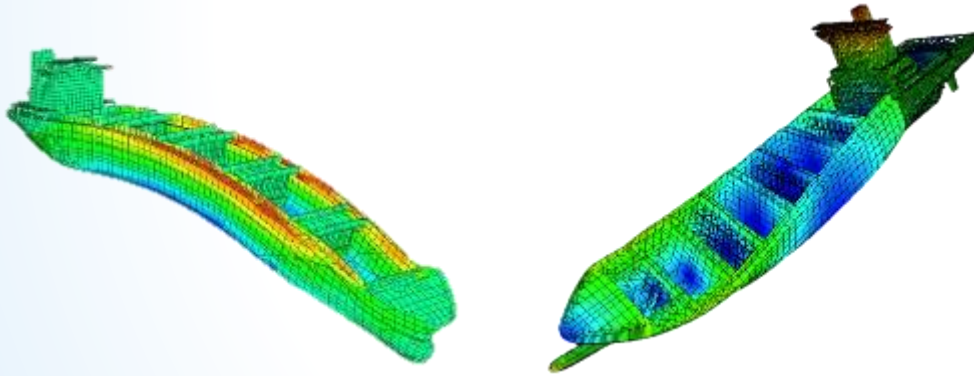


Topics in Ship Structures

(Advanced Local Structural Design & Analysis of Marine Structures)



* Ultimate loads on beams (Topic 2)

Do Kyun Kim
Seoul National Univer



<https://sites.google.com/snu.ac.kr/ost>

[Theory of Plates and Grillages]

[Part I] Plastic Design of Structures

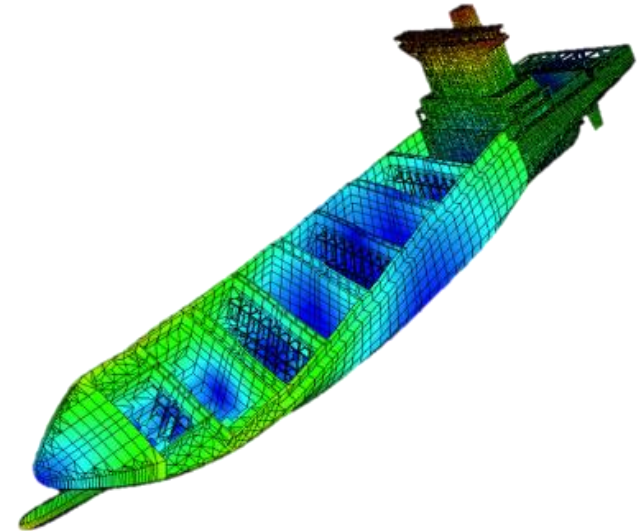
- Plastic theory of bending (Topic 1)
- Ultimate loads on beams (Topic 2)
- Collapse of frames and grillage structures (Topic 3)

[Part II] Elastic Plate Theory under Pressure

- Basic (Topic 4)
- Simply supported plates under Sinusoidal Loading (Topic 5)
- Long clamped plates (Topic 6)
- Short clamped plates (Topic 7)
- Low aspect ratio plates, strength & permanent set (Topic 7A)

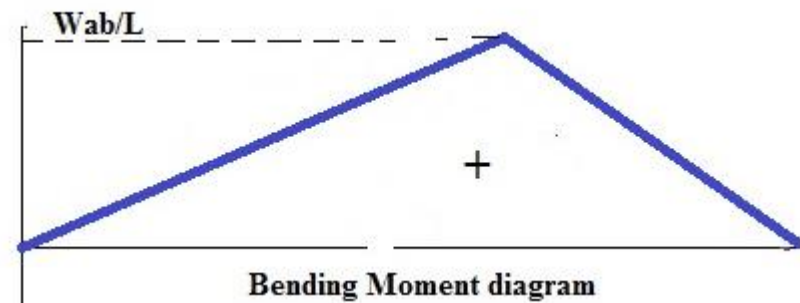
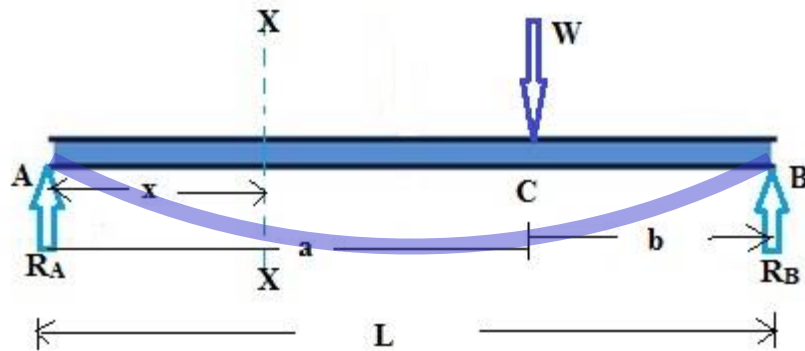
[Part III] Buckling of Stiffened Panels

- Failure modes (Topic 8)
- Tripping (Topic 9) + Post-buckling strength of plate (Topic 9A)
- Post-buckling behaviour (Topic 10)



The aim of this lecture is:

- To **equip** you with the necessary skills to carry out **plastic analysis** of beams.



At the end of this lecture, you should be able to:

- Discuss **three conditions** that must be satisfied in **plastic analysis**.
- Apply the **mechanism method** or the **principle of virtual work** to calculate **ultimate load** on a beam.
- Be aware of **upper bound theorem** and **lower bound theorem**.



- In plastic design of structures, the **criterion of failure** is the **collapse of structures**.
- Therefore, it is necessary to find out the **ultimate strength** or **load**.
- These can be estimated by means of **mechanism method** or the **principle of virtual work**.



(a) Simply supported beam with central point load

- The **max bending** moment occurs at **mid-span** and is $WL/4$.
- As the load increases, the yield first occurs at the **mid-span**
- The **yield moment** and **yield load** are, respectively,

$$M_Y = \frac{W_Y L}{4}$$

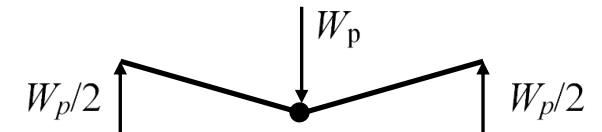
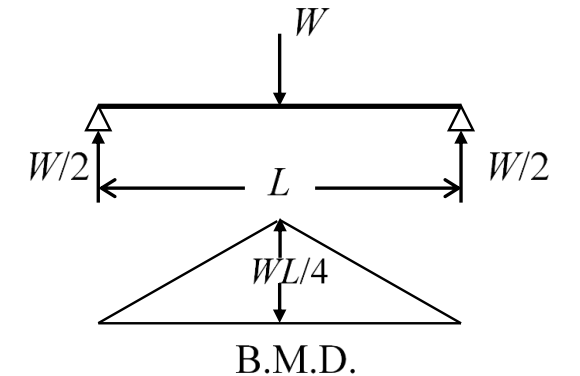
&

$$W_Y = \frac{4M_Y}{L}$$

- Further increasing the load to W_p , a **plastic hinge** will form at the **mid-span** and the **plastic moment** is

$$M_p = \frac{W_p L}{4}$$

- As there are **three hinges**: two at **simple supports** and one at the **mid-span**, no more load can be taken and so a **collapse mechanism** occurs.



Plastic mechanism



(a) Simply supported beam with central point load

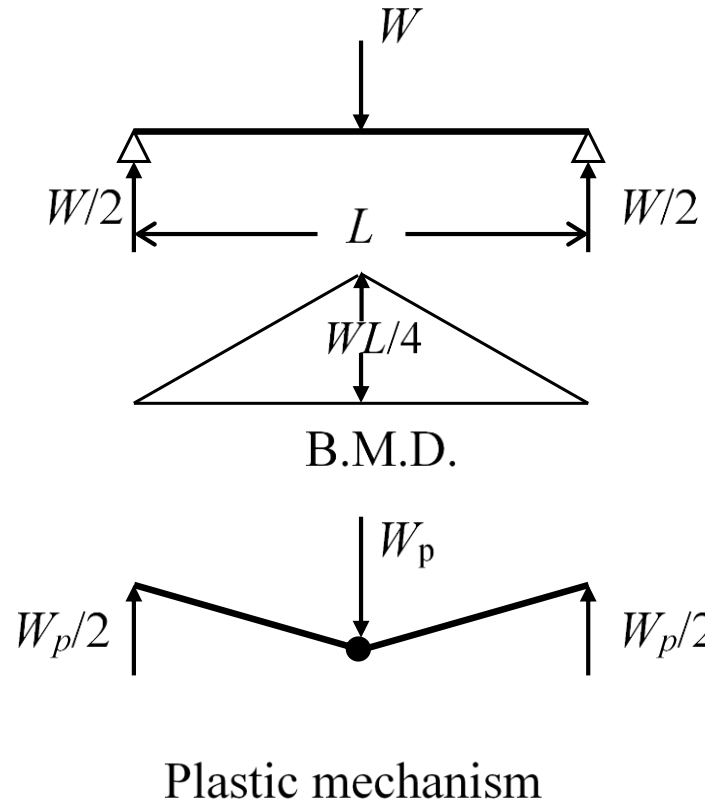
- Thus, **the ultimate load** is

$$W_p = \frac{4M_p}{L}$$

- Hence,

$$\frac{W_p}{W_Y} = \frac{M_p}{M_Y} = \phi$$

$$W_Y = \frac{4M_Y}{L}$$



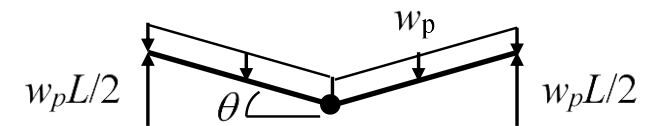
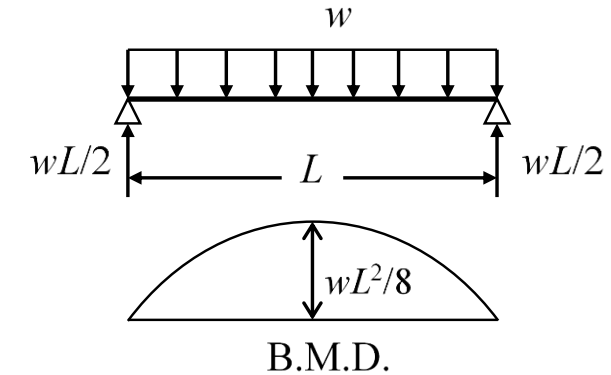
(b) Simply supported beam with uniform distributed load

- The B.M.D. indicates that the **max bending moment** occurs at **mid-span** and will reach the yield moment first

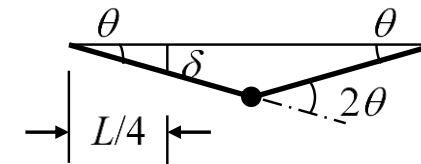
$$M_Y = \frac{w_Y L^2}{8}$$

- Thus, the **yield load** is

$$w_Y = \frac{8M_Y}{L^2}$$



Plastic mechanism

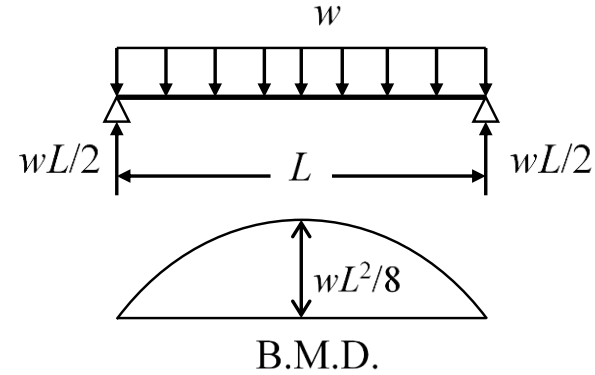


Displacements

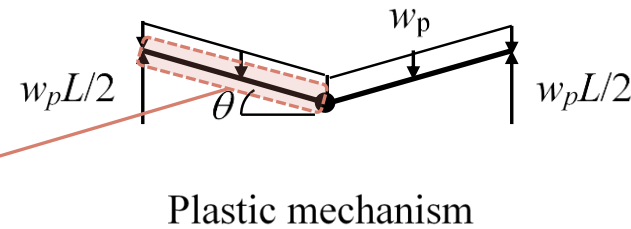


(b) Simply supported beam with uniform distributed load

- Further increase in load to w_p will make a plastic hinge at the mid-span and no more load can be taken. The beam will collapse.

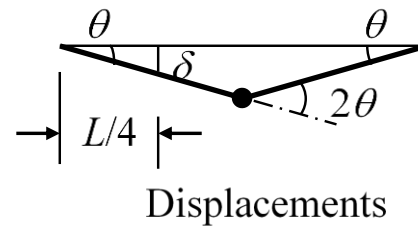


- Internal work = $2 M_p \theta$



- External work =

$$2 \left(\frac{w_p L}{2} \delta \right) = 2 \left(\frac{w_p L}{2} \frac{L \theta}{4} \right) = \frac{w_p L^2}{4} \theta$$



(b) Simply supported beam with uniform distributed load

- By the principle of virtual work,

$$\frac{w_p L^2}{4} \theta = 2M_p \theta$$

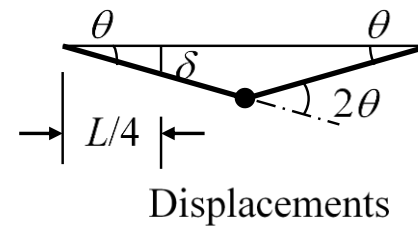
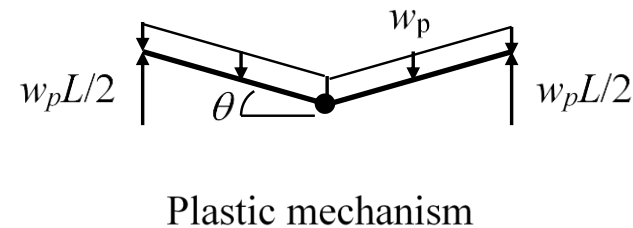
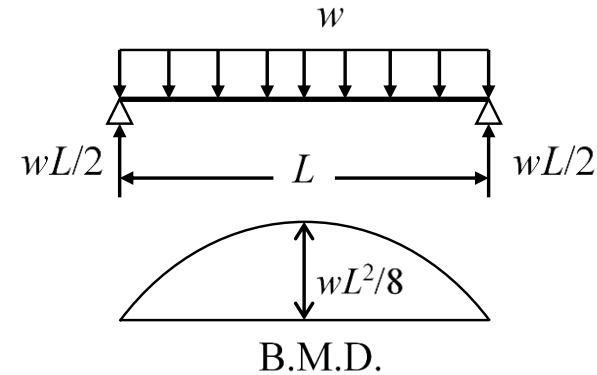
- Thus, the ultimate load is

$$w_p = \frac{8M_p}{L^2}$$

- Hence,

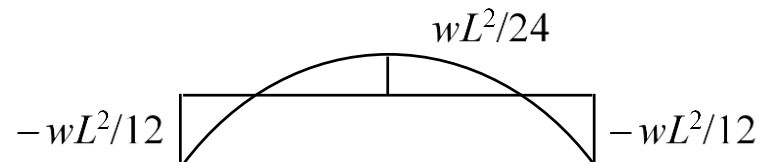
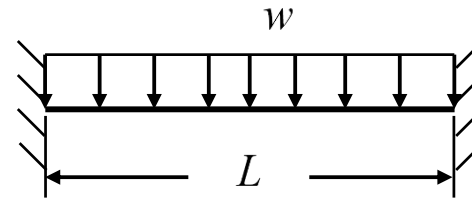
$$w_Y = \frac{8M_Y}{L^2}$$

$$\frac{w_p}{w_Y} = \frac{M_p}{M_Y} = \phi$$



(c) Fixed end beam with uniform distributed load

- As w increases, first yield will occur at the extreme fibre at the supports (**max. B.M.**)
- Then, we have **Yield moment**



B.M.D.

$$M_Y = \frac{w_Y L^2}{12}$$

- And **yield load**

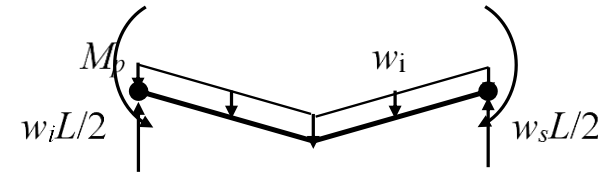
$$w_Y = \frac{12M_Y}{L^2}$$

Refer to Chapter 6

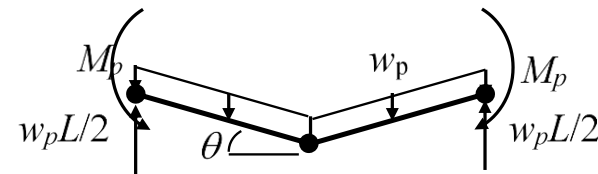


(c) Fixed end beam with uniform distributed load

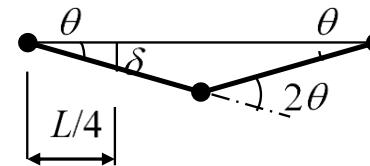
- Further increase in w will increase the end moments up to M_p , at which loading hinges will form at the supports.
- With further loading, moment at the supports remains constant as the hinge rotates; it acts like a simply supported beam.
- Next cross-section with critical moment is the mid-span. First it suffers extreme fibre yield. Then as yield progresses, a hinge forms.
- Once 3 hinges have formed, collapse will occur.



First hinges at supports



Plastic mechanism



Displacements



(c) Fixed end beam with uniform distributed load

- Internal work = $4 M_p \theta$

- External work =

$$2 \left(\frac{w_p L}{2} \delta \right) = 2 \left(\frac{w_p L}{2} \frac{L\theta}{4} \right) = \frac{w_p L^2}{4} \theta$$

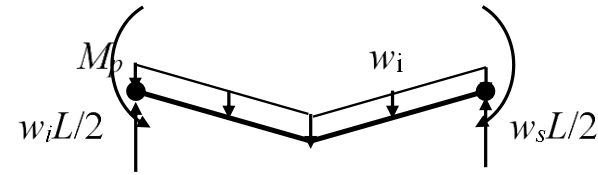
- By the principle of virtual work,

$$\frac{w_p L^2}{4} \theta = 4 M_p \theta$$

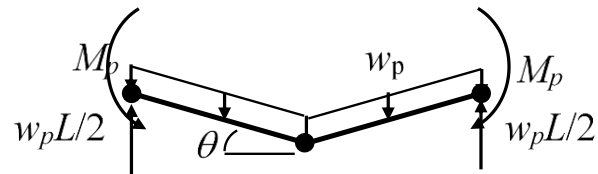
- Thus, the ultimate load

$$w_Y = \frac{12M_Y}{L^2}$$

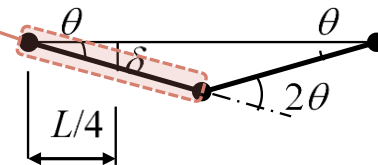
$$w_p = \frac{16M_p}{L^2}$$



First hinges at supports



Plastic mechanism



Displacements



(c) Fixed end beam with uniform distributed load

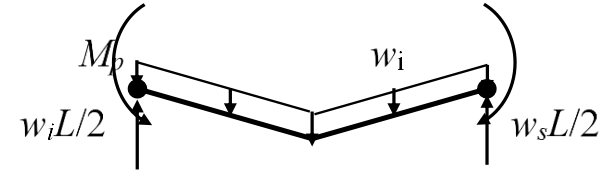
- Hence,

$$\frac{w_p}{w_Y} = \frac{16M_p}{12M_Y} = \frac{4}{3} \phi$$

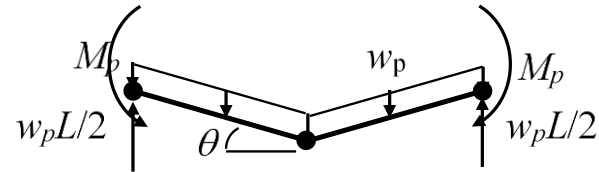
- Typical value of shape factor for stiffened plate is about 1.3, which gives

$$\frac{w_p}{w_y} = \frac{4}{3} \times 1.3 \approx 1.73$$

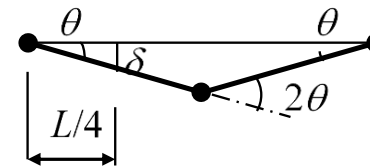
- The above example shows that plastic hinges form at the supports of the beam while the moment increases at the mid-span to maintain equilibrium with the load.
- This redistribution of moment continues through the attainment of yielding at the mid-span until the third plastic hinge is formed. Then a mechanism is formed.



First hinges at supports



Plastic mechanism



Displacements



Requirements of plastic analysis

- It has been pointed out that **full yielding** of a cross-section of a member results in a **plastic hinge** if no **instability** occurs.
- For **statically indeterminate structures**, the formation of a **plastic hinge** reduces the **indeterminacy** as shown in example (**Page 11-14**).
- After first **plastic hinges** have formed, further increases in load are **possible** until the formation of a **sufficient number** of plastic hinges
- This results in unrestricted plastic flow, that is, until a **plastic mechanism** of part, or of the whole structure has been **reached**.
- When the **mechanism** is formed, the structure **CANNOT** take **any additional load**.
- It is necessary to find the **correct mechanism** or its corresponding **equilibrium moment diagram** for strength evaluation.
- This is because the **plastic strength** of a beam depends on the formation of **plastic hinges** and on the redistribution of **moments to form a mechanism**,
- There are **three conditions** which must be satisfied in **plastic analysis**.



Requirements of plastic analysis

1 - **Equilibrium:** $\sum F = 0$ and $\sum M = 0$

2 - **Mechanism:** Sufficient plastic hinges form a plastic mechanism

3 - **Plastic moment:** $M = M_p$ is reached at each plastic hinge & $M < M_p$ at the remaining part of the beam.



Methods of plastic analysis

1. Mechanism Method

2. Principle of Virtual Work



1. Mechanism Method

- To fulfill all the conditions required for plastic analysis and to find the **plastic strength**, **mechanism method** may be used.
- The procedures of the mechanism method are:
 1. Assume a **plastic mechanism**.
 2. Find unknown reactions in terms of M_p by means of **equilibrium condition**.
 3. Finally find the **ultimate load** in terms of M_p .



2. Principle of virtual work

- Instead of **equilibrium condition**, the principle of **virtual work** can be used for alternative mechanism method
 1. Assume a **plastic mechanism**.
 2. Find **displacement relationships** from displacement diagram.
 3. By the principle of **virtual work** to find **ultimate load** in terms of M_p .
- If the **plastic moment** condition ($M \leq M_p$) everywhere is satisfied, the assumed mechanism is **CORRECT** and the load is the **true ultimate load**.



2. Principle of virtual work (Continued)

- However, if $M > M_p$ occurs at locations other than the assumed **plastic hinges**, the load is **higher** than the **true load**. This is the **Upper Bound Theorem**
- Upper bound theorem
A load, computed on the basis of an assumed **plastic mechanism**, is at best **equal** to or **greater** than the **true plastic limit load**.
- Lower bound theorem
A load, computed on the basis of a **bending moment distribution** in which no moment **exceeds** M_p , is at best equal to or less than the **true plastic limit load**.



- We have **investigated** the **Ultimate Loads on Beams**.
- Now we are able to:
 - Discuss three condition which must be satisfied in **plastic analysis**.
 - Apply the **mechanism method** or the **principle of virtual work** to calculate **ultimate load on a beam**.
 - Be aware of **upper bound theorem** and **lower bound theorem**.
- Details can be referred to **topics 2** in the lecture notes.



[Theory of Plates and Grillages]

[Part I] Plastic Design of Structures

- Plastic theory of bending (Topic 1)
- Ultimate loads on beams (Topic 2)
- Collapse of frames and grillage structures (Topic 3)

[Part II] Elastic Plate Theory

- Basic (Topic 4)
- Simply supported plates under Sinusoidal Loading (Topic 5)
- Long clamped plates (Topic 6)
- Short Clamped plates (Topic 7)
- Additional (Low aspect ratio plates, strength & permanent set)

[Part III] Buckling of Stiffened Panels

- Failure modes (Topic 8)
- Tripping (Topic 9)
- Post-buckling behaviour (Topic 10)





Kam Sa Hab Ni Da

감사합니다

Thank you!

Questions?

Aerial View of Korean Presidential Archives in Sejong city
(Construction Completed in 2014)

