

2009 spring

*Advanced Physical Metallurgy*  
*“Amorphous Materials”*

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# Ease of glass formation

- Glass forming ability: basically depending on glass transition
  - ➡ unsolved mystery ➡ no universal rule: empirical rules
  - ➡ still alchemy stage: by trial & error considering various aspects

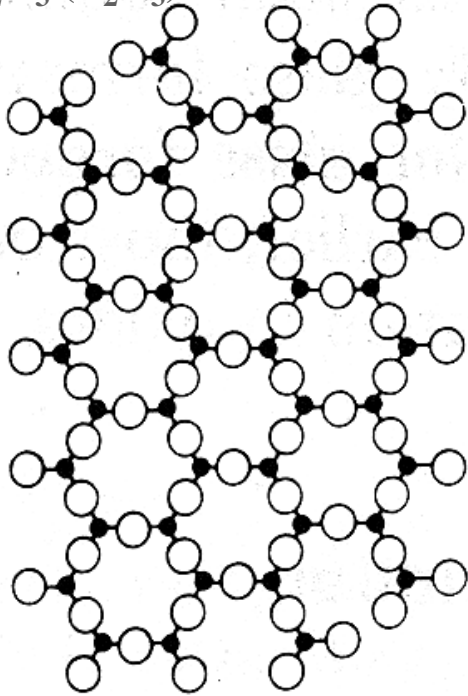
## 1. Structure & topology

- **Internal energy** : mainly considered in oxide glasses
    - ➡ Depends on the bonding types and arrangements of constituent element
    - ➡ similar types and arrangements of atomic bonding in crystal and amorphous (=similar atomic structure)
- (1) Continuous Random Network (CRN) → GFA ↑

# 1. Structure & topology: CRN

Oxygen is shared by two  $\text{AO}_3$  triangles

$\text{A}_2\text{O}_3$  ( $\text{B}_2\text{O}_3$ )



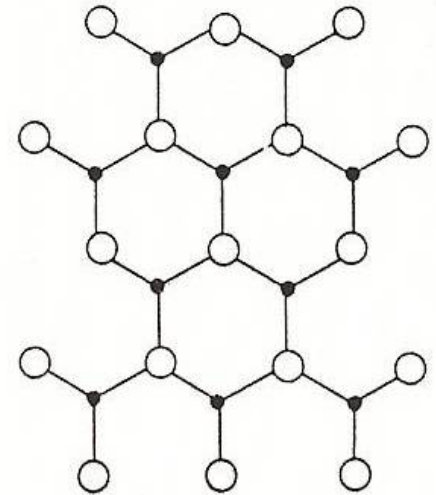
(a)

Small gap of internal energy between crystal and glass

→ GFA ↑

by three  $\text{AO}_3$  triangles

crystal AO



(b)

Energy for orientation change is relatively large.

→ GFA ↓

## (2) Randomly dense packed structure in metallic glasses

### 1) Atomic size difference: TM – metalloid (M, ex) Boron)

- M is located at **interstitial site** of random packed structure of TM.
- denser → by increasing resistivity of crystallization, GFA ↑
- Ex) Fe-B: tetrahedron with B on the center position

### 2) min. solute content, $C_B^*$ : empirical rule

By Egami & Waseda: in A-B binary system

$$C_B^{\min} \left| \frac{(v_B - v_A)}{v_A} \right| = C_B^{\min} \left| \left( \frac{r_B}{r_A} \right)^3 - 1 \right| \approx 0.1$$

v: atomic volume  
A: matrix, B: solute

minimum concentration of B for glass formation

- Inversely proportional to atomic volume mismatch

### 3) Multi-component system (over 3 elements)

with large atomic size difference : **confusion theory**

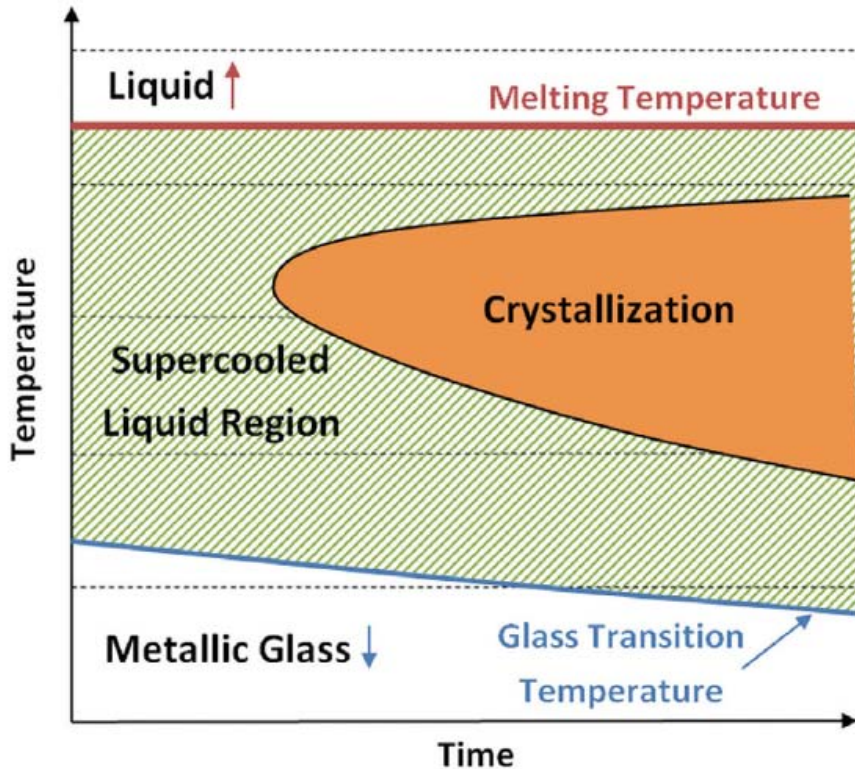
- **packing density** ↑ → **dense random packed structure**

## 2. Thermodynamic aspect

### 1) deep eutectic condition

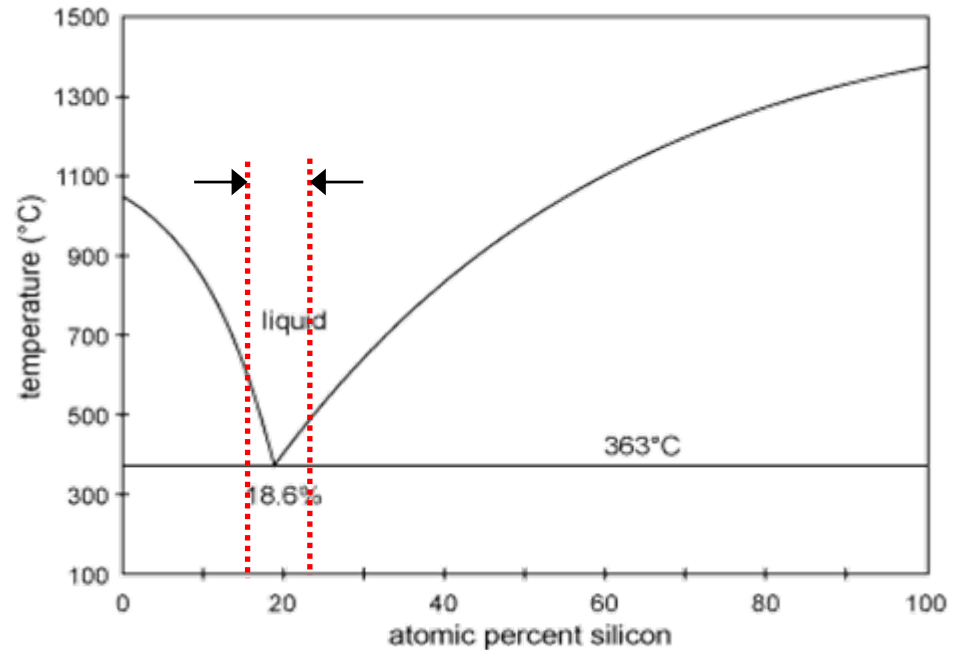
- decreasing melting point → less supercooled at  $T_g$

ex) metallic / inorganic system



**Glass forming region:**

**Compositions near the eutectic**



## 2. Thermodynamic aspect

- ***How much can decrease the eutectic temperature at real state rather than that at ideal state?***
- ***Main points***
  - 1) ***If the liquid has large negative heat of mixing, the eutectic temperature at real state decreases than that at ideal state.***
  - 2) ***Eutectic composition depends on the magnitude of free energy for solid formation of A and B.***
    - ***The composition is not changed by other special properties of liquid.***
  - 3) ***Excess entropy of mixing at high temperature is positive.***

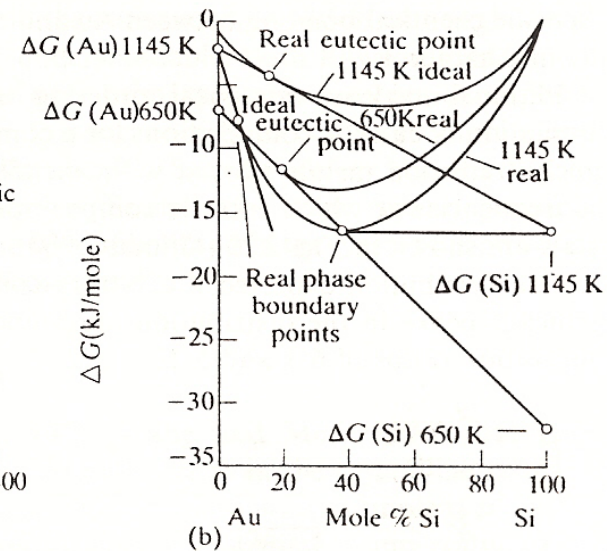
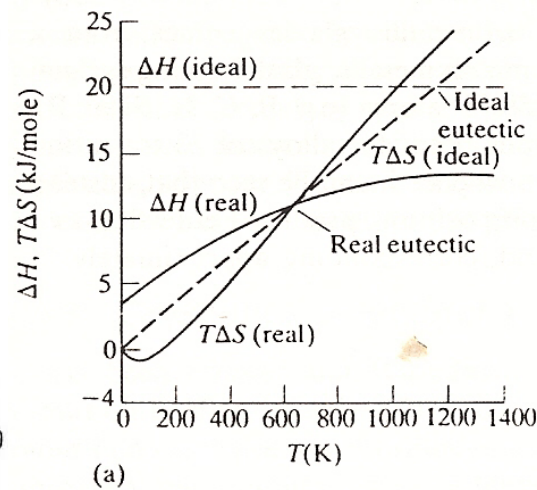
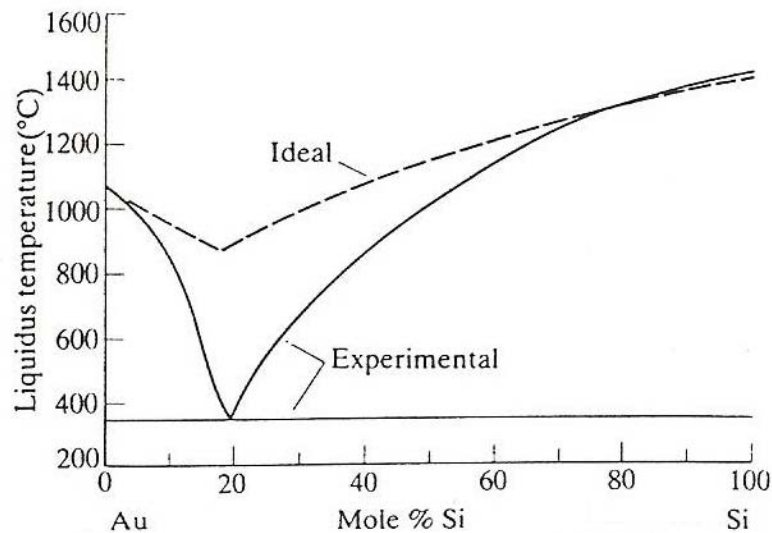
***With decreasing the temperature, the value changes negative near eutectic temperature.***

    - ***This phenomena is not matched to decrease eutectic temperature.***

## 2. Thermodynamic aspect

- **In Au-Si alloy system,**

- **The real eutectic temp. is lowered considerably from the value of expected for an ideal solution.**
- **The large decrease in  $T_E$  is shown to result from a large negative excess free energy of mixing, for which the dominant contribution is the **enthalpy**.**



## 2. Thermodynamic aspect

→ Enthalpy of deep eutectic (A-B)

$$G = G_0 + G_{AB}^E$$

.....  
Excess free energy of mixing

$$G_{AB}^E(x, T) = H^E(x, T) - TS^E(x, T) \quad \text{x: composition, T: temperature}$$

$$\begin{aligned} ex) = \{ & a_0 + a_1x + a_2x^2 + T[b_0 + b_1x + b_2x^2 + b_3x^3 + b_4x^4] \\ & + cT \ln T + dT^2 \} x(1-x) \end{aligned}$$

decision of  $(a_i, b_i, c, d)$  →  $G_{AB}^E$  can be calculated.



## 2. Thermodynamic aspect

→ Free energy of liquid

$$G^L = (1-x)G_A^L + xG_B^L + G_{AB}^L$$

Pure A
Pure B
mixing

$$G_{AB}^L = G_{AB}^I + G_{AB}^E \quad (G_{AB}^E = H_{AB}^E - TS_{AB}^E)$$

Ideal
Excess

$$G_{AB}^I = -TS^I \quad (H^{ideal} = 0)$$

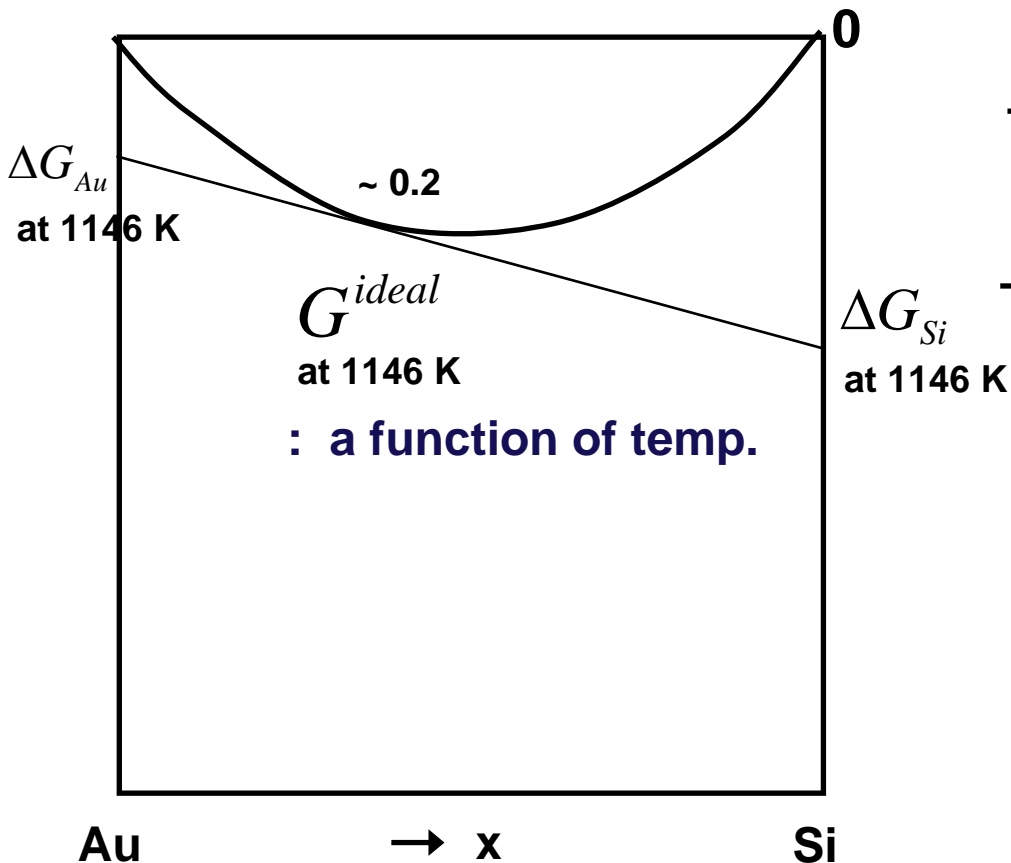
$$= RT(x \ln x + (1-x) \ln(1-x)) \quad \text{If } x, T \text{ is const., } \Rightarrow \text{ fixed.}$$

{	<b>Ideal state</b>	→	$G_{AB}^{ideal} (G_{AB}^E = 0)$	
	<b>real state</b>	→	$G_{AB}^{real} (G_{AB}^E \neq 0)$	↑    ⇒ <b>deep eutectic</b>

## 2. Thermodynamic aspect

- **Au-Si system**

→ Eutectic composition and temperature: common tangent method



Left & Right axes

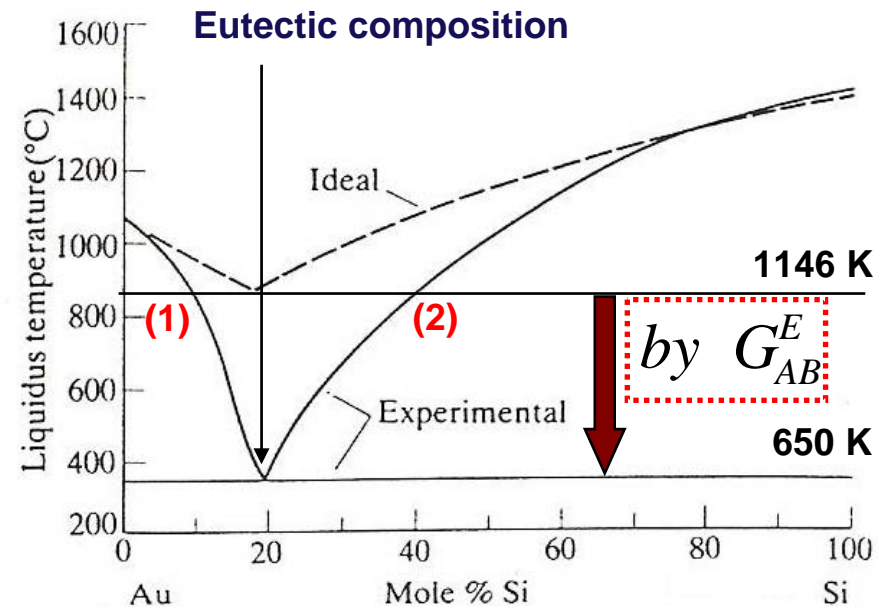
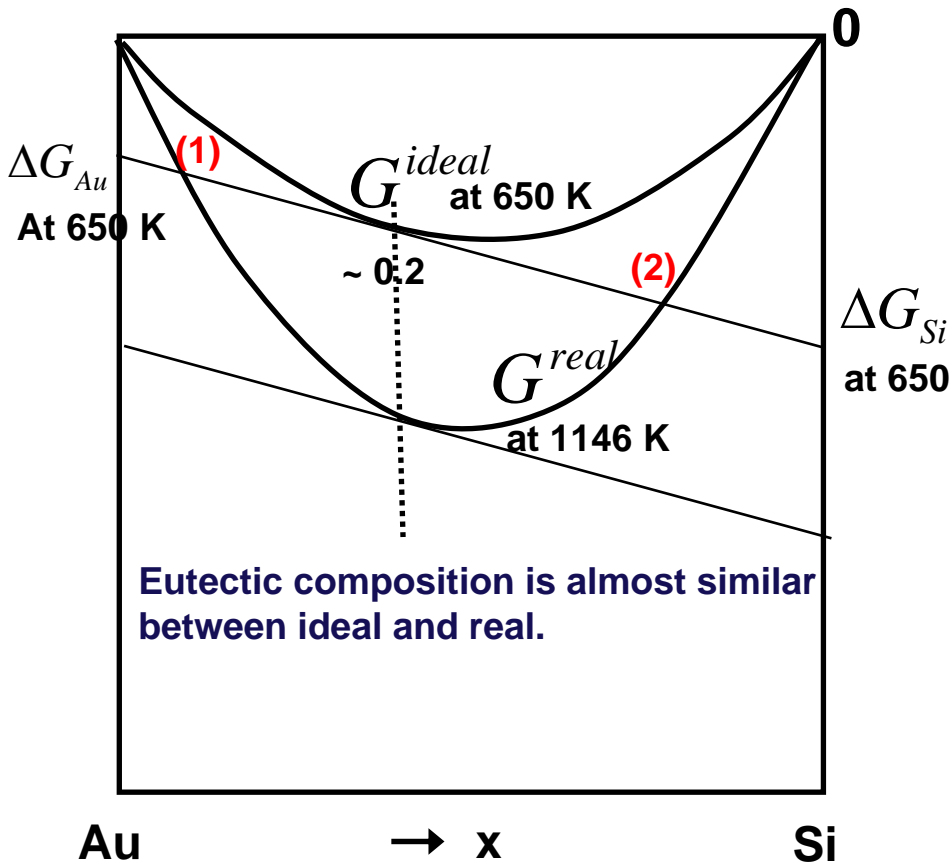
→ **Free energy difference between Solid and liquid in Au and Si**

→  $G_A^S - G_A^L$ : a function of temp.

$$ex) \Delta G_{Au} = -12550(1 - T / 1336)$$

## 2. Thermodynamic aspect

- **Au-Si system : decision of composition using G values**



1)  $G_{AB}^E \uparrow \rightarrow$  **deep eutectic**

2) *eutectic composition* :

- Almost similar between ideal and real
- Approximately calculated by pure component A and B of  $\Delta G^{S-L}$

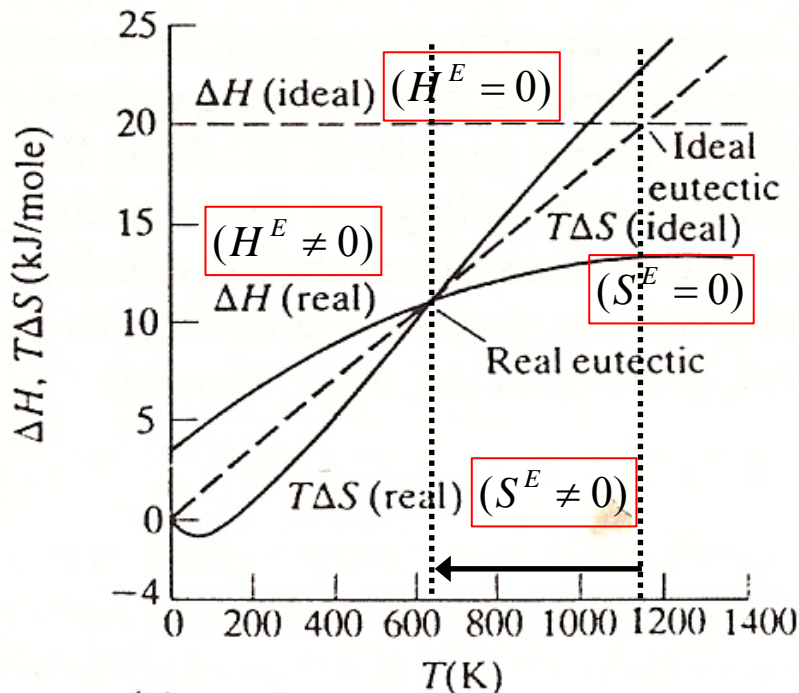
- Contribution of enthalpy in excess free energy**

$$G = H - TS$$

At eutectic point,  $G^L = G^S \rightarrow \boxed{\Delta H = T\Delta S}$

$$\Delta H = H^L - H^S = \underbrace{H^E}_{(H^I = 0)} + (1-x)[H_A^L - H_A^S] + x[H_B^L - H_B^S]$$

$$\Delta S = S^L - S^S = S^I + S^E + (1-x)[S_A^L - S_A^S] + x[S_B^L - S_B^S]$$



\* **Temperature dependence of the S and H contributions to the free energy balance at the eutectic points of real and ideal liquids**

$T\Delta S^{ideal}$  vs  $T\Delta S^{real}$  : **Similar**

$\Delta H^{ideal}$  vs  $\Delta H^{real}$  : **Big different**

∴ **decrease of  $T_E$  by excess enthalpy of mixing**

→ **deep eutectic** → **GFA** ↑

(a)

- **deep eutectic** →  $H^E$  ↓ → **Occurrence of Short range ordering at liquid state, amorphous state**  
→ **Increase A-B bonding**

- **Excess entropy: relatively less dominant to decrease eutectic temperature**

Ex) Au-Si system

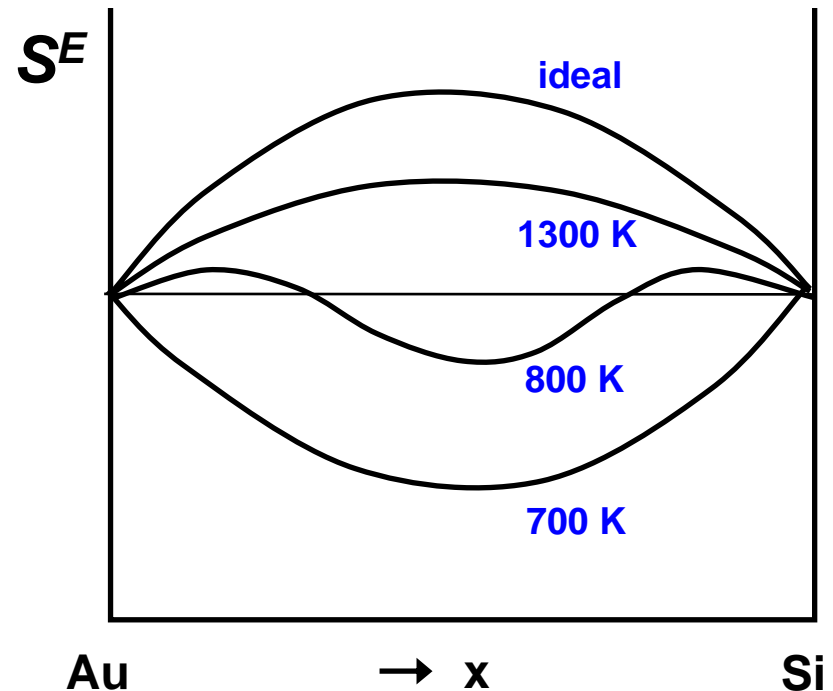
→ **Positive excess entropy**

→ **But, at eutectic temperature**

$$S^E < 0 \text{ by SRO}$$

disturb to decrease of eut. temp.

→ **canceled out by effect of enthalpy**

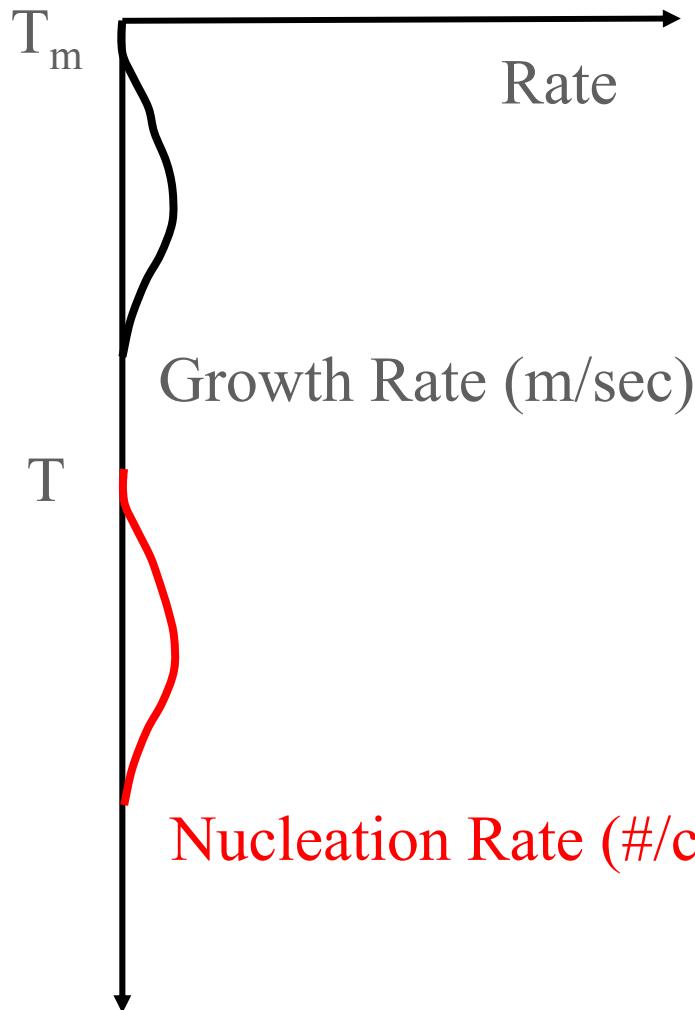


- ∴ **Occurrence of SRO at eutectic composition (especially deep eutectic)**

Ex) eut. comp. in TM-metalloid system- **TM: Metalloid** → **6 : 1 or 5 : 1**  
**most frequent ratio**

### 3. Kinetic aspect

➔ Decrease of nucleation and growth rate



Nucleation Rate  $I(T)$

$$I = n \nu \exp \left\{ \left( \frac{16\pi\Delta H_{cryst}}{81RT} \right) \left( \frac{T_m}{\Delta T} \right)^2 \right\} \exp \left\{ \frac{-\Delta E_D}{RT} \right\}$$

Growth Rates  $\mu(T)$

$$\mu(T) = \left( \frac{fRT}{3N\pi a^2 \eta(T)} \right) \left( 1 - \exp \left[ \left( \frac{\Delta H_m}{RT} \right) \left( \frac{\Delta T}{T_m} \right) \right] \right)$$

Nucleation Rate (#/cm<sup>3</sup>-sec)

# *Glass formation*

*Retention of liquid phase*

*Formation of crystalline phases*

*Thermodynamical point*

Small change in free E. (liq. → cryst.)

*Kinetic point*

Low nucleation and growth rates

*Structural point*

Highly packed random structure

## *Empirical rules*

- (1) multi-component alloy system
- (2) significant difference in atomic size ratios
- (3) negative heats of mixing
- (4) close to a eutectic composition
- (5) compositions far from a Laves phase region

- **Higher degree of dense random packed structure**
- *Suppression* of nucleation and growth of crystalline phase



*High glass-forming ability (GFA)*

# REFERENCE

- Phase Transformation in Metals and Alloys  
< Chapter 1 >  
D.A. Porter and K.E. Easterling