



**457.562 Special Issue on
River Mechanics
(Sediment Transport)
.06 Sediment Transport Basic**



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1. Sediment transport

- Sediment load
 - Classification based on mechanism
 - Suspended load
 - Bed load
 - Classification based on particle size
 - Wash load
 - Bed-material (sediment) load
- Total sediment load
 - Wash load
 - Suspended load (bed material load)
 - Bed load (bed material load)



2. Sediment transport modes: bed-material load and Wash load

- While bed-material load (suspended and bed) can be quantified, wash load is hardly done.
- Wash load can deliver clay, silt (<0.062) and from the land surface erosion rather than from the channel bed.
- Also many pollutants are attached and delivered by wash load.
- But, still hard to know exact amount



2. Sediment transport modes: bed-material load and Wash load

- Energy balance equation of suspended load
- This is not accepted but...the average rate of work (power)

$$P_g \equiv \rho g S U H + \rho R g S C U H - \rho R g H C v_s$$

- The first term of the right hand side is mean rate of energy input to the fluid phase
- The second is mean rate of energy input to the mean flow through solid phase
- Mean rate of energy loss by mean flow through turbulent mixing required for maintain sediment in suspension



2. Sediment transport modes: bed-material load and Wash load

$$P_g \equiv \rho g S U H + \rho R g S C U H - \rho R g H C v_s$$

- If second term is larger than the third term, suspended load contribute energy to the flow.
- In opposite condition, suspended particle depletes energies from the flow.
- In the turbidity current, the first term (clean water) do not contribute to the current.
- Also to produce current, second term need to be larger than the third term

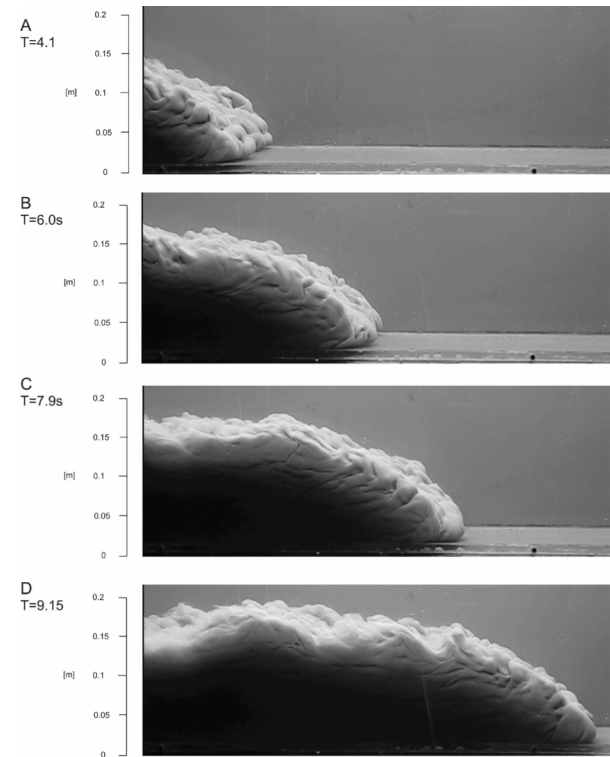
$$\rho R g S C U H > \rho R g H C v_s$$

$$\frac{U S}{v_s} > 1 \quad (\text{Bagnold criterion for turbidity currents})$$



2. Sediment transport modes: bed-material load and Wash load

- Bagnold criterion for turbidity current ensures that the sediment supplies more energy than it consumes.
- It must be satisfied if a self-sustaining turbidity current is to occur.
- As in the reading material, there are several criteria on the suspended load, but not anything can tell the quantity of the suspended load.
- But still it needs to be understood for the morphological variability

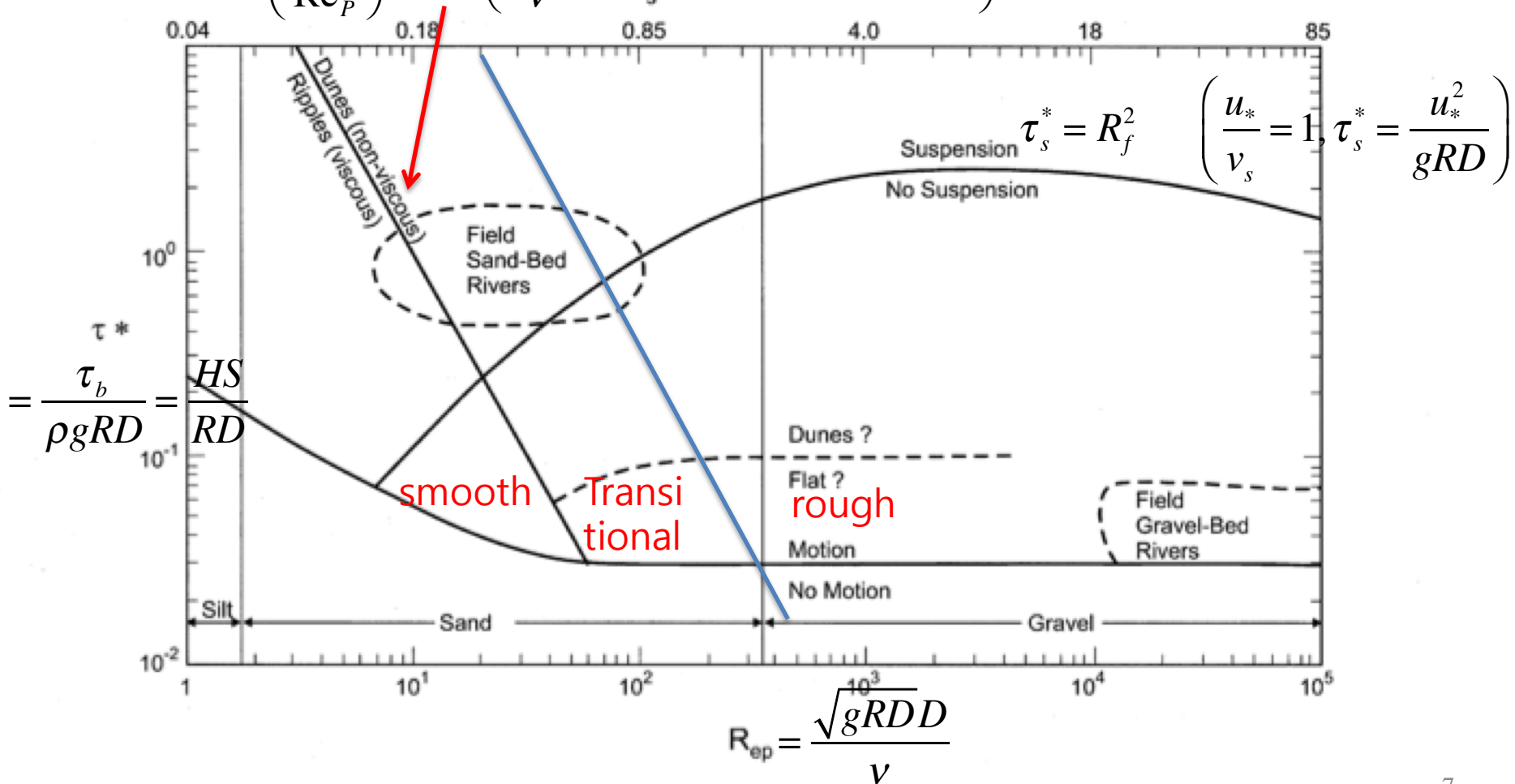




3. Shields-Parker River Sedimentation Diagram

$$\tau_v^* = \left(\frac{11.6}{Re_P} \right)^2 \quad \left(\frac{u_* D}{\nu} = 11.6, \text{ viscous sublayer} \right)$$

D_s in mm at 20°C





4. Bedload Transport Function

- The transport occurs tangential to the bed.
- All of the transport is directed in the streamwise, or s direction.
- The volume bedload transport rate per unit width (n -direction) is given by usually q . And q is function of boundary shear stress and other parameters;

$$q = q(\tau_b, \text{other parameters})$$



5. Erosion into and deposition from, suspension

- The volume rate of erosion of bed material into suspension per unit bed area denoted a E .
- A dimensionless sediment entrainment rate E can thus be defined in terms of the sediment fall velocity v_s .

$$E = v_s E$$

- In general, E can be expected to be a function of boundary shear stress and other parameters.
- Erosion into suspension can be taken to be directed upward normal, i.e., in the positive z , direction (parallel to e_3)



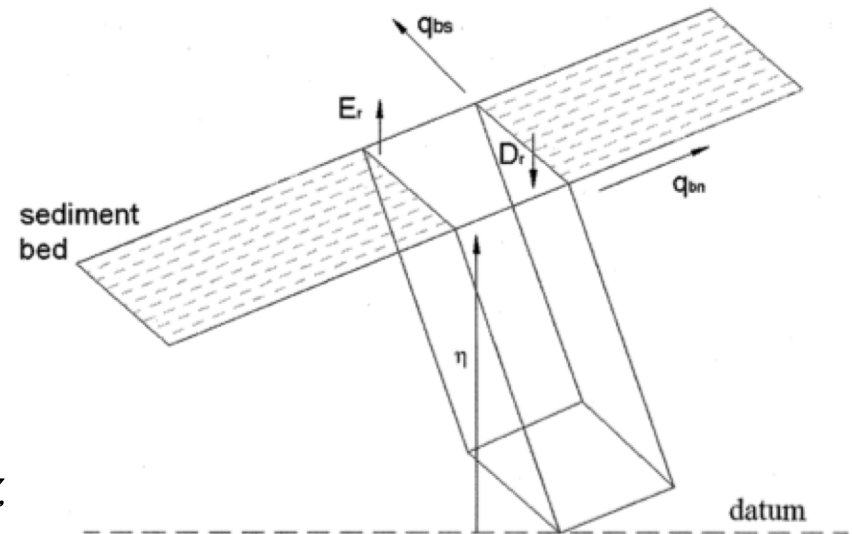
5. Erosion into and deposition from, suspension

- Let $\bar{c}(x_i, t)$ denote the volume concentration of suspended sediment, averaged over turbulence.
- The streamwise volume transport of sediment per unit width is given by

$$q_s = \int_0^H \bar{c} u \, dz$$

- In a two-dimensional case, two components q_{Ss} and q_{Sn} result, where

$$q_{Ss} = \int_0^H \bar{c} u \, dz; \quad q_{Sn} = \int_0^H \bar{c} v \, dz$$

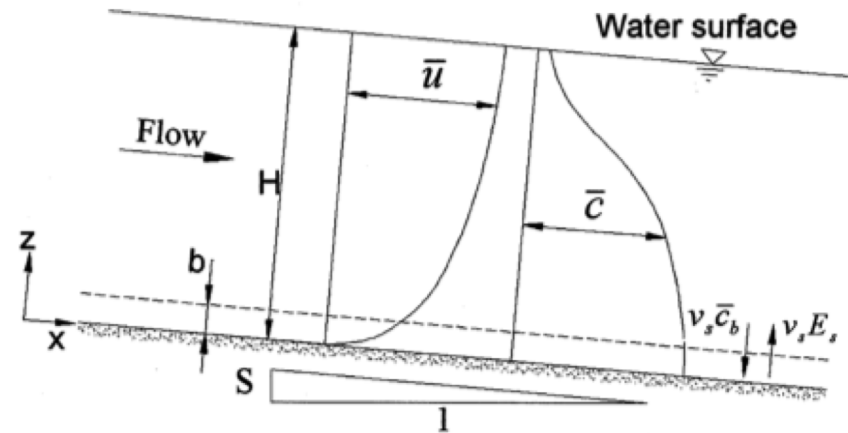




5. Erosion into and deposition from, suspension

- Deposition onto the bed is by means of settling. The rate at which material is fluxed vertically downward onto the bed is given by $v_s \bar{c}_b$ where \bar{c}_b is a near bed value of \bar{c} .
- The deposition rate D realized at the bed is obtained by computing the component of this flux that is actually directed normal to the bed:

$$D = v_s \bar{c}_b \vec{k} \cdot \vec{e}_3$$





5. The Exner (founder of morphodynamics) equation

- Exner equation of sediment mass continuity uniform material
- The bed material is taken to have a (constant) porosity λ_p
- Mass balance of sediment requires that the following equation be satisfied

$$\frac{\partial}{\partial t} [\text{mass of bed material}] = \text{net mass bedload inflow rate}$$

+ net mass rate of deposition from suspension

- The time rate of change of bed position is given by

$$\dot{z}_b \equiv \frac{\partial z_b}{\partial t}$$



5. The Exner equation

- The equation translates to

$$\rho_s (1 - \lambda_p) \frac{\partial}{\partial t} z_b dsdn =$$

$$\rho_s (q_s|_s - q_s|_{s+ds}) dn + \rho_s (q_n|_n - q_n|_{n+dn}) ds + \rho_s (D - E) dsdn$$

- It reduces to

$$(1 - \lambda_p) \dot{z}_b = -\frac{\partial q_s}{\partial s} - \frac{\partial q_n}{\partial n} + v_s (\bar{c}_b \vec{k} \cdot \vec{e}_3 - E)$$

- If the bed is horizontal (or nearly horizontal), so that z is directed upward vertical, $\dot{z}_b = \partial \eta / \partial t$ and $\vec{k} \cdot \vec{e}_3 = 1$

$$(1 - \lambda_p) \frac{\partial \eta}{\partial t} = -\frac{\partial q_s}{\partial s} - \frac{\partial q_n}{\partial n} + v_s (\bar{c}_b - E)$$



5. The Exner equation

- Bed level changes with time t due to bed load transport, sediment entrainment into suspension, and sediment deposition onto the bed can be predicted by Exner's equation.
- To solve this equation, it is necessary to have relations to compute bed load transport, near-bed suspended sediment concentration and sediment entrainment into suspension.