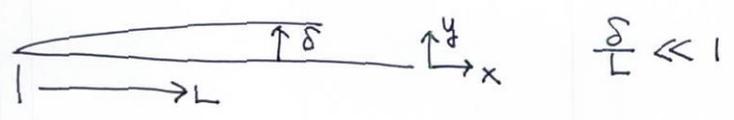


# Chap. 8. Velocity Gradients and Boundary Layers

## \* Boundary - Layer Theory.



$$\frac{\partial p}{\partial y} \ll \frac{\partial p}{\partial x} \quad p = p(x)$$

momentum eq:  $\rho (u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y}) = -\frac{dp}{dx} + \mu (\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2})$

continuity:  $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0.$

$$\frac{O(\frac{\partial^2 u}{\partial x^2})}{O(\frac{\partial^2 u}{\partial y^2})} \sim \frac{\frac{U}{L^2}}{\frac{U}{\delta^2}} \sim (\frac{\delta}{L})^2 \ll 1.$$

momentum eq. :  $\rho (u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y}) = -\frac{dp}{dx} + \mu \frac{\partial^2 u}{\partial y^2}$

on flat plate:  $\frac{dp}{dx} = 0$

scaling analysis.

$$\rho U \frac{U}{L} \sim \mu \frac{U}{\delta^2}$$

$$\delta^2 \sim \frac{\mu L}{\rho U}$$

$$\delta_x \sim (\frac{x \mu}{\rho U})^{1/2}$$

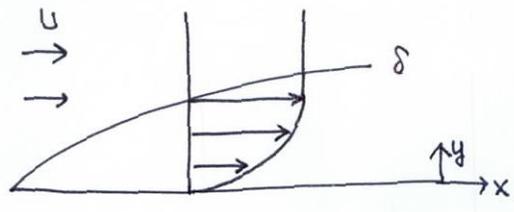
$u(\delta_{99}) = 0.99 U_{\infty}$  :

$$\delta_{99\%} = 5.0 (\frac{x \mu}{\rho U})^{1/2}.$$

$$\frac{\delta}{x} = 5.0 Re_x^{-1/2}$$

Blasius (1908)

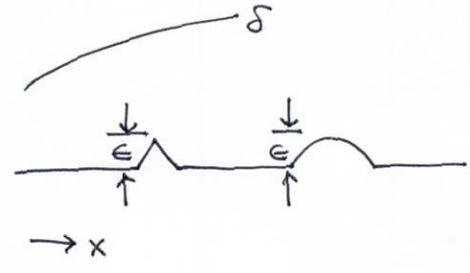
: laminar B.L. ( $Re_x < \sim 5 \times 10^5$ )



velocity approximation.

$$y < \frac{\delta}{2} : \quad \frac{u}{U} = 0.32 y \left( \frac{\rho U}{x \mu} \right)^{1/2}$$

How rough can a surface be without materially affecting the flow over it?

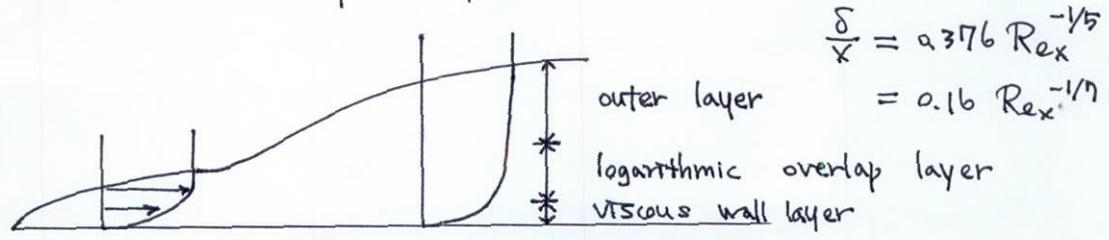


$$\frac{\epsilon}{x} \leq 9.5 Re_x^{-3/4} \quad (\text{pointed})$$

$$\frac{\epsilon}{x} \leq 12.2 Re_x^{-3/4} \quad (\text{rounded})$$

$Re_x \uparrow - \frac{\epsilon}{x} \downarrow$  (for fixed  $\epsilon - x \uparrow$ )

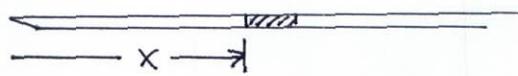
\* Turbulent boundary layer



real biological flat surfaces (leaves)  
 : turbulence occurs  $Re < Re_{tr}$  (flat plate)  
 heat/mass transfer > theory.

§ Forces at and near surfaces

\* drag on a spot on a flat plate



$$\tau_w = \mu \frac{\partial u}{\partial y} \Big|_{y=0}$$

$$= 0.32 U \left( \frac{\rho U}{x \mu} \right)^{1/2} \cdot \mu \quad (\text{linear vel. approximation})$$

local drag coefficient  $C_{Dl}$

$$C_{Dl} = \frac{F_D}{\frac{1}{2} \rho U^2 S} = \frac{2 \tau_w}{\rho U^2}$$

$$= 0.64 \left( \frac{\mu}{\rho U x} \right)^{1/2} = 0.64 \cdot Re_x^{-1/2}$$

total drag (0 → x)

$$F_D = \int_0^x \tau_w dx$$

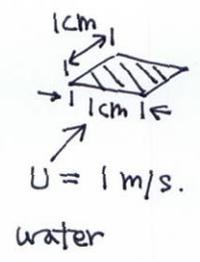
$$= 0.32 \int_0^x \frac{\rho^{1/2} U^{3/2} \mu^{1/2}}{x^{1/2}} dx$$

$$= 0.64 \rho^{1/2} U^{3/2} \mu^{1/2} x^{1/2}$$

$$C_D = \frac{F_D}{\frac{1}{2} \rho U^2 x} = 1.28 Re^{-1/2} \sim (7.1) \text{ p. 135}$$

(1.33  $Re^{-1/2}$ )

eg.



(1) on flat plate.  $x = 0.5 \text{ m}$

$$Re_x = 5 \times 10^5$$

$$C_{Dl} = 9 \times 10^{-4} = 0.64 Re_x^{-1/2}$$

$$F_D = 4.5 \times 10^{-5} \text{ N.}$$

(2) In the free stream,

$$Re = \frac{\rho U (1\text{cm})}{\mu} = \frac{10^3 \times 10^{-2}}{10^{-3}} = 10^4.$$

$$C_D = 1.33 Re^{-1/2} = 0.0133$$

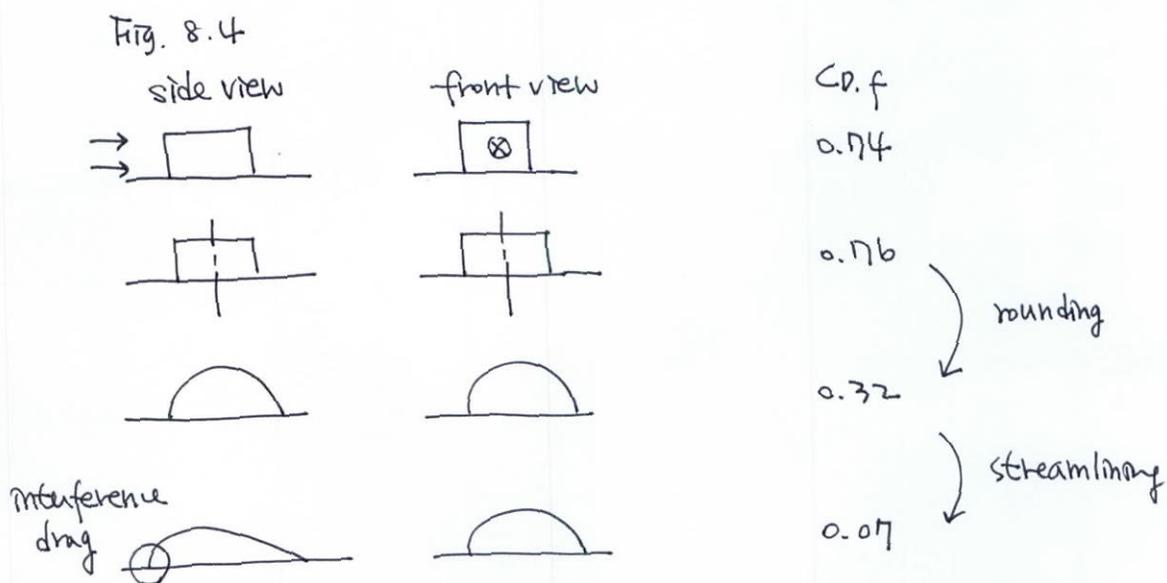
$$F_D = \frac{1}{2} \rho U^2 (\underset{\substack{\uparrow \\ \text{wetted area}}}{2\text{cm}^2}) C_D = \frac{1}{2} (10^3)(10^{-4})(0.0133) \quad (2)$$

$$= 0.00133 \text{ N}$$

$$= 1.33 \times 10^{-3} \text{ N.}$$

$$F_{D(2)} \approx 30 F_{D(1)}$$

\* Drag coefficients of protuberances on flat plates



$$Re_{dra} = 2 \times 10^4 \sim 5 \times 10^4.$$

$$\delta_{BL} \ll \text{height}$$



lengthen and flatten the leading edge -  $C_{Df} = 0.03$

§ Unbounded boundary layers

· flat plate with no leading edge

e.g. surface of the earth (ex: Table 8.1)



$$u_x = \frac{u^*}{\kappa} \ln \left( \frac{z-d}{z_0} \right)$$

$$\kappa \approx 0.41$$

$u^*$  (friction velocity / shear velocity)

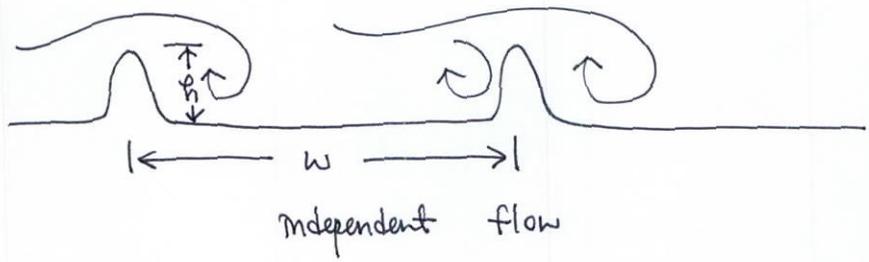
$$= \sqrt{\frac{\tau}{\rho}}$$

turbulent B.L.  
: logarithmic overlap layer

§ Flow right on bumpy bottoms

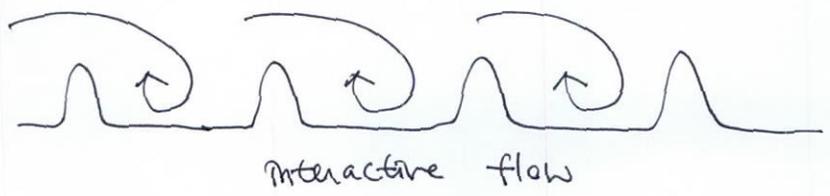
e.g. canopy of forest, top leaves of field of crop,  
top of forest of tall sea anemones on a subtidal rock face

Fig. 8.7



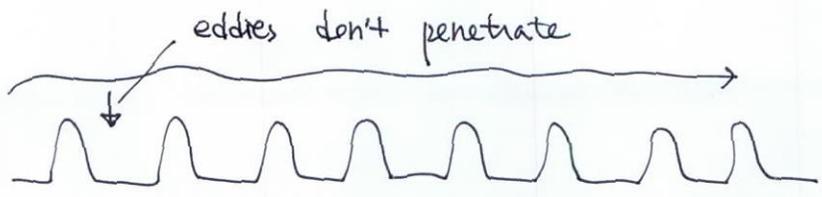
$$\frac{h}{w} \ll 1$$

independent flow



$$\frac{h}{w} \uparrow$$

interactive flow



$$\frac{h}{w} \uparrow \uparrow$$

skimming flow (protrusions > 12% surface)