

Generalized Hamilton's Principle

$$\int_{t_1}^{t_2} [\delta T - \delta U_1^M + \delta U_1^E + \delta W_1^M - \delta W_1^E] dt = 0$$

Generalized Hamilton's Principle for Elastoelectric Bodies

$$\int_V \delta E^T D dV$$

$$S = L_u \vec{U}(x, y, z) \Rightarrow \begin{Bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \end{Bmatrix} = \begin{bmatrix} \frac{\partial}{\partial x} & 0 & 0 \\ 0 & \frac{\partial}{\partial y} & 0 \\ 0 & 0 & \frac{\partial}{\partial z} \\ 0 & \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial z} & 0 & \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial z} & 0 \end{bmatrix} \begin{Bmatrix} U_1(x, y, z) \\ U_2(x, y, z) \\ U_3(x, y, z) \end{Bmatrix}$$

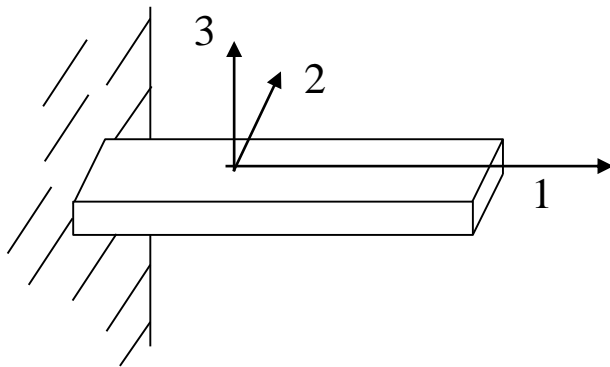
$\hookrightarrow L_U$

Generalized Hamilton's Principle

$$\begin{bmatrix} E_1 \\ E_2 \\ E_3 \end{bmatrix} = \begin{bmatrix} -\frac{\partial}{\partial x} \\ -\frac{\partial}{\partial y} \\ -\frac{\partial}{\partial z} \end{bmatrix} \phi(x)$$

$L_p \leftarrow$

For Euler- Bernoulli beam,

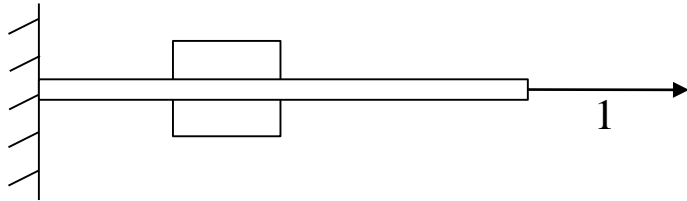


$$\begin{Bmatrix} U_1(x, y, z) \\ U_2(x, y, z) \\ U_3(x, y, z) \end{Bmatrix} = \begin{bmatrix} 1 & -y \frac{\partial}{\partial x} & -z \frac{\partial}{\partial x} \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \bar{U}_1(x) \\ \bar{U}_2(x) \\ \bar{U}_3(x) \end{bmatrix}$$

L_{u2}

$\Rightarrow L_u L_{u2}$

Generalized Hamilton's Principle



$$\begin{bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \end{bmatrix} = \begin{bmatrix} \frac{\partial}{\partial x} & -y \frac{\partial^2}{\partial x^2} & -z \frac{\partial^2}{\partial x^2} \\ & & \\ & & \\ & 0 & \\ & & \\ & & \end{bmatrix} \begin{bmatrix} \bar{U}_1(x) \\ \bar{U}_2(x) \\ \bar{U}_3(x) \end{bmatrix}$$

Generalized Hamilton's Principle

- Classical plate

$$\begin{bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \end{bmatrix} = \begin{bmatrix} \frac{\partial}{\partial x} & 0 & -z \frac{\partial^2}{\partial x^2} \\ 0 & \frac{\partial}{\partial y} & -z \frac{\partial^2}{\partial y^2} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial x} & -2z \frac{\partial^2}{\partial x \partial y} \end{bmatrix} \begin{bmatrix} U_1(x, y) \\ U_2(x, y) \\ U_3(x, y) \end{bmatrix}$$

$$\vec{U}(\vec{x}, t) = \psi_r(\vec{x}) \vec{r}(t)$$

Generalized Coordinate

↑

$$= \begin{bmatrix} \psi_{r_1}(\vec{x}) & \cdots & \psi_{r_n}(\vec{x}) \end{bmatrix} \begin{bmatrix} r_1(t) \\ \vdots \\ r_n(t) \end{bmatrix}$$

Generalized Hamilton's Principle

- Classical Plate

$$\begin{aligned}\varphi(\vec{x}, t) &= \psi_v(\vec{x}) \vec{V}(t) \\ &= \left[\psi_{V_1}(\vec{x}) \cdots \psi_{V_m}(\vec{x}) \right] \begin{bmatrix} V_1(t) \\ \vdots \\ V_m(t) \end{bmatrix}\end{aligned}$$

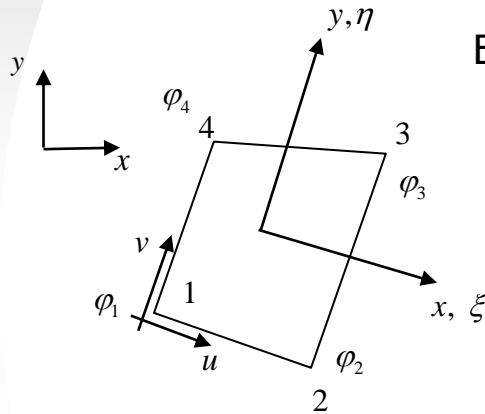
$$\vec{U}(\vec{x}, t) = \psi_r(\vec{x}) \vec{r}(t)$$

$$\varphi(\vec{x}, t) = \psi_v(\vec{x}) \vec{V}(t)$$

Rayleigh–Ritz \Rightarrow over the whole domain

Generalized Hamilton's Principle

- Finite Elements
 - Displacement – voltage based finite elements are directly analogous to Rayleigh-Ritz procedure



- Example - 2-D quadrilateral
- 3 DOF's per node 2 mechanical, 1 electrical

$$\begin{aligned} & [u(x, y) \quad v(x, y) \quad \varphi(x, y)] \\ &= \frac{1}{4} \sum_{i=1}^4 (1 - \xi_i \xi)(1 - \eta_i \eta) [u_i \quad v_i \quad \varphi_i] \end{aligned}$$

ξ_i, η_i are $\xi - \eta$ coordinate for the nodes

Combining shapes with differential operators

$$S(x, t) = L_u \psi_r(x) \vec{r}(t)$$

$$N_r(x)$$

$$E(x, t) = L_\varphi \psi_v(x) V(t)$$

$$N_v(x)$$