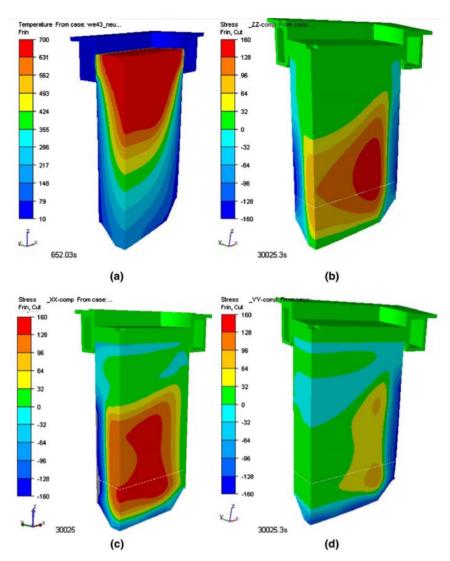
Correlation between Microstructure and Residual Stress in Selective Laser Melting

A.S.R.M 2019. 05. 20.

Residual Stress in As-cast material

Normal Cast Ingot





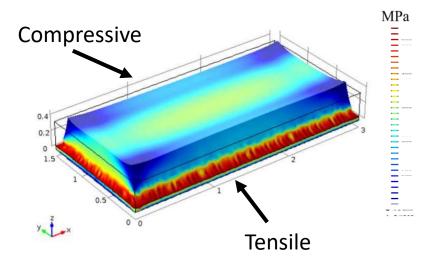
M. Tursky et al., Metallurgical and Materials Transactions A 43(5) · May 2012

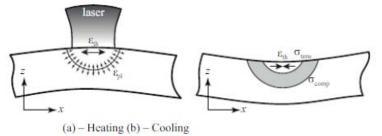


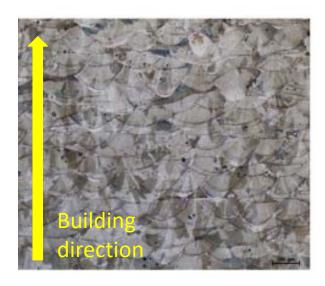
Residual Stress in As-cast material

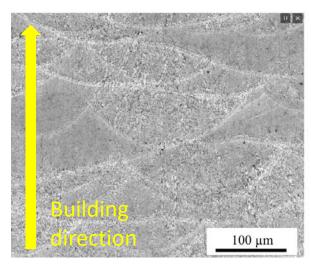
Residual stress in SLM



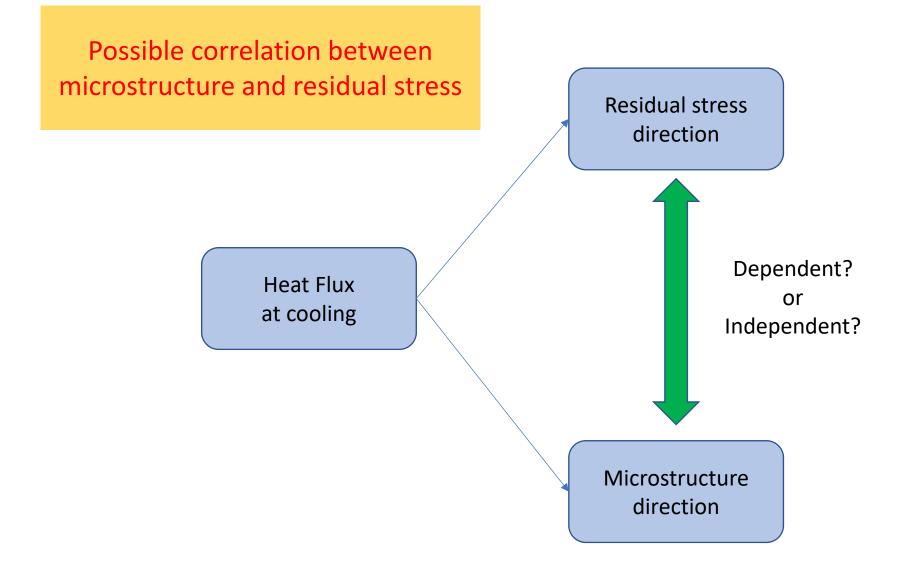














As-cast vs After stress relieving

Microstructure

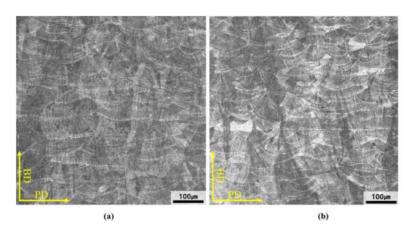


Fig. 2. Microstructures of SLMed AISI 316L alloys; (a) as fabricated (F) and (b) Heat treated (H).

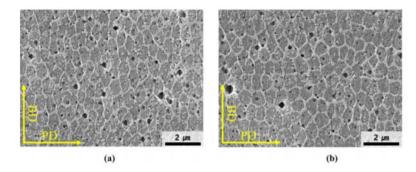
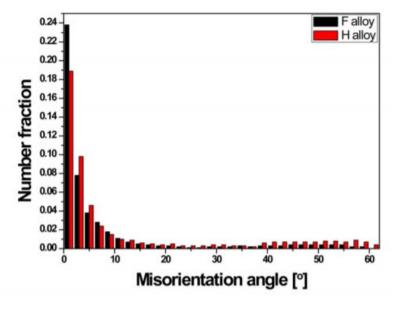


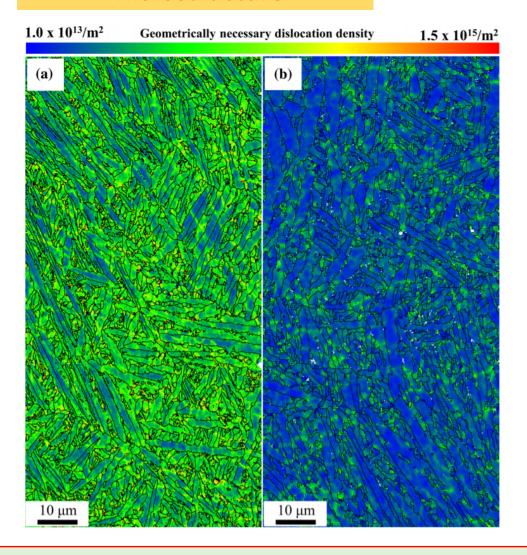
Fig. 3. High magnification microstructures of SLMed AISI 316L alloys; (a) as fabricated (F) and (b) Heat treated (H).

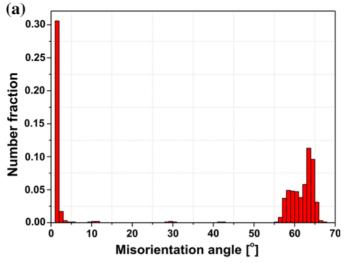


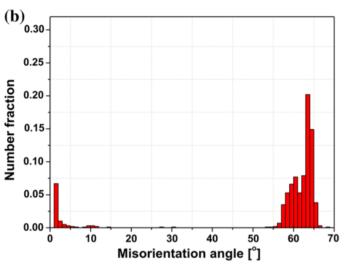
G.S. Ham et al., Korean J. Met. Mater., Vol. 57, No. 5 (2019) pp.295-303

As-cast vs After stress relieving

Microstructure



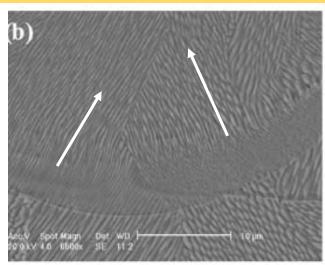




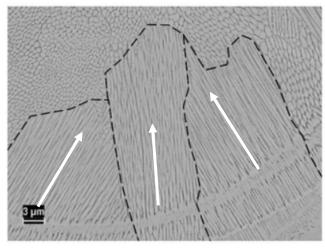
Y.K. Kim et al., Metallurgical and Materials Transactions A 49(11) · Nov 2018

Presumption

Cellular Microstructure in SLM



A lot of interfaces



As-SLMed

- Production of many interfaces
- Directional growth



After stress relief heat treatment

- Reducing interfacial area
- Decreasing directionality



Presumption

 Directional interfaces induce the residual stress

Surface Stress

Definition of surface free energy is seemly the amount of reversible work dw performed to create new area dA of surface,

$$dw = \gamma dA$$
 Surface free energy (Surface tension)

Gibbs was the first to define another surface quantity, different from the surface tension γ ,

that is associated with the reversible work per unit area needed to elastically stretch a pre-existing surface.

$$d(\gamma A) = A f_{ij} d\epsilon_{ij}$$

$$f_{ij} = \gamma \delta_{ij} + \partial \gamma / \partial e_{ij}$$
 $f = \gamma + \partial \gamma / \partial e$ Surface stress (Same unit with γ)

FCC Metal surfaces (111) [edit]

Metal	γ [J/m^2]	f [J/m^2]
Al	0.96	1.25
lr	3.26	5.30
Pt	2.19	5.60
Au	1.25	2.77
Pb	0.50	0.82

$$h_{ij} = \sigma \delta_{ij} + \partial \sigma / \partial e_{ij}$$
. Interface stress

h for (100) interface (J/m ²)	h for (111) interface (J/m²)	
0.83	0.32	_
0.71	-0.08	
0.53	0.32	
0.33	10.0	
0.04	-0.57	
	0.83 0.71 0.53 0.33	h for (100) interface (J/m²) 0.83 0.71 0.53 0.32 0.01

Positive: Tensile, Negative: Compressive

Research design

a hydrostatic pressure acting on this sphere equal to $\Delta P = 2f/r$ Hooke's Law is $\Delta P = -3K\varepsilon$, where K is the bulk modulus $f = -3K\varepsilon r/2$.

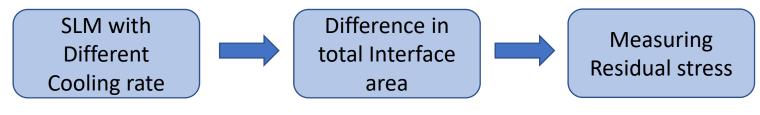
Modeling

Integrating
Interface stress

Dividing by
Surface area

Comparing
Residual stress
value

Experimental method



Cell spacing, Aspect ratio of the cell, etc.

Thank you for listening!

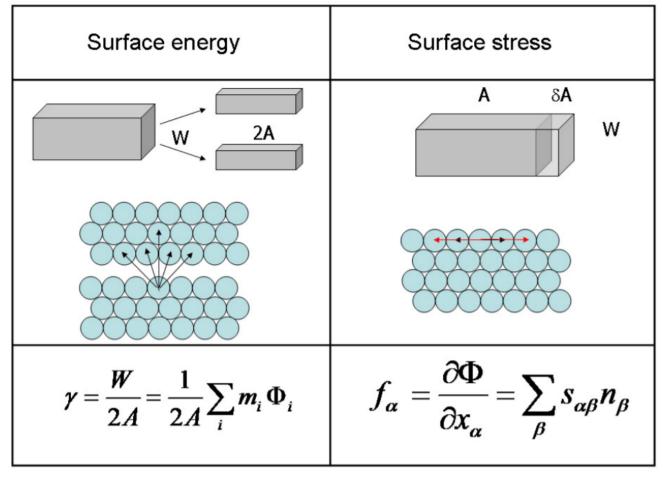


Figure 3. Sketch of the difference between surface stress and surface energy. The surface stress originates from an elastic deformation and thus from bonds stretching. It is an excess of stress in the surface (double arrows). Surface energy originates from a cleaving process and thus from breaking bonds. It is thus calculated as the sum of bonds (A is the surface area, n_i the number of ith neighbours whose bonding energy Φ are sketched by the arrows).

Surface Stress

Table 1. Basic thermodynamics equations valid for isotropic solid and liquid spheres of radius *R* illustrating the deep difference between surface energy and surface stress.

	Excess of pressure	Excess of chemical potential
Solid	$\sigma_{33} = \frac{2s}{R}$	$\Delta \mu = \frac{2\gamma}{R}$
Liquid	$\Delta P = \frac{2\gamma}{R}$	$\Delta P = \frac{2\gamma}{R}$

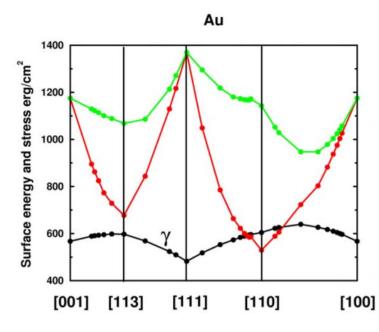


Figure 4. Cu surface energy and surface stress anisotropy calculated using a semi-empirical SMA potential. The two branches of surface stress (green and red) correspond to the two principal components of surface stress. For high symmetry directions the two branches merge in a single value (isotropic surface stress).