

노트 제목

2010-05-06

inner layer ($y/\delta < 0.1$)

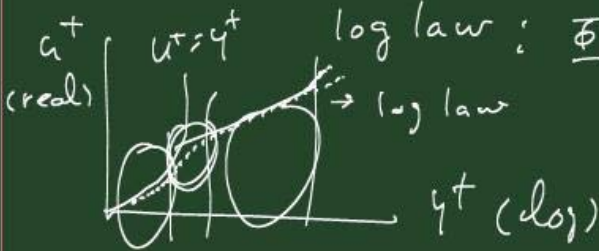
$$\frac{d\langle U \rangle}{dy} / \frac{u_\tau}{y} = \Phi\left(\frac{y}{\delta}, \frac{y}{\delta}\right)$$

Law of the wall $\Rightarrow \Phi\left(\frac{y}{\delta}\right)$

$$\rightarrow u^+ = f_w(y^+)$$

$$\frac{\langle U \rangle}{u_\tau} \approx$$

viscous sublayer: $u^+ = y^+ + O(y^{+2})$



log law: $\Phi\left(\frac{y}{\delta}\right) = \frac{1}{\kappa} \Rightarrow u^+ = \frac{1}{\kappa} \ln y^+ + B$



• Velocity-defect law

In outer layer ($y^+ > 50$), $\Phi\left(\frac{y}{\delta}, \frac{y}{\delta}\right)$ is indep. of ν .

$$\rightarrow \frac{d\langle U \rangle}{dy} / \frac{u_\tau}{y} = \Phi_0\left(\frac{y}{\delta}\right)$$

integration from y to δ

$$\rightarrow \frac{U_0 - \langle U \rangle}{u_\tau} = F_0\left(\frac{y}{\delta}\right)$$

velocity-defect law



At sufficiently high Re, there is an overlap region bet. inner layer ($y/\delta < 0.1$) and outer layer ($y/\delta > 50$).

y^+

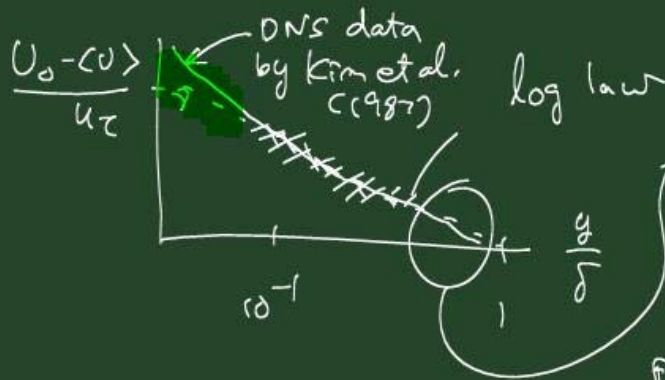


In this region, $\frac{d\langle U \rangle}{dy} / \frac{u_\tau}{y} = \frac{F_1(y/\delta)}{y}$ for $\delta \ll y \ll \delta$
 " = $\frac{F_0(y/\delta)}{y}$

$\rightarrow \frac{d\langle U \rangle}{dy} / \frac{u_\tau}{y} = \frac{1}{K}$ const
 for $\delta_v \ll y \ll \delta$
 Millikan (1938)

again log law!

or, $\frac{U_0 - \langle U \rangle}{u_\tau} = F_D(y/\delta) = -\frac{1}{K} \ln \frac{y}{\delta} + B$ for $y/\delta \ll 1$



there exists a deviation from log law (but small)

Deviation is larger in the outer layer of turb. boundary layer.

① Friction law & Reynolds number
 Relations among U_0 , \bar{U} & u_τ .

• bulk velocity \bar{U} from log law

$$\frac{U_0 - \langle U \rangle}{u_\tau} = -\frac{1}{\kappa} \ln \frac{y}{\delta} + B_1$$

✓ @ $y = \delta$, $\langle U \rangle \doteq U_0 \Rightarrow B_1 = 0$

$$\frac{U_0 - \bar{U}}{u_\tau} = \frac{U_0 - \frac{1}{\delta} \int_0^\delta \langle U \rangle dy}{u_\tau} = \frac{1}{\delta} \int_0^\delta \frac{U_0 - \langle U \rangle}{u_\tau} dy$$

$$\approx \frac{1}{\delta} \int_0^\delta \left(-\frac{1}{\kappa} \ln \frac{y}{\delta} \right) dy = \frac{1}{\kappa} \approx 2.4$$

error near the wall is small

agrees well with exp. data.

Inner layer $\frac{\langle U \rangle}{u_\tau} = \frac{1}{\kappa} \ln \frac{y}{\delta_V} + B$

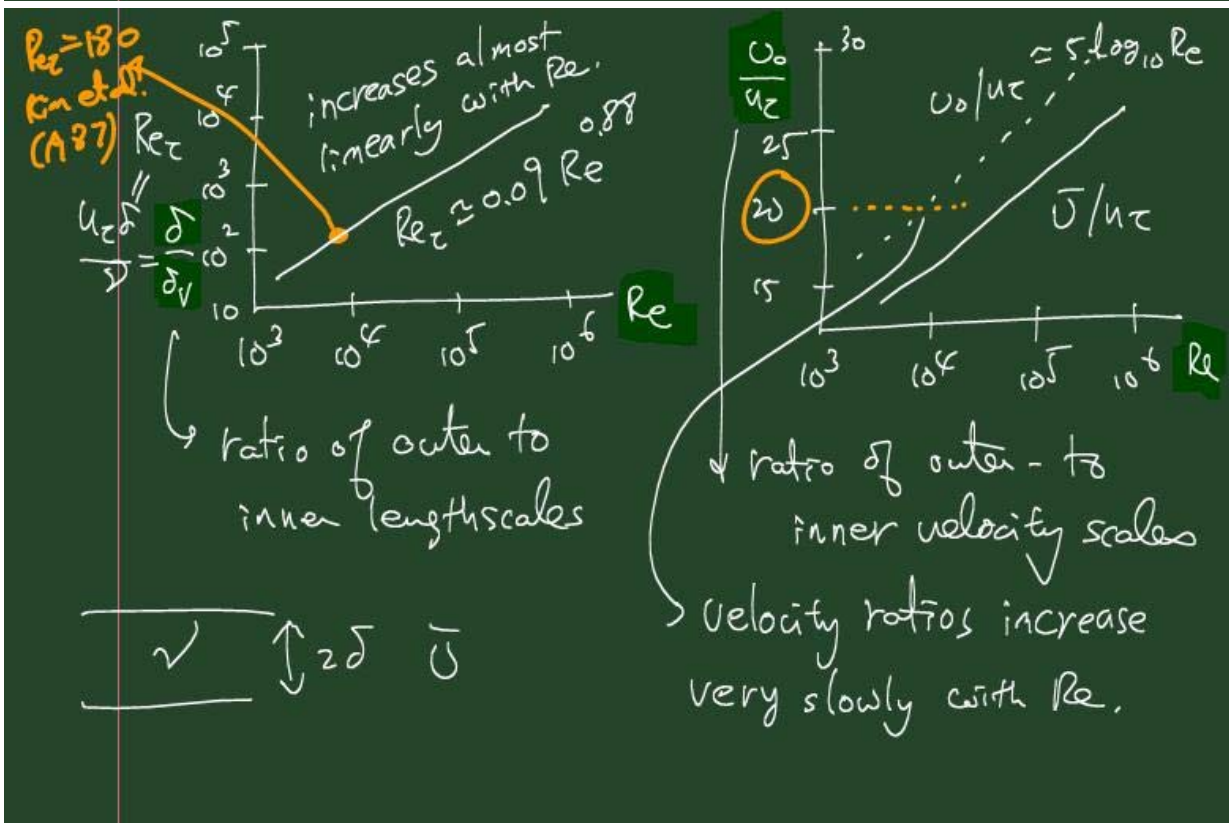
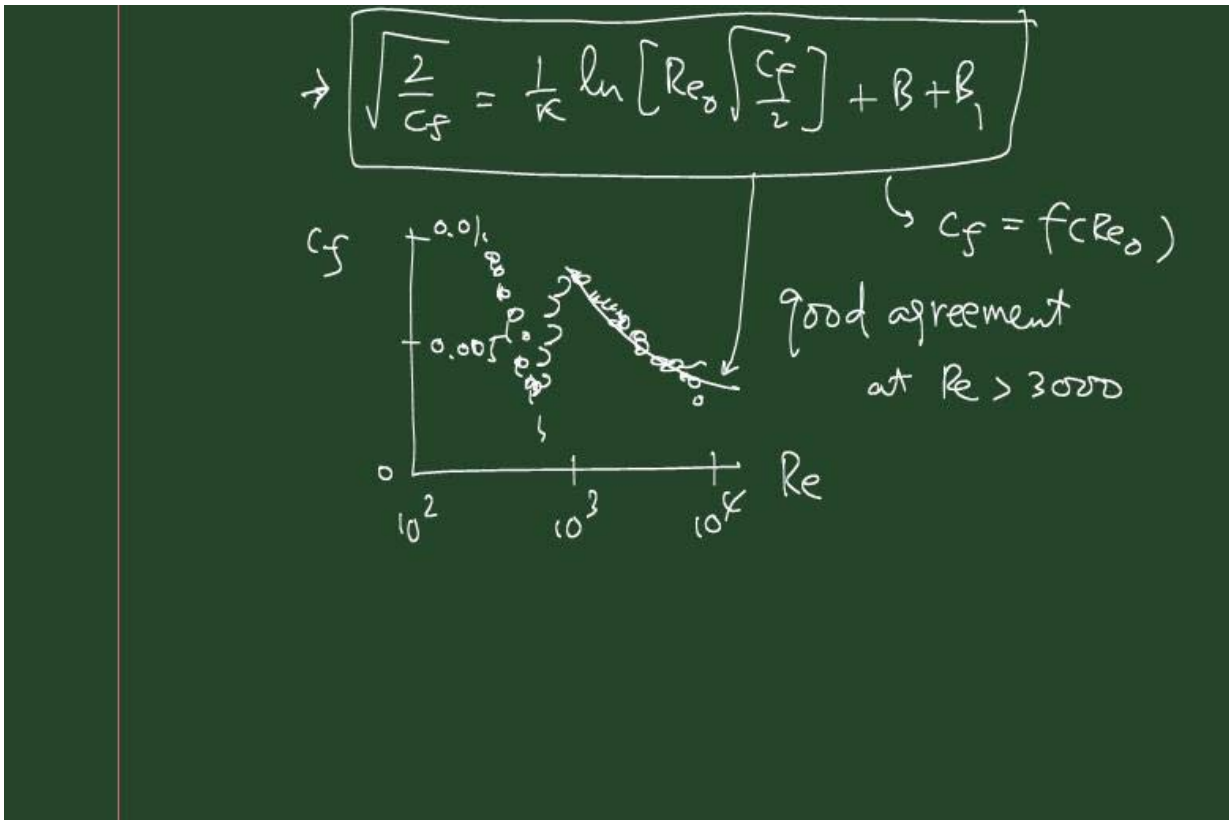
Outer layer $\frac{U_0 - \langle U \rangle}{u_\tau} = -\frac{1}{\kappa} \ln \frac{y}{\delta} + B_1$

$$\frac{U_0}{u_\tau} = \frac{1}{\kappa} \ln \frac{\delta}{\delta_V} + B + B_1$$

$$\left(\frac{\delta}{\delta_V} = \delta \cdot \frac{1}{\nu/u_\tau} = \frac{\delta u_\tau}{\nu} = \frac{\delta U_0}{\nu} \cdot \frac{u_\tau}{U_0} \right)$$

$$\rightarrow \frac{U_0}{u_\tau} = \frac{1}{\kappa} \ln \left[Re_\delta \left(\frac{U_0}{u_\tau} \right)^{-1} \right] + B + B_1$$

friction coeff. $c_f \equiv \frac{\tau_{co}}{\frac{1}{2} \rho U_0^2} = 2 \left(\frac{u_\tau}{U_0} \right)^2 \Rightarrow \frac{U_0}{u_\tau} = \sqrt{\frac{2}{c_f}} \xrightarrow{\text{}} \frac{U_0}{u_\tau} = f(Re_\delta)$



At high Re , viscous lengthscale is very small.
 e.g. $\delta = 2\text{cm}$, $Re = 10^5 \rightarrow \delta_v = 10^{-5}\text{m}$

$$y^+ = 100 \rightarrow 1\text{mm}$$



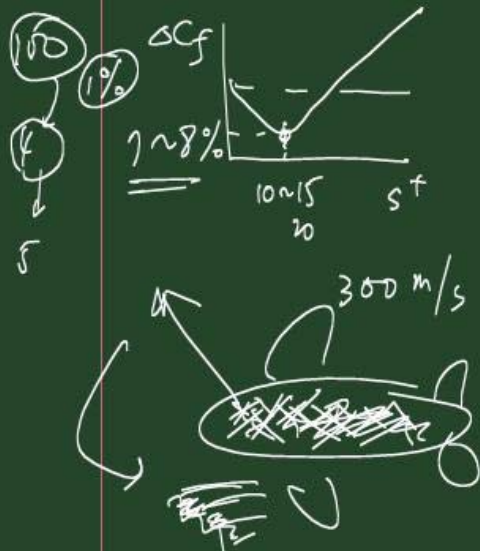
Significant fraction of the increase in the mean velocity bet. wall and centerline occurs in the viscous wall region.

e.g. $\delta = 2\text{cm}$, $Re = 10^5 \rightarrow y^+ = 10 \rightarrow y \approx 0.1\text{mm}$

$$\langle U \rangle_{y=0.1\text{mm}} \approx 0.3 U_0!$$



shark skin riblet



airplane ~~S^+~~

$$S^+ = \frac{S u_c}{\nu} \Rightarrow S = \frac{S^+ \nu}{u_c} = \frac{15 \times 1.5 \times 10^{-5}}{15}$$

$$u_c = \frac{300}{30} = 15\text{ m/s}$$

$$S = \frac{15 \times 1.5 \times 10^{-5}}{15} = 1.5 \times 10^{-5} = 15\mu\text{m}$$

gave up

