2009 fall

Advanced Physical Metallurgy "Phase Equilibria in Materials"

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Eun Soo Park

Office: 33-316

Telephone: 880-7221

Email: espark@snu.ac.kr

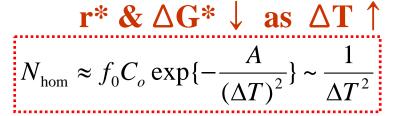
Office hours: by an appointment

Contents for previous class

Solidification: Liquid ----- Solid

- Nucleation in Pure Metals
- Homogeneous Nucleation

$$r^* = \frac{2\gamma_{SL}}{\Delta G_V} \Delta G^* = \frac{16\pi\gamma_{SL}^3}{3(\Delta G_V)^2} = \left(\frac{16\pi\gamma_{SL}^3 T_m^2}{3L_V^2}\right) \frac{1}{(\Delta T)^2}$$



• Heterogeneous Nucleation

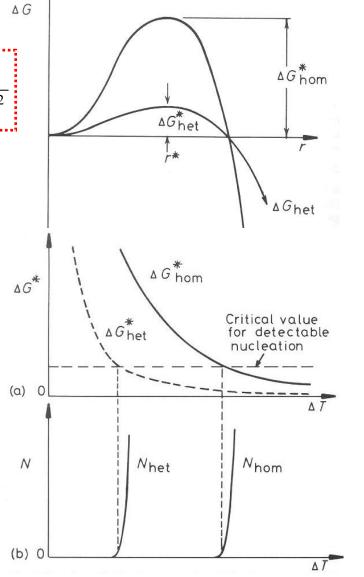
$$\Delta G_{het}^* = S(\theta) \Delta G_{hom}^*$$

$$\frac{V_A}{V_A + V_B} = \frac{2 - 3\cos\theta + \cos^3\theta}{4} = S(\theta)$$

Nucleation of melting

$$\gamma_{SL} + \gamma_{LV} < \gamma_{SV}$$
 (commonly)

- Undercooling ΔT
- Interfacial energy $\gamma_{SL} / S(\theta)$ wetting angle



4.1.4. Nucleation of melting

Although nucleation during solidification usually requires some undercooling, melting invariably occurs at the equilibrium melting temperature even at relatively high rates of heating.

Why?

$$\gamma_{SL} + \gamma_{LV} < \gamma_{SV}$$
 (commonly)



In general, wetting angle = 0 \Longrightarrow No superheating required!

Contents for today's class

Solidification: Liquid ----- Solid

- < Nucleation >
- Nucleation in Pure Metals
- Homogeneous Nucleation

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- Heterogeneous Nucleation
- Nucleation of melting

- < Growth >
- Equilibrium Shape and Interface Structure on an Atomic Scale
- Growth of a pure solid
- 1) Continuous growth
 - : Atomically rough or diffuse interface
- 2) Lateral growth
 - : Atomically flat of sharply defined interface
- Heat Flow and Interface Stability

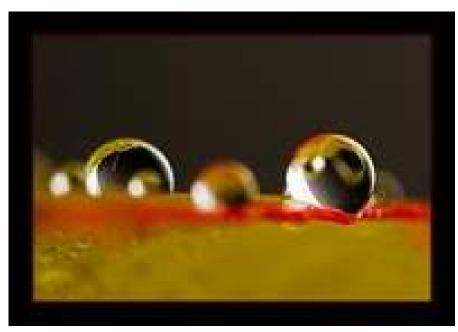
"Growth"

- We have learned nucleation.
 Once nucleated, the nucleus will grow.
 How does it grow?
- In order to see the details of growth,
 we need to know the structure of the surface on an atomic scale.
- How does it look like?
- Do liquid and solid nuclei differ in growth mechanism?

Water Drops



Natural Minerals



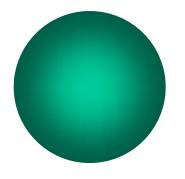




Topaz (황옥)

Stibnite (휘안광)

Equilibrium Shape and Interface Structure on an Atomic Scale





How do you like to call them?

rough interface

singular (smooth) interface

What about the dependence of surface energy on crystal directions?

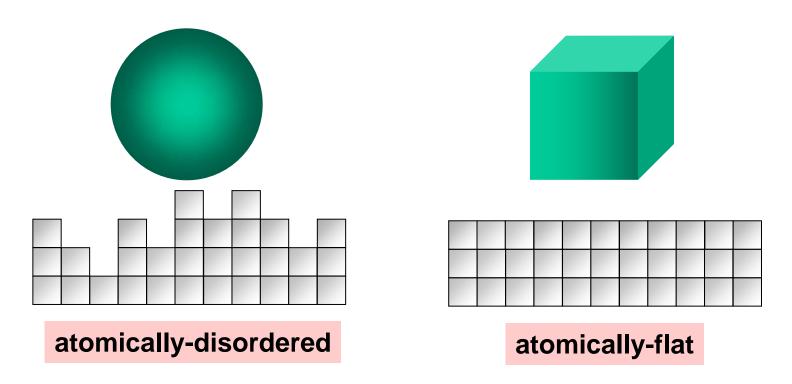
isotropic γ

anisotropic γ

Compare the kinetic barrier for atomic attachment.

Which has a low growth barrier?

Equilibrium Shape and Interface Structure on an Atomic Scale



Apply thermodynamics to this fact and derive more information.

Entropy-dominant

weak bonding energy

stable at high T

결정학적 방위에 무관: γ-plot이 구형임

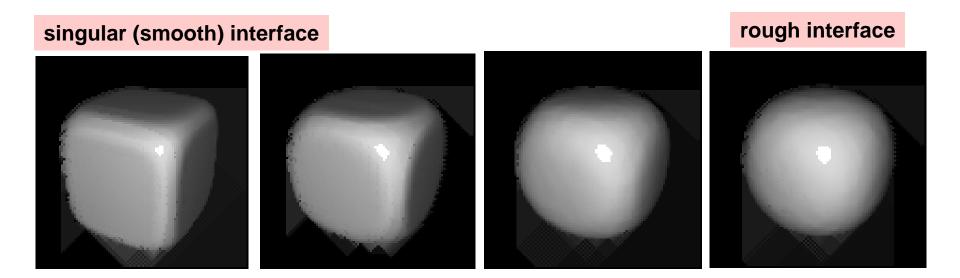
Enthalpy-dominant

strong bonding energy

stable at low T

결정학적 이방성 효과: 낮은 지수 갖는 조밀면으로 둘러싸인 형상

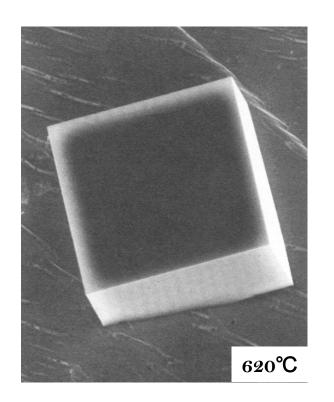
Thermal Roughening

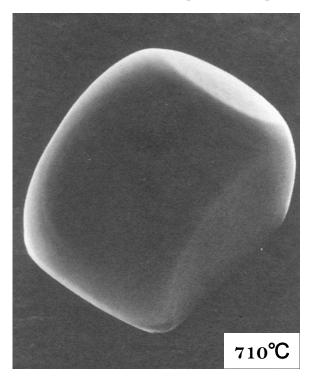


Heating up to the roughening transition.

✓ Equilibrium shape of NaCl crystal

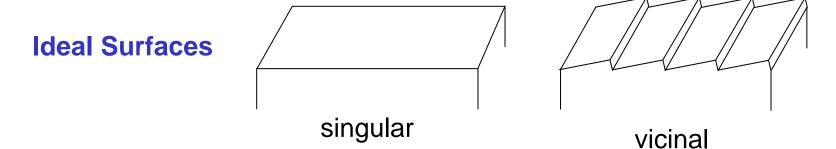


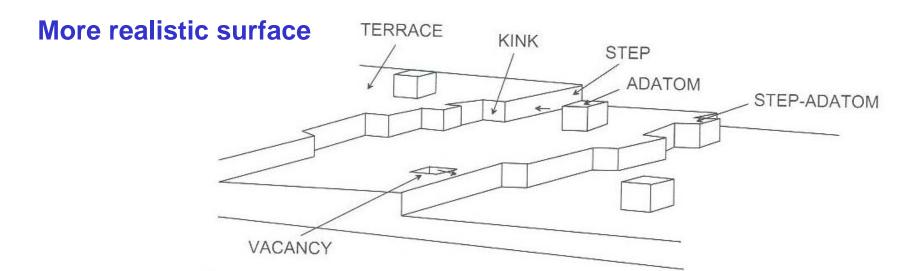




J.C. Heyraud, J.J. Metois, J. Crystal Growth, 84, 503 (1987)

Atomic View



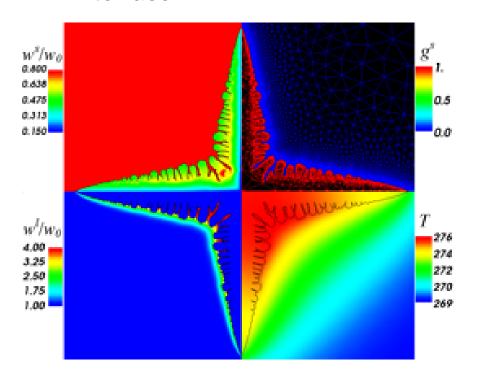


- Realistic surfaces of crystals typically look like this at low temperature
- At sufficiently high temperature, the structure becomes atomically rough

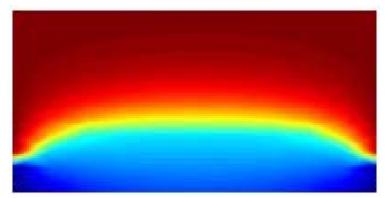
4.2. Growth of a pure solid

Two types of solid-liquid interface

- 1. Continuous growth
 - : Atomically rough or diffuse interface

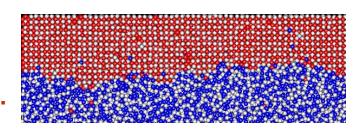


- 2. Lateral growth
 - : Atomically flat of sharply defined interface



4.2.1 Continuous growth

The migration of a rough solid/liquid interface can be treated in a similar way to the migration of a random high angle grain boundary.

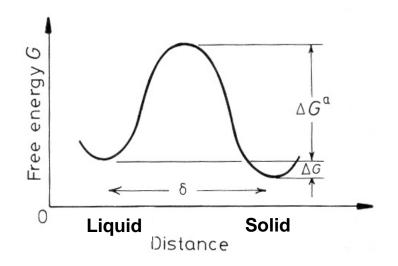


- Driving force for solidification

$$\Delta G = \frac{L}{T_m} \Delta T_i$$

L: latent heat of melting

 ΔT_i : undercooling of the interface



- Net rate of solidification

$$\nu = k_1 \Delta T_i$$

 k_1 : properties of boundary mobility

Reference (eq. 3.21) $v = M \cdot \Delta G / V_m$

The solidification of metals is usually a diffusion controlled process.

- Pure metal grow at a rate controlled by heat conduction.
- Alloy grow at a rate controlled by solute diffusion.

4.2.2 Lateral growth

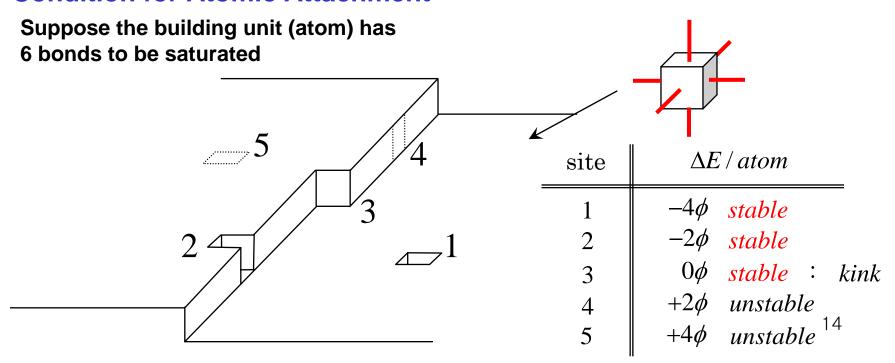
- Materials with a high entropy of melting prefer to form atomically smooth, closed-packed interfaces.
- For this type of interface the minimum free energy also corresponds to the minimum internal energy, i.e. a minimum number of broken 'solid' bonds.

Two ways in which ledges and jogs (kinks) can be provided.

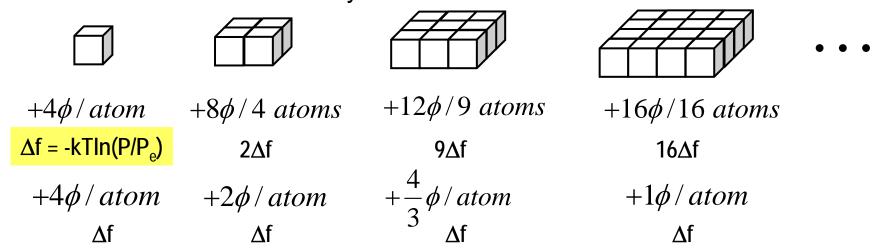
1) Surface (2-D) nucleation

2) Spiral growth

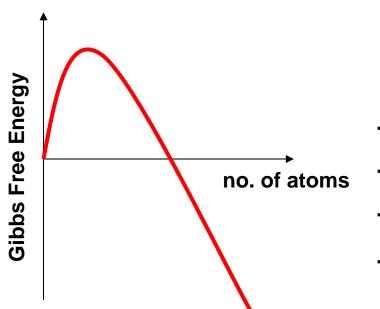
Condition for Atomic Attachment



How many unsaturated bonds are there if they are epitaxial to the underneath atomic layer?



Draw the plot showing how the free energy varies with the number of atoms in the presence of supersaturation (driving force) for growth.



→ 2- Dimensional Nucleation

- if large # of atoms → form a disc-shaped layer,
- self-stabilized and continue to grow.
- ΔT becomes large, r* ↓.

-
$$v \propto \exp(-k^2/\Delta T_i)$$

2) Spiral growth: Growth by Screw Dislocation

Crystals grown with a low supersaturation were always found to have a 'growth spirals' on the growing surfaces.

- addition of atoms to the ledge cause it to rotate around the axis of screw dislocation
- If atoms add at an equal rate to all points along the step, the angular velocity of the step will be initially greatest nearest to the dislocation core.
- the spiral tightens until it reaches
 a min radius of r*
- v (growth rate) = $k_3(\Delta T_i)^2$

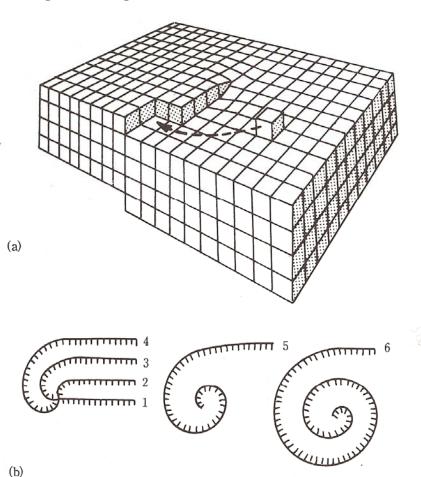
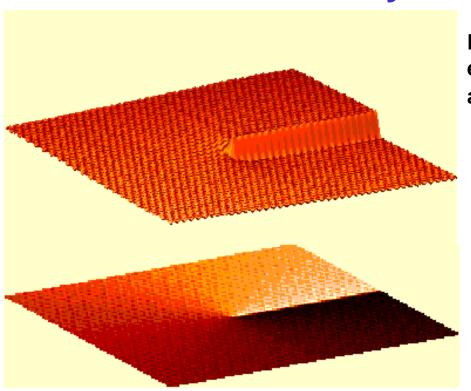


그림 4.13 나선형 성장 (b) 나선전위가 표면과 만나면 표면에는 돌출맥이 생김 (b) 원자가 이 돌출맥에 붙을 때 이 돌출맥은 면상에서 회전을 하며 회전속도는 전위로부터 멀어질수록 감소함.

Growth by Screw Dislocation



Burton, Cabrera and Frank (BCF, 1948) elaborated the spiral growth mechanism, assuming steps are atomically disordered...

Their interpretation successfully explained the growth velocity of crystals as long as the assumption is valid...

3) Growth from twin boundary

- another permanent source of steps like spiral growth
 - → not monoatomic height ledge but macro ledge

Kinetic Roughening

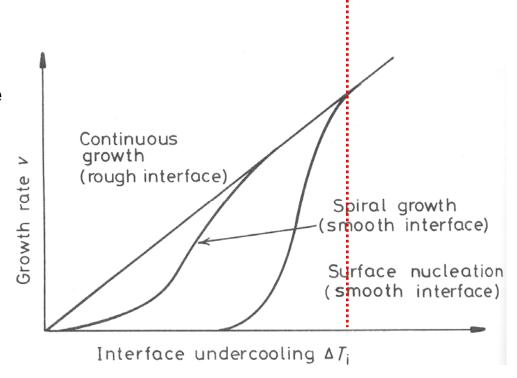
Rough interface - Ideal Growth → diffusion-controlled → dendritic growth

Singular interface - Growth by Screw Dislocation
Growth by 2-D Nucleation

The growth rate of the singular interface cannot be higher than ideal growth rate.

When the growth rate of the singular Interface is high enough, it follows the ideal growth rate like a rough interface.

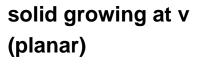
→ kinetic roughening

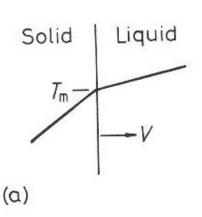


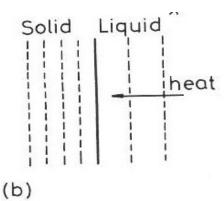
4.2.3 Heat Flow and Interface Stability - Planar interface

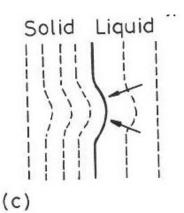
1) Superheated liquid

Consider the solidification front with heat flow from L to S.









Heat flow away from the interface through the solid $K_{\circ}T'$

 \longleftrightarrow

- Heat flow from the liquid

 VL_V - Latent heat generated at the interface

Heat Balance Equation

$$K_{S}T_{S}' = K_{L}T_{L}' + vL_{V}$$

K: thermal conductivity

If r is so large \rightarrow Gibbs-Thompson effect can be ignored the solid/liquid interface remain at T_m (r : radius of curvature of the protrusion)

dT/dx in the liquid ahead of the protrusion will increase more positively. T_L ? $^{\uparrow}$ & T_S ? \downarrow

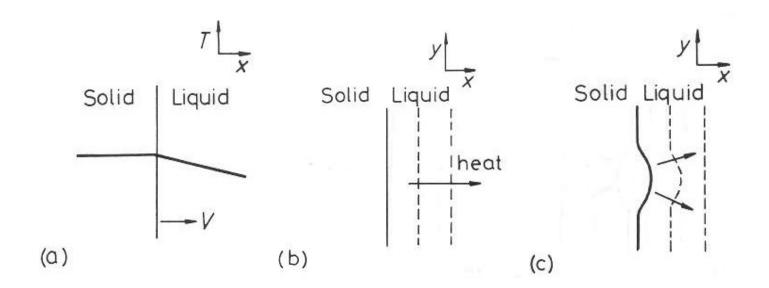
More heat to the protrusion \rightarrow melt away v of protrusion \downarrow to match other v in planar region

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mould walls

4.2.3 Heat Flow and Interface Stability - Planar interface

2) Solid growing into supercooled liquid



- protrusion
$$\frac{dT_L}{dX} < 0$$
 becomes more negative

- heat flow from solid = the protrusion grows preferentially.

Development of Thermal Dendrite

cf) constitutional supercooling

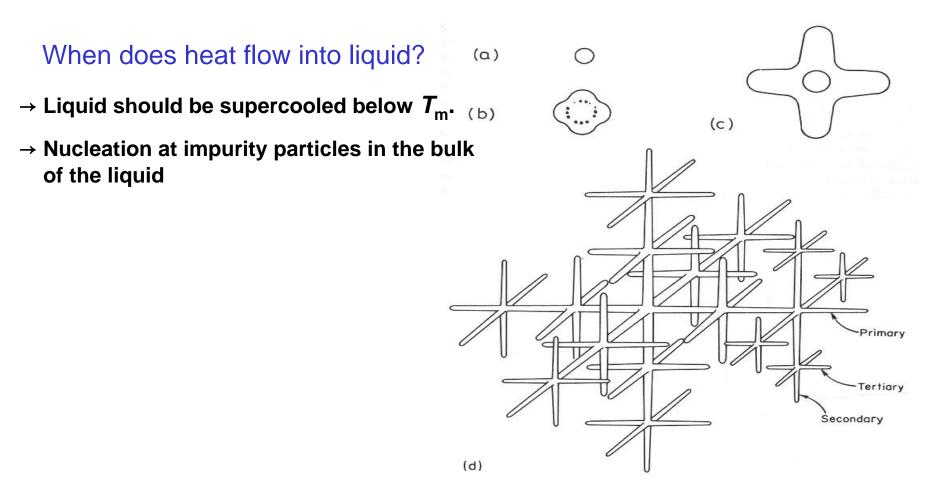


Fig. 4.17 The development of thermal dendrites: (a) a spherical nucleus; (b) the interface becomes unstable; (c) primary arms develop in crystallographic directions (<100> in cubic crystals); (d) secondary and tertiary arms develop

Closer look at the tip of a growing dendrite

different from a planar interface because heat can be conducted away from the tip in three dimensions.

Assume the solid is isothermal $(T'_S = 0)$

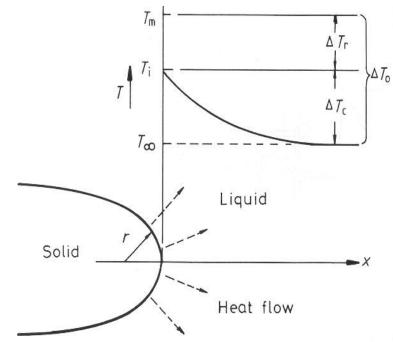
From
$$K_S T_S' = K_L T_L' + v L_V$$

If
$$T_{S}' = 0$$
, $V = \frac{-K_{L}T_{L}'}{L_{V}}$

A solution to the heat-flow equation for a hemispherical tip:

$$T_{L}'(negative) \cong \frac{\Delta T_{C}}{r} \Delta T_{C} = T_{i} - T_{\infty}$$

$$v = \frac{-K_{L}T_{L}'}{L_{V}} \cong \frac{K_{L}}{L_{V}} \cdot \frac{\Delta T_{C}}{r} \qquad v \propto \frac{1}{r}$$



However, ΔT also depends on r. How?

Thermodynamics at the tip?

Gibbs-Thomson effect: melting point depression

$$\Delta G = \frac{L_V}{T_m} \Delta T_r = \frac{2\gamma}{r} \qquad \Delta T_r = \frac{2\gamma T_m}{L_V r}$$

Minimum possible radius (r)?

$$r_{min}: \Delta T_r \to \Delta T_0 = T_m - T_\infty \to r^*$$
The crit.nucl.radius

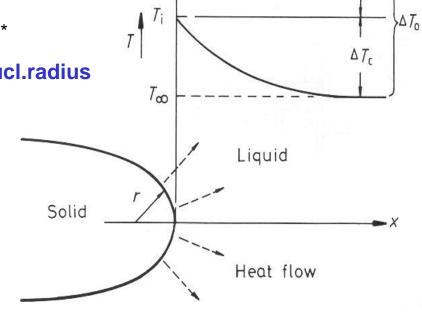
$$r^* = \frac{2\gamma T_m}{L_v \Delta T_o}$$

$$\Delta T_r = \frac{2\gamma T_m}{L_v r}$$

$$\Delta T_r = \frac{2\gamma T_m}{L_V r}$$

Express ΔT_r by r, r^* and ΔT_o .

$$\Delta T_r = \frac{r}{r} \Delta T_o$$



$$V \cong \frac{K_L}{L_V} \cdot \frac{\Delta T_c}{r} = \frac{K_L}{L_V} \cdot \frac{\left(\Delta T_0 - \Delta T_r\right)}{r} = \frac{K_L}{L_V} \cdot \frac{\Delta T_0}{r} \left(1 - \frac{r^*}{r}\right)$$

 $v \rightarrow 0$ as $r \rightarrow r^*$ due to Gibbs-Thomson effect as $r \to \infty$ due to slower heat condution

Maximum velocity?

$$\rightarrow r = 2r^*$$

Heat Flow and Interface Stability - Planar interface

