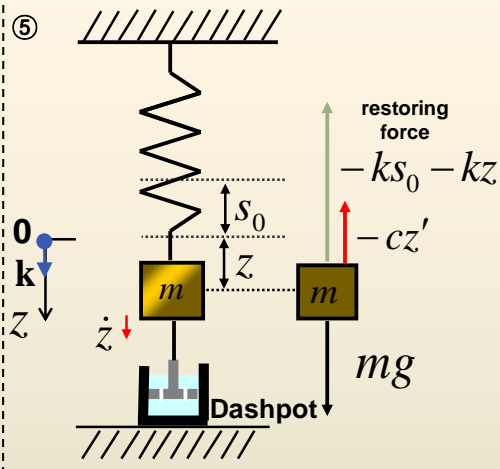
$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k\mathbf{z}
 \end{aligned}$$

$$\mathbf{F}_{gravity} = -mg\mathbf{k}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system



$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} - cz'\mathbf{k} \\
 &= -kz\mathbf{k} - cz'\mathbf{k}
 \end{aligned}$$

정수 중 선박의 강제 운동에 의해 발생한 힘

Radiation Force

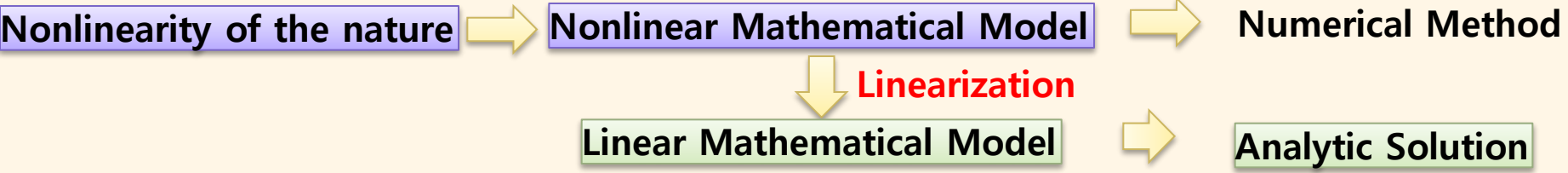
$$\begin{aligned}
 \mathbf{F}_{radiation} &= \iint_{S_B} P_{radiation} \mathbf{n} dS \\
 &= -c\dot{\mathbf{z}}
 \end{aligned}$$

$c$  : damping coefficient

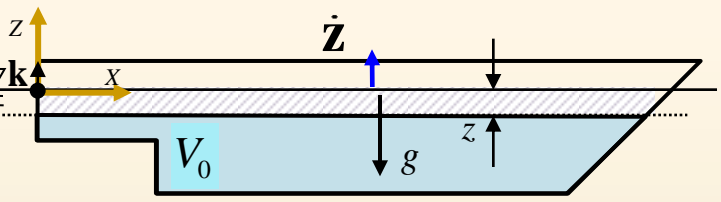
opposite to velocity



# Nonlinearity



## Ex) Heave Motion of a Ship – step 5



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} \\
 &= -mg\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k\mathbf{z} \\
 \mathbf{F}_{radiation} &= -c\dot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -mg\mathbf{k}
 \end{aligned}$$

opposite to velocity

정수 중 선박의 강제 운동에 의해 발생한 힘

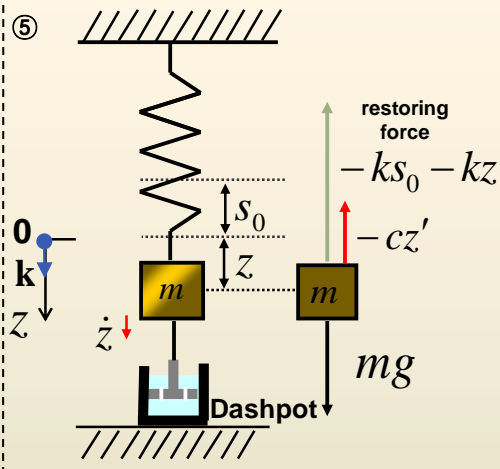
Radiation Force

$$\begin{aligned}
 \mathbf{F}_{radiation} &= \iint_{S_B} P_{radiation} \mathbf{n} dS \\
 &= -c\dot{\mathbf{z}}
 \end{aligned}$$

$c$  : damping coefficient

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

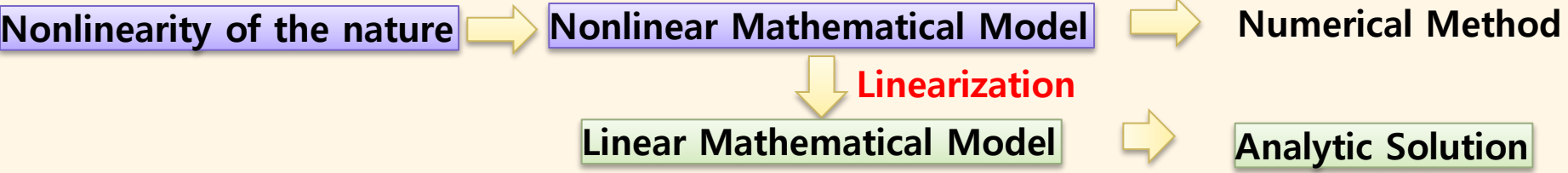


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= mg\mathbf{k} - ks_0\mathbf{k} - kz\mathbf{k} - c\dot{\mathbf{z}}\mathbf{k} \\
 &= -kz\mathbf{k} - c\dot{\mathbf{z}}\mathbf{k}
 \end{aligned}$$

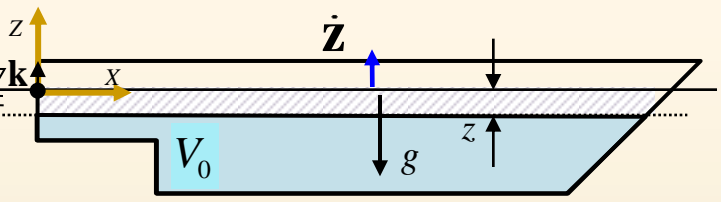




# Nonlinearity



## Ex) Heave Motion of a Ship – step 5



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 &= -\rho g A_{wp} \mathbf{z} \\
 &= -k\mathbf{z}
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 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
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opposite to velocity

정수 중 선박의 강제 운동에 의해 발생한 힘

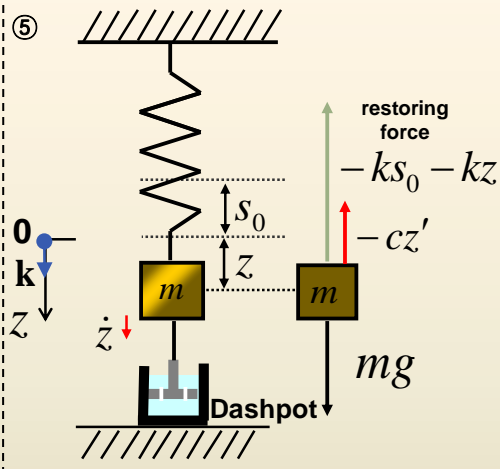
Radiation Force

$$\mathbf{F}_{radiation} = \iint_{S_B} P_{radiation} \mathbf{n} dS = -c\dot{\mathbf{z}}$$

$c$ : damping coefficient

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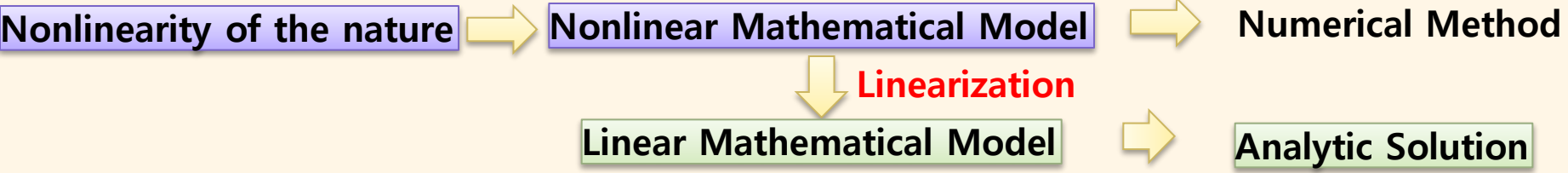
✓ Mass-Spring-Damper system



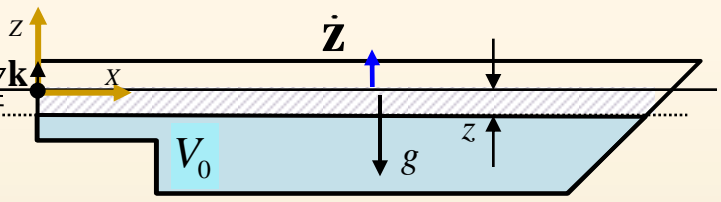
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 &= -kz\mathbf{k} - c\dot{\mathbf{z}}\mathbf{k}
 \end{aligned}$$



# Nonlinearity



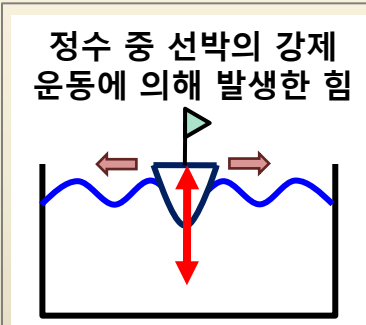
## Ex) Heave Motion of a Ship – step 5



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Radiation Force

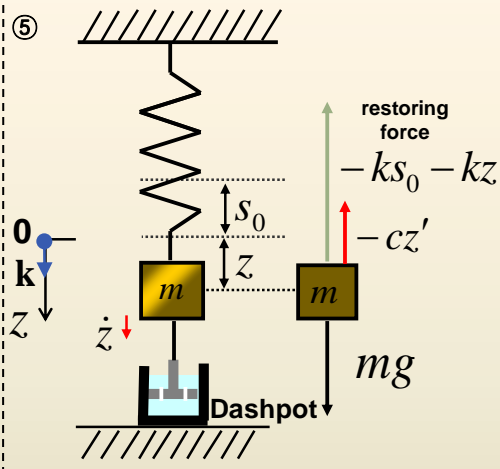
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opposite to velocity

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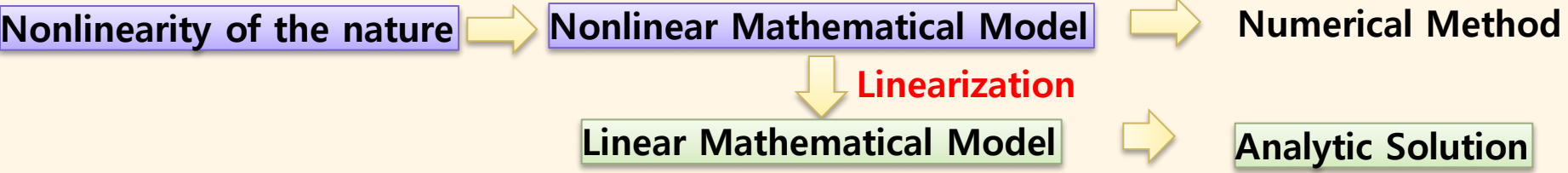
✓ Mass-Spring-Damper system



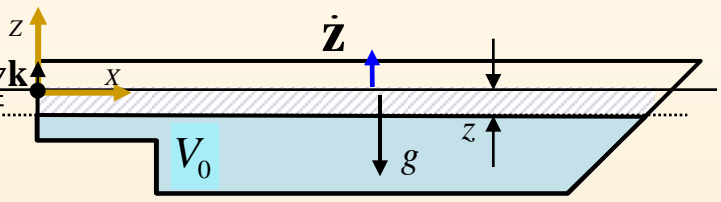
$$\begin{aligned}
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# Nonlinearity



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정수 중 선박의 강제 운동에 의해 발생한 힘

Radiation Force

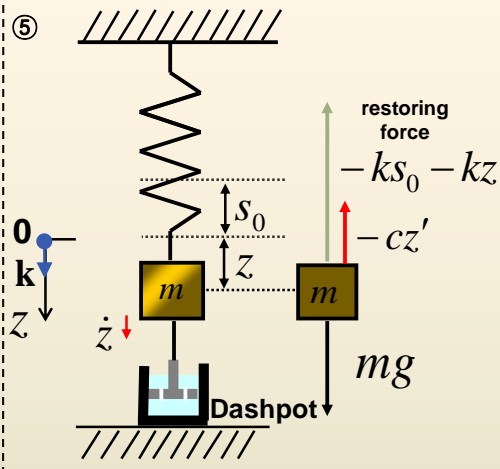
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opposite to velocity

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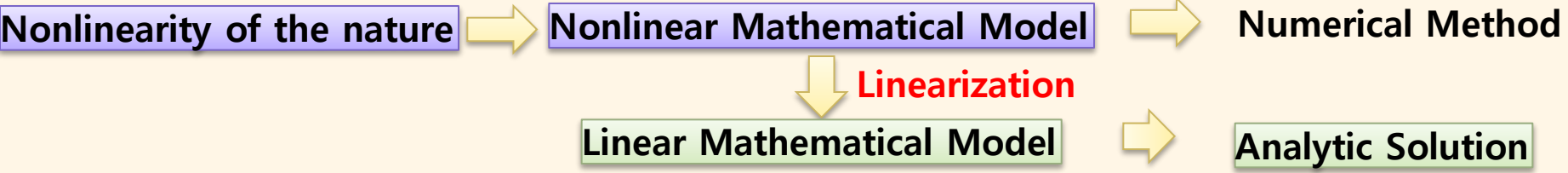
✓ Mass-Spring-Damper system



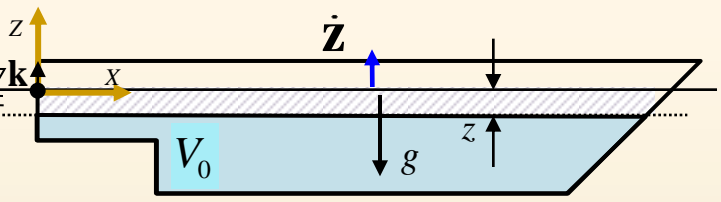
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# Nonlinearity



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정수 중 선박의 강제 운동에 의해 발생한 힘

Radiation Force

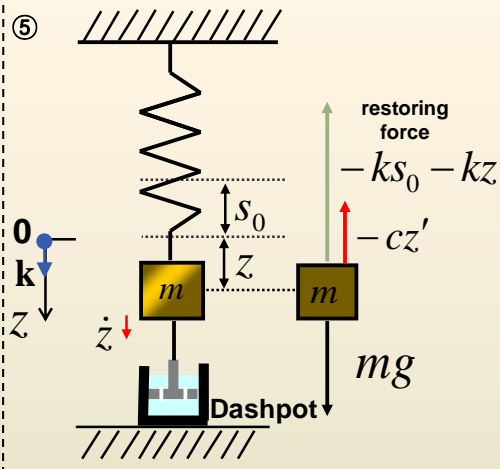
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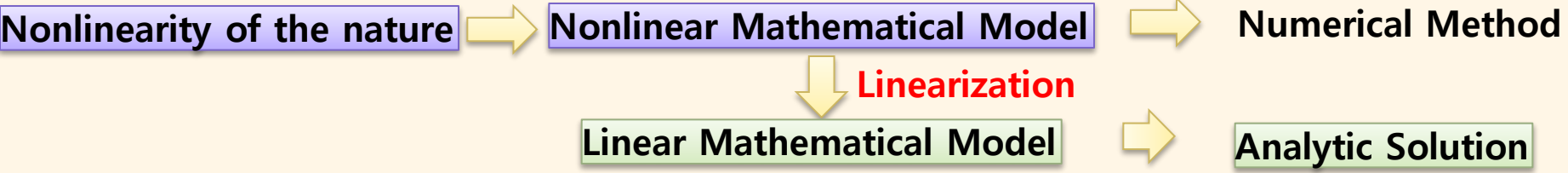
✓ Mass-Spring-Damper system



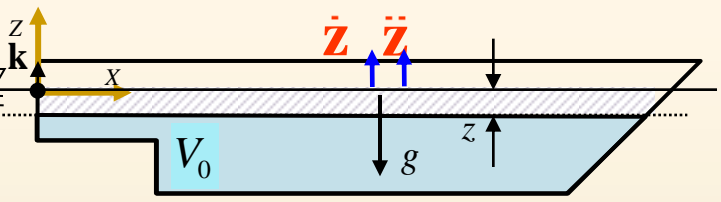
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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 &= -kz\mathbf{k} - cz'\mathbf{k}
 \end{aligned}$$



# Nonlinearity



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정수 중 선박의 강제 운동에 의해 발생한 힘

Radiation Force

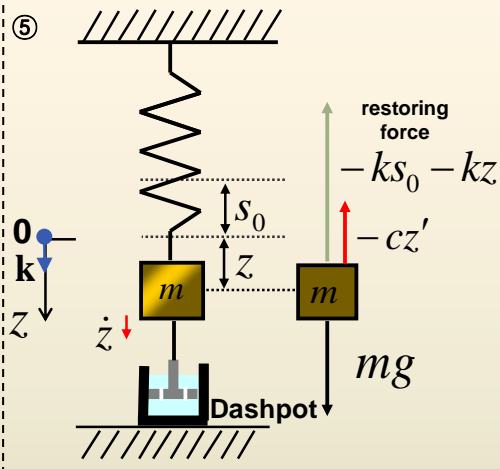
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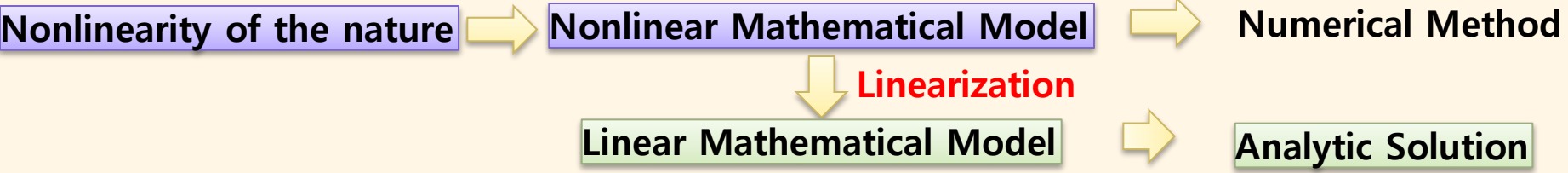
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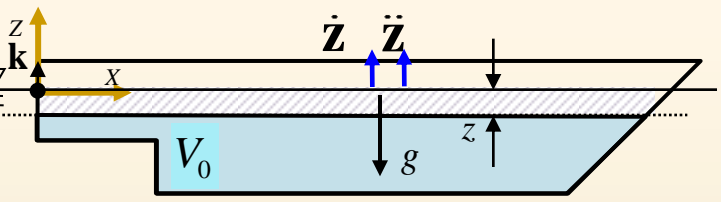
$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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 &= -kz\mathbf{k} - c\dot{\mathbf{z}}\mathbf{k}
 \end{aligned}$$



# Nonlinearity



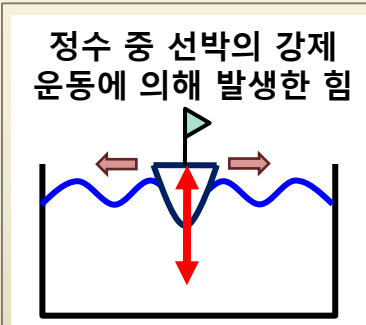
## Ex) Heave Motion of a Ship – step 5



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 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
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 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}}
 \end{aligned}$$



Radiation Force

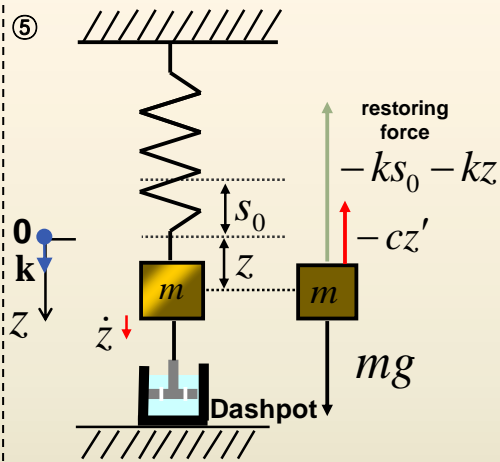
$$\begin{aligned}
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$c$ : damping coefficient

opposite to velocity  
 opposite to acceleration

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

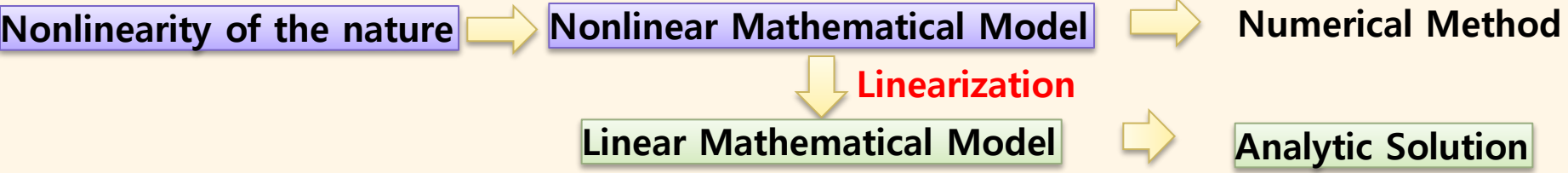
✓ Mass-Spring-Damper system



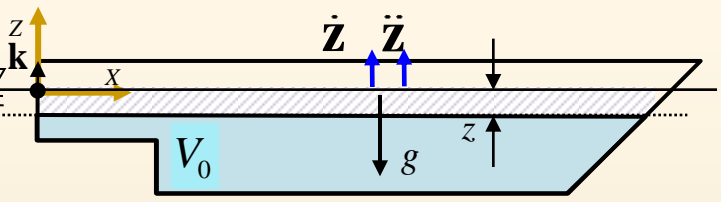
$$\begin{aligned}
 m z'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} \\
 &= -k z \mathbf{k} - c z' \mathbf{k}
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# Nonlinearity



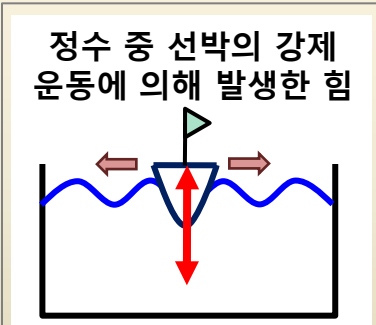
## Ex) Heave Motion of a Ship – step 5



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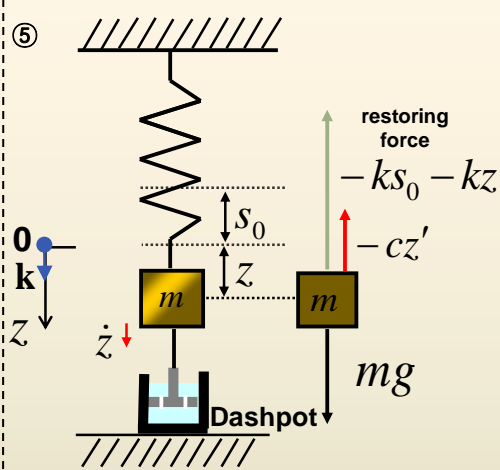
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 \end{aligned}$$

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 $m_a$ : added mass

opposite to velocity  
 opposite to acceleration

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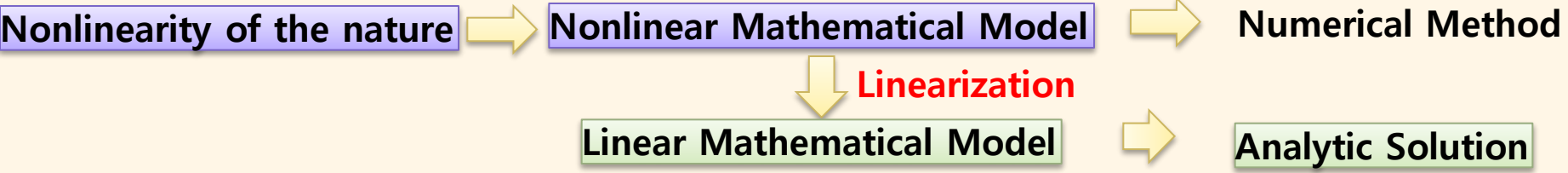
✓ Mass-Spring-Damper system



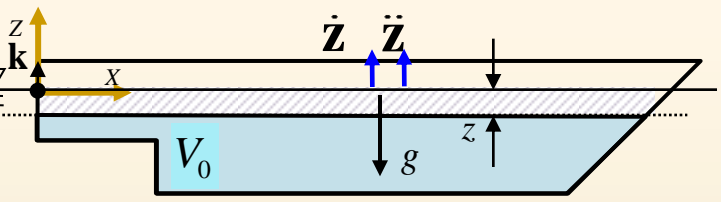
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# Nonlinearity



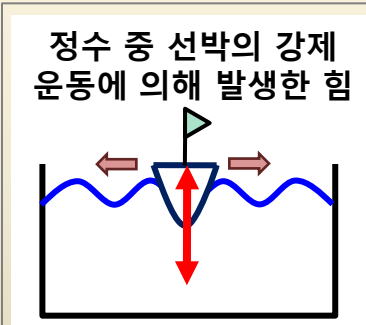
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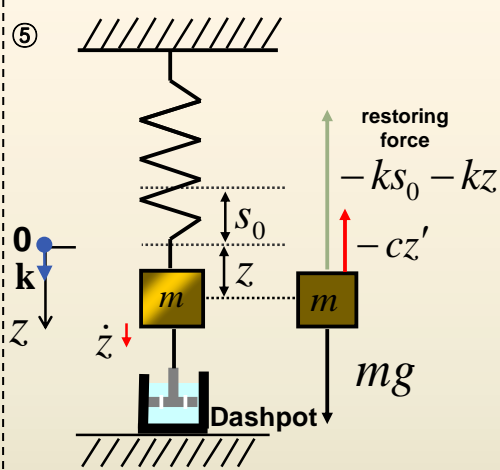
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 opposite to acceleration

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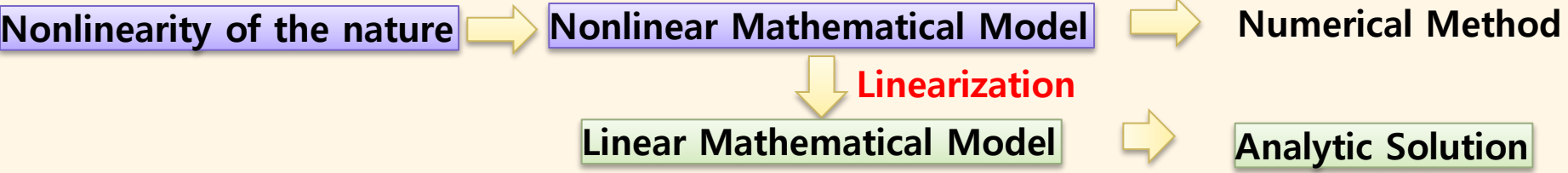


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
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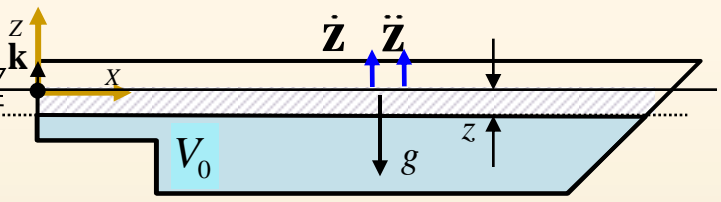




# Nonlinearity



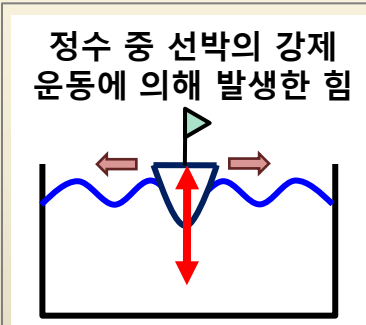
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 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}}
 \end{aligned}$$



Radiation Force

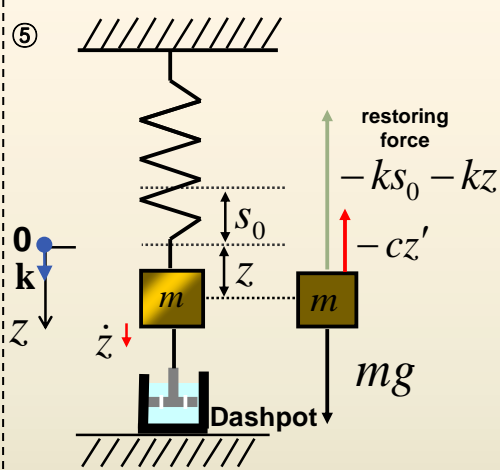
$$\begin{aligned}
 \mathbf{F}_{radiation} &= \iint_{S_B} P_{radiation} \mathbf{n} dS \\
 &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$ : damping coefficient  
 $m_a$ : added mass

opposite to velocity  
 opposite to acceleration

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

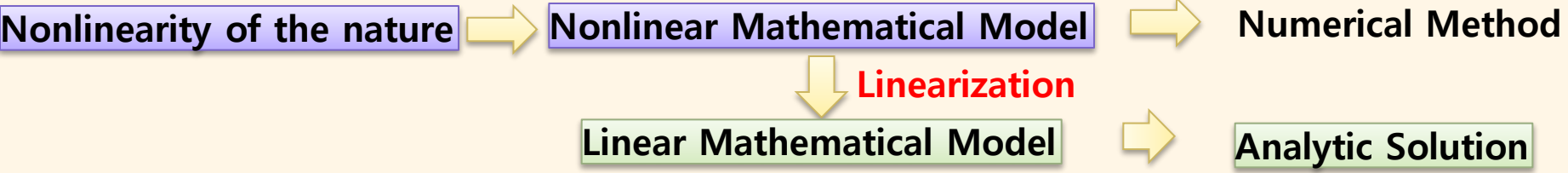
✓ Mass-Spring-Damper system



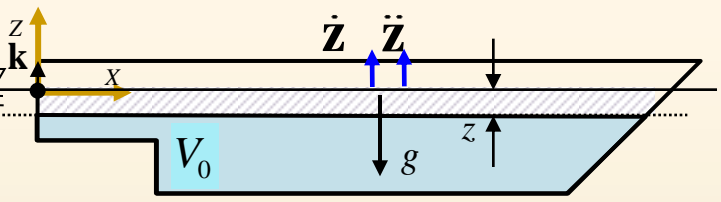
$$\begin{aligned}
 m z'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} \\
 &= -k z \mathbf{k} - c z' \mathbf{k}
 \end{aligned}$$



# Nonlinearity



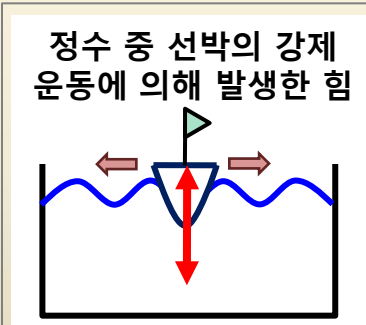
## Ex) Heave Motion of a Ship – step 5



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}}
 \end{aligned}$$



Radiation Force

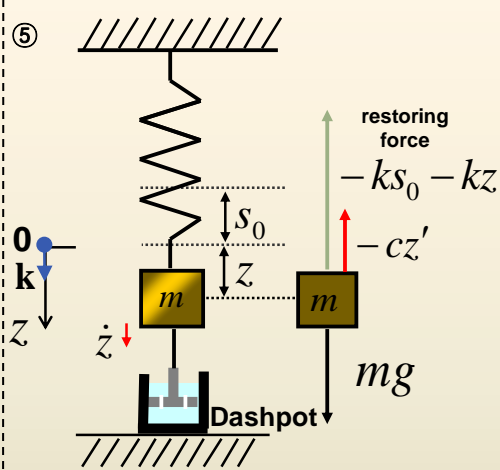
$$\begin{aligned}
 \mathbf{F}_{radiation} &= \iint_{S_B} P_{radiation} \mathbf{n} dS \\
 &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$ : damping coefficient  
 $m_a$ : added mass

opposite to velocity  
 opposite to acceleration

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

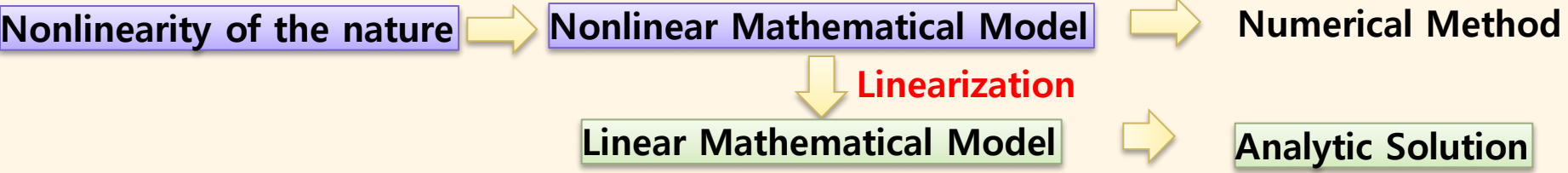
✓ Mass-Spring-Damper system



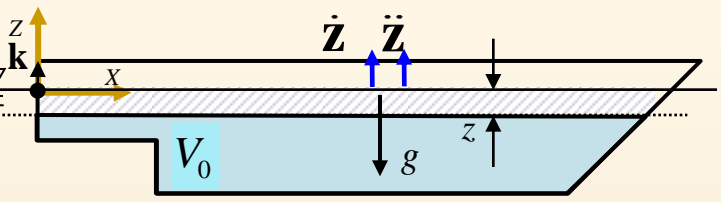
$$\begin{aligned}
 m z'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} \\
 &= -k z \mathbf{k} - c z' \mathbf{k}
 \end{aligned}$$



# Nonlinearity



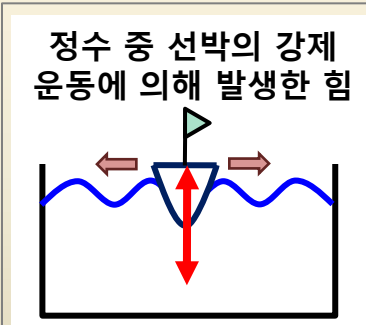
## Ex) Heave Motion of a Ship – step 5



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$



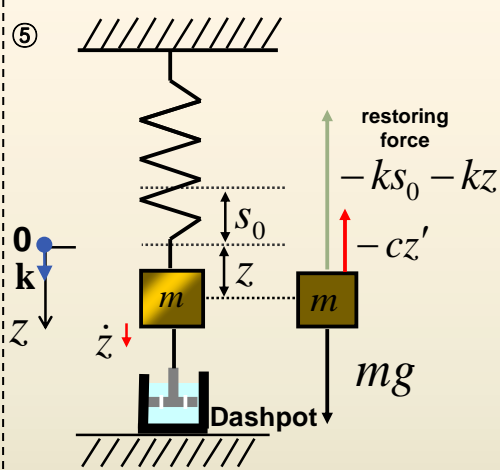
$$\begin{aligned}
 \mathbf{F}_{radiation} &= \iint_{S_B} P_{radiation} \mathbf{n} dS \\
 &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$ : damping coefficient  
 $m_a$ : added mass

opposite to velocity  
 opposite to acceleration

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

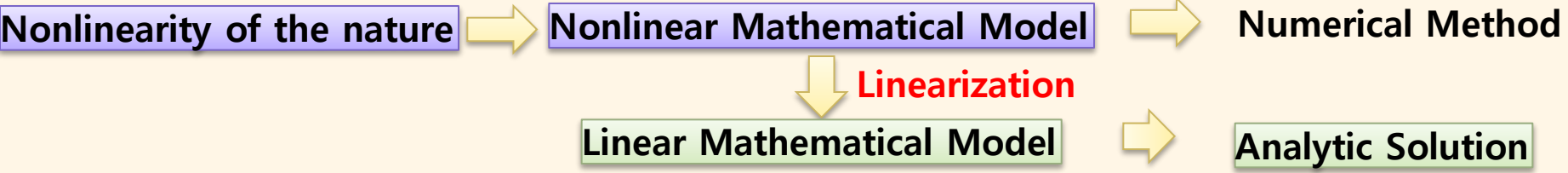
✓ Mass-Spring-Damper system



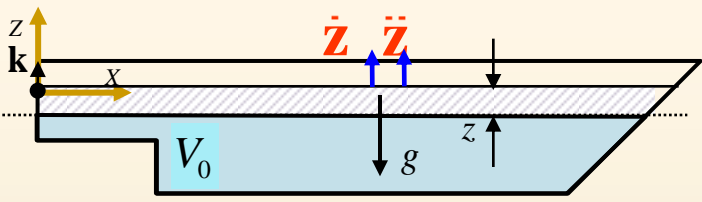
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} \\
 &= -k z \mathbf{k} - c z' \mathbf{k}
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

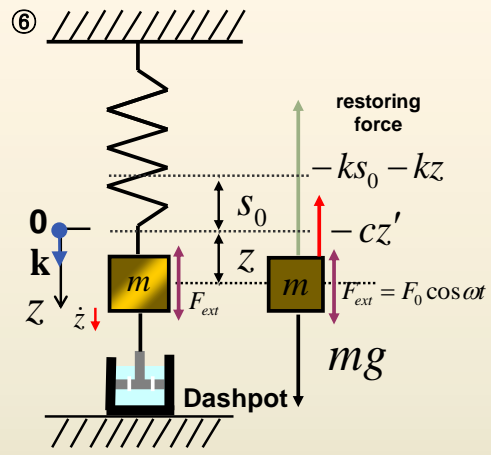
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$  : damping coefficient  
 $m_a$  : added mass

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

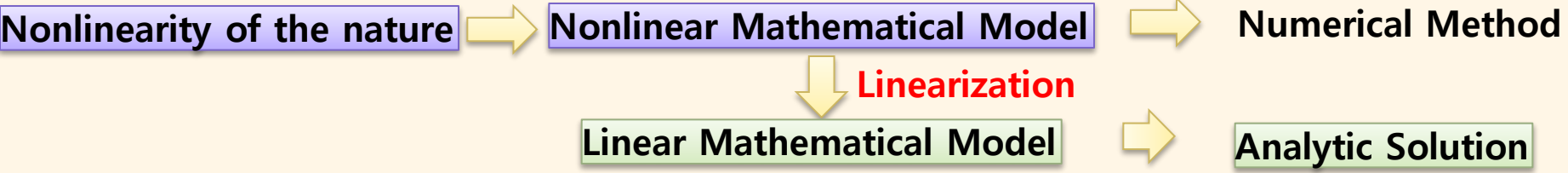
✓ Mass-Spring-Damper system



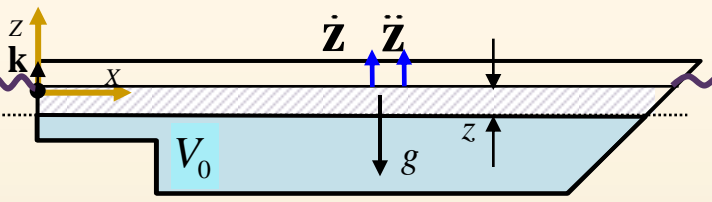
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

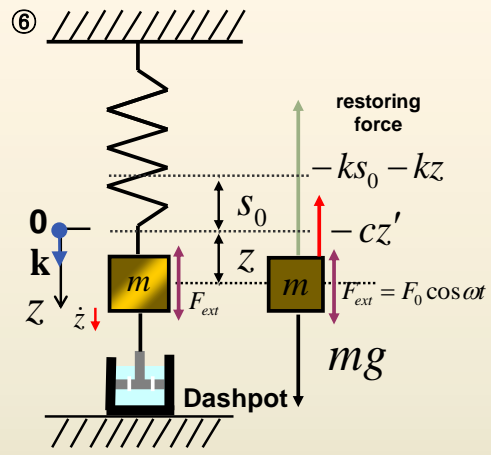
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$  : damping coefficient  
 $m_a$  : added mass

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

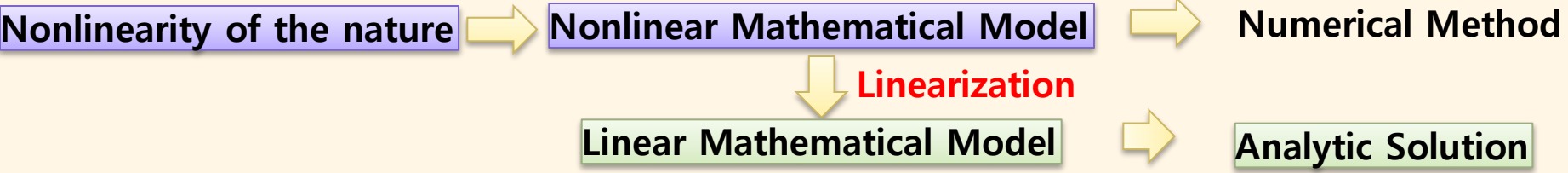
✓ Mass-Spring-Damper system



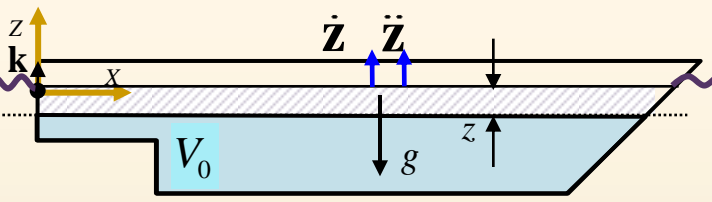
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

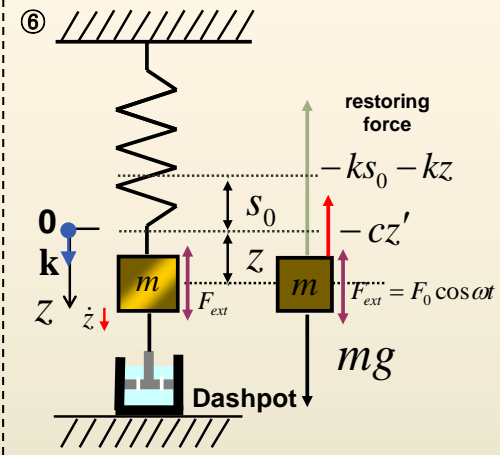
$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$  : damping coefficient  
 $m_a$  : added mass

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system



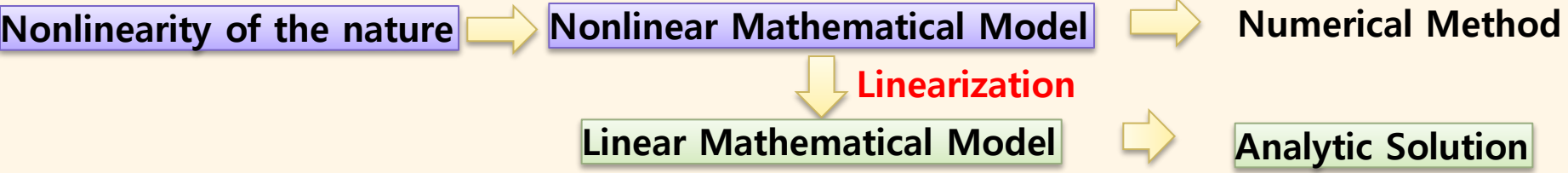
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$

### Wave force

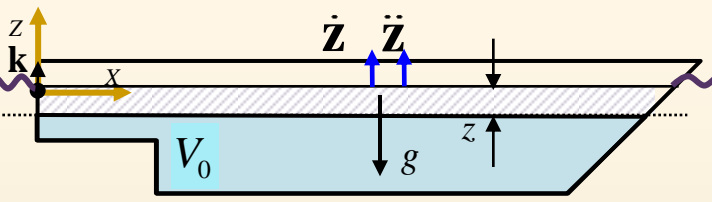
$\mathbf{F}_{wave\ exciting}$   
 $= \iint_{S_B} P_{wave\ exciting} \mathbf{n} dS$   
 $(= \mathbf{F}_{exciting})$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

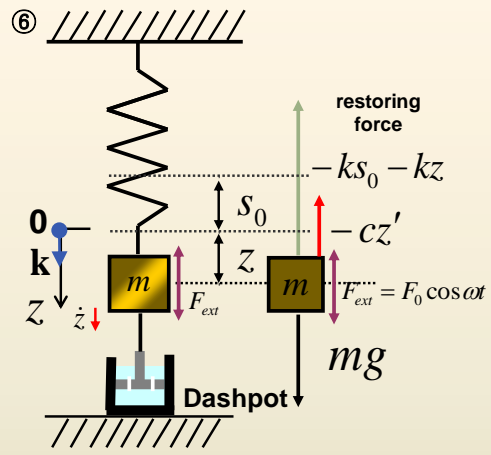
$c$  : damping coefficient  
 $m_a$  : added mass

### Wave force

$$\begin{aligned}
 \mathbf{F}_{wave\ exciting} &= \iint_{S_B} P_{wave\ exciting} \mathbf{n} dS \\
 &= \mathbf{F}_{exciting}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

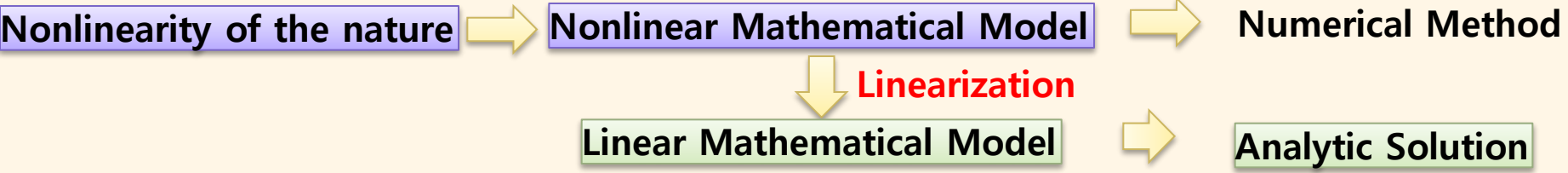
✓ Mass-Spring-Damper system



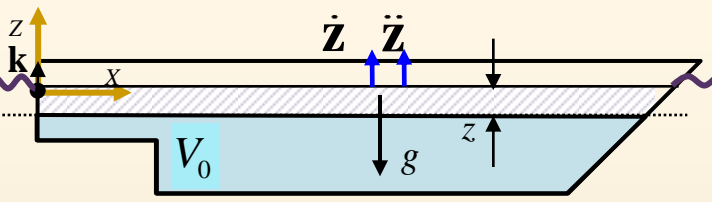
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} + \mathbf{F}_{exciting} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

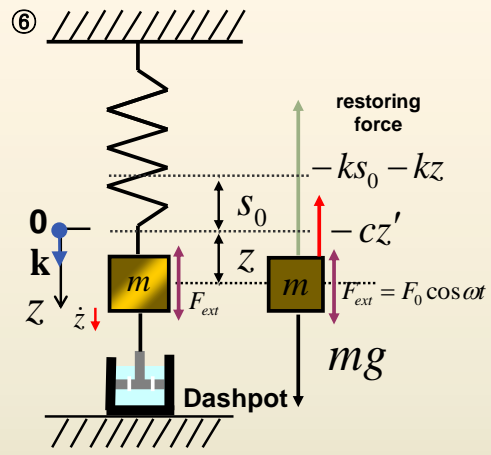
$c$  : damping coefficient  
 $m_a$  : added mass

### Wave force

$$\begin{aligned}
 \mathbf{F}_{wave\ exciting} &= \iint_{S_B} P_{wave\ exciting} \mathbf{n} dS \\
 &= \mathbf{F}_{exciting}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

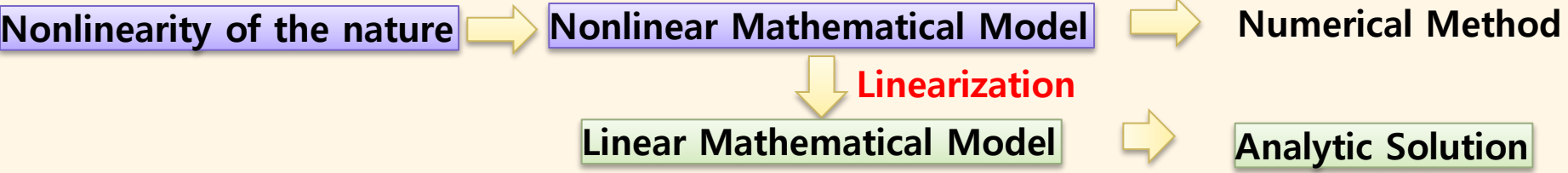


$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$

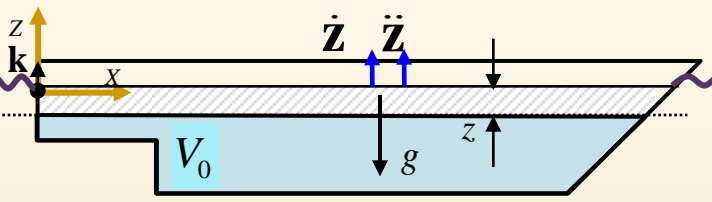




# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} + \mathbf{F}_{exciting} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

$c$  : damping coefficient  
 $m_a$  : added mass

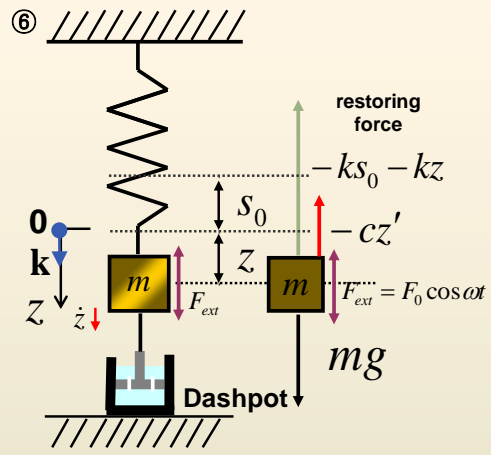
**Wave force**

Froude-Kriloff Force      Diffraction Force

$$\begin{aligned}
 \mathbf{F}_{wave\ exciting} &= \iint_{S_B} P_{wave\ exciting} \mathbf{n} dS \\
 &= \mathbf{F}_{exciting}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

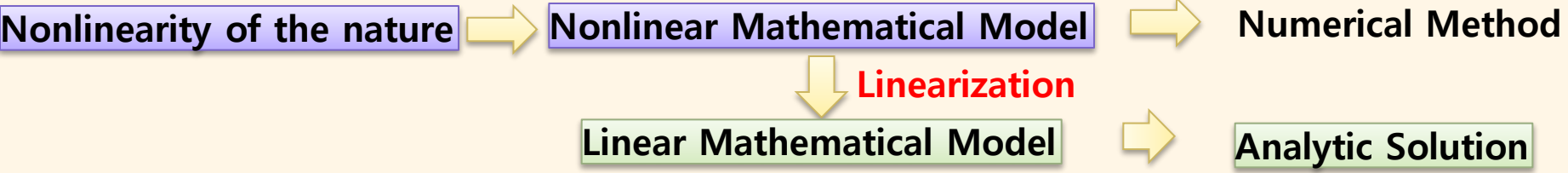
✓ Mass-Spring-Damper system



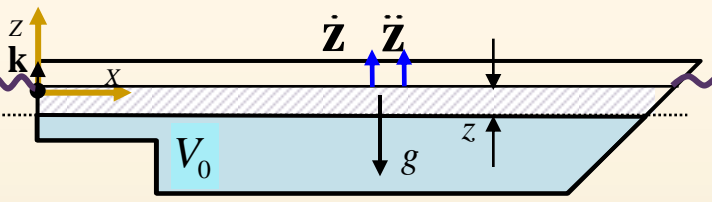
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} + \mathbf{F}_{exciting} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}}
 \end{aligned}$$

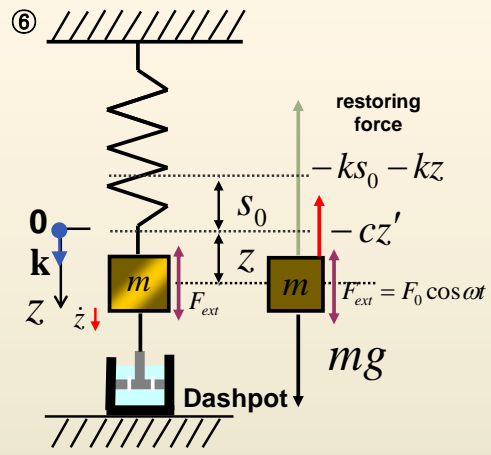
$c$  : damping coefficient  
 $m_a$  : added mass

### Wave force

$$\begin{aligned}
 \mathbf{F}_{wave\ exciting} &= \iint_{S_B} P_{wave\ exciting} \mathbf{n} dS \\
 &= \mathbf{F}_{exciting}
 \end{aligned}$$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

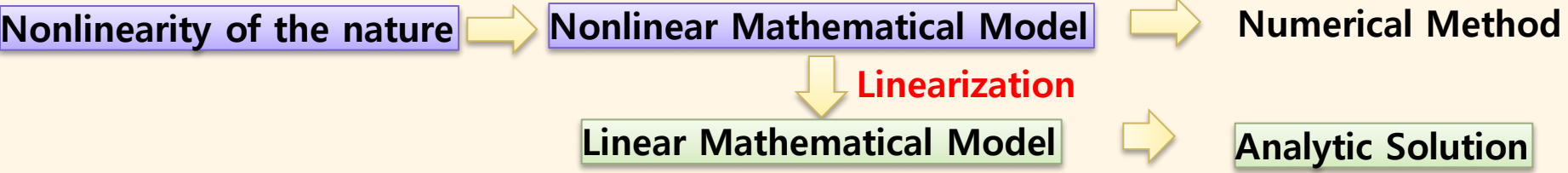
✓ Mass-Spring-Damper system



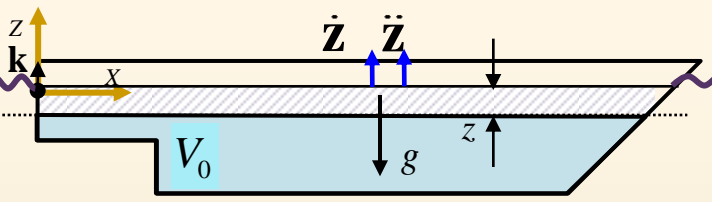
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} + \mathbf{F}_{exciting} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting}
 \end{aligned}$$

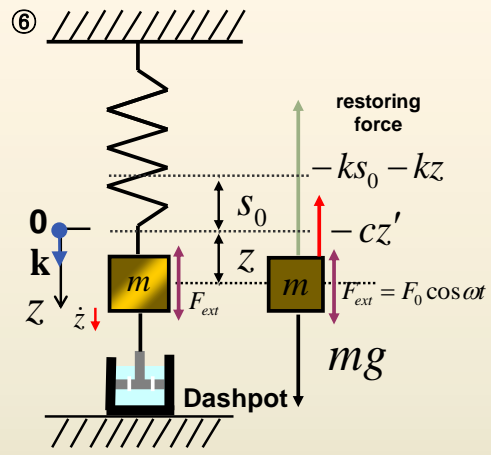
$c$  : damping coefficient  
 $m_a$  : added mass

**Wave force**

$\mathbf{F}_{wave\ exciting}$   
 $= \iint_{S_B} P_{wave\ exciting} \mathbf{n} dS$   
 $(= \mathbf{F}_{exciting})$

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

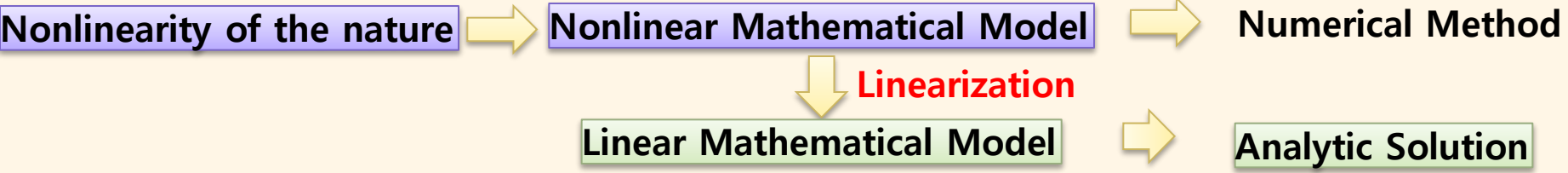
✓ Mass-Spring-Damper system



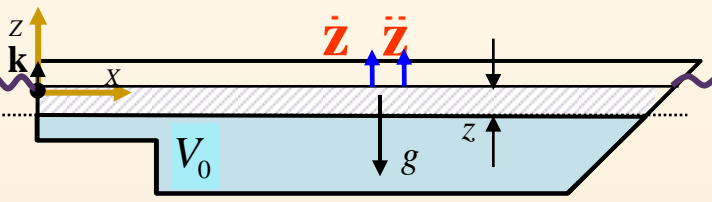
$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c \dot{z} \mathbf{k} + F_0 \cos \omega t \\
 &= -k z \mathbf{k} - c \dot{z} \mathbf{k} + F_0 \cos \omega t
 \end{aligned}$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$ : mass       $\rho$ : density of sea water  
 $V_0$ : submerged volume  
 $S_B$ : submerged surface area  
 $A_{wp}$ : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k \mathbf{z} \\
 \mathbf{F}_{radiation} &= -c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m g \mathbf{k}
 \end{aligned}$$

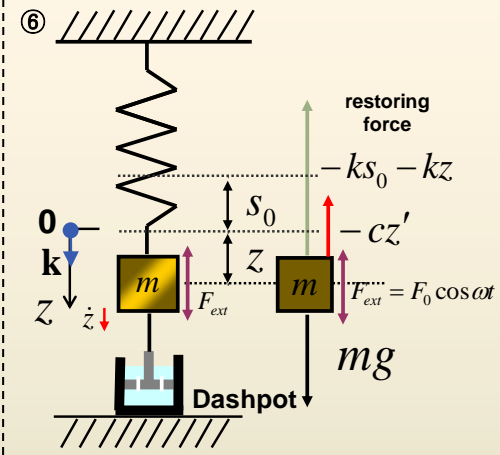
$$\begin{aligned}
 m \ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} + \mathbf{F}_{exciting} \\
 &= -m g \mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -\rho g A_{wp} \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -k \mathbf{z} - c \dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting}
 \end{aligned}$$

$$(m + m_a) \ddot{\mathbf{z}} + c \dot{\mathbf{z}} + k \mathbf{z} = \mathbf{F}_{exciting}$$

$c$ : damping coefficient  
 $m_a$ : added mass

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

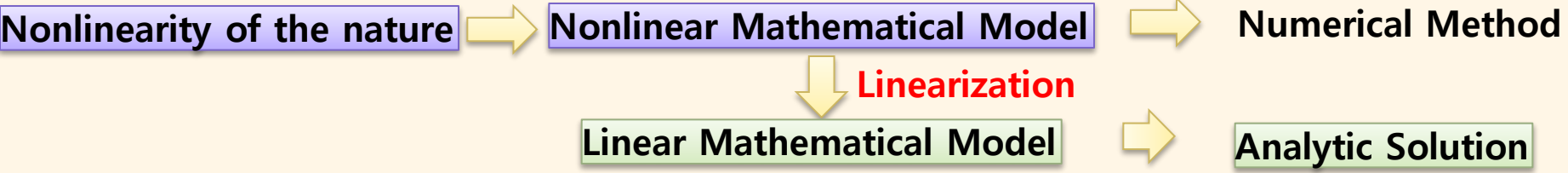


$$\begin{aligned}
 m \mathbf{z}'' &= \mathbf{F} \\
 &= m g \mathbf{k} - k s_0 \mathbf{k} - k z \mathbf{k} - c z' \mathbf{k} + \mathbf{F}_0 \cos \omega t \\
 &= -k z \mathbf{k} - c z' \mathbf{k} + \mathbf{F}_0 \cos \omega t
 \end{aligned}$$

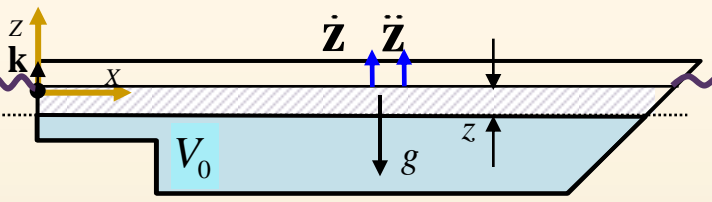
$$m \mathbf{z}'' + c \mathbf{z}' + k \mathbf{z} = \mathbf{F}_0 \cos \omega t$$



# Nonlinearity



## Ex) Heave Motion of a Ship – step 6



$m$  : mass       $\rho$  : density of sea water  
 $V_0$  : submerged volume  
 $S_B$  : submerged surface area  
 $A_{wp}$  : waterplane area

$$\begin{aligned}
 \mathbf{F}_{static} &= \iint_{S_B} P_{static} \mathbf{n} dS \\
 &= \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} \\
 &= \rho g V_0 \mathbf{k} - k\mathbf{z} \\
 \mathbf{F}_{radiation} &= -c\dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} \\
 \mathbf{F}_{gravity} &= -m\mathbf{g}\mathbf{k}
 \end{aligned}$$

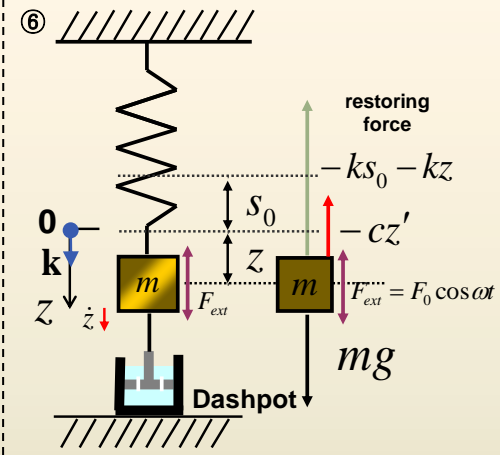
$$\begin{aligned}
 m\ddot{\mathbf{z}} &= \mathbf{F} \\
 &= \mathbf{F}_{gravity} + \mathbf{F}_{static} + \mathbf{F}_{radiation} + \mathbf{F}_{exciting} \\
 &= -m\mathbf{g}\mathbf{k} + \rho g V_0 \mathbf{k} - \rho g A_{wp} \mathbf{z} - c\dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -\rho g A_{wp} \mathbf{z} - c\dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting} \\
 &= -k\mathbf{z} - c\dot{\mathbf{z}} - m_a \ddot{\mathbf{z}} + \mathbf{F}_{exciting}
 \end{aligned}$$

$$(m + m_a)\ddot{\mathbf{z}} + c\dot{\mathbf{z}} + k\mathbf{z} = \mathbf{F}_{exciting}$$

$c$  : damping coefficient  
 $m_a$  : added mass

✓ Archimedes' Principle  $\mathbf{F}_{static} = \rho g V_0 \mathbf{k}$

✓ Mass-Spring-Damper system

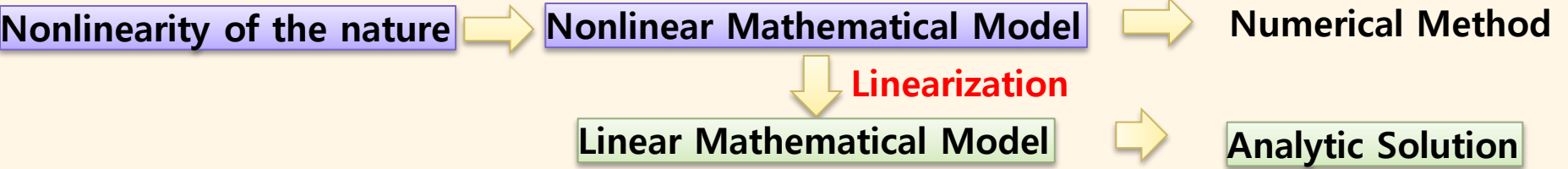


$$\begin{aligned}
 m\mathbf{z}'' &= \mathbf{F} \\
 &= m\mathbf{g}\mathbf{k} - k\mathbf{s}_0\mathbf{k} - k\mathbf{z}\mathbf{k} - c\mathbf{z}'\mathbf{k} + \mathbf{F}_0 \cos \omega t \\
 &= -k\mathbf{z}\mathbf{k} - c\mathbf{z}'\mathbf{k} + \mathbf{F}_0 \cos \omega t
 \end{aligned}$$

$$m\mathbf{z}'' + c\mathbf{z}' + k\mathbf{z} = \mathbf{F}_0 \cos \omega t$$



# Nonlinearity



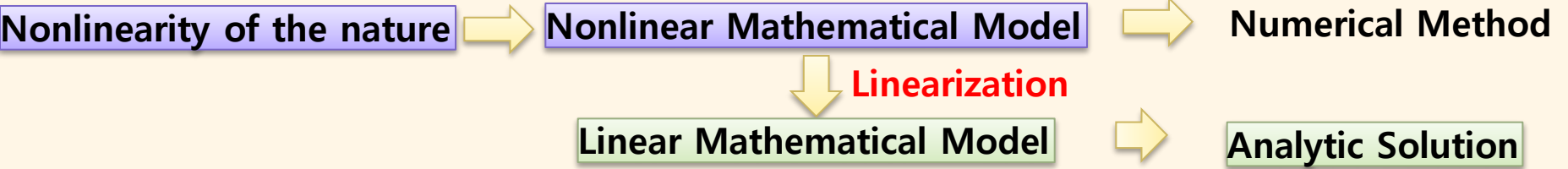
Ex) Roll Motion of a Ship

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# Nonlinearity



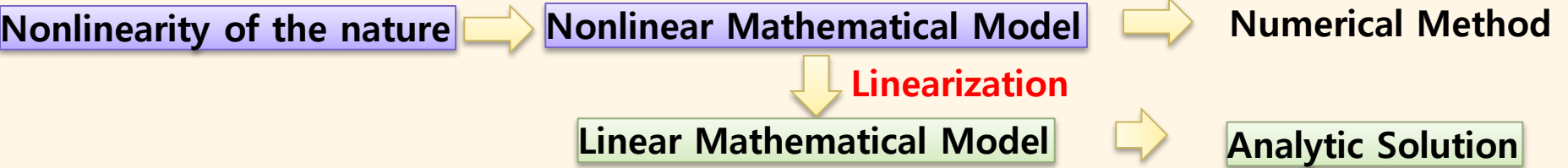
Ex) Roll Motion of a Ship

[Dynamics for roll motion]

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# Nonlinearity



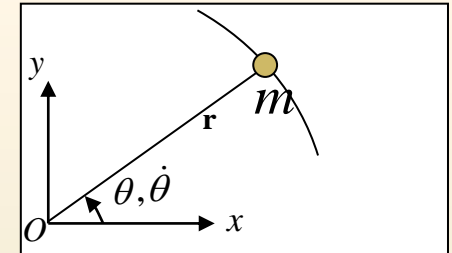
Ex) Roll Motion of a Ship

[Dynamics for roll motion]

Angular momentum defined :  $L = I\dot{\theta}$

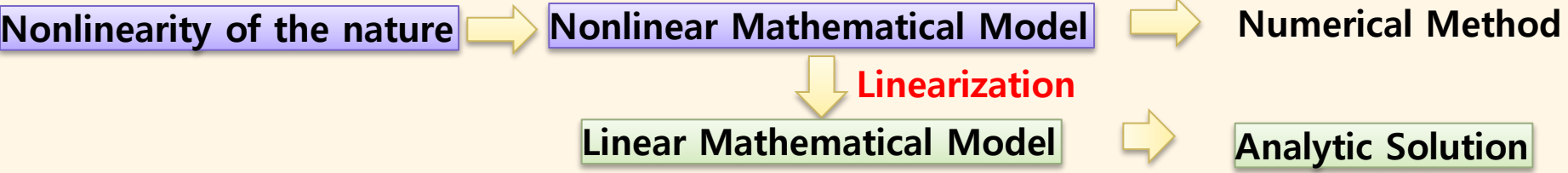
where,  $I = mr^2$  : moment of inertia

$$\theta = \theta(t)$$





# Nonlinearity



Ex) Roll Motion of a Ship

[Dynamics for roll motion]

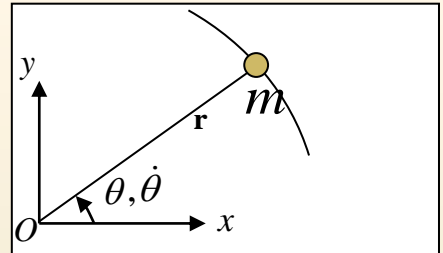
Angular momentum defined :  $L = I\dot{\theta}$

where,  $I = mr^2$  : moment of inertia

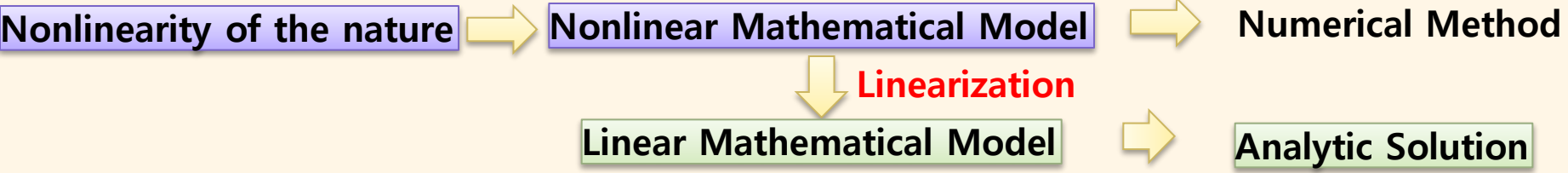
$\theta = \theta(t)$

Rate of change of Angular momentum :

$$\frac{dL}{dt} = I \frac{d(\dot{\theta})}{dt} = I\ddot{\theta} \quad (I : \text{constant})$$



# Nonlinearity



**Ex) Roll Motion of a Ship**

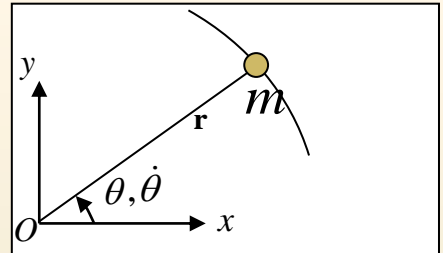
[Dynamics for roll motion]

Angular momentum defined :  $L = I\dot{\theta}$   
 where,  $I = mr^2$  : moment of inertia  
 $\theta = \theta(t)$

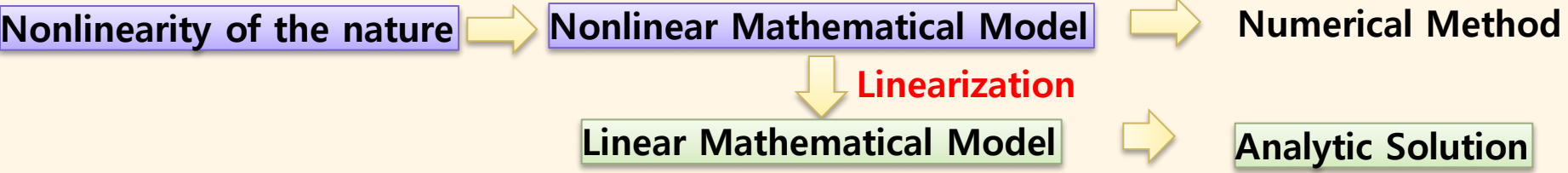
Rate of change of Angular momentum :

$$\frac{dL}{dt} = I \frac{d(\dot{\theta})}{dt} = I\ddot{\theta} \quad (I : \text{constant})$$

Euler's Equation:  $\frac{dL}{dt} = I\ddot{\theta} = \tau_{net}$



# Nonlinearity



**Ex) Roll Motion of a Ship**

[Dynamics for roll motion]

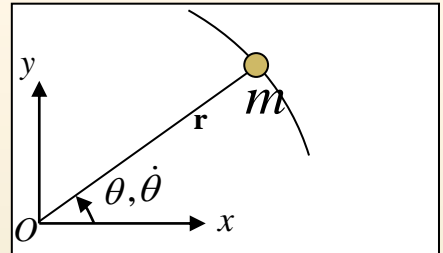
Angular momentum defined :  $L = I\dot{\theta}$

where,  $I = mr^2$  : moment of inertia

$\theta = \theta(t)$

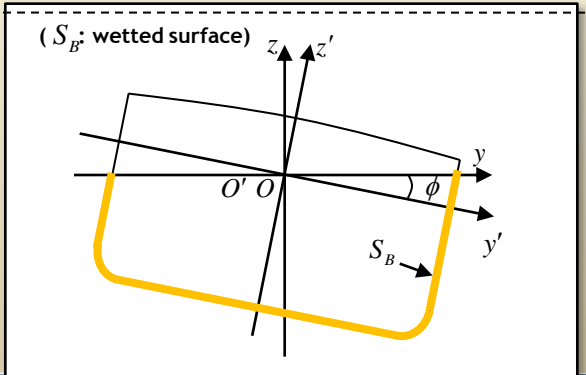
Rate of change of Angular momentum :

$$\frac{dL}{dt} = I \frac{d(\dot{\theta})}{dt} = I\ddot{\theta} \quad (I : \text{constant})$$

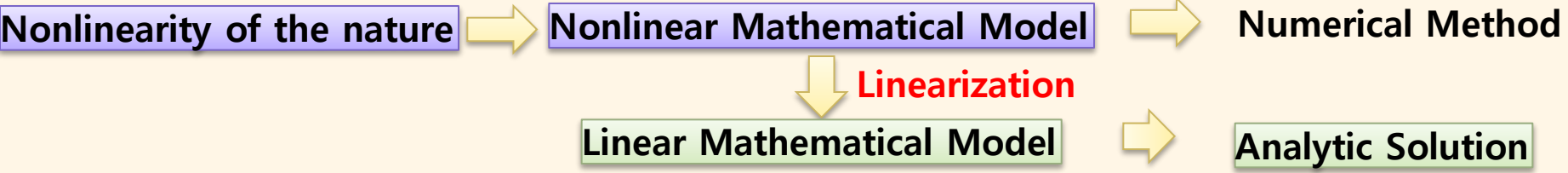


Euler's Equation:  $\frac{dL}{dt} = I\ddot{\theta} = \tau_{net}$

Euler's Equation for roll motion:



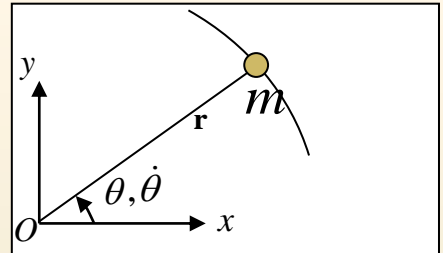
# Nonlinearity



## Ex) Roll Motion of a Ship

[Dynamics for roll motion]

Angular momentum defined :  $L = I\dot{\theta}$   
 where,  $I = mr^2$  : moment of inertia  
 $\theta = \theta(t)$



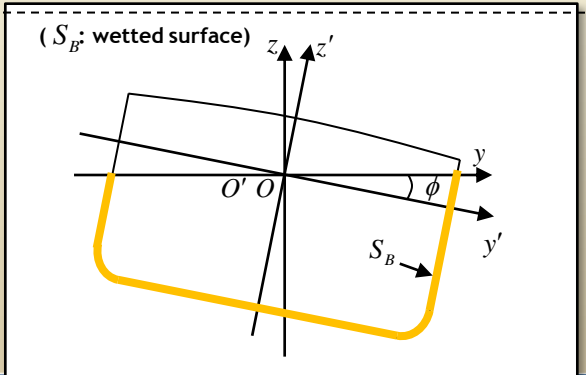
Rate of change of Angular momentum :

$$\frac{dL}{dt} = I \frac{d(\dot{\theta})}{dt} = I\ddot{\theta} \quad (I : \text{constant})$$

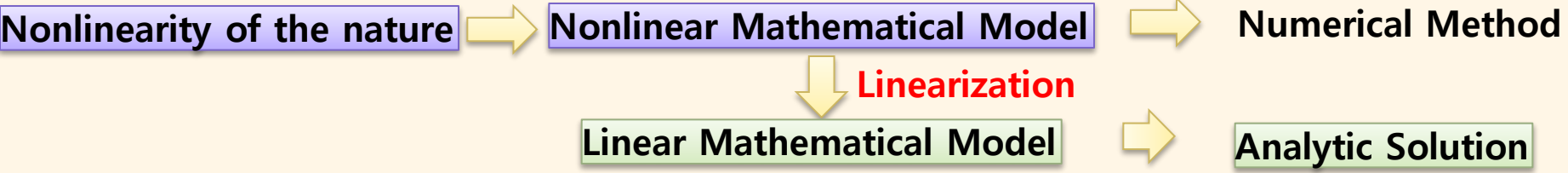
Euler's Equation: 
$$\frac{dL}{dt} = I\ddot{\theta} = \tau_{net}$$

Euler's Equation for roll motion:

$$I\phi'' = \sum M$$



# Nonlinearity



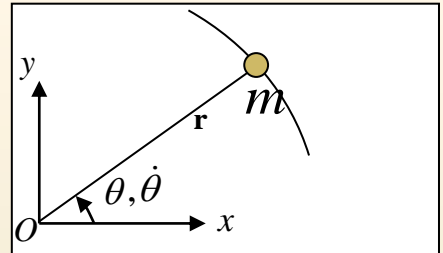
## Ex) Roll Motion of a Ship

[Dynamics for roll motion]

Angular momentum defined :  $L = I\dot{\theta}$

where,  $I = mr^2$  : moment of inertia

$\theta = \theta(t)$



Rate of change of Angular momentum :

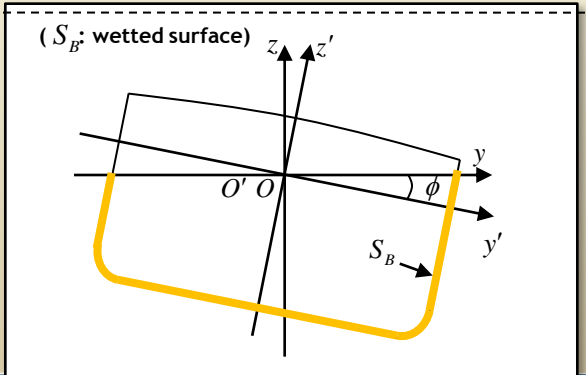
$$\frac{dL}{dt} = I \frac{d(\dot{\theta})}{dt} = I\ddot{\theta} \quad (I : \text{constant})$$

Euler's Equation: 
$$\frac{dL}{dt} = I\ddot{\theta} = \tau_{net}$$

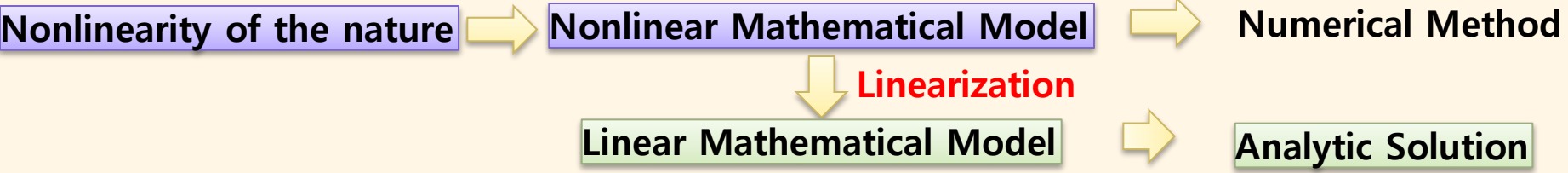
Euler's Equation for roll motion:

$$I\phi'' = \sum M$$

$$I\phi'' = M_{body} + M_{surface}$$



# Nonlinearity



## Ex) Roll Motion of a Ship

( $S_B$ : wetted surface)

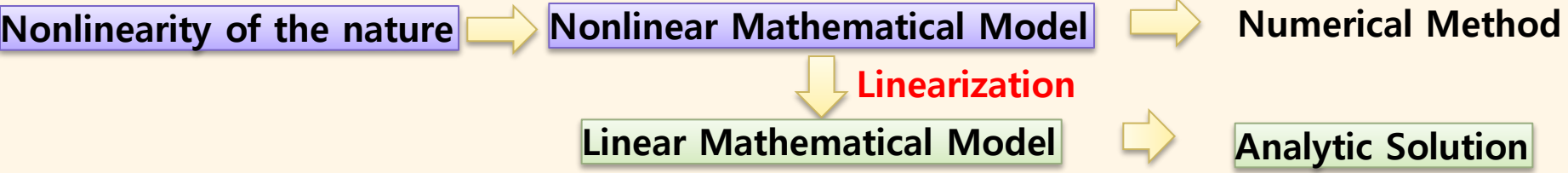
$d\mathbf{F} = P d\mathbf{S} = P n dS$   
 (미소 면적에 작용하는 힘)  
 (미소 면적)

$\mathbf{M} = \mathbf{r} \times d\mathbf{F} = \mathbf{r} \times P n dS = P(\mathbf{r} \times \mathbf{n}) dS$

- Hydrostatic Moment : (모멘트) = (거리) × (힘)
- ✓ 미소 면적에 작용하는 모멘트 :
- ✓ Total moment :

$$\mathbf{M} = \iint_{S_B} P(\mathbf{r} \times \mathbf{n}) dS$$


# Nonlinearity



Ex) Roll Motion of a Ship

$$I\phi'' = \sum M$$

( $S_B$ : wetted surface)

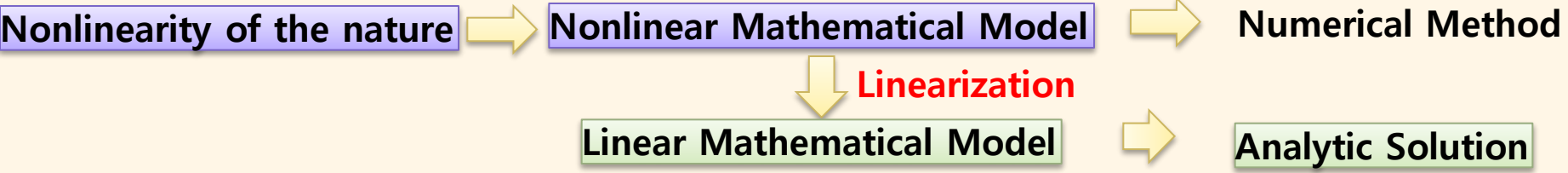
$d\mathbf{F} = P d\mathbf{S} = P n dS$   
 (미소 면적에 작용하는 힘)  
 (미소 면적)

$\mathbf{M} = \mathbf{r} \times d\mathbf{F} = \mathbf{r} \times P n dS = P(\mathbf{r} \times \mathbf{n}) dS$

- Hydrostatic Moment : (모멘트) = (거리) × (힘)
- ✓ 미소 면적에 작용하는 모멘트 :
- ✓ Total moment :

$$\mathbf{M} = \iint_{S_B} P(\mathbf{r} \times \mathbf{n}) dS$$


# Nonlinearity



## Ex) Roll Motion of a Ship

$$I\phi'' = \sum M$$

$$I\phi'' = M_{body} + M_{surface}$$

( $S_B$ : wetted surface)

(미소 면적에 작용하는 힘)  
 $dF = PdS = PndS$   
 (미소 면적)

Hydrostatic Moment : (모멘트)=(거리) X (힘)

✓ 미소 면적에 작용하는 모멘트 :

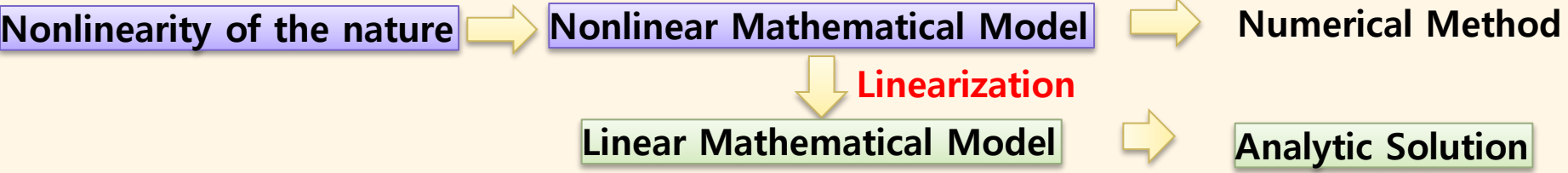
$$dM = \mathbf{r} \times d\mathbf{F} = \mathbf{r} \times PndS = P(\mathbf{r} \times \mathbf{n})dS$$

✓ Total moment :

$$\mathbf{M} = \iint_{S_B} P(\mathbf{r} \times \mathbf{n})dS$$




# Nonlinearity



## Ex) Roll Motion of a Ship

$$I\phi'' = \sum M$$

$$I\phi'' = M_{body} + M_{surface}$$

$$= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external}$$

$$= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}$$

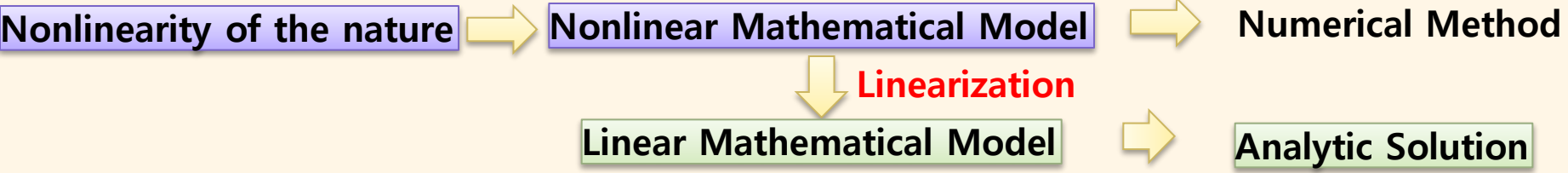
( $S_B$ : wetted surface)

Hydrostatic Moment : (모멘트)=(거리) X (힘)

- ✓ 미소 면적에 작용하는 모멘트 :  $d\mathbf{M} = \mathbf{r} \times d\mathbf{F} = \mathbf{r} \times PndS = P(\mathbf{r} \times \mathbf{n})dS$
- ✓ Total moment :  $\mathbf{M} = \iint_{S_B} P(\mathbf{r} \times \mathbf{n})dS$

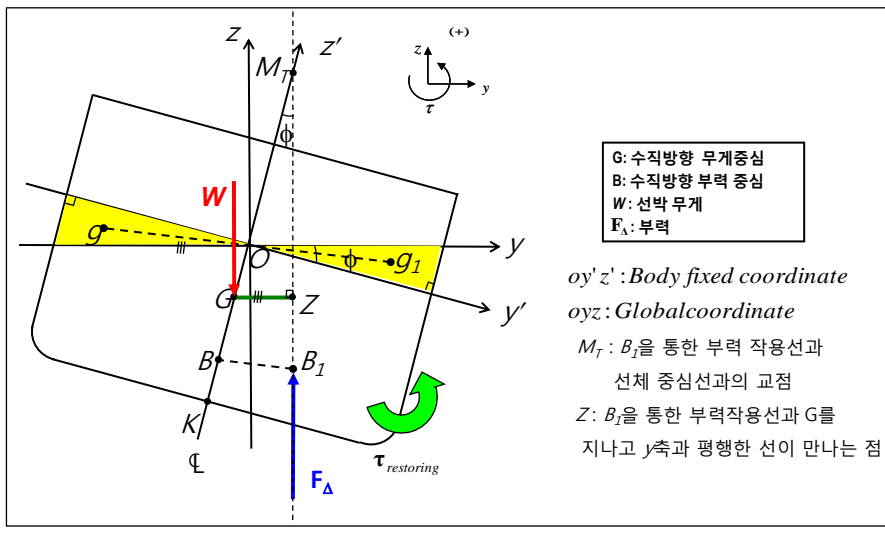


# Nonlinearity

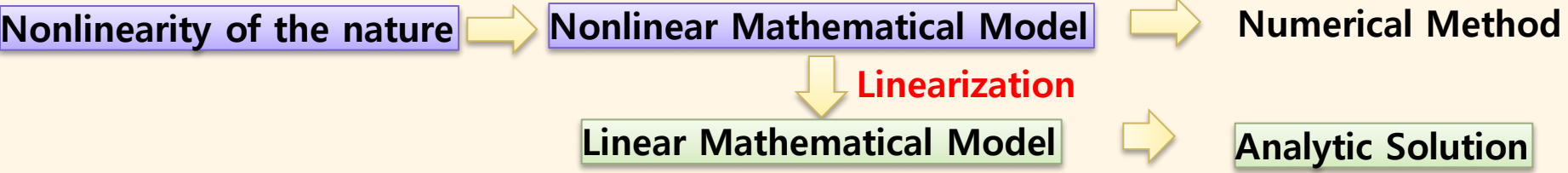


## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$



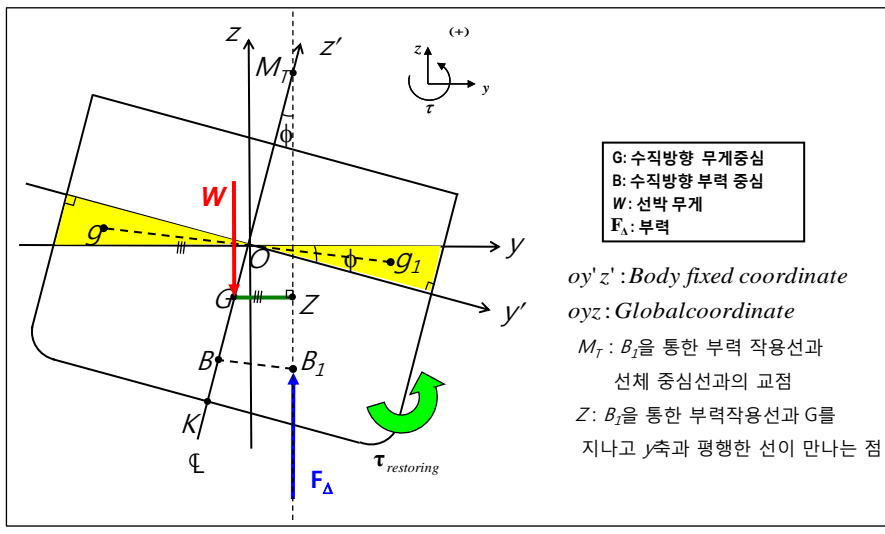
# Nonlinearity



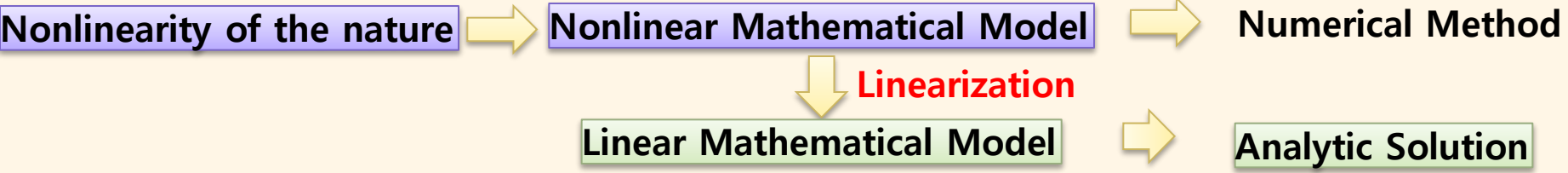
## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$

1)  $M_{gravity} = (-W) \times 0 = 0$



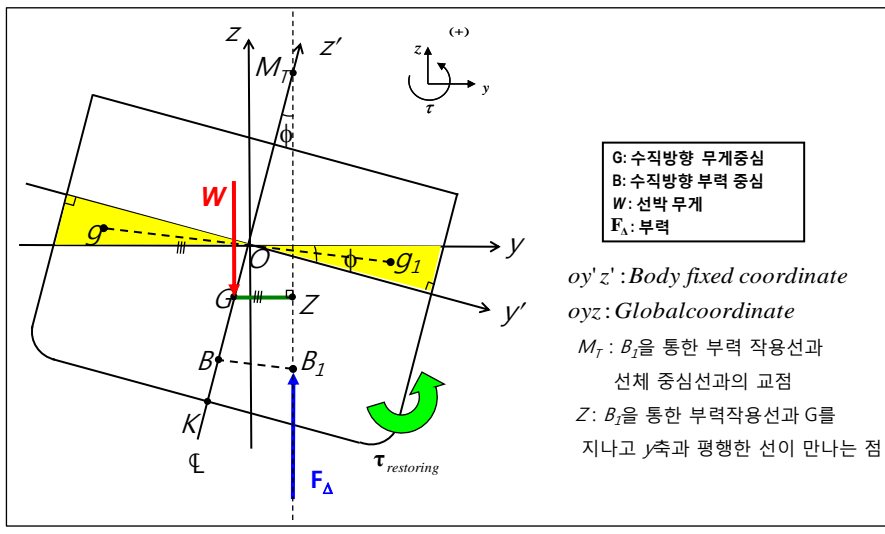
# Nonlinearity



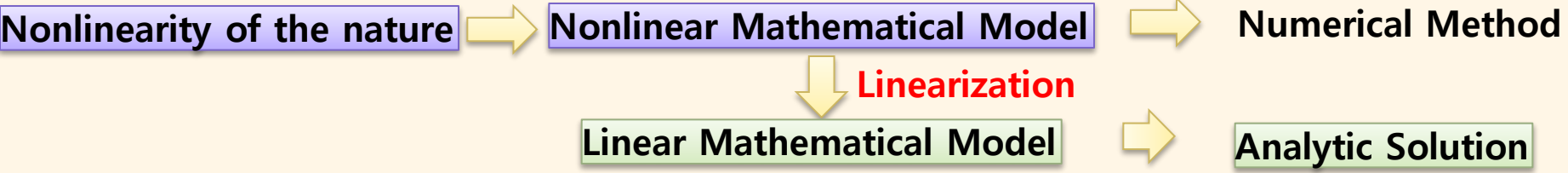
## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$

- 1)  $M_{gravity} = (-W) \times 0 = 0$
- 2)  $M_{buoyancy} = \Delta \overline{GZ}$



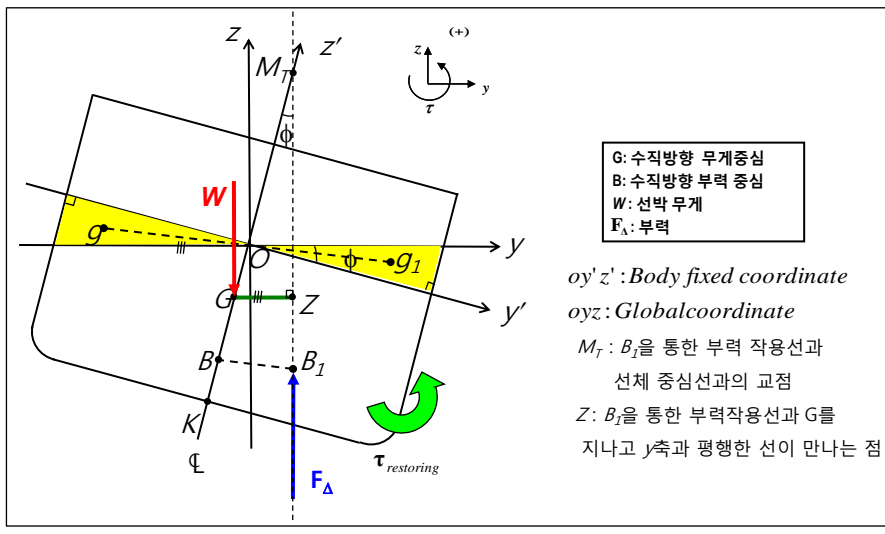
# Nonlinearity



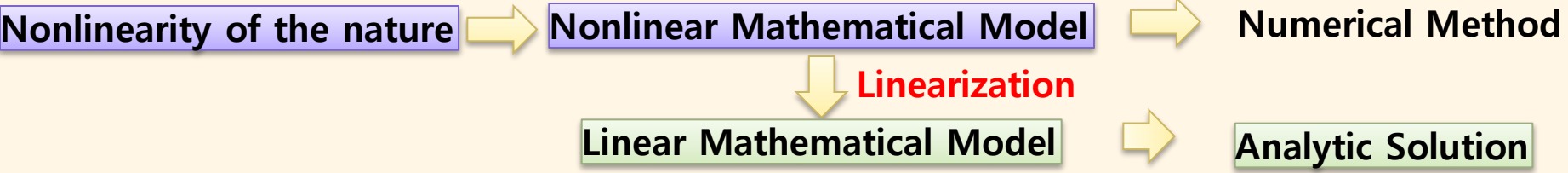
## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$

- 1)  $M_{gravity} = (-W) \times 0 = 0$
- 2)  $M_{buoyancy} = \Delta \overline{GZ}$
- 3)  $M_{damping} = -b\phi'$  , b:damping coeff.



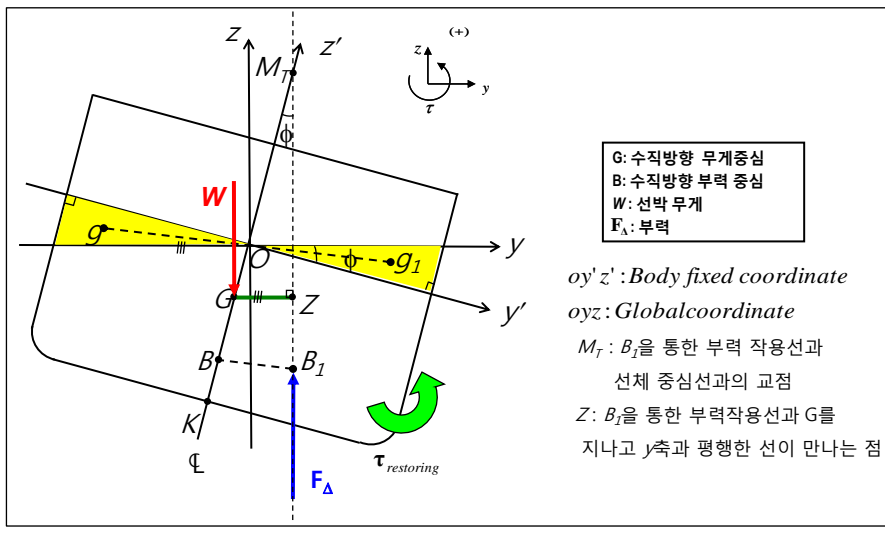
# Nonlinearity



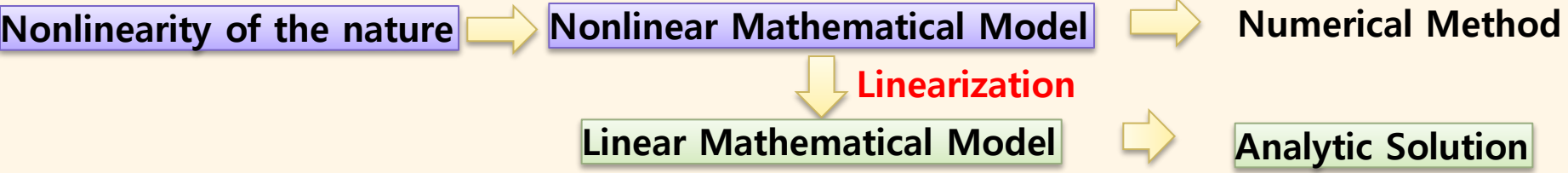
## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$

- 1)  $M_{gravity} = (-W) \times 0 = 0$
- 2)  $M_{buoyancy} = \Delta \overline{GZ}$
- 3)  $M_{damping} = -b\phi'$  , b:damping coeff.
- 4)  $M_{added} = -I_{add}\phi''$  ,  $I_{add}$  : added Mass moment of inertia



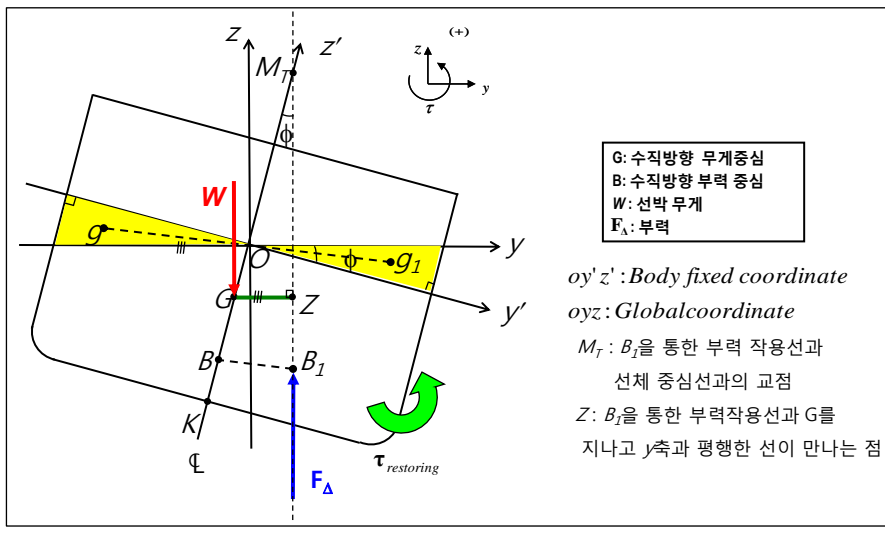
# Nonlinearity



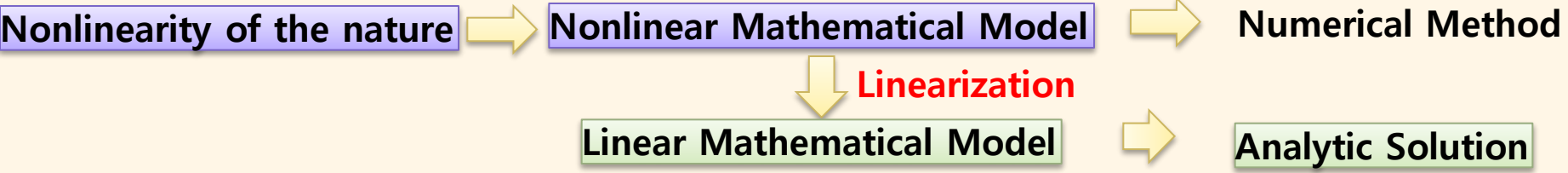
## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$

- 1)  $M_{gravity} = (-W) \times 0 = 0$
- 2)  $M_{buoyancy} = \Delta \overline{GZ}$
- 3)  $M_{damping} = -b\phi'$  , b:damping coeff.
- 4)  $M_{added} = -I_{add}\phi''$  ,  $I_{add}$  : added Mass moment of inertia
- 5)  $M_{external}$  : external moment



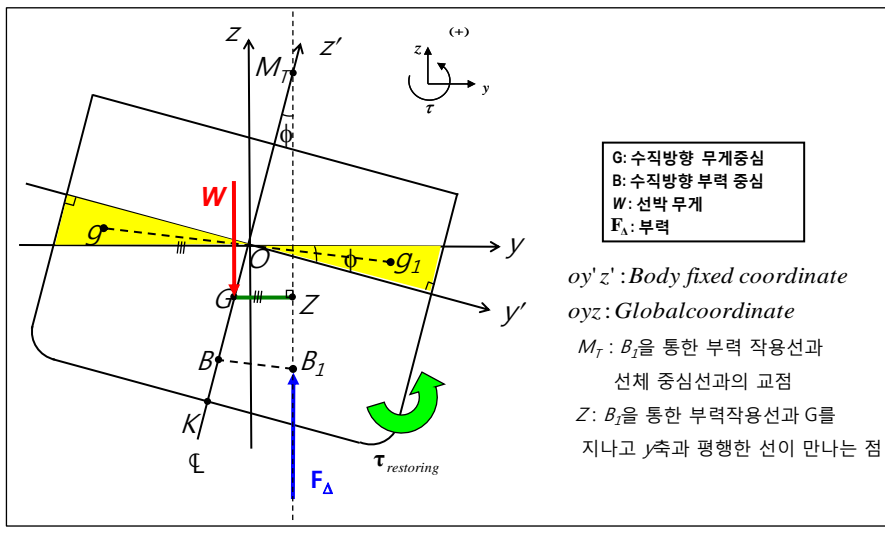
# Nonlinearity



## Ex) Roll Motion of a Ship

$$\begin{aligned}
 I\phi'' &= M_{body} + M_{surface} \\
 &= M_{body} + \iint P_{static} (\mathbf{r} \times \mathbf{n}) ds + \iint P_{dynamic} (\mathbf{r} \times \mathbf{n}) ds + M_{external} \\
 &= M_{gravity} + M_{buoyancy} + M_{damping} + M_{added} + M_{external}
 \end{aligned}$$

- 1)  $M_{gravity} = (-W) \times 0 = 0$
- 2)  $M_{buoyancy} = \overline{\Delta GZ}$
- 3)  $M_{damping} = -b\phi'$  , b:damping coeff.
- 4)  $M_{added} = -I_{add}\phi''$  ,  $I_{add}$  : added Mass moment of inertia
- 5)  $M_{external}$  : external moment

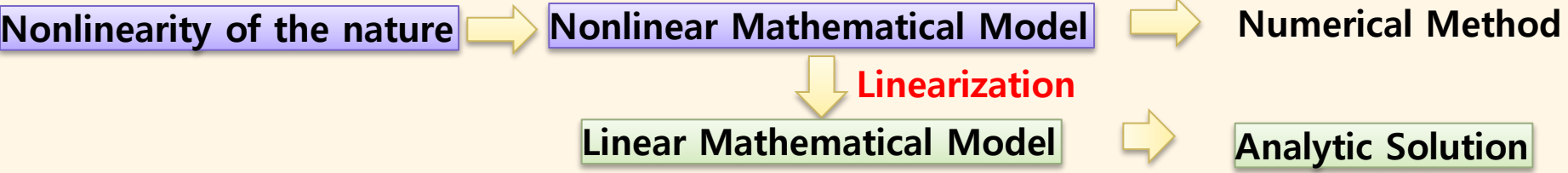


$$\therefore I\phi'' = (-W) \times 0 + (\overline{\Delta GZ}) + (-b\phi') + (-I_{add}\phi'') + M_{ext}$$





# Nonlinearity

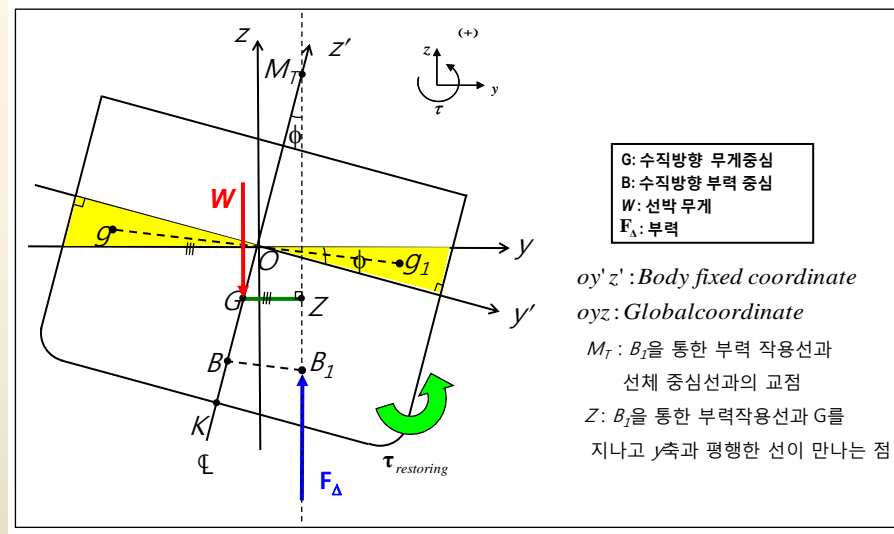


## Ex) Roll Motion of a Ship

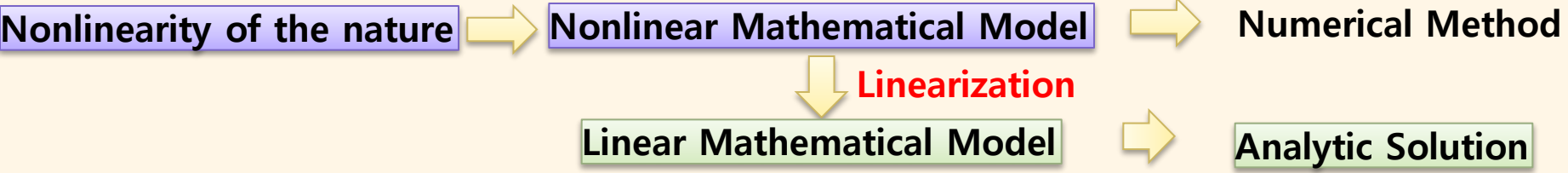
$$I\phi'' = (-W)\times 0 + (\Delta\overline{GZ}) + (-b\phi') + (-I_{add}\phi'') + M_{ext}$$

✓ Archimedes' Principle

$$W = \Delta$$



# Nonlinearity



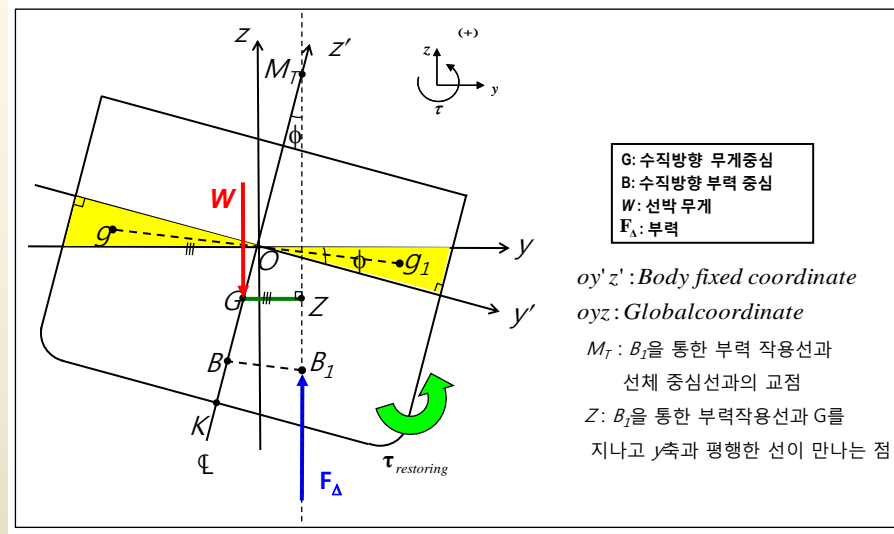
## Ex) Roll Motion of a Ship

$$I\phi'' = (-W)\times 0 + (\Delta\overline{GZ}) + (-b\phi') + (-I_{add}\phi'') + M_{ext}$$

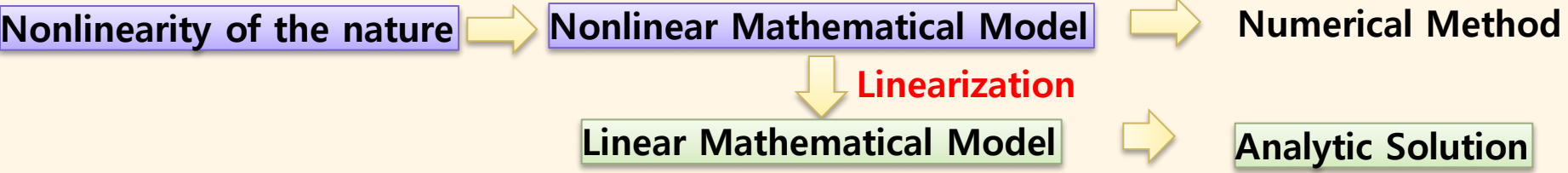
$$\therefore (I + I_{add})\phi'' + b\phi' - \Delta\overline{GZ} = M_{external}$$

✓ Archimedes' Principle

$$W = \Delta$$



# Nonlinearity



## Ex) Roll Motion of a Ship

$$I\phi'' = (-W) \times 0 + (\Delta \overline{GZ}) + (-b\phi') + (-I_{add}\phi'') + M_{ext}$$

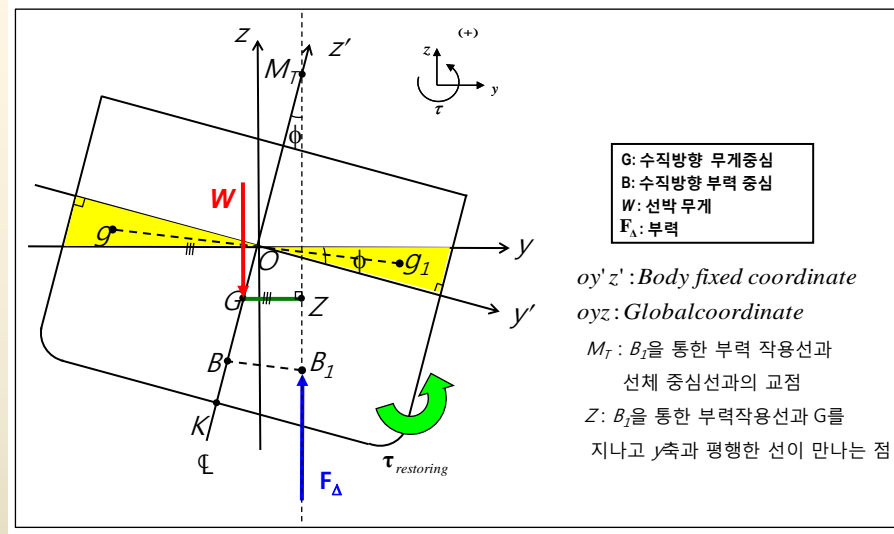
$$\therefore (I + I_{add})\phi'' + b\phi' - \Delta \overline{GZ} = M_{external}$$

✓ Archimedes' Principle

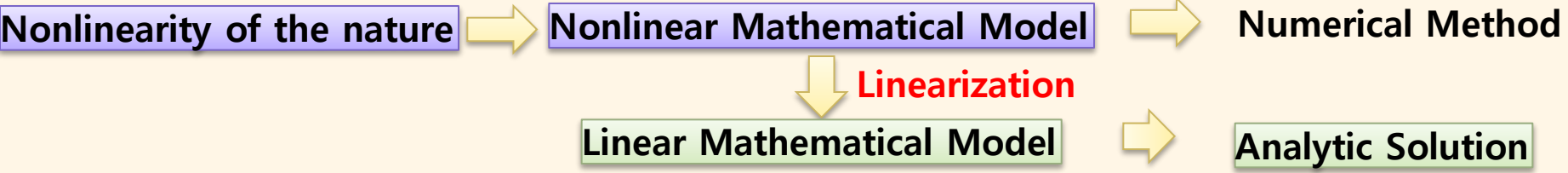
$$W = \Delta$$

Consider restoring moment for the point G

$$\tau_{restoring} = \Delta \overline{GZ}, \Delta = -W$$



# Nonlinearity



## Ex) Roll Motion of a Ship

$$I\phi'' = (-W) \times 0 + (\Delta \overline{GZ}) + (-b\phi') + (-I_{add}\phi'') + M_{ext}$$

$$\therefore (I + I_{add})\phi'' + b\phi' - \Delta \overline{GZ} = M_{external}$$

✓ Archimedes' Principle

$$W = \Delta$$

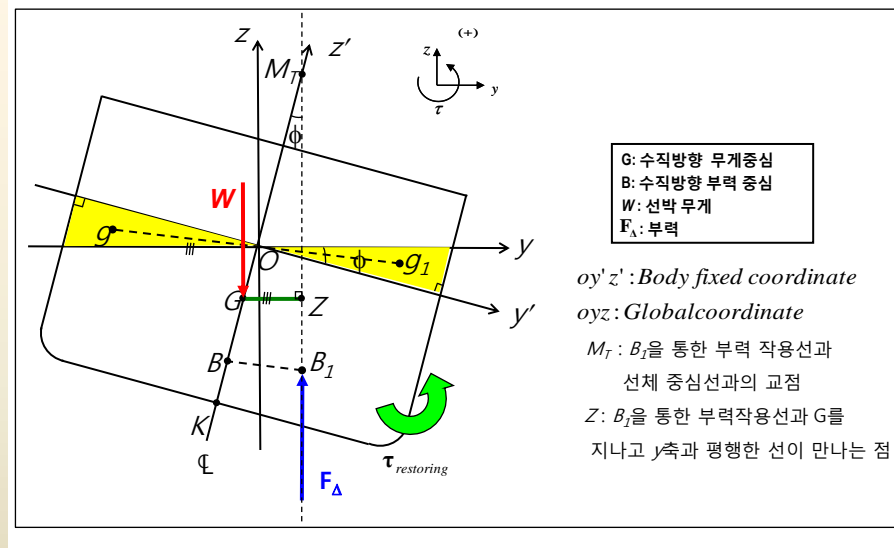
Consider restoring moment for the point G

$$\tau_{restoring} = \Delta \overline{GZ}, \Delta = -W$$

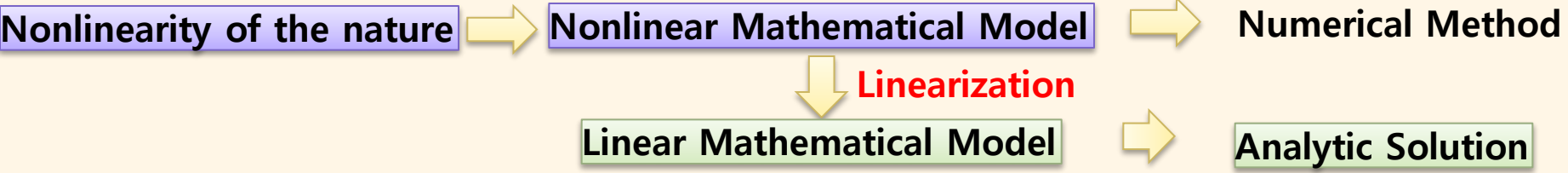
Assum.  $M_T$  doesn't change for small  $\phi$  ( $< 10^\circ$ )

$\overline{GM}_T$ : Metacenter Height

$$\overline{GZ} \approx -\overline{GM}_T \cdot \sin \phi$$



# Nonlinearity



## Ex) Roll Motion of a Ship

$$I\phi'' = (-W) \times 0 + (\overline{\Delta GZ}) + (-b\phi') + (-I_{add}\phi'') + M_{ext}$$

✓ Archimedes' Principle

$$W = \Delta$$

$$\therefore (I + I_{add})\phi'' + b\phi' - \overline{\Delta GZ} = M_{external}$$

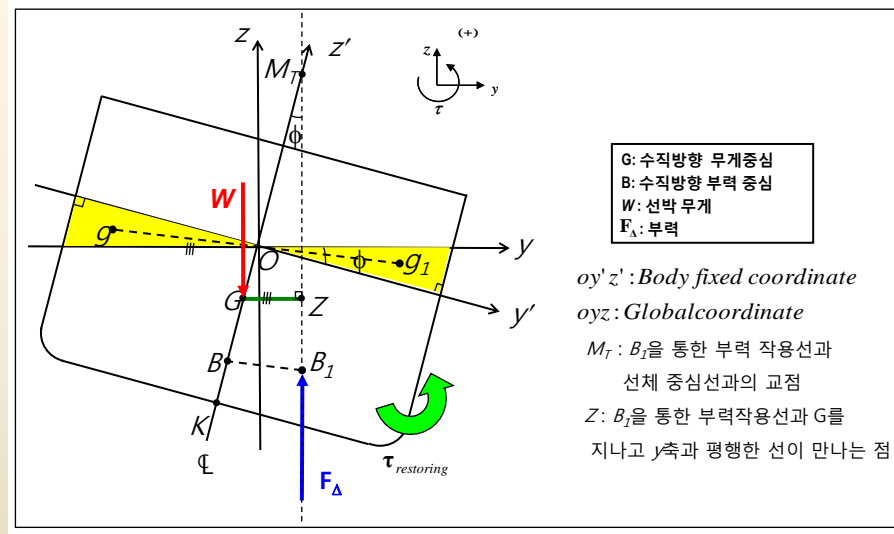
Consider restoring moment for the point G

$$\tau_{restoring} = \overline{\Delta GZ}, \Delta = -W$$

Assum.  $M_T$  doesn't change for small  $\phi$  ( $< 10^\circ$ )

$\overline{GM}_T$ : Metacenter Height

$$\overline{GZ} \approx -\overline{GM}_T \cdot \sin \phi$$

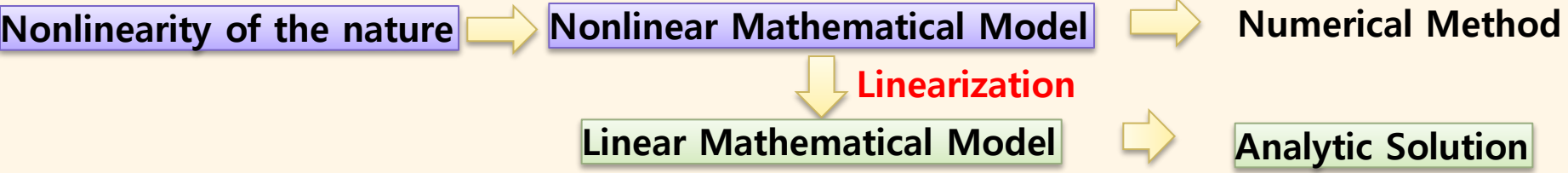


$$\therefore (I + I_{add})\phi'' + b\phi' + \overline{\Delta GM}_T \sin \phi = M_{external}$$



# Nonlinearity

$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots$$



## Ex) Roll Motion of a Ship

$$\therefore (I + I_{add})\phi'' + b\phi' + \overline{\Delta GM}_T \sin \phi = M_{external}$$

✓ Archimedes' Principle  
 $W = \Delta$

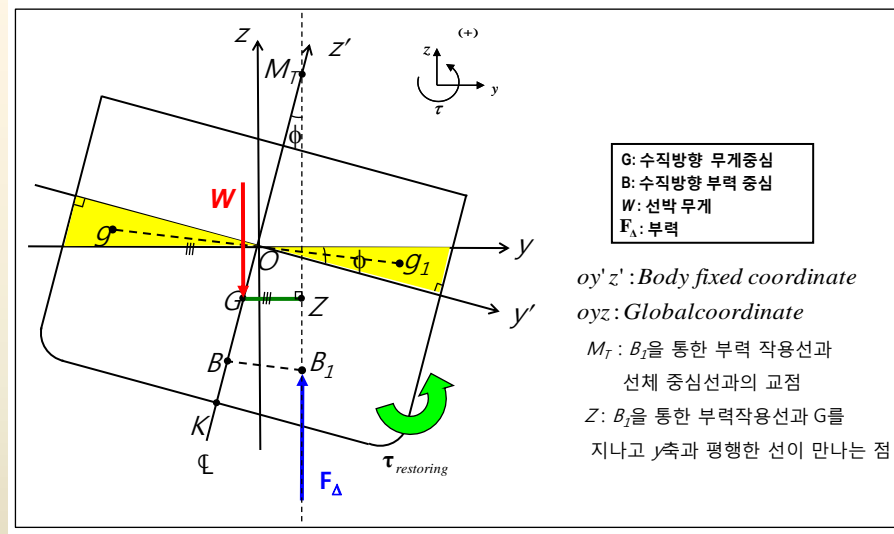
For small  $\phi$   $\sin \phi \cong \phi$

$$(I + I_{add})\phi'' + b\phi' + \overline{\Delta GM}_T \phi = M_{external}$$

정적 평형상태 서는 가속도와 속도 성분이 사라지므로,

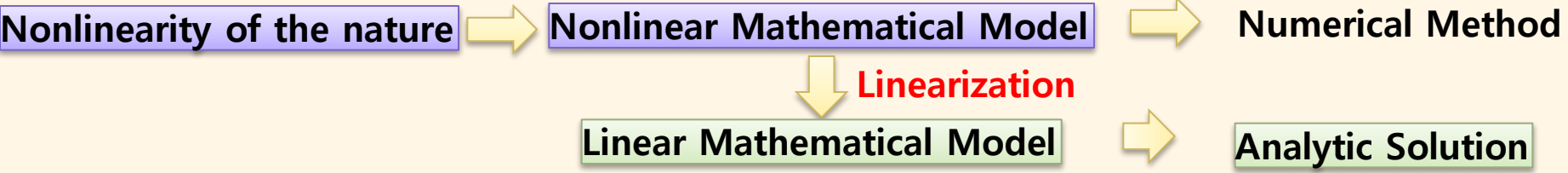
$$\overline{\Delta GM}_T \phi = M_{external}$$

양변의 모멘트가 같아지는  $\phi$  까지 기울어 진다.



# Nonlinearity

$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots$$



## Ex) Roll Motion of a Ship

$$\therefore (I + I_{add})\phi'' + b\phi' + \overline{\Delta GM}_T \sin \phi = M_{external}$$

✓ Archimedes' Principle  
 $W = \Delta$

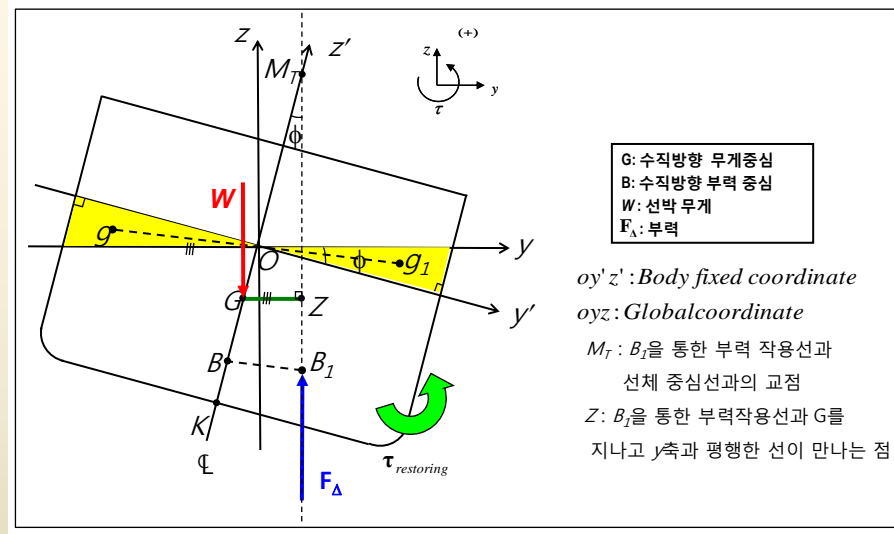
For small  $\phi$   $\sin \phi \cong \phi$

$$(I + I_{add})\phi'' + b\phi' + \overline{\Delta GM}_T \phi = M_{external}$$

정적 평형상태 서는 가속도와 속도 성분이 사라지므로,

$$\overline{\Delta GM}_T \phi = M_{external}$$

양변의 모멘트가 같아지는  $\phi$  까지 기울어 진다.

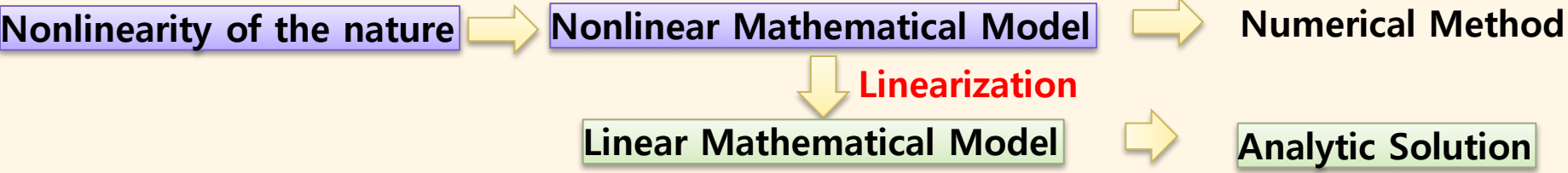


$$\therefore (I + I_{add})\phi'' + b\phi' + \overline{\Delta GM}_T \phi = M_{external}$$

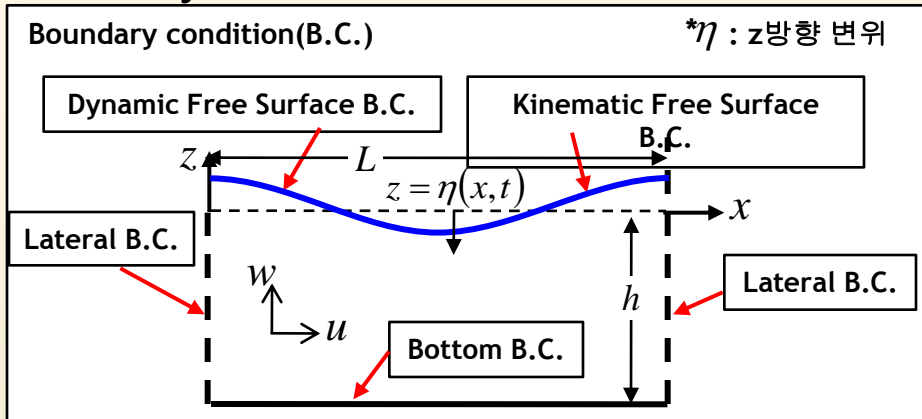
← Second order Linear Ordinary Differential Equation



# Nonlinearity



## Ex) 해양파 Free surface Boundary Condition



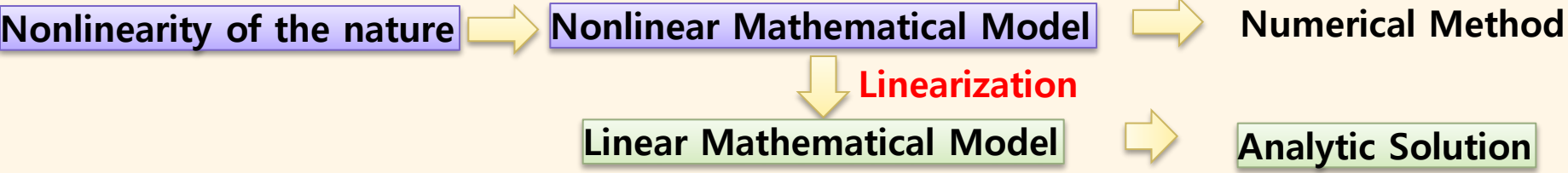
**<Summary of the 2-D periodic water wave boundary condition>**

<p>① Kinematic Free Surface B.C.(KFSBC)</p> $\frac{\partial \Phi}{\partial z} - \frac{\partial \eta}{\partial t} - \frac{\partial \Phi}{\partial x} \frac{\partial \eta}{\partial x} = 0 \quad (\text{on } z = \eta)$ <p>② Bottom B.C. (BBC)</p> $\frac{\partial \Phi}{\partial z} \Big _{z=-h} = 0$	<p>③ Dynamic Free Surface B.C. (DFSBC)</p> $\frac{\partial \Phi}{\partial t} + \frac{1}{2}  \nabla \Phi ^2 + g\eta = 0 \quad (\text{on } z = \eta)$ <p>④ Lateral B.C.</p> $\Phi(x, z, t) = \Phi(x, z, t + T)$ $\Phi(x, z, t) = \Phi(x + L, z, t)$
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# Nonlinearity



Ex) 해양파 Free surface Boundary Condition

① Kinematic Free Surface B.C.(KFSBC)

$$\frac{\partial \Phi}{\partial z} - \frac{\partial \eta}{\partial t} - \frac{\partial \Phi}{\partial x} \frac{\partial \eta}{\partial x} = 0 \quad (\text{on } z = \eta)$$

Taylor series로 전개하면,

$$\left( \frac{\partial \Phi}{\partial z} - \frac{\partial \eta}{\partial t} - \frac{\partial \Phi}{\partial x} \frac{\partial \eta}{\partial x} \right)_{z=\eta} = \left( \frac{\partial \Phi}{\partial z} - \frac{\partial \eta}{\partial t} - \frac{\partial \Phi}{\partial x} \frac{\partial \eta}{\partial x} \right)_{z=0} + \eta \frac{\partial}{\partial z} \left( \frac{\partial \Phi}{\partial z} - \frac{\partial \eta}{\partial t} - \frac{\partial \Phi}{\partial x} \frac{\partial \eta}{\partial x} \right)_{z=0} + \cancel{H.O.T} = 0$$

(High Order Term)  
↓

여기서 파장에 비해 파고가 작다고 가정했으므로,  $\eta \ll 1$

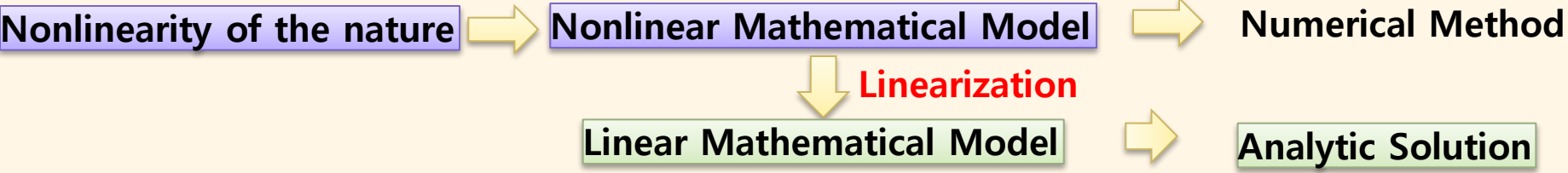
$$u|_{z=0} = \frac{\partial \Phi}{\partial x} \Big|_{z=0} \ll 1, \quad w|_{z=0} = \frac{\partial \Phi}{\partial z} \Big|_{z=0} \ll 1$$

작은 텀이 두 개 이상 곱해진 경우를 무시하면,

$$\left( \frac{\partial \Phi}{\partial z} - \frac{\partial \eta}{\partial t} \right)_{z=0} = 0 \Rightarrow \text{Linearized Kinematic Free Surface B.C.(KFSBC)}$$



# Nonlinearity



Ex) 해양파 Free surface Boundary Condition

③ Dynamic Free Surface B.C. (DFSBC)

$$\frac{\partial \Phi}{\partial t} + \frac{1}{2} |\nabla \Phi|^2 + g\eta = 0 \quad (\text{on } z = \eta)$$

Taylor series로 전개하면,

$$\left( \frac{\partial \Phi}{\partial t} + \frac{1}{2} |\nabla \Phi|^2 + g\eta \right)_{z=\eta} = \left( \frac{\partial \Phi}{\partial t} + \frac{1}{2} |\nabla \Phi|^2 + g\eta \right)_{z=0} + \eta \frac{\partial}{\partial z} \left( \frac{\partial \Phi}{\partial t} + \frac{1}{2} |\nabla \Phi|^2 + g\eta \right)_{z=0} + \overset{\text{(High Order Term)}}{H.O.T} = 0$$

여기서 파장에 비해 파고가 작다고 가정했으므로,  $\eta \ll 1$

$$u|_{z=0} = \frac{\partial \Phi}{\partial x} \Big|_{z=0} \ll 1, \quad w|_{z=0} = \frac{\partial \Phi}{\partial z} \Big|_{z=0} \ll 1$$

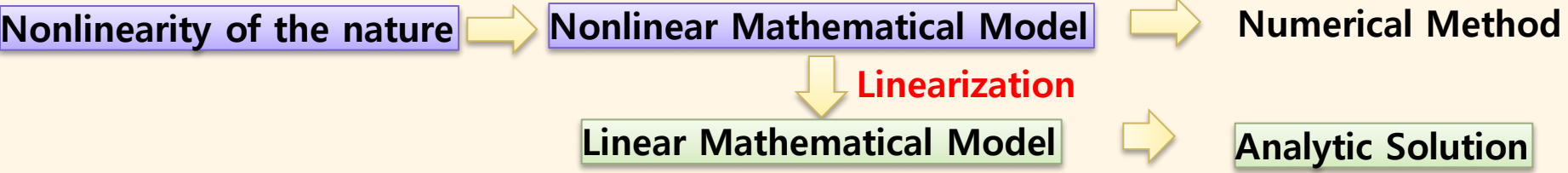
작은 틱이 두 개 이상 곱해진 경우를 무시하면,

$$\left( \frac{\partial \Phi}{\partial t} + g\eta \right)_{z=0} = 0 \Rightarrow \eta = -\frac{1}{g} \frac{\partial \Phi}{\partial t} \quad (\text{on } z = 0)$$

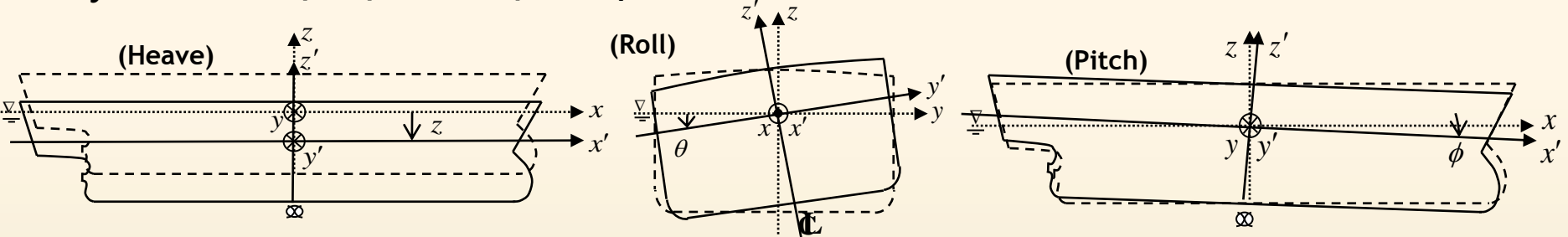
=> Linearized Dynamic Free Surface B.C.(DFSBC)



# Nonlinearity



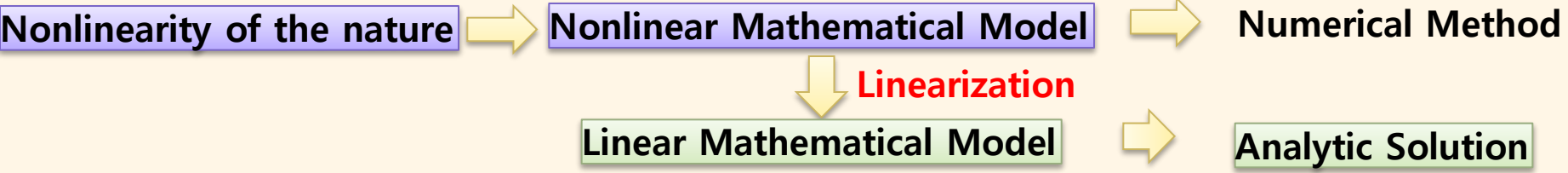
Ex) hydrostatics : 복원력(모멘트)의 선형화



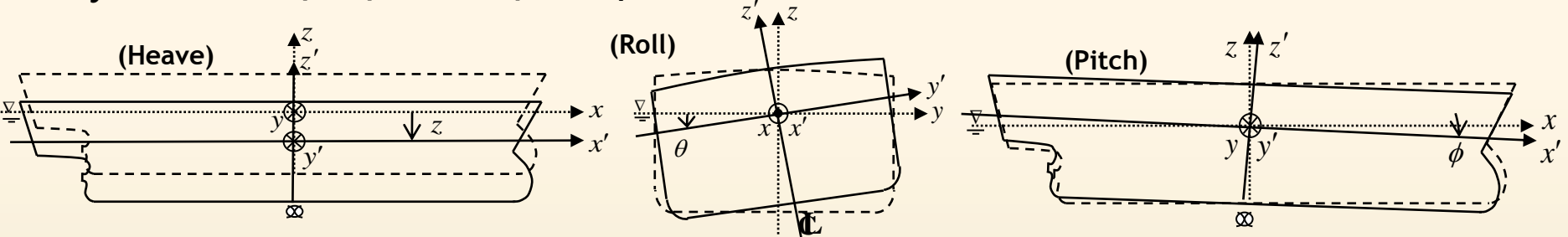
초기 자세( $z, \theta, \phi$ )에서 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )는?



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )는?

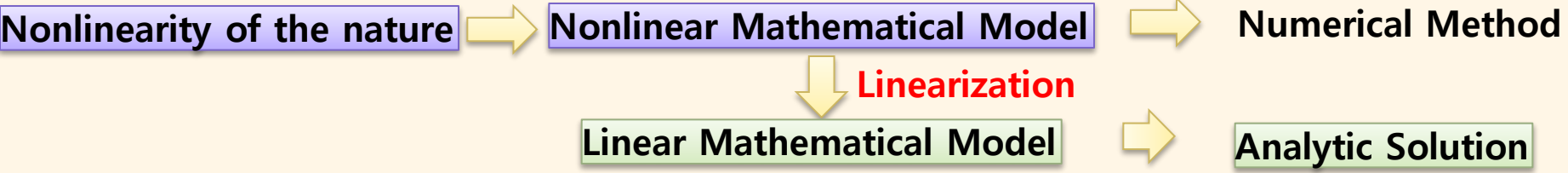
$$F(z, \theta, \phi)$$

$$M_T(z, \theta, \phi)$$

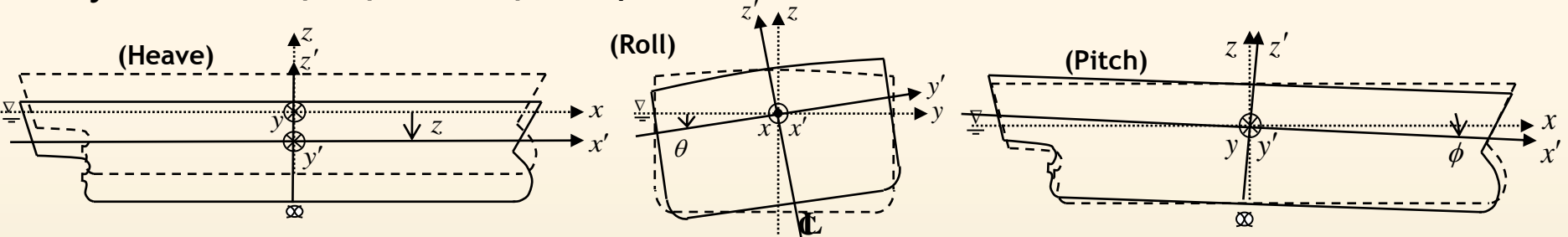
$$M_L(z, \theta, \phi)$$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화

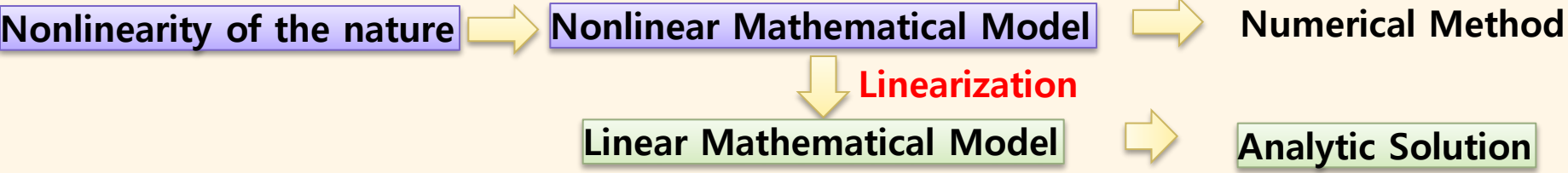


초기 자세( $z, \theta, \phi$ )에서 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )는?

$F(z, \theta, \phi)$		$F(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$M_T(z, \theta, \phi)$		$M_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$M_L(z, \theta, \phi)$		$M_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화

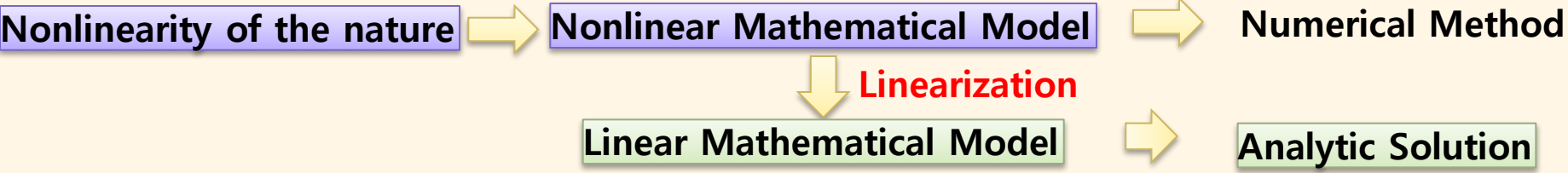


초기 자세( $z, \theta, \phi$ )에서  
 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )를 알고 있을 때,  
 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의  
 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )는?

$\mathbf{F}(z, \theta, \phi)$		$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$\mathbf{M}_T(z, \theta, \phi)$		$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$\mathbf{M}_L(z, \theta, \phi)$		$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )는?

$\mathbf{F}(z, \theta, \phi)$	?	$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$\mathbf{M}_T(z, \theta, \phi)$		$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$\mathbf{M}_L(z, \theta, \phi)$		$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$

Taylor series expansion

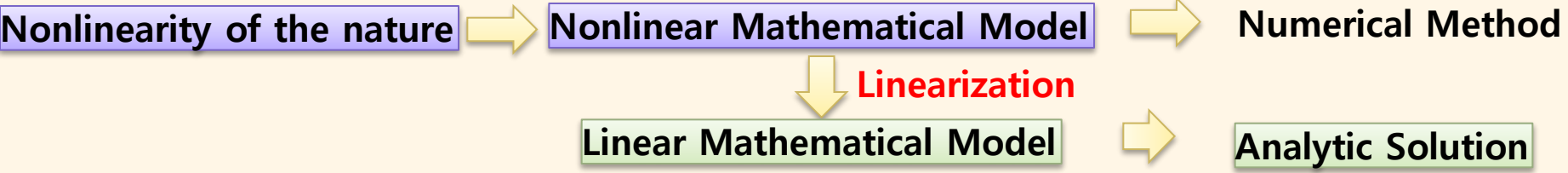
$$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) = \mathbf{F}(z, \theta, \phi) + \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi + \dots$$

$$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) = \mathbf{M}_T(z, \theta, \phi) + \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi + \dots$$

$$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) = \mathbf{M}_L(z, \theta, \phi) + \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi + \dots$$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )는?

$\mathbf{F}(z, \theta, \phi)$		$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$\mathbf{M}_T(z, \theta, \phi)$		$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$
$\mathbf{M}_L(z, \theta, \phi)$		$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi)$

**Taylor series expansion**

$$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) = \mathbf{F}(z, \theta, \phi) + \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi + \dots$$

↗ 선형화

$$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) = \mathbf{M}_T(z, \theta, \phi) + \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi + \dots$$

↗ 선형화

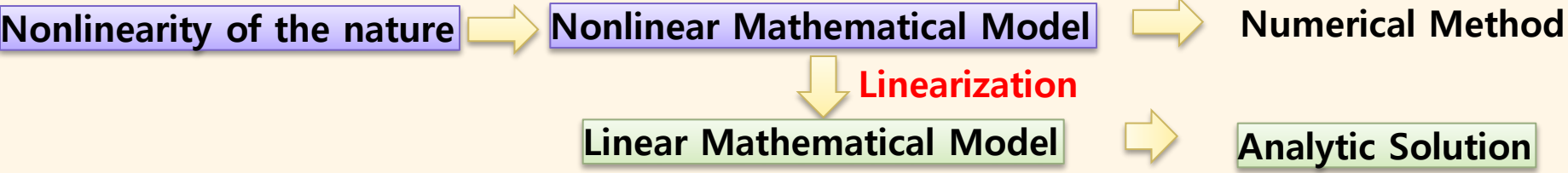
$$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) = \mathbf{M}_L(z, \theta, \phi) + \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi + \dots$$

↗ 선형화





# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )는?

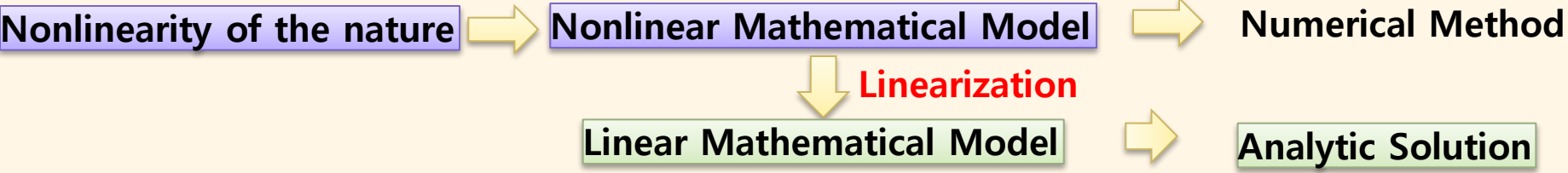
$$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) - \mathbf{F}(z, \theta, \phi) = \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi$$

$$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) - \mathbf{M}_T(z, \theta, \phi) = \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi$$

$$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) - \mathbf{M}_L(z, \theta, \phi) = \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi$$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )는?

$$\mathbf{F}(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) - \mathbf{F}(z, \theta, \phi) = \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi$$

$$\mathbf{M}_T(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) - \mathbf{M}_T(z, \theta, \phi) = \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi$$

$$\mathbf{M}_L(z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi) - \mathbf{M}_L(z, \theta, \phi) = \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi$$



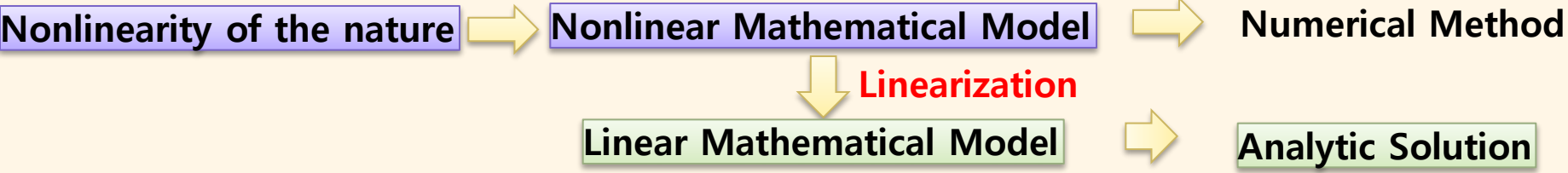
$$\Delta \mathbf{F} = \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi$$

$$\Delta \mathbf{M}_T = \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi$$

$$\Delta \mathbf{M}_L = \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi$$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서  
 복원력(  $\mathbf{F}$  ), 횡 방향 복원 모멘트(  $\mathbf{M}_T$  ), 종 방향 복원 모멘트(  $\mathbf{M}_L$  )를 알고 있을 때,  
 미소 변화된 자세(  $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$  )에서의  
 복원력(  $\mathbf{F}$  ), 횡 방향 복원 모멘트(  $\mathbf{M}_T$  ), 종 방향 복원 모멘트(  $\mathbf{M}_L$  )는?

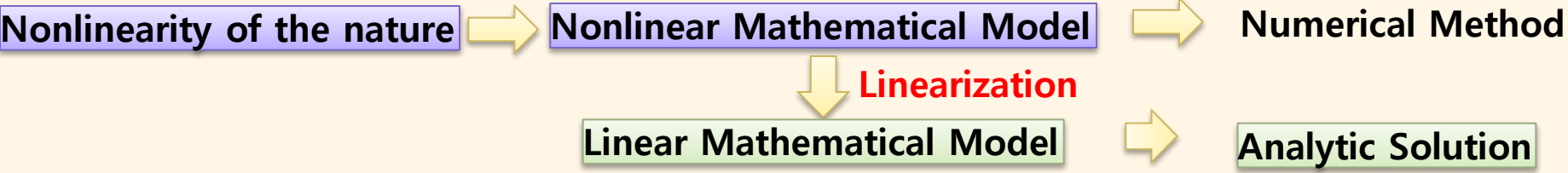
$$\Delta \mathbf{F} = \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi$$

$$\Delta \mathbf{M}_T = \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi$$

$$\Delta \mathbf{M}_L = \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi$$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $\mathbf{F}$ ), 횡 방향 복원 모멘트( $\mathbf{M}_T$ ), 종 방향 복원 모멘트( $\mathbf{M}_L$ )는?

✓ Matrix로 표현  $\mathbf{b} = \mathbf{Ax}$

$$\Delta \mathbf{F} = \frac{\partial \mathbf{F}}{\partial z} \Delta z + \frac{\partial \mathbf{F}}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{F}}{\partial \phi} \Delta \phi$$

$$\Delta \mathbf{M}_T = \frac{\partial \mathbf{M}_T}{\partial z} \Delta z + \frac{\partial \mathbf{M}_T}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_T}{\partial \phi} \Delta \phi$$

$$\Delta \mathbf{M}_L = \frac{\partial \mathbf{M}_L}{\partial z} \Delta z + \frac{\partial \mathbf{M}_L}{\partial \theta} \Delta \theta + \frac{\partial \mathbf{M}_L}{\partial \phi} \Delta \phi$$

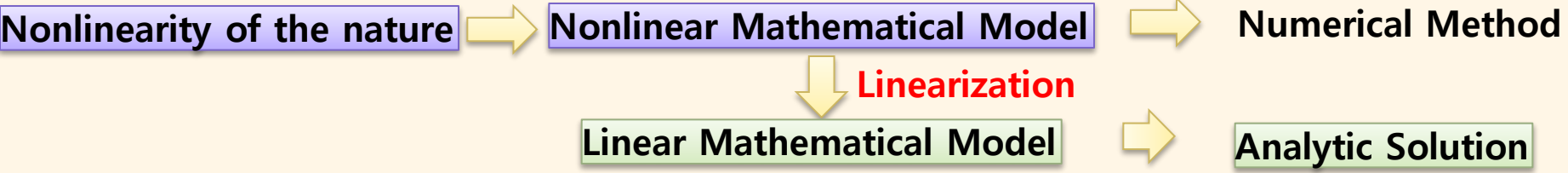
변수 3개, 식 3개



$$\begin{pmatrix} \Delta \mathbf{F} \\ \Delta \mathbf{M}_T \\ \Delta \mathbf{M}_L \end{pmatrix} = \begin{pmatrix} \frac{\partial \mathbf{F}}{\partial z} & \frac{\partial \mathbf{F}}{\partial \theta} & \frac{\partial \mathbf{F}}{\partial \phi} \\ \frac{\partial \mathbf{M}_T}{\partial z} & \frac{\partial \mathbf{M}_T}{\partial \theta} & \frac{\partial \mathbf{M}_T}{\partial \phi} \\ \frac{\partial \mathbf{M}_L}{\partial z} & \frac{\partial \mathbf{M}_L}{\partial \theta} & \frac{\partial \mathbf{M}_L}{\partial \phi} \end{pmatrix} \begin{pmatrix} \Delta z \\ \Delta \theta \\ \Delta \phi \end{pmatrix}$$



# Nonlinearity



Ex) hydrostatics : 복원력(모멘트)의 선형화



초기 자세( $z, \theta, \phi$ )에서 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )를 알고 있을 때, 미소 변화된 자세( $z + \Delta z, \theta + \Delta \theta, \phi + \Delta \phi$ )에서의 복원력( $F$ ), 횡 방향 복원 모멘트( $M_T$ ), 종 방향 복원 모멘트( $M_L$ )는?

1. 자세의 변화량이 주어질 때, 힘(모멘트)의 변화량을 구하는 경우

$$\Delta F = \frac{\partial F}{\partial z} \Delta z + \frac{\partial F}{\partial \theta} \Delta \theta + \frac{\partial F}{\partial \phi} \Delta \phi$$

$$\Delta M_T = \frac{\partial M_T}{\partial z} \Delta z + \frac{\partial M_T}{\partial \theta} \Delta \theta + \frac{\partial M_T}{\partial \phi} \Delta \phi$$

$$\Delta M_L = \frac{\partial M_L}{\partial z} \Delta z + \frac{\partial M_L}{\partial \theta} \Delta \theta + \frac{\partial M_L}{\partial \phi} \Delta \phi$$

$$b = Ax$$

$$\begin{pmatrix} \Delta F \\ \Delta M_T \\ \Delta M_L \end{pmatrix} = \begin{pmatrix} \frac{\partial F}{\partial z} & \frac{\partial F}{\partial \theta} & \frac{\partial F}{\partial \phi} \\ \frac{\partial M_T}{\partial z} & \frac{\partial M_T}{\partial \theta} & \frac{\partial M_T}{\partial \phi} \\ \frac{\partial M_L}{\partial z} & \frac{\partial M_L}{\partial \theta} & \frac{\partial M_L}{\partial \phi} \end{pmatrix} \begin{pmatrix} \Delta z \\ \Delta \theta \\ \Delta \phi \end{pmatrix}$$

Find  $\Delta F, \Delta M_T, \Delta M_L$  (left column), Given  $\Delta z, \Delta \theta, \Delta \phi$  (right column)

※ A가 선형화되어 있기 때문에 반복 계산(iteration)을 해야 함

2. 힘(모멘트)의 변화량이 주어질 때, 자세의 변화량을 구하는 경우

$$x = A^{-1}b$$

$$\begin{pmatrix} \Delta F \\ \Delta M_T \\ \Delta M_L \end{pmatrix} = \begin{pmatrix} \frac{\partial F}{\partial z} & \frac{\partial F}{\partial \theta} & \frac{\partial F}{\partial \phi} \\ \frac{\partial M_T}{\partial z} & \frac{\partial M_T}{\partial \theta} & \frac{\partial M_T}{\partial \phi} \\ \frac{\partial M_L}{\partial z} & \frac{\partial M_L}{\partial \theta} & \frac{\partial M_L}{\partial \phi} \end{pmatrix} \begin{pmatrix} \Delta z \\ \Delta \theta \\ \Delta \phi \end{pmatrix}$$

Given  $\Delta F, \Delta M_T, \Delta M_L$  (left column), Find  $\Delta z, \Delta \theta, \Delta \phi$  (right column)

