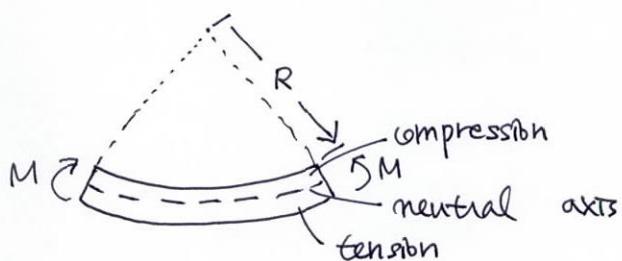


Mechanics of slender bodies

Why slender rods? ($L \gg d$)

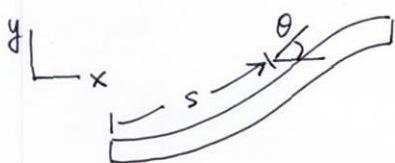
good models for biological polymers (DNA, protein filaments)
 cilia, flagella, ...

Beam equations



$$M = EI \frac{1}{R}$$

$I = \int y^2 dA$: second moment of inertia of the cross-section



$$\frac{1}{R} = \frac{d\theta}{ds}$$

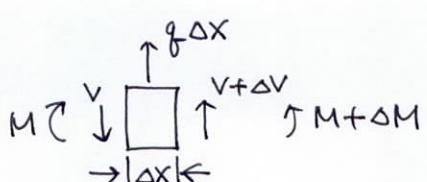
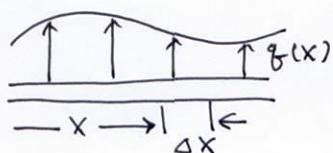
$$\frac{d\theta}{ds} = \frac{1}{EI} M$$

for small α , $x \approx s$, $\frac{dy}{dx} \approx \frac{dy}{ds} = \sin \theta \approx \theta$

$$\frac{dy}{dx^2} \equiv \frac{d\theta}{ds}$$

$$\frac{d^2y}{dx^2} = \frac{M(x)}{EI}$$

Beam under distributed loading



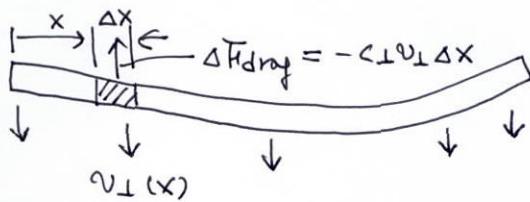
q : load-intensity fm

$$\frac{dV}{dx} + q = 0, \quad \frac{dM}{dx} + V = 0$$

$$\frac{d^2M}{dx^2} = q$$

$$\frac{d^2}{dx^2} (EI \frac{d^2v}{dx^2}) = f(x)$$

* Hydrodynamics of slender rods



drag force per unit length

$$f_{\perp}(x) = -C_{\perp}v_{\perp}(x) = -C_{\perp} \frac{\partial y}{\partial x}(x)$$

bending moment at pt x due to drag force on the RHS of pt

$$M(x) = \int_x^L f_{\perp}(x') (x' - x) dx'$$

$$\frac{\partial^2 M}{\partial x^2} = f_{\perp}(x) = -C_{\perp} \frac{\partial y}{\partial t}$$

$$EI \frac{\partial^2 y}{\partial x^2} = M$$

$$EI \frac{\partial^4 y}{\partial x^4} = \frac{\partial^2 M}{\partial x^2} = -C_{\perp} \frac{\partial y}{\partial t}$$

$$\frac{\partial^4 y}{\partial x^4} = -\frac{C_{\perp}}{EI} \frac{\partial y}{\partial t} : \text{hydrodynamic beam equation}$$

* Hydrodynamic bending modes

B.C. for an unconstrained filament

$$\frac{\partial^2 y}{\partial x^2} = \frac{\partial^3 y}{\partial x^3} = 0 \quad \text{at} \quad x=0 \quad \text{for} \quad x=L$$

by separation of variables

$$y_n(x, t) = e^{-t/\tau_n} \left[\sinh \alpha_n \cos \frac{2\alpha_n}{L} (x - \frac{L}{2}) - \sin \alpha_n \cosh \frac{2\alpha_n}{L} (x - \frac{L}{2}) \right]$$

n odd

$$y_n(x, t) = e^{-t/\tau_n} \left[\cosh \alpha_n \sin \frac{2\alpha_n}{L} (x - \frac{L}{2}) + \sin \alpha_n \sinh \frac{2\alpha_n}{L} (x - \frac{L}{2}) \right]$$

n even

where

$$\gamma_n = \frac{C_L}{EI} \left(\frac{L}{2\alpha_n} \right)^4 . \quad \tan \alpha_n = (-1)^n \tanh \alpha_n \quad n=1, 2, 3, \dots$$

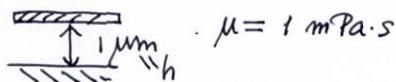
approximate values for α_n

$$\alpha_n \approx (n + \frac{1}{2}) \frac{\pi}{2} \quad n=1, 2, 3, \dots \quad (\alpha_1 \approx 2.365)$$

e.g. Relaxation of microtubules and actin filaments

microtubule

$$L = 50 \mu\text{m}, \quad \text{radius} = 15 \text{ nm}, \quad EI = 30 \times 10^{-24} \text{ N} \cdot \text{m}^2$$



relaxation time for $n=1$.

$$\gamma_1 = \frac{2.6 \times 10^{-3}}{30 \times 10^{-24}} \left(\frac{50 \times 10^{-6}}{2 \times 2.365} \right)^4$$

$$C_L = \frac{4\pi G}{\ln(2h/r)} = \frac{4\pi (10^{-3})}{\ln(2 \times 10^{-6} / 15 \times 10^{-9})} \\ = 2.5 \times 10^{-3}$$

$$= 1.1 \text{ s}$$

* Thermal bending of filaments

thermal forces \rightarrow shape fluctuations of flexible filaments

Persistence length L_p .

: length of filament over which thermal bending becomes appreciable

if $L \gg L_p$: tangent angles at the two ends uncorrelated.



time average of the cosine of $\theta(s) - \theta(0)$ decreases exponentially as the arc length s increases :

$$\langle \cos [\theta(s) - \theta(0)] \rangle = \exp \left(-\frac{s}{2L_p} \right)$$

Using the principle of equipartition of energy
 (average energy of a molecule $\langle U \rangle = \frac{1}{2} kT$)

$$L_p = \frac{EI}{kT}$$

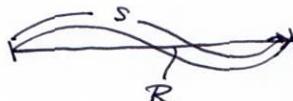
Polymer	L_p
DNA	50 nm
actin filament	15 μm
microtubule	6 mm

In 3-D, a filament can bend in two different directions

$$\Delta\theta_1, \Delta\theta_2.$$

$$\langle \cos[\Delta\theta_{3D}(s)] \rangle = \exp\left(-\frac{s}{L_p}\right)$$

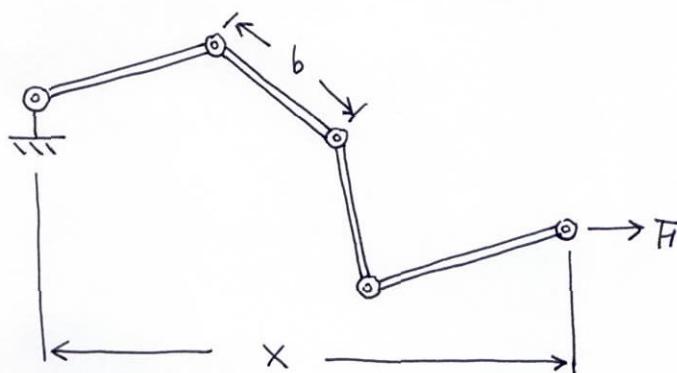
• end-to-end length



$$\langle R^2 \rangle = 2L_p^2 \left[\exp\left(-\frac{L}{L_p}\right) - 1 + \frac{L}{L_p} \right]$$

: statistical physics.

* Entropic elasticity of a freely jointed chain



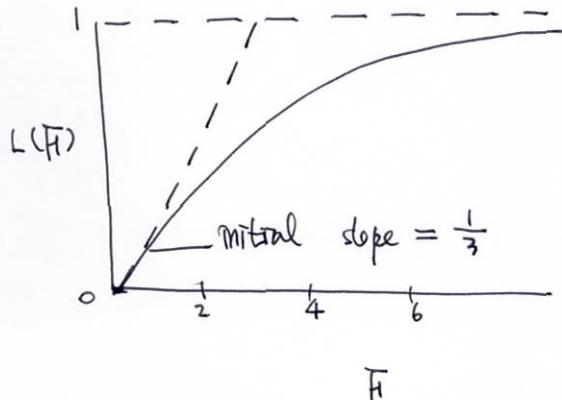
• entropic spring : { proteins that have segmental flexibility (antibodies, motor proteins)
 unfolded proteins
 DNA

• resistance to extension

← extension decreases the disorder
 and the corresponding decrease in entropy costs free energy

$$\langle X \rangle = nb \cdot L\left(\frac{Fb}{kT}\right)$$

$L\left(\frac{Fb}{kT}\right)$: Langevin function , $L(x) \equiv \frac{e^x + e^{-x}}{e^x - e^{-x}} - \frac{1}{x}$.



$$\text{for small } F, \quad L\left(\frac{Fb}{kT}\right) \approx \frac{Fb}{3kT}.$$

$$F = \frac{3kT}{nb^2} \langle X \rangle$$

$$kT = 4.1164 \times 10^{-21} \text{ J} \quad (T=25^\circ\text{C})$$