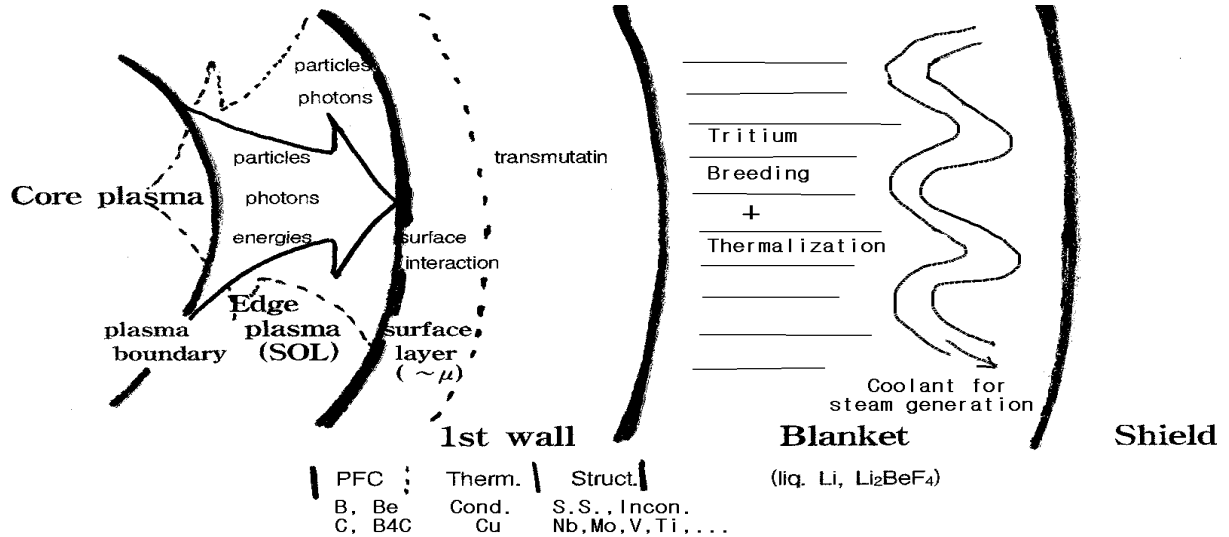


Chapter 5. Plasma-Surface Interaction

Reading assignment: Stacey Chap. 6, Harms Chap. 13



1. Fluxes to the surface

A. Particle fluxes

- Ions: Diffusing fuel ions (H, D, T)
Fusion α
Diffusing impurities (wall materials, residual gases in chamber, adsorbed gases in surface)
Energetic ions from NBI
- Electrons: Diffusing plasma electrons
Runaway electrons
- Neutrals: Recycling neutrals
NBI neutrals
- Fusion neutrons

Note)

Incident fluxes on the wall

$$\Gamma_w^{i,e} \approx \frac{\bar{n}V}{\tau_{pS}} = \frac{\bar{n}\pi a^2 L}{\tau_p 2\pi r_w L}, \quad \Gamma_w^{imp}, \Gamma_w^{\alpha} \ll \Gamma_w^{i,e}$$

B. Photon fluxes

Bremst., cyclotron, impurity radiations

C. Energy fluxes

Particle energies, Radiation energies, Heat conduction

→ Wall load : $1 \text{ MW/m}^2 \approx 14.1 \text{ MeV-n flux of } 4.43 \times 10^{17} \text{ n/m}^2\text{s thru wall.}$

2. Surface interaction phenomena

Alteration of surface (wall erosion) } → impurities
 Production of particle and photon fluxes }

A. Reflection by backscattering

B. Adsorption and desorption

Residual cooler gases implanted inside wall

→ Release of gases

C. Physical sputtering - Erosion

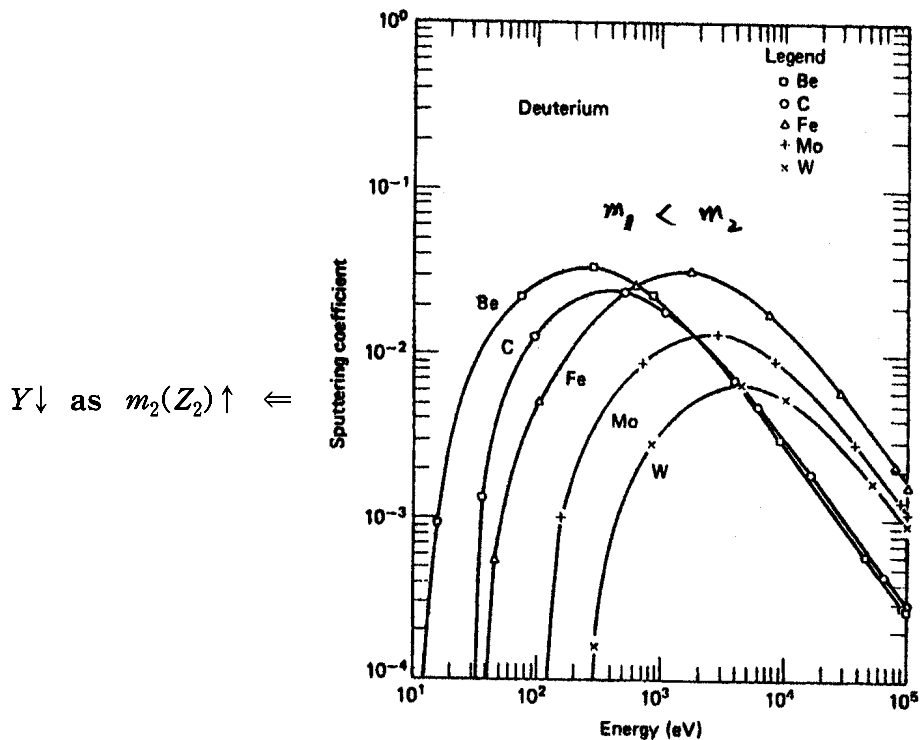
Ejection of surface atom from (low-temperature) wall
 as a result of collision cascade in the lattice atoms by n, i, a
 when acquired energy > surface binding energy U_o (~25 eV)

Sputtering yield : $Y \equiv$ ejected atoms/incident particles

Semi-theoretical value

$$Y(E) \uparrow \approx \frac{20}{U_o} (Z_1 Z_2)^2 \frac{m_1 \uparrow}{m_2} \frac{E}{(E + 50 Z_1 Z_2)^2} \text{ atoms/particle} \quad (1)$$

Y for D : Fig 6.1.1

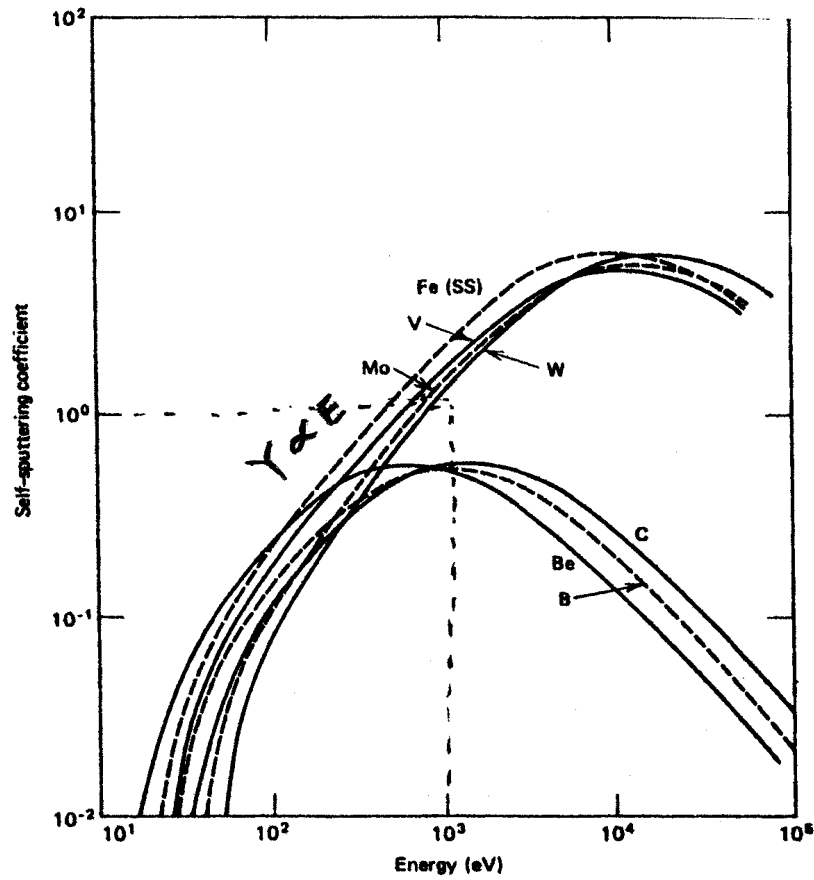


Stacey⁴⁾ Fig. 6.1.1 Physical Sputtering Yield for a Number of Materials for Deuterons

Threshold incident energy to produce sputtering

$$E_{th} = \frac{(m_1 + m_2)^2}{4m_1 m_2} U_o \quad (2)$$

Self-sputtering yield for reincident ions : Fig 6.1.2



Stacey⁴⁾ Fig. 6.1.2. Self-sputtering yield for a number of materials

For large Z_2 $Y(E) \approx 10^{-3}E$
 > 1 for $E \geq 10^3$ eV
 \rightarrow avalanche effect of impact
 \rightarrow tolerable limit

Neutron sputtering:

$$Y \approx 10^{-4} \sim 10^{-5} \text{ atoms/neutron}$$

D. Chemical sputtering

(e.g.) (H, D, T) + C

incident particle + surface atom \rightarrow chemical compound + reduced U_0

$$\Rightarrow Y_c(E) \geq 2Y_p(E)$$

E. Vaporization and melting

Disruptive instabilities \rightarrow Thermal shock on the wall

\rightarrow spalling, cracking, melting, evaporation

Fig.6.1.3: Calculated melting zone (s.s) \uparrow as energy density \uparrow , disrupt. time \uparrow .
Stacey⁴⁾

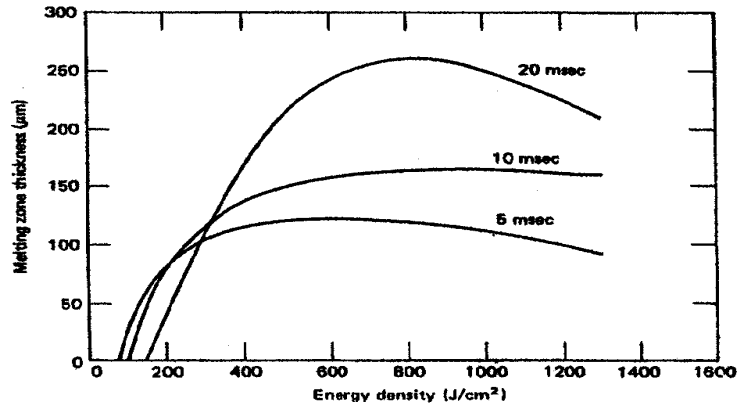
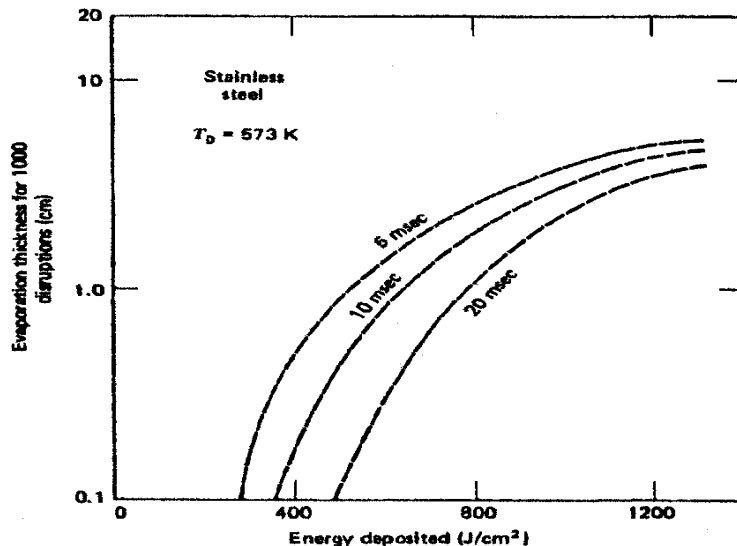


Fig.6.1.4: Evap. thickness for 1000 disrupt.(s.s) as E \uparrow , t \downarrow
Stacey⁴⁾



F. Blistering and Flaking

Blistering: gas bubble in $\sim\mu$ -thick surface layer (insoluble, He)

Flaking: Blister rupture by lateral stress and surface layer breaking

G. Electron emission (photoelectric, thermionic, X-ray, secondary)

H. Radiation damage & Transmutation by 14.1-MeV Neutron

Knock-on collisions --> interstitial, spikes, voids, displacements, ...

n capture reactions: (n,p), (n, α) \rightarrow production of p, α in 1st wall

\rightarrow swelling, radiation damage of wall, diffuse back to plasma

* Interactions in the plasma boundary

- NBI and recycling atoms \leftarrow (CX, I_i , I_e , R) \rightarrow Plasma ions, electrons
- Impurity atoms (ions) from 1st wall \leftarrow (I, Exc., R, Coul. collision) \rightarrow
Plasma electrons (ions) \Rightarrow Radiation cooling

3. Impurity radiation

= Bremsstr. + line radiation due to electron collision and excitation
+ radiative recombination loss

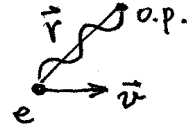
A. Bremsstrahlung (Braking radiation)

Mainly due to e-i collisions (In e-e or i-i colls., rad. fields exactly cancel)

Radiation fields (dipole approx.):

$$E \approx \frac{e}{4\pi\epsilon_0 c^2} \frac{\mathbf{r} \times (\mathbf{r} \times \dot{\mathbf{v}})}{r^3} \propto \frac{1}{r}, \quad r \gg \lambda \quad (3)$$

$$B \approx \frac{\mu_0 e}{4\pi c} \frac{\dot{\mathbf{v}} \times \mathbf{r}}{r^2} \propto \frac{1}{r}, \quad r \gg \lambda \quad (4)$$

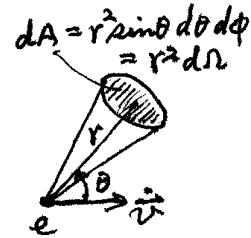


Poynting vector (instantaneous e.m. energy flux)

$$P_{rad} = \mathbf{E} \times \mathbf{H} = \frac{e^2}{16\pi^2 \epsilon_0 c^3} \frac{\mathbf{r} \times (\mathbf{r} \times \dot{\mathbf{v}}) \times (\dot{\mathbf{v}} \times \mathbf{r})}{r^5} \quad (5)$$

Radiative power per unit solid angle emitted from a charge

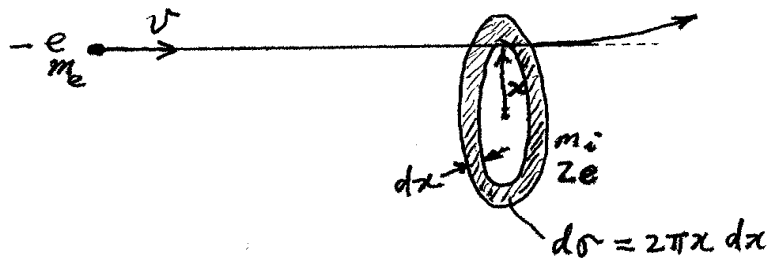
$$\frac{dW_{rad}}{d\Omega} = r^2 P_{rad} \cdot \hat{\mathbf{r}} = \frac{e^2}{16\pi^2 \epsilon_0 c^3} |\dot{\mathbf{v}}|^2 \sin^2 \theta \quad (6)$$



Total power radiated by an accelerated charge

$$W_{rad} = \int_0^{2\pi} d\phi \int_0^\pi d\theta \sin \theta r^2 P_{rad} \cdot \hat{\mathbf{r}} = \frac{1}{6\pi\epsilon_0} \frac{e^2 |\dot{\mathbf{v}}|^2}{c^3} \quad (7)$$

Assume small-angle Coulomb scattering



$$\tau \approx \frac{x}{v} \ll 1 \quad \text{otherwise continuous spectrum} \quad (8)$$

$$F = m_e |\dot{\mathbf{v}}| = \frac{Ze^2}{4\pi\epsilon_0 x^2} \Rightarrow |\dot{\mathbf{v}}| \approx \frac{Ze^2}{4\pi\epsilon_0 m_e x^2} \quad (9)$$

Power radiated from a single e-i collision

(9) in (7):

$$W_{rad} = \frac{Z^2 e^6}{96\pi^3 \epsilon_0^2 c^3 m_e^2 x^4} \quad (7)^*$$

Number of collisions per unit volume of n_e with n_i in $d\sigma$ during τ

$$dN = n_e n_i d\sigma v \tau = n_e n_i 2\pi x^2 dx \quad (10)$$

Total bremsstrahlung power density at all impact parameter x

$$\begin{aligned}
 P_{br} &= \int_{x_{\min}}^{x_{\max}} W_{rad} dN = \frac{Z^6 n_e n_Z}{48\pi^2 \epsilon_0^3 c^3 m_e^2} \int_{h/2\pi m_e v}^{\lambda_D} \frac{dx}{x^2} \\
 &= \frac{Z^2 e^6 n_e n_Z v}{24\pi \epsilon_0^3 c^3 m_e h} = \left(\frac{e^6 \sqrt{2}}{12\pi^{3/2} \epsilon_0^3 c^3 m_e^{3/2} h} \right) Z^2 n_e n_Z T_e^{1/2} \quad (11)
 \end{aligned}$$

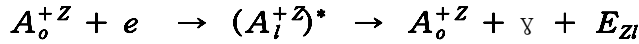
where $v = \sqrt{8kT_e/\pi m_e}$, $h/2\pi m_e v \rightarrow \frac{\hbar}{\Delta p}$ since $\Delta x \Delta p = \hbar$

Quantum correction: $g_f = \sqrt{\frac{3}{2}}$ = Gaunt factor by Spitzer

$$\begin{aligned}
 P_{br} &= \left(\frac{e^6 \sqrt{3}}{12(m_e \pi)^{3/2} \epsilon_0^3 c^3 h} \right) Z^2 n_Z n_e (kT_e)^{1/2} \\
 &\approx 4.8 \times 10^{-43} Z^2 n_Z n_e T_e^{1/2} (keV) \text{ MW/m}^3 \quad (12) \\
 &\approx 4.8 \times 10^{-43} Z_{eff}^2 n_e^2 T_e^{1/2} (keV) \text{ MW/m}^3
 \end{aligned}$$

B. Power loss by line radiation due to radiative decay

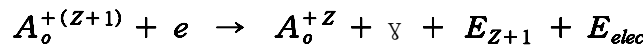
after electron collision excitation



$$P_L = n_e \sum_Z \sum_i n_Z E_{Zi} X_{Zi} \quad (X_{Zi}: \text{elec. coll. exc. rate})$$

$$\approx 1.8 \times 10^{-44} Z^4 n_e n_Z T_e^{-\frac{1}{2}} (keV) \text{ MW/m}^3 \quad (13)$$

C. Power loss by radiative recombination



ioniz. pot. free elect. K.E.

$$P_R = n_e \sum_Z n_{Z+1} \langle (E_{Z+1} + E_{elec})_{Rv} \rangle_{Z+1}$$

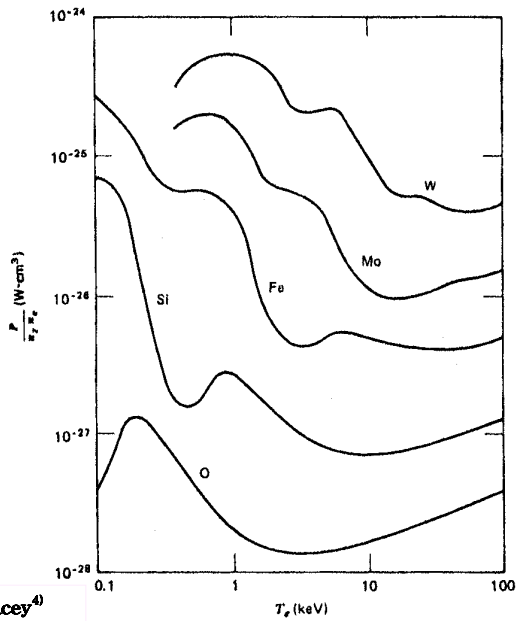
$$\approx 4.1 \times 10^{-46} Z^6 n_e n_Z T_e^{-\frac{3}{2}} (keV) \text{ MW/m}^3 \quad (14)$$

D. Normalized impurity radiative power

$$\propto Z^2 T^{1/2} \quad \propto Z^4 / T^{1/2} \quad \propto Z^6 / T^{3/2}$$

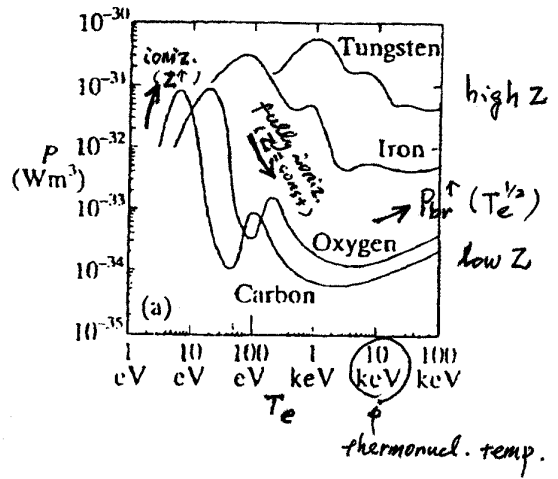
$$W_{rad}^{\uparrow} \equiv \frac{P_{imp}}{n_e n_Z} = \frac{P_{br} + P_L + P_R}{n_e n_Z} = f(T_e, Z^{\uparrow}) \quad (15)$$

\Rightarrow Fig. 6.2.2

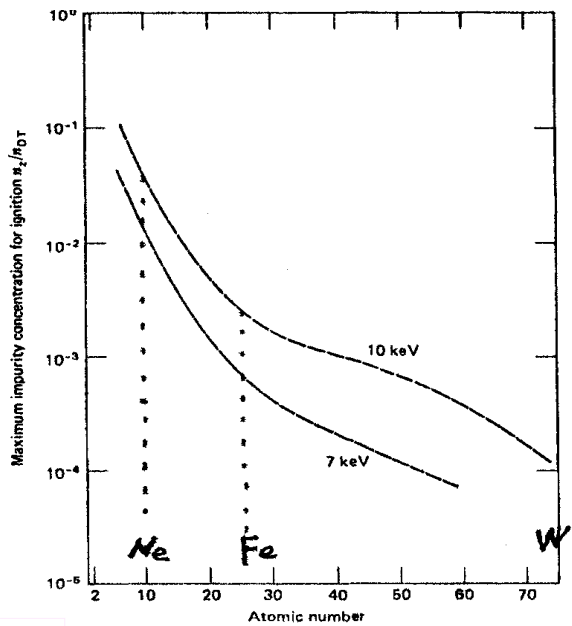


Stacey⁴⁾

Figure 6.2.2. Impurity radiative power loss from a plasma.



E. Maximum permissible impurity concentration



$$\left(\frac{n_Z}{n_{DT}}\right)_{\max}^{\uparrow} = f(Z^{\downarrow}, T^{\uparrow})$$

Stacey⁴⁾ Fig. 6.2.3 Maximum impurity concentration for which ignition can be achieved

At 10 keV

- Low Z (~ 10): $\left(\frac{n_Z}{n_{DT}}\right)_{\max} \approx 10\%$ Ne
- Medium Z (~ 26): $\left(\frac{n_Z}{n_{DT}}\right)_{\max} \approx 0.5\%$ Fe
- High Z (~ 74): $\left(\frac{n_Z}{n_{DT}}\right)_{\max} \approx 0.01\%$ W

4. Impurity control

→ maintain $\frac{n_z}{n_{DT}} < \left(\frac{n_z}{n_{DT}}\right)_{\max}$

A. Wall surface control

Suppression of high- z impurity formation or impurity formation itself

Eq.(1) Fig. 6.1.1; Eq.(15) Figs. 6.2.2, 6.2.3

$$\Rightarrow Y(E) \uparrow, P_{imp} \downarrow, \left(\frac{n_z}{n_{DT}}\right)_{\max} \uparrow \text{ as } Z \downarrow$$

1) Low- z wall surface

($\sim \mu m$ coating, $< 1 cm$ curtain or shingle)

C, Li, Be, B

high chem. sputt. easy evap. toxic, low m.p. (n, α), (n,p) \rightarrow He, H

$$\left(\frac{n_z}{n_{DT}}\right)_{\max} \geq 10 \%$$

2) Wall modification

Bake-out, Discharge cleaning, Gettering, Honey comb surface

B. Plasma boundary region control

1) Gas blanket model

High density cold neutral gas refreshed continuously in boundary region

→ (particle and energy fluxes) \downarrow with low energies ($< E_{fl}$)

→ wall erosion \downarrow → $n_z \downarrow$

Eq.(2)

Expected thickness $\approx 1m$ and high P drives instabilities

⇒ impractical !

2) Vacuum model

Low particle densities in SOL by divertor and/or limiter

→ (particle, energy, impurity fluxes) \downarrow

a. Divertors

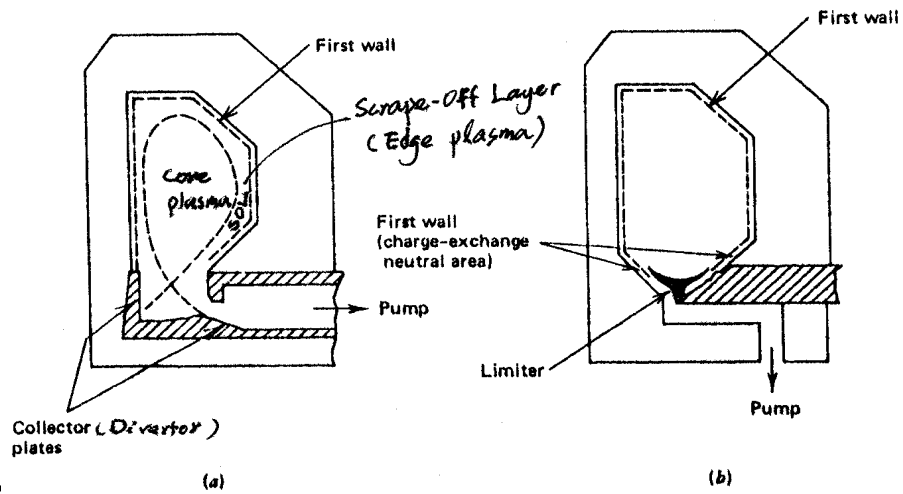
i) Principle

Bending outer magnetic fields away from plasma

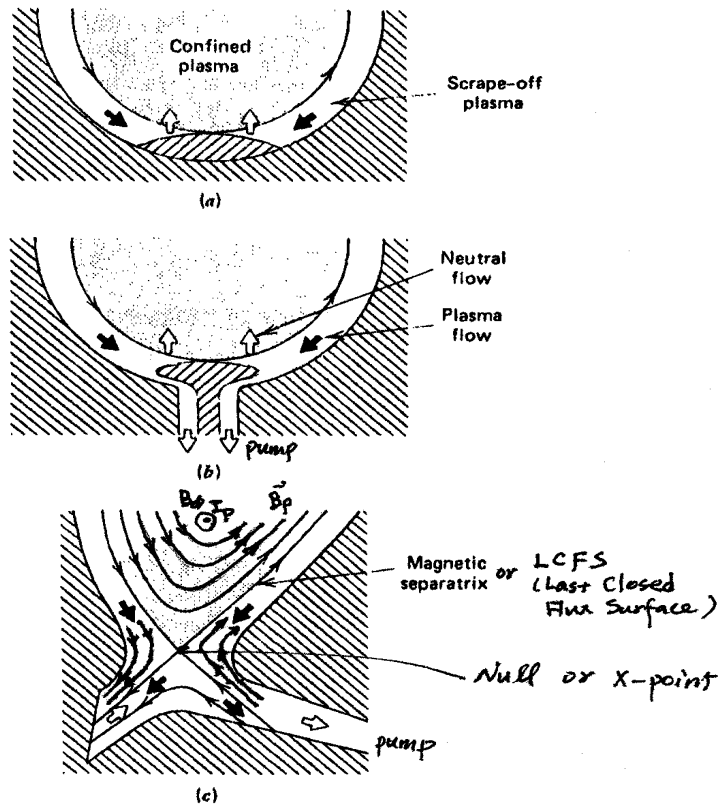
→ Removing outer layer of plasma to external chamber

→ Cooling → Neutralizing → Pumping away

Figs. 6.3.2 & 6.3.3



Stacey⁴⁾ Figure 6.3.2. Poloidal divertor and pumped-limiter configurations in a tokamak: (a) divertor; (b) limiter.

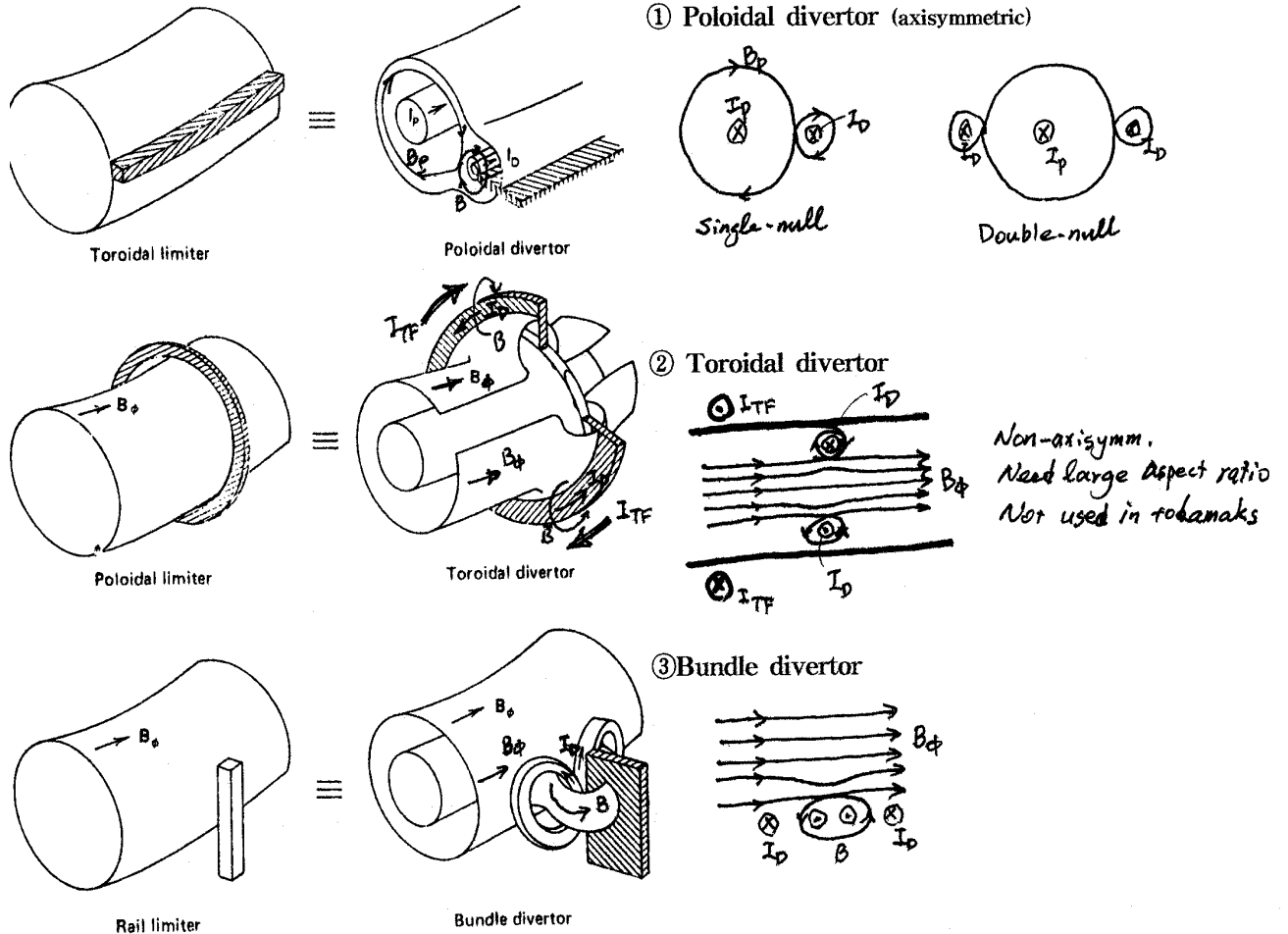


Stacey⁴⁾ Figure 6.3.3. Limiter and divertor plasma flow patterns: (a) simple limiter; (b) pumped limiter; (c) divertor.

ii) Functions

- ① Reduction of 1st wall bombardment (Unloading)
- ② Reduction of impurity flow into plasma
(Shielding for impurity control)
- ③ Exhaust plasma particles and power and Removal of He ash

iii) Types (Stacey⁴) Fig 6.3.1



iv) Problems

- ① Complex coil systems
- ② High cost
- ③ Difficult maintenance

b. Limiters (Figs. 6.3.1 - 6.3.3)

Scrape-off plasma by solid conductor

→ (refl. neutrals) → Pumping out

Type : Toroidal, Poloidal, Rail

Problem :

High heat load and sputtering rate on limiter → impurities

→ low-Z coating of limiters (C or Be on W)

(Note) H-mode discharge (disch. with divertors and/or limiters)

→ global confine time ↑ : exactly not understood

Homework Stacy 6- 2, 3, 4, 7, 9; Harms 13- 2, 3, 4, 5