

Lecture 3.3:

Torsion Analysis for Multiply-Connected Section

노트 제목



C_0 : outer boundary ↷

$C_i (i=1, \dots, n)$: inner boundary ↷

multiply-
connected
cross-section

- warping ftn formulation
 - ↳ no need to consider compatibility
- Prandtl ftn approach
 - ↳ must consider compatibility for single-valuedness

<warping ftn formulation>

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0 \text{ in } R$$

$$\frac{d\phi}{ds} = yv_x - xv_y \text{ on } C_i \quad (i=0, 1, \dots, n)$$

<Prandtl Approach>

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = -2$$

$$\psi = k_i \text{ on } C_i \quad \text{with } k_0 = 0$$

↑
constant k_i

physical meaning t_z on $C_i = 0$

What are the values of $k_i = ?$

↳ "n" additional conditions are needed

↑
"must satisfy single-valuedness"

We will show

$$\oint_{C_i} \frac{d\psi}{dv} dl = 2A_i \quad (i=1, \dots, n) \quad (*)$$

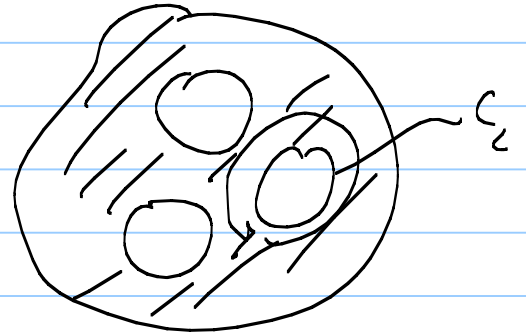
↑
Area of a hole
bounded by C_i

< Derivation of (*) >

$$0 = \oint_{C_i} d u_z$$

$$= \oint_{C_i} \alpha d\varphi$$

$$= \alpha \left[\oint_{C_i} \frac{\partial \varphi}{\partial x} dx + \frac{\partial \varphi}{\partial y} dy \right]$$



$$0 = \alpha \left[\oint_{C_i} \left(\frac{\partial \psi}{\partial y} + y \right) dx - \left(x + \frac{\partial \psi}{\partial x} \right) dy \right]$$

or

$$\oint_{C_i} \left(\frac{\partial \psi}{\partial y} dx - \frac{\partial \psi}{\partial x} dy \right) = \oint_{C_i} (-y dx + x dy)$$

$$\begin{aligned}
 \text{LHS} &= \oint \left(\frac{\partial \psi}{\partial x}, \frac{\partial \psi}{\partial y} \right) \cdot (dy, -dx) \\
 &= - \oint \nabla \psi \cdot \left(\frac{dy}{ds}, -\frac{dx}{ds} \right) dS \\
 &\quad \quad \quad \downarrow \quad \downarrow \\
 &\quad \quad \quad v_x, \quad v_y \\
 &= - \oint \nabla \psi \cdot \underline{v} dS = - \oint \frac{d\psi}{ds} dS
 \end{aligned}$$

$$\begin{aligned}
 \text{RHS} &= \oint -y dx + x dy \\
 &= \oint (x, y) \cdot (dy, -dx) \\
 &= \oint (x, y) \cdot \left(\frac{dy}{ds}, -\frac{dx}{ds} \right) dS \\
 &= \oint_{C_i} (x, y) \cdot \underline{v} dS \\
 \text{div} &= \oint_{C_i} \nabla \cdot (x, y) dA = 2 \oint_{C_i} dA \\
 &= 2 A_i
 \end{aligned}$$

Thus

$$\oint_{C_i} \frac{d\psi}{d\vec{v}} dS = -2\dot{A}_i \quad (i=1, \dots, n) \quad (*)$$

Physical meaning of (*):

use

$$\tau = -\mu\alpha \frac{d\psi}{d\vec{v}}$$

Then

$$\oint_{C_i} \tau dS = 2\mu\alpha \dot{A}_i$$

circulation of τ // Area enclosed

▣ ①, ②, ③ satisfy (a) and (b).

Check:

$$\begin{aligned} \text{PDE: } \nabla^2 \psi &= \nabla^2 \psi_p + \sum_{i=1}^n d_i \psi_c^{(i)} \\ &= -2 + 0 \Rightarrow (a) \end{aligned}$$

BC:

$$\begin{aligned} \psi|_{c_0} &= \psi_p|_{c_0} + \sum d_i \psi_c^{(i)}|_{c_0} \\ &= 0 + \sum d_i 0 = 0 \end{aligned}$$

$$\begin{aligned} \psi|_{c_k} &= \psi_p|_{c_k} + \sum_{i=1}^n d_i \psi_c^{(i)}|_{c_k} \\ (k \neq 0) &= 0 + d_k (1) = d_k \\ &\quad \text{constant} \end{aligned}$$

To determine d_k :

$$\oint_{C_i} \frac{d\psi}{dV} dS = -2A_i \quad (i=1, \dots, n)$$

$$\rightarrow \left[\sum_{j=1}^n d_j \oint_{C_i} \frac{d\psi_c^{(j)}}{dV} dS + \oint_{C_i} \frac{d\psi_p}{dV} dS \right]$$

$$= -2A_i \quad (i=1, \dots, n)$$

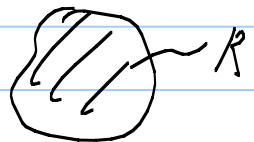
n additional equations

Torsional Rigidity C_t :

$$\text{Recall } C_t = M_t / \alpha$$

$$= \int_R (x\sigma_{yz} - y\sigma_{xz}) dA / \alpha$$

$$= -\mu \int_R \left(x \frac{\partial \psi}{\partial x} + y \frac{\partial \psi}{\partial y} \right) dA$$



$$= -\mu \int_R \left[\frac{\partial}{\partial x} (x\psi) + \frac{\partial}{\partial y} (y\psi) \right] dA$$

$$+ 2\mu \int_R \psi dA$$

=

Divergence Th

$$- \mu \oint_C \psi (xv_x + yv_y) dl$$

$$+ 2\mu \int_R \psi dA$$

applies only in simply connected Region

To deal with multiply-connected region;
trick:



Introduce C

$$C = C_0 - \sum_{i=1}^n C_i + \lim_{\epsilon \rightarrow 0} \sum_{i=1}^n (\Gamma_{0i}^+ + \Gamma_{0i}^-)$$

\Rightarrow With C , R is now treated as a simply-connected region!!

Then

$$C_t = -\mu \int_R \left(\frac{\partial}{\partial x} (x\psi) + \frac{\partial}{\partial y} (y\psi) \right) dA + 2\mu \int_R \psi dA$$

$$= -\mu \oint_C (x\psi v_x + y\psi v_y) dl + 2\mu \int_R \psi dA$$

$$= -\mu \left(\oint_{C_0} - \oint_{C_1} - \oint_{C_2} \dots - \oint_{C_n} \right)$$

$$+ \lim_{\epsilon \rightarrow 0} \sum_{i=1}^n \left(\int_{\Gamma_{0i}^+} + \int_{\Gamma_{0i}^-} \right) \psi (xv_x + yv_y) dl$$

$$+ 2\mu \int_R \psi dA$$

$$\begin{aligned}
&= -\mu \left[\oint_{k_0} (xv_x + yv_y) dl \right. \\
&\quad \left. - \sum_{i=1}^n k_i \oint (xv_x + yv_y) dl \right] \\
&\quad + 2\mu \int_R dA \\
&= \mu \sum_{i=1}^n \oint_{C_i} k_i (xv_x + yv_y) dl \\
&\quad + 2\mu \int_R dA \\
&= 2\mu \left(\sum_{i=1}^n k_i A_i + \int_R \psi dA \right)
\end{aligned}$$

$A_i =$ Area enclosed by C_i
 $(i=1, \dots, n)$

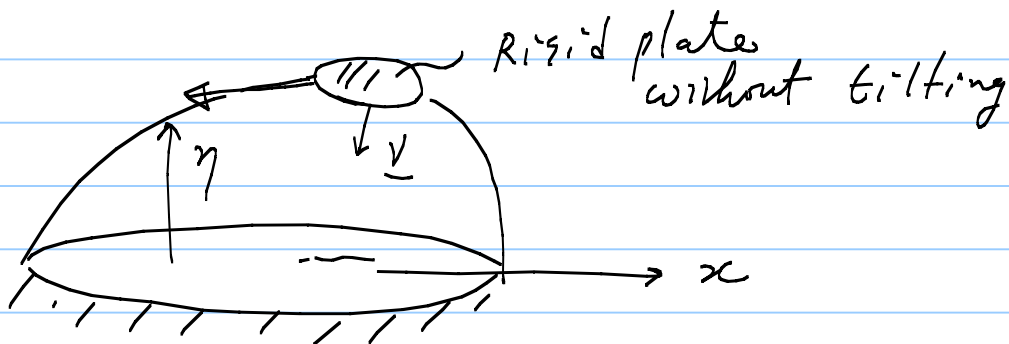
(Membrane Analogy)

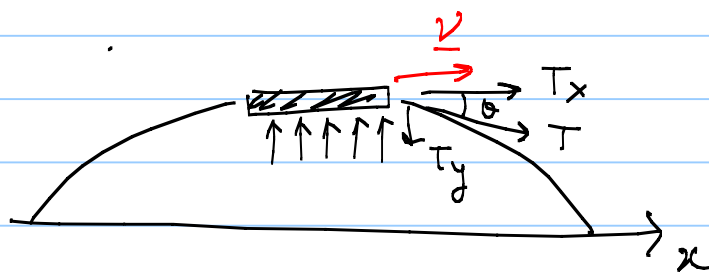
$$\oint_{C_i} \frac{d\psi}{dV} dS = -2A_i$$

$$\oplus \quad \psi = \frac{2T}{\rho} \eta$$

$$\oint_{C_i} \left(-T \frac{d\eta}{dV} \right) dS = \rho A_i$$

($\eta = \text{CONST}$ on C_i)





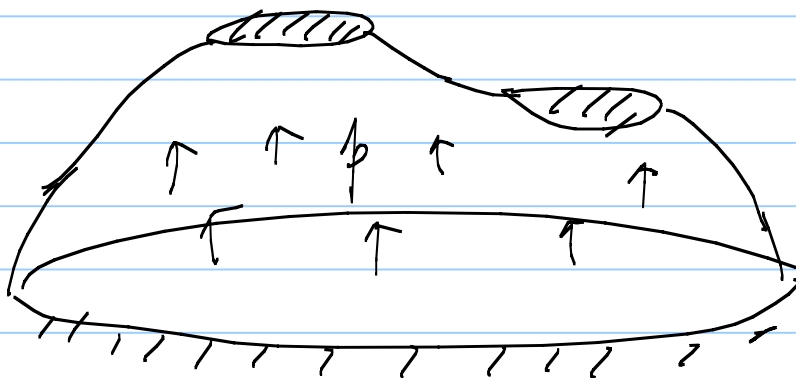
$$\begin{aligned} T_y &= T \sin \theta \\ &= T \left(-\frac{\Delta \eta}{\Delta x} \right) \\ &= -T \frac{d\eta}{dx} \end{aligned}$$

$$\oint T_y ds = p A_i$$

$$\text{or } \int \left(-T \frac{d\eta}{dx} \right) ds = p A_i$$

Eqm Condition

⇒ Hole surrounded by C_i
 \equiv frictionless rigid plate



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Torsional Rigidity

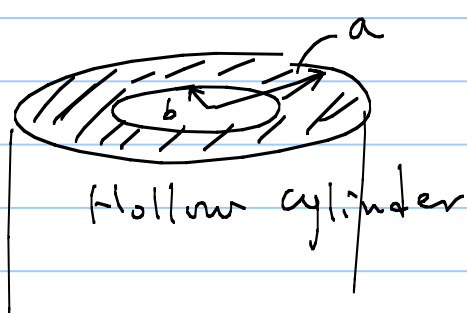
$$C_t = 2\mu \left(\int \sum_{i=1}^n k_i A_i + \int_R \psi dA \right)$$

$$= \frac{4\mu T}{\phi} \left(\sum_{i=1}^n K_i A_i + \int_R \eta dA \right)$$

\uparrow
 value of η
 along C_i

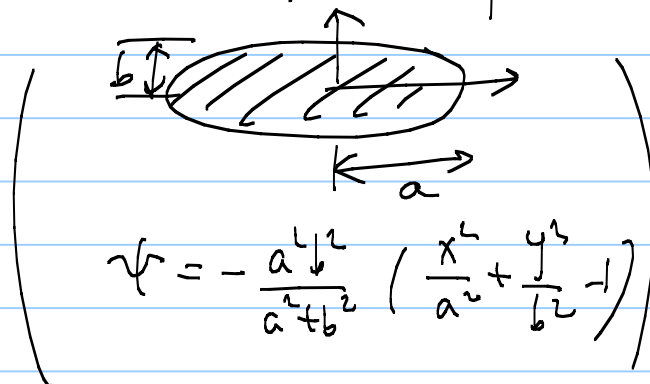
"Total volume enclosed by R with rigid plates"

Special case



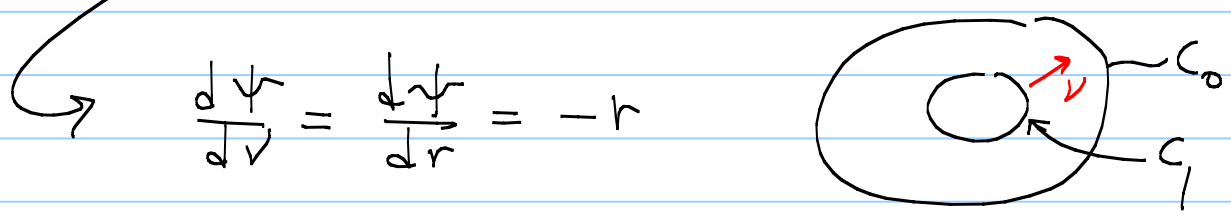
$$\psi = \frac{1}{2} (a^2 - r^2) \quad (a)$$

\uparrow solution from elliptic section



ψ satisfies $\nabla^2 \psi = -2$ Yes
 (a) $\psi = 0$ on C_0 ($r=a$) Yes
 (b) $\psi = k_1$ on C_1 ($r=b$) Yes
 $= \frac{1}{2}(a^2 - b^2)$

$$\textcircled{3} \oint_{C_1} \frac{d\psi}{dr} ds = -2A_1$$



$$\therefore \oint_{C_1} \frac{d\psi}{dr} ds = \int_0^{2\pi} (-b)(b) d\theta$$

$$= -2\pi b^2 = -2A_1$$

(Yes)

In this case

$$C_t = \frac{\mu\pi}{2} (a^4 - b^4)$$