

# Ch. 10 Vector Integral Calculus. Integral Theorems

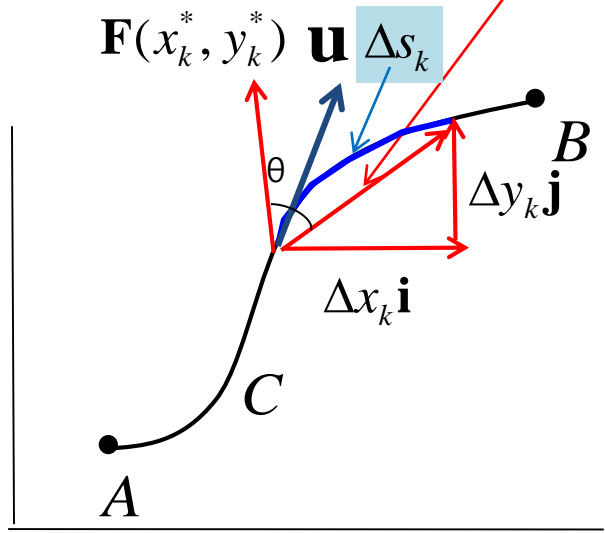
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# Introduction

## Work Done Equals the Gain in Kinetic Energy (운동에너지)

$$\Delta \mathbf{r}_k = \Delta x_k \mathbf{i} + \Delta y_k \mathbf{j}$$



If  $\Delta s_k$  is small,  $\mathbf{F}(x_k^*, y_k^*)$  is constant force, and  $\Delta s_k \approx \Delta r_k$

Approximate work done by  $\mathbf{F}$  over the subarc is

$$\begin{aligned} (\|\mathbf{F}(x_k^*, y_k^*)\| \cos \theta) \|\Delta \mathbf{r}_k\| &= \mathbf{F}(x_k^*, y_k^*) \cdot \Delta \mathbf{r}_k \\ &= F_1(x_k^*, y_k^*) \Delta x_k + F_2(x_k^*, y_k^*) \Delta y_k \end{aligned}$$

By summing the elements of work and passing to limit,

$$W = \int_C F_1(x, y) dx + F_2(x, y) dy \quad \text{or} \quad W = \int_C \mathbf{F} \cdot d\mathbf{r}$$

**The work done by a force  $F$  along a curve  $C$  is due entirely to the tangential component of  $F$**

# 10.1 Line Integrals

## ☑ Concept of a line integral (선적분)

: A simple and natural generalization of a definite integral known from calculus

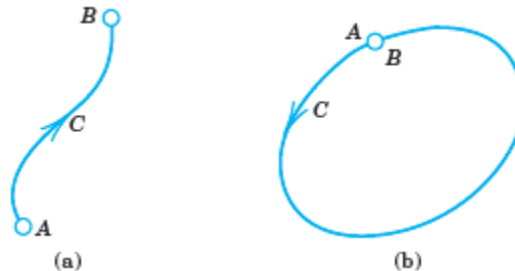
- Line Integral (선적분) or Curve Integral (곡선적분): We integrate a given function (Integrand, 피적분함수) along a curve  $C$  in space (or in the plane).

- Path of Integration

$$C : \mathbf{r}(t) = [ x(t) , y(t) , z(t) ] = x(t)\mathbf{i} + y(t)\mathbf{j} + z(t)\mathbf{k} \quad ( a < t < b )$$

- General Assumption

: Every path of integration of a line integral is assumed to be piecewise smooth.



**Oriented Curve**

# 10.1 Line Integrals

## ☑ Definition and Evaluation of Line Integrals

- A line integral of  $\mathbf{F}(\mathbf{r})$  over a curve  $C$  (= work integral)

$$\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt \quad \mathbf{r}' = \frac{d\mathbf{r}}{dt}$$

$$\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_C (F_1 dx + F_2 dy + F_3 dz) = \int_a^b (F_1 x' + F_2 y' + F_3 z') dt$$

- The interval  $a \leq t \leq b$  on  $t$ -axis: the positive direction, the increasing  $t$

# 10.1 Line Integrals

$$\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$$

## ☑ Example 1 Evaluation of a Line Integral in the Plane

- Find the value of the line integral when  $\mathbf{F}(\mathbf{r}) = [-y, -xy] = -y\mathbf{i} - xy\mathbf{j}$  along  $C$ .  $C : \mathbf{r}(t) = [\cos t, \sin t] = \cos t \mathbf{i} + \sin t \mathbf{j}$ , where  $0 \leq t \leq \pi/2$ .
- $x(t) = \cos t, y(t) = \sin t$ ,

**Sol)**  $\mathbf{F}(\mathbf{r}(t)) = -y(t)\mathbf{i} - x(t)y(t)\mathbf{j} = -\sin t \mathbf{i} - \cos t \sin t \mathbf{j}$

- By differentiation

$$\Rightarrow \int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_0^{\pi/2} [-\sin t, -\cos t \sin t] \cdot [-\sin t, \cos t] dt$$

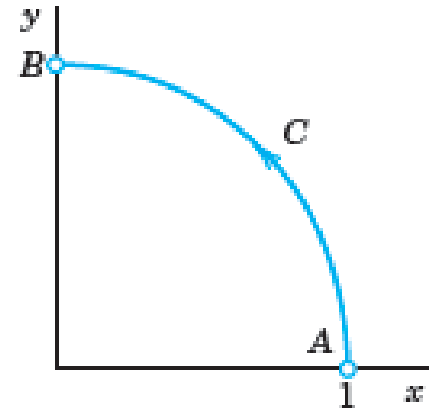
$$\mathbf{r}'(t) = [-\sin t, \cos t] = -\sin t \mathbf{i} + \cos t \mathbf{j}$$

$$= \int_0^{\pi/2} (\sin^2 t - \cos^2 t \sin t) dt$$

$$\sin^2 t = \frac{1}{2}(1 - \cos 2t)$$

$$\text{set } \cos t = u, \quad -\sin t = du$$

$$= \int_0^{\pi/2} \frac{1}{2}(1 - \cos 2t) dt - \int_1^0 u^2 (-du) = \frac{\pi}{4} - 0 - \frac{1}{3} \approx 0.4521$$



Example 1

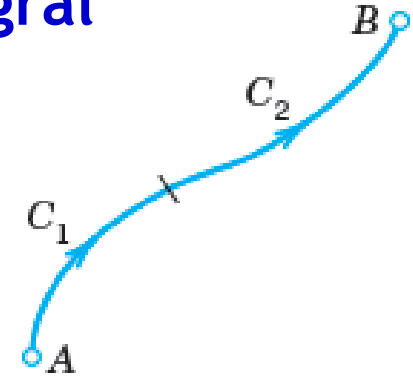
# 10.1 Line Integrals

## ☑ Simple general properties of the line integral

$$(5a) \quad \int_C k\mathbf{F} \cdot d\mathbf{r} = k \int_C \mathbf{F} \cdot d\mathbf{r} \quad (k \text{ constant})$$

$$(5b) \quad \int_C (\mathbf{F} + \mathbf{G}) \cdot d\mathbf{r} = \int_C \mathbf{F} \cdot d\mathbf{r} + \int_C \mathbf{G} \cdot d\mathbf{r}$$

$$(5c) \quad \int_C \mathbf{F} \cdot d\mathbf{r} = \int_{C_1} \mathbf{F} \cdot d\mathbf{r} + \int_{C_2} \mathbf{F} \cdot d\mathbf{r}$$



Formula (5c)

## ☑ Theorem 1 Direction-Preserving Parametric Transformations (방향을 유지하는 매개변수 변환)

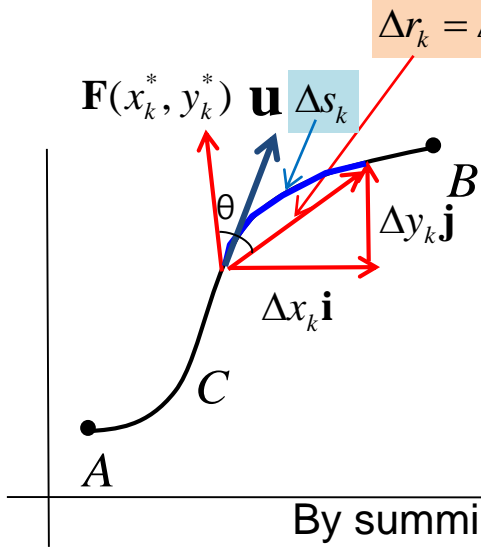
- Any representations of  $C$  that give the same positive direction on  $C$  also yield the same value of the line integral

$$\text{ex) } \mathbf{r}(t) = [2t^2, t^4], 1 \leq t \leq 3 \Rightarrow t^* = t^2, \mathbf{r}(t^*) = [2t^*, t^{*2}], 1 \leq t^* \leq 9$$

$$\Rightarrow \int_C \mathbf{F}(\mathbf{r}^*) \cdot d\mathbf{r}^* = \int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r}$$

# 10.1 Line Integrals

## ☑ Work Done Equals the Gain in Kinetic Energy



$$\Delta \mathbf{r}_k = \Delta x_k \mathbf{i} + \Delta y_k \mathbf{j}$$

If  $\Delta s_k$  is small,  $\mathbf{F}(x_k^*, y_k^*)$  is constant force, and  $\Delta s_k \approx \Delta r_k$

Approximate work done by  $\mathbf{F}$  over the subarc is

$$\begin{aligned} (\|\mathbf{F}(x_k^*, y_k^*)\| \cos \theta) \|\Delta \mathbf{r}_k\| &= \mathbf{F}(x_k^*, y_k^*) \cdot \Delta \mathbf{r}_k \\ &= F_1(x_k^*, y_k^*) \Delta x_k + F_2(x_k^*, y_k^*) \Delta y_k \end{aligned}$$

By summing the elements of work and passing to limit,

$$W = \int_C F_1(x, y) dx + F_2(x, y) dy \quad \text{or} \quad W = \int_C \mathbf{F} \cdot d\mathbf{r}$$

$$\frac{d\mathbf{r}}{dt} = \frac{d\mathbf{r}}{ds} \frac{ds}{dt} = \mathbf{u}(s) \frac{ds}{dt} \quad d\mathbf{r} = \mathbf{u} ds$$

$$W = \int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_C \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}' dt = \int_C \mathbf{F}(\mathbf{r}) \cdot \mathbf{u} ds \quad \mathbf{u} = \frac{d\mathbf{r}}{ds}, \quad \mathbf{r}' = \frac{d\mathbf{r}}{dt}$$

The work done by a force  $\mathbf{F}$  along a curve  $C$  is due entirely to the tangential component of  $\mathbf{F}$

# 10.1 Line Integrals

## ☑ Ex.4 Work Done Equals the Gain in Kinetic Energy

Let  $F$  be a force and  $t$  be time, then  $d\mathbf{r}/dt = \mathbf{v}$ , velocity.

By Newton's second law,

$$W = \int_C \mathbf{F} \cdot d\mathbf{r} = \int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{v}(t) dt$$

$$\mathbf{F} = m\mathbf{r}''(t) = m\mathbf{v}'(t)$$

$$\Rightarrow W = \int_a^b \mathbf{F} \cdot \mathbf{r}' dt = \int_a^b m\mathbf{v}'(t) \cdot \mathbf{v}(t) dt$$

$$= \int_a^b m \left( \frac{\mathbf{v} \cdot \mathbf{v}}{2} \right)' dt = \frac{m}{2} |\mathbf{v}|^2 \Big|_{t=a}^{t=b}$$

$$\boxed{(\mathbf{u} \cdot \mathbf{v})' = \mathbf{u}' \cdot \mathbf{v} + \mathbf{u} \cdot \mathbf{v}'}$$



$$W = \int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_C \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$$

# 10.1 Line Integrals

## Example

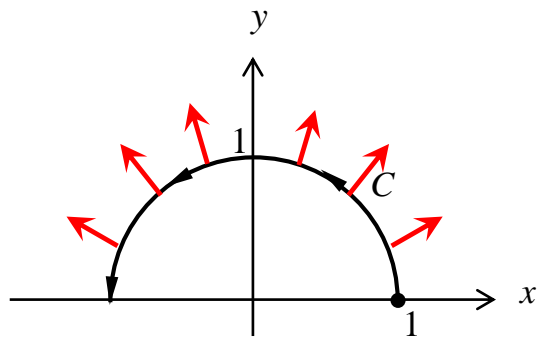
Find the work done by

(a)  $\mathbf{F} = x\mathbf{i} + y\mathbf{j}$  and

(b)  $\mathbf{F} = \frac{3}{4}\mathbf{i} + \frac{1}{2}\mathbf{j}$  along the curve  $C$  traced by  $\mathbf{r}(t) = \cos t \mathbf{i} + \sin t \mathbf{j}$  from  $t=0$  to  $t=\pi$ .

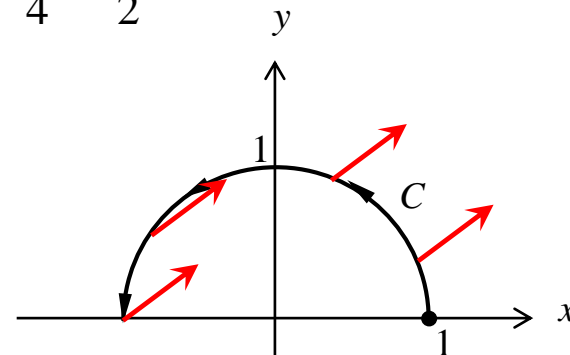
Solution)

(a)  $\mathbf{F} = x\mathbf{i} + y\mathbf{j}$



$$\begin{aligned} W &= \int_C \mathbf{F} \cdot d\mathbf{r} = \int_C (x\mathbf{i} + y\mathbf{j}) \cdot d\mathbf{r} \\ &= \int_0^\pi (\cos t \mathbf{i} + \sin t \mathbf{j}) \cdot (-\sin t \mathbf{i} + \cos t \mathbf{j}) dt \\ &= \int_0^\pi (-\cos t \sin t + \sin t \cos t) dt = 0 \end{aligned}$$

(b)  $\mathbf{F} = \frac{3}{4}\mathbf{i} + \frac{1}{2}\mathbf{j}$



$$\begin{aligned} W &= \int_C \mathbf{F} \cdot d\mathbf{r} = \int_C \left( \frac{3}{4}\mathbf{i} + \frac{1}{2}\mathbf{j} \right) \cdot d\mathbf{r} \\ &= \int_0^\pi \left( \frac{3}{4}\mathbf{i} + \frac{1}{2}\mathbf{j} \right) \cdot (-\sin t \mathbf{i} + \cos t \mathbf{j}) dt \\ &= \int_0^\pi \left( -\frac{3}{4}\sin t + \frac{1}{2}\cos t \right) dt \\ &= \left[ \frac{3}{4}\cos t + \frac{1}{2}\sin t \right]_0^\pi = -\frac{3}{2} \end{aligned}$$

# 10.1 Line Integrals

$$\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$$

## ☑ Other Forms of Line Integrals:

- When  $\mathbf{F} = F_1\mathbf{i}$  or  $F_2\mathbf{j}$  or  $F_3\mathbf{k}$

$$\int_C F_1 dx, \int_C F_2 dy, \int_C F_3 dz$$

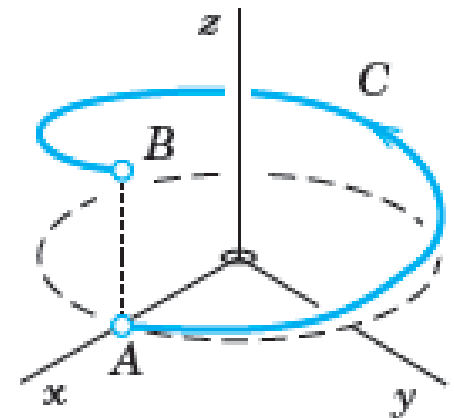
- When without taking a dot product, we can obtain a line integral whose value is a vector rather than a scalar

$$\int_C \mathbf{F}(\mathbf{r}) dt = \int_a^b \mathbf{F}(\mathbf{r}(t)) dt = \int_a^b [F_1(\mathbf{r}(t)), F_2(\mathbf{r}(t)), F_3(\mathbf{r}(t))] dt$$

## ☑ Ex.5 Integrate $\mathbf{F}(\mathbf{r}) = [xy, yz, z]$ along the helix.

$$\mathbf{r}(t) = [\cos t, \sin t, 3t] = \cos t \mathbf{i} + \sin t \mathbf{j} + 3t \mathbf{k}$$

$$\begin{aligned} \int_0^{2\pi} \mathbf{F}(\mathbf{r}(t)) dt &= \left[ -\frac{1}{2} \cos^2 t, 3 \sin t - 3t \cos t, \frac{3}{2} t^2 \right] \Bigg|_0^{2\pi} \\ &= [0, -6\pi, 6\pi^2] \end{aligned}$$



# 10.1 Line Integrals

## ☑ Theorem 2 Path Dependence (경로 관련성)

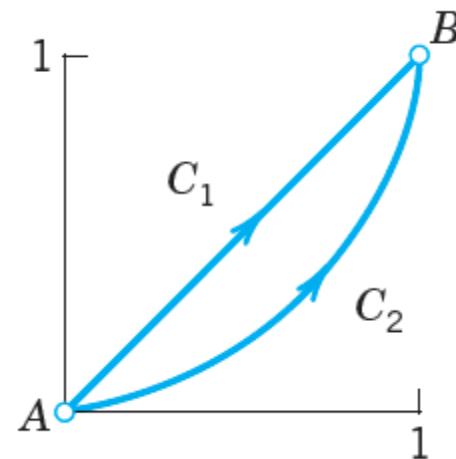
- The line integral generally depends not only on  $F$  and on the endpoints  $A$  and  $B$  of the path, but also on the path itself which the integral is taken.

- ☑ **Ex.** Integrate  $\mathbf{F} = [0, xy, 0]$  on the straight segment  $C_1 : \mathbf{r}_1(t) = [t, t, 0]$  and the parabola  $C_2 : \mathbf{r}_2(t) = [t, t^2, 0]$  with  $0 \leq t \leq 1$ , respectively.

Sol)

$$\mathbf{F}(\mathbf{r}_1(t)) \cdot \mathbf{r}'_1(t) = t^2 \quad \Rightarrow \quad \int_{C_1} \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r}_1 = \frac{1}{3}$$

$$\mathbf{F}(\mathbf{r}_2(t)) \cdot \mathbf{r}'_2(t) = 2t^4 \quad \Rightarrow \quad \int_{C_2} \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r}_2 = \frac{2}{5}$$



Proof of Theorem 2

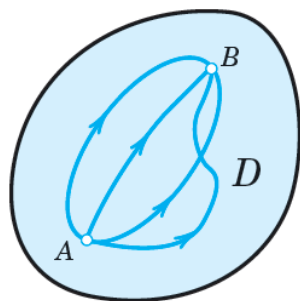
# 10.2 Path Independence of Line Integrals

## ☑ Theorem 1 Path Independence (경로 독립성, 경로 무관성)

- A line integral with continuous  $F_1, F_2, F_3$  in a domain  $D$  in space is path independent in  $D$  if and only if  $\mathbf{F} = [F_1, F_2, F_3]$  is the gradient of some function  $f$  in  $D$  ( $\mathbf{F}$  is gradient field),

$$\mathbf{F} = \text{grad } f \quad \left( F_1 = \frac{\partial f}{\partial x}, F_2 = \frac{\partial f}{\partial y}, F_3 = \frac{\partial f}{\partial z} \right) \Rightarrow \int_A^B (F_1 dx + F_2 dy + F_3 dz) = f(B) - f(A)$$

✓ Proof



$$\therefore \int_C (F_1 dx + F_2 dy + F_3 dz) = f(B) - f(A)$$

A line integral is independent of path.

$$\int_C (F_1 dx + F_2 dy + F_3 dz) = \int_C \left( \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy + \frac{\partial f}{\partial z} dz \right)$$

$$= \int_a^b \left( \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt} + \frac{\partial f}{\partial z} \frac{dz}{dt} \right) dt$$

$$= \int_a^b \frac{df}{dt} dt = f[x(t), y(t), z(t)] \Big|_{t=a}^{t=b}$$

$$= f(x(b), y(b), z(b)) - f(x(a), y(a), z(a))$$

$$= f(B) - f(A)$$

# 10.2 Path Independence of Line Integrals

## ☑ Ex.1 Path Independence

Show that the integral  $\int_C (2x dx + 2y dy + 4z dz)$  is path independent in any domain in space and find its value in the integration from A : (0, 0, 0) to B : (2, 2, 2).

Sol)  $\mathbf{F} = [2x, 2y, 4z] = \text{grad } f$

$$\Rightarrow \frac{\partial f}{\partial x} = 2x = F_1, \quad \frac{\partial f}{\partial y} = 2y = F_2, \quad \frac{\partial f}{\partial z} = 4z = F_3$$

$$\Rightarrow f = x^2 + y^2 + 2z^2$$

Hence the integral is independent of path according to Theorem 1.

$$\int_C (2x dx + 2y dy + 4z dz) = f(B) - f(A) = f(2, 2, 2) - f(0, 0, 0) = 4 + 4 + 8 = 16$$

# 10.2 Path Independence of Line Integrals

## ✓ Theorem 2 Path Independence

- The integral is path independent in a domain  $D$  if and only if its value around every closed path in  $D$  is zero.

**Proof 1)** path independence  $\rightarrow$  integral is zero

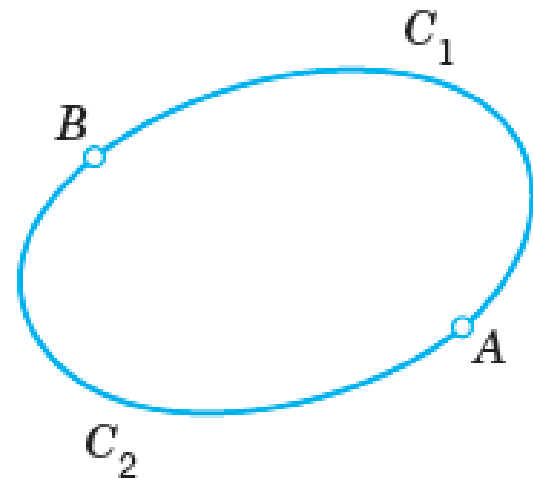
$$\int_{C_1} \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_{C_2} \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} \quad C_1 : A \rightarrow B, C_2 : B \rightarrow A$$

$$\int_A^B \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r} = \int_A^B \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r} \quad \Rightarrow \quad \int_A^B \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r} - \int_A^B \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r} = 0$$

$$\Rightarrow \int_A^B \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r} + \int_B^A \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r} = 0$$

$$\Rightarrow \int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = 0$$

The integral around closed path is zero.



# 10.2 Path Independence of Line Integrals

## ✓ Theorem 2 Path Independence

- The integral is path independent in a domain  $D$  if and only if its value around every closed path in  $D$  is zero.

**Proof 2)** path independence  $\leftarrow$  integral is zero

for given any points  $A$  and  $B$  and any two curves  $C_1$  and  $C_2$  from  $A$  to  $B$

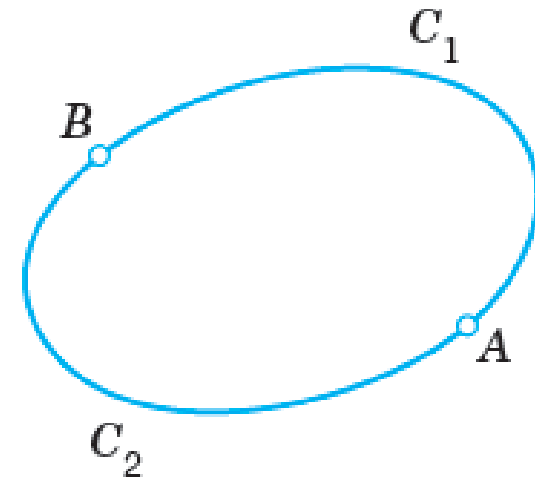
$$\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_{C_1} \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r}_1 + \int_{C_2} \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r}_2 = 0$$

$$C_1 : A \rightarrow B, \quad C_2 : B \rightarrow A$$

$$\int_A^B \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r}_1 + \int_B^A \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r}_2 = 0$$

Move 2<sup>nd</sup> term to the right.

$$\underline{\int_A^B \mathbf{F}(\mathbf{r}_1) \cdot d\mathbf{r}_1} = -\int_B^A \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r}_2 = \underline{\int_A^B \mathbf{F}(\mathbf{r}_2) \cdot d\mathbf{r}_2}$$



In conclusion, a line integral is path independent .

# 10.2 Path Independence of Line Integrals

## ☑ Work. Conservative and Nonconservative (Dissipative, 소산하는) Physical Systems

- **Theorem 2:** work is path independent in  $D$  if and only if its value is zero for displacement around every closed path in  $D$ .
- **Theorem 1:** this happens if and only if  $F$  is the gradient of a potential in  $D$ .

⇒  $F$  and the vector field defined by  $F$  are called **conservative** in  $D$  because mechanical energy is conserved

⇒ no work is done in the displacement from a point  $A$  and back to  $A$ .

- For instance, the gravitational force is conservative;
- ✓ if we throw a ball vertically up, it will return to our hand with the same kinetic energy it had when it left our hand.
- ✓ If this does not hold, nonconservative or dissipative physical system.



# 10.2 Path Independence of Line Integrals

## ✓ Theorem 3\* Path Independence

- The integral is path independent in a domain  $D$  in space if and only if the differential form has continuous coefficient functions  $F_1, F_2, F_3$  and is exact in  $D$ .

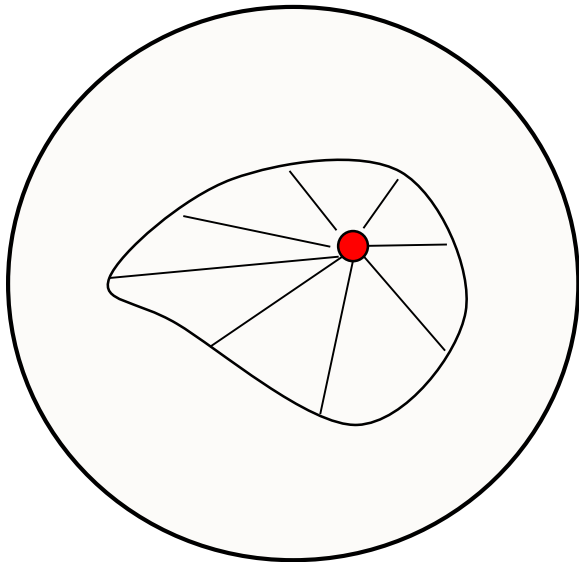
$\Rightarrow \mathbf{F} \cdot d\mathbf{r} = F_1 dx + F_2 dy + F_3 dz$  is exact if and only if there is  $f$  in  $D$  such that  $\mathbf{F} = \text{grad } f$ .

# 10.2 Path Independence of Line Integrals

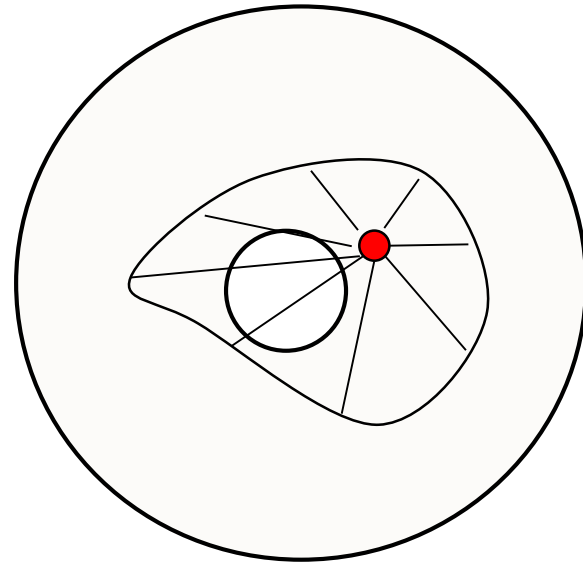
- Simple connected (단순 연결됨)

A domain  $D$  is called **simply connected** if every closed curve in  $D$  can be continuously shrunk to any point in  $D$  without leaving  $D$ .

it can shrink to a point in  $D$   
continuously



it can't shrink to a point in  $D$   
continuously



# 10.2 Path Independence of Line Integrals

## ☑ Theorem 3 Criterion for Exactness (완전성) and Path Independence (경로 독립성)

- Let  $F_1, F_2, F_3$  in the line integral,  $\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_C (F_1 dx + F_2 dy + F_3 dz)$  be continuous and have continuous first partial derivatives in a domain  $D$  in space.

a. If the differential form  $\mathbf{F} \cdot d\mathbf{r} = F_1 dx + F_2 dy + F_3 dz$  is exact in  $D$

- and thus line integral is path independent (from Theorem 3\*), -

then in  $D$ ,  $\text{curl } \mathbf{F} = \mathbf{0}$ ; in components  $\frac{\partial F_3}{\partial y} = \frac{\partial F_2}{\partial z}, \frac{\partial F_1}{\partial z} = \frac{\partial F_3}{\partial x}, \frac{\partial F_2}{\partial x} = \frac{\partial F_1}{\partial y}$ .

$$\left( \text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ F_1 & F_2 & F_3 \end{vmatrix} = \left[ \frac{\partial F_3}{\partial y} - \frac{\partial F_2}{\partial z}, \frac{\partial F_1}{\partial z} - \frac{\partial F_3}{\partial x}, \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right] \right)$$

**Proof a)** From Theorem 3\*,  $\mathbf{F} = \text{grad } f \Rightarrow \text{curl } \mathbf{F} = \text{curl } (\text{grad } f) = \mathbf{0}$

# 10.2 Path Independence of Line Integrals

## ☑ Theorem 3 Criterion for Exactness and Path Independence

- b. If  $\text{curl } \mathbf{F} = \mathbf{0}$  holds in  $D$  and  $D$  is simply connected, then  $\mathbf{F} \cdot d\mathbf{r} = F_1 dx + F_2 dy + F_3 dz$  is exact in  $D$  and thus line integral is path independent.

### Proof b)

To prove this, we need "Stokes's theorem" that will be presented later.

# [Review] 1.4 Exact ODEs, Integrating Factors

## ❖ Exact Differential Equation (완전미분 방정식):

The ODE  $M(x, y)dx + N(x, y)dy = 0$  whose the differential form  $M(x, y)dx + N(x, y)dy$  is **exact** (완전미분), that is, this form is the differential  $du = \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy$  of  $u(x, y)$

- If ODE is an exact differential equation, then

$$M(x, y)dx + N(x, y)dy = 0 \quad \Rightarrow \quad du = 0 \quad \Rightarrow \quad u(x, y) = c$$

❖ Condition for exactness:  $\frac{\partial M}{\partial y} = \frac{\partial N}{\partial x}$   $\left( \because \frac{\partial M}{\partial y} = \frac{\partial}{\partial y} \left( \frac{\partial u}{\partial x} \right) = \frac{\partial^2 u}{\partial x \partial y} = \frac{\partial}{\partial x} \left( \frac{\partial u}{\partial y} \right) = \frac{\partial N}{\partial x} \right)$

- ❖ Solve the exact differential equation.

$$M(x, y) = \frac{\partial u}{\partial x} \quad \Rightarrow \quad u(x, y) = \int M(x, y) dx + k(y) \quad \Rightarrow \quad \frac{\partial u}{\partial y} = N(x, y) \quad \Rightarrow \quad \frac{dk}{dy} \quad \& \quad k(y)$$

$$N(x, y) = \frac{\partial u}{\partial y} \quad \Rightarrow \quad u(x, y) = \int N(x, y) dy + l(x) \quad \Rightarrow \quad \frac{\partial u}{\partial x} = M(x, y) \quad \Rightarrow \quad \frac{dl}{dx} \quad \& \quad l(x)$$

# 10.2 Path Independence of Line Integrals

## ☑ Ex.3 Exactness and Independence of Path. Determination of a Potential

Show that the differential form under the integral sign of

$$I = \int_C \left[ 2xyz^2 dx + (x^2 z^2 + z \cos yz) dy + (2x^2 yz + y \cos yz) dz \right]$$

is exact, so that we have independence of path in any domain, and find the value of  $I$  from A:  $(0, 0, 1)$  to B:  $(1, \pi/4, 2)$ .

Solution)

$$\text{Exactness: } (F_3)_y = 2x^2 z + \cos yz - yz \sin yz = (F_2)_z,$$

$$(F_1)_z = 4xyz = (F_3)_x,$$

$$(F_2)_x = 2xz^2 = (F_1)_y$$

$$\frac{\partial F_3}{\partial y} = \frac{\partial F_2}{\partial z}, \quad \frac{\partial F_1}{\partial z} = \frac{\partial F_3}{\partial x}, \quad \frac{\partial F_2}{\partial x} = \frac{\partial F_1}{\partial y}$$

# 10.2 Path Independence of Line Integrals

## ☑ Ex.3 Exactness and Independence of Path. Determination of a Potential

Show that the differential form under the integral sign of

$$I = \int_C \left[ 2xyz^2 dx + (x^2 z^2 + z \cos yz) dy + (2x^2 yz + y \cos yz) dz \right]$$

A: (0, 0, 1) to B: (1,  $\pi/4$ , 2)

To find  $f$      $\mathbf{F} = \text{grad } f$      $\left( F_1 = \frac{\partial f}{\partial x}, F_2 = \frac{\partial f}{\partial y}, F_3 = \frac{\partial f}{\partial z} \right)$

$$f = \int F_2 dy = \int (x^2 z^2 + z \cos yz) dy = x^2 yz^2 + \sin yz + g(x, z)$$

$$f_x = 2xyz^2 + g_x = F_1 = 2xyz^2 \quad \Rightarrow \quad g_x = 0 \quad \Rightarrow \quad g = h(z)$$

$$f_z = 2x^2 yz + y \cos yz + h' = F_3 = 2x^2 yz + y \cos yz \quad \Rightarrow \quad h' = 0 \quad \Rightarrow \quad h = \text{const}$$

(If we assume  $h = 0$ )

$$\therefore f = x^2 yz^2 + \sin yz, \quad f(B) - f(A) = 1 \cdot \frac{\pi}{4} \cdot 4 + \sin \frac{\pi}{2} - 0 = \pi + 1$$

# 10.2 Path Independence of Line Integrals

## ✓ Example

Show that the vector field

$\mathbf{F} = (y^2 + 5)\mathbf{i} + (2xy - 8)\mathbf{j}$  is a **gradient field**.

Find a potential function for  $\mathbf{F}$

( $\mathbf{F} = \text{grad } \phi$ ).

Solution)

$$\begin{aligned}\mathbf{F} &= (y^2 + 5)\mathbf{i} + (2xy - 8)\mathbf{j} \\ &= P(x, y)\mathbf{i} + Q(x, y)\mathbf{j}\end{aligned}$$

$$\frac{\partial P}{\partial y} = 2y, \quad \frac{\partial Q}{\partial x} = 2y$$

$$\frac{\partial P}{\partial y} = \frac{\partial Q}{\partial x} \quad (\text{exact})$$

∴ Vector field  $\mathbf{F}$  is a gradient field.

$$P = \frac{\partial \phi}{\partial x} = y^2 + 5$$

$$Q = \frac{\partial \phi}{\partial y} = 2xy - 8$$

$$\phi = \int (y^2 + 5)dx = y^2x + 5x + g(y)$$

$$\frac{\partial \phi}{\partial y} = 2xy + g'(y)$$

$$\therefore g'(y) = -8, \quad g(y) = -8y + C$$

$$\phi = y^2x + 5x - 8y + C$$

$$\nabla \phi = \frac{\partial \phi}{\partial x}\mathbf{i} + \frac{\partial \phi}{\partial y}\mathbf{j} = (y^2 + 5)\mathbf{i} + (2xy - 8)\mathbf{j}$$



# 10.2 Path Independence of Line Integrals

## ☑ Ex.4 On the Assumption of Simple Connectedness

Let  $F_1 = -\frac{y}{x^2 + y^2}$ ,  $F_2 = \frac{x}{x^2 + y^2}$ ,  $F_3 = 0$  (not defined in the origin).

Differentiation show that  $\frac{\partial F_3}{\partial y} = \frac{\partial F_2}{\partial z}$ ,  $\frac{\partial F_1}{\partial z} = \frac{\partial F_3}{\partial x}$ ,  $\frac{\partial F_2}{\partial x} = \frac{\partial F_1}{\partial y}$  is satisfied in any domain of the  $xy$ -plane not containing the origin in the domain D:

$$\frac{1}{2} < \sqrt{x^2 + y^2} < \frac{3}{2}$$

Solution)

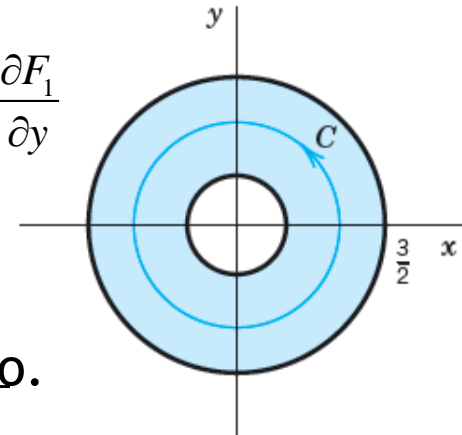
1)  $F_1$  and  $F_2$  do not depend on  $z$ , and  $F_3 = 0 \Rightarrow \frac{\partial F_3}{\partial y} = \frac{\partial F_2}{\partial z}$ ,  $\frac{\partial F_1}{\partial z} = \frac{\partial F_3}{\partial x}$

By differentiation:

$$\frac{\partial F_2}{\partial x} = \frac{x^2 + y^2 - x \cdot 2x}{(x^2 + y^2)^2} = \frac{y^2 - x^2}{(x^2 + y^2)^2} = -\frac{x^2 + y^2 - y \cdot 2y}{(x^2 + y^2)^2} = \frac{y^2 - x^2}{(x^2 + y^2)^2} = \frac{\partial F_1}{\partial y}$$

2) D is not simply connected

$\Rightarrow$  the integral on any closed curve in D is not zero.



# 10.2 Path Independence of Line Integrals

## ☑ Ex.4 On the Assumption of Simple Connectedness

$$\text{Let } F_1 = -\frac{y}{x^2 + y^2}, \quad F_2 = \frac{x}{x^2 + y^2}, \quad F_3 = 0$$

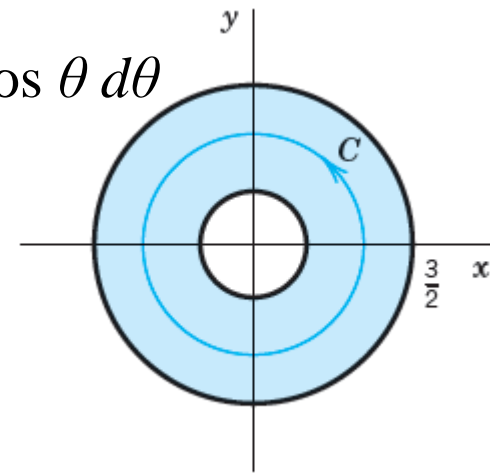
3) For example, on the circle  $x^2 + y^2 = 1$ ,

$$x = r \cos \theta, \quad y = r \sin \theta, \quad r = 1 \Rightarrow dx = -\sin \theta d\theta, \quad dy = \cos \theta d\theta$$

$$I = \int_c (F_1 dx + F_2 dy) = \int_c \frac{-y dx + x dy}{x^2 + y^2}$$

$$= \int_c \frac{\sin^2 \theta d\theta + \cos^2 \theta d\theta}{1} = \int_c \frac{d\theta}{1} = \int_0^{2\pi} \frac{d\theta}{1} = \boxed{2\pi}$$

≠ 0 (integral is not zero)



“Since  $D$  is not simply connected, we cannot apply Theorem 3 and  $I$  is not independent of path in  $D$ .”

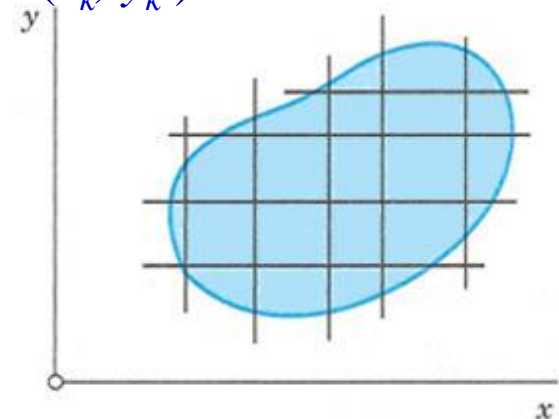
# 10.3 Calculus Review: Double Integrals

## ☑ Double integral (이중적분)

: Volume of the region between the surface defined by the function and the plane

## ☑ Definition of the double integral

- Subdivide the region  $R$  by drawing parallels to the  $x$ - and  $y$ -axes.
- Number the rectangles that are entirely within  $R$  from 1 to  $n$ .
- In each such rectangle we choose a point  $(x_k, y_k)$  in the  $k$ th rectangle, whose area is  $\Delta A_k$

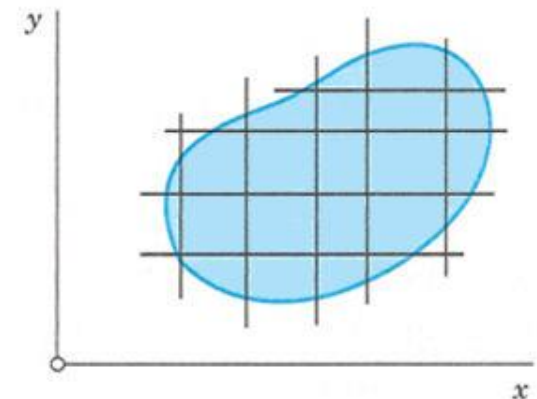


Subdivision of a region  $R$

# 10.3 Calculus Review: Double Integrals

- The length of the maximum diagonal of the rectangles approaches zero as  $n$  approaches infinity.
- We form the sum  $J_n = \sum_{k=1}^n f(x_k, y_k) \Delta A_k$
- Assuming that  $f(x, y)$  is continuous in  $R$  and  $R$  is bounded by finitely many smooth curves,
- one can show that this sequence  $J_{n_1}, J_{n_2}, \dots$  converges and its limit is independent of the choice of subdivisions and corresponding points  $(x_k, y_k)$ .
- This limit is called the **double integral of  $f(x, y)$  over the region  $R$** .

$$\iint_R f(x, y) dx dy \quad \text{or} \quad \iint_R f(x, y) dA$$



Subdivision of a region  $R$

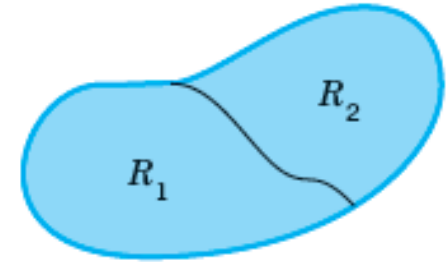
# 10.3 Calculus Review: Double Integrals

## ☑ Properties of double integrals

$$\iint_R kf \, dx dy = k \iint_R f \, dx dy \quad (k \text{ constant})$$

$$\iint_R (f + g) \, dx dy = \iint_R f \, dx dy + \iint_R g \, dx dy$$

$$\iint_R f \, dx dy = \iint_{R_1} f \, dx dy + \iint_{R_2} f \, dx dy \quad (\text{See Figure})$$



## ☑ Mean Value Theorem

- $R$  is simply connected, then there exists at least one point  $(x_0, y_0)$  in  $R$  such that we have

$$\iint_R f(x, y) \, dx dy = f(x_0, y_0) A$$

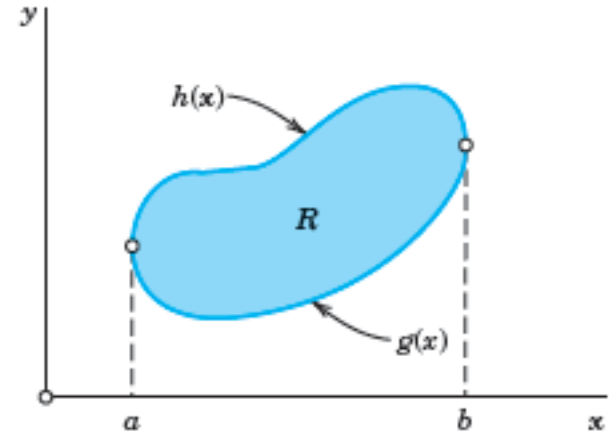
where  $A$  is the area of  $R$ .

# 10.3 Calculus Review: Double Integrals

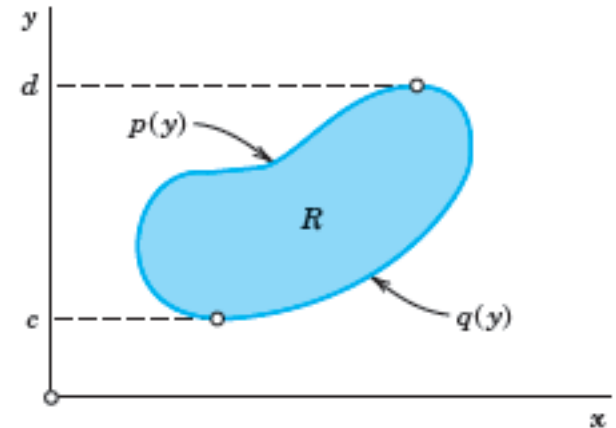
## ☑ Evaluation of Double Integrals by Two Successive Integrations

$$\iint_R f(x, y) dx dy = \int_a^b \left[ \int_{g(x)}^{h(x)} f(x, y) dy \right] dx$$

$$\iint_R f(x, y) dx dy = \int_c^d \left[ \int_{p(y)}^{q(y)} f(x, y) dx \right] dy$$



Evaluation of a double integral



Evaluation of a double integral

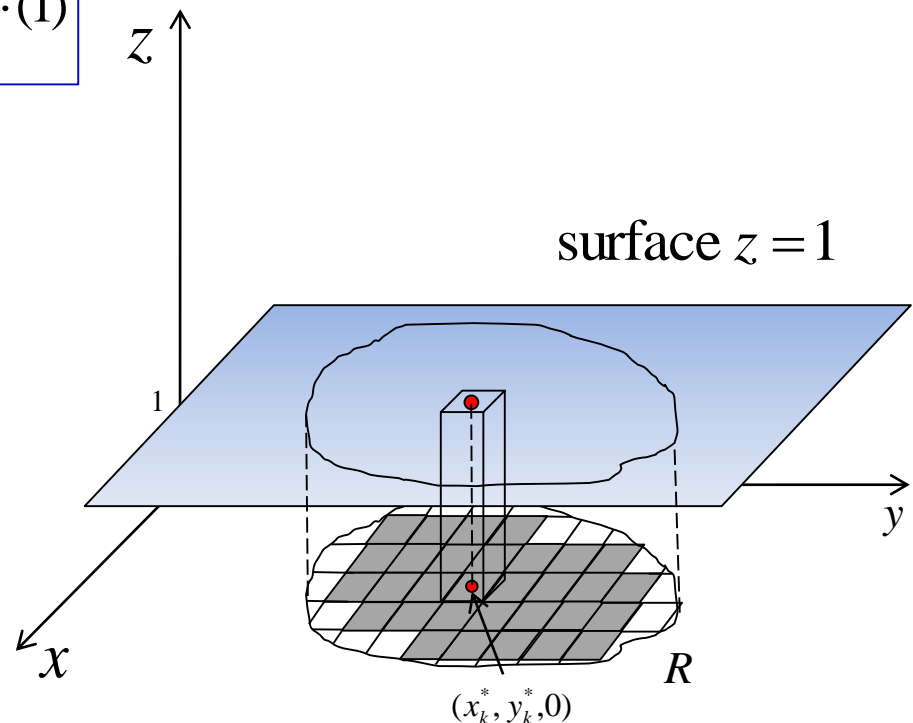
# 10.3 Calculus Review: Double Integrals

## ✓ Applications of Double Integrals: Area

when  $f(x, y) = 1$  on  $R$ , then  $\lim_{\|P\| \rightarrow 0} \sum_{k=1}^n \Delta A$  simply give the **area**  $A$  of the region

$$\iint_R f(x, y) dA = \lim_{\|P\| \rightarrow 0} \sum_{k=1}^n f(x_k^*, y_k^*) \Delta A_k \cdots (1)$$

$$A = \iint_R dA$$



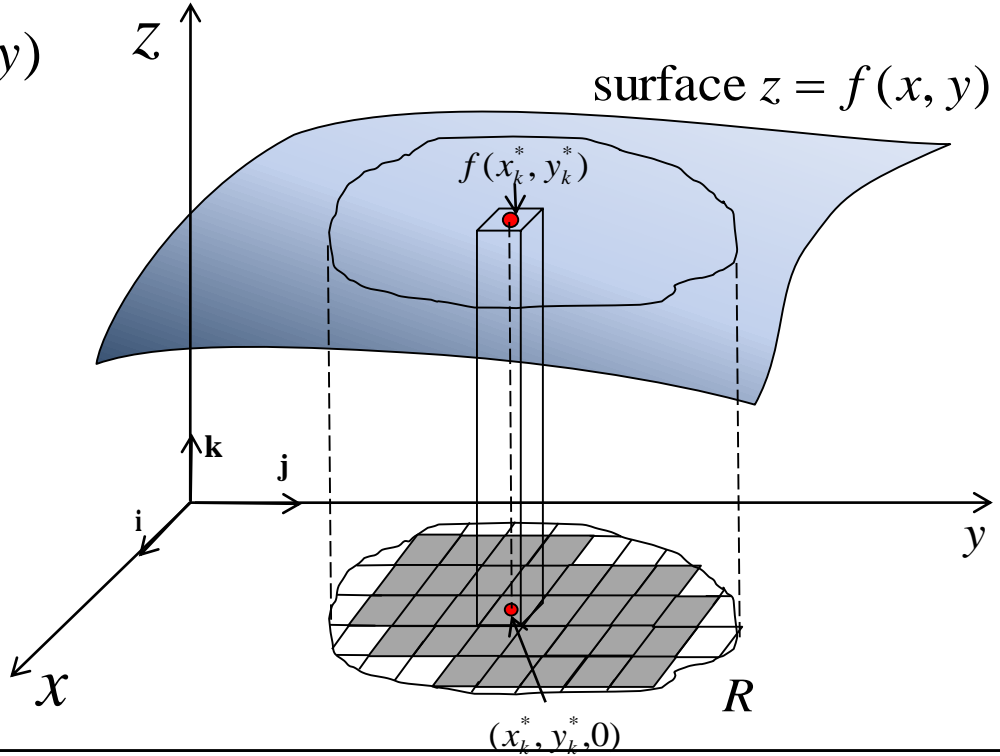
# 10.3 Calculus Review: Double Integrals

## ☑ Applications of Double Integrals: Volume

If  $f(x, y) > 0$  on  $R$ , then the product  $f(x_k^*, y_k^*)\Delta A_k$  give the volume of rectangular prism. The summation of volume  $\sum_{k=1}^n f(x_k^*, y_k^*)\Delta A_k$  is approximation to the **volume  $V$ , of the solid above the region  $R$  and below the surface  $z = f(x, y)$**

The limit of this sum as  $\|P\| \rightarrow 0$

$$V = \iint_R f(x, y) dA$$





# 10.3 Calculus Review: Double Integrals

## ☑ Applications of Double Integrals

- Let  $f(x, y)$  be the density (= mass per unit area) of a distribution of mass in  $xy$ -plane

- Total mass  $M$  in  $R$ : 
$$M = \iint_R f(x, y) dx dy$$

- Center of gravity of the mass in  $R$ :

$$\bar{x} = \frac{1}{M} \iint_R x f(x, y) dx dy, \quad \bar{y} = \frac{1}{M} \iint_R y f(x, y) dx dy$$

- Moments of inertia of the mass in  $R$  about the  $x$ - and  $y$ -axes

$$I_x = \iint_R y^2 f(x, y) dx dy, \quad I_y = \iint_R x^2 f(x, y) dx dy$$

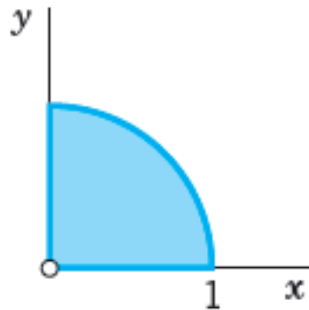
- Polar moment of inertia about the origin of mass in  $R$ :

$$I_0 = I_x + I_y = \iint_R (x^2 + y^2) f(x, y) dx dy$$

# 10.3 Calculus Review: Double Integrals

## ☑ Change of Variables in Double Integrals. Jacobian

$$M = \iint_R f(x, y) dx dy$$

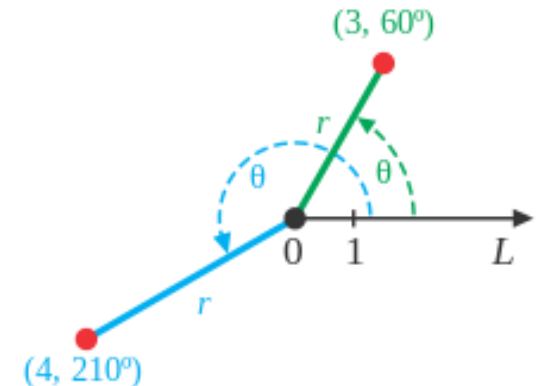


How to apply????

Polar coordinate (극좌표계)

Change of variables !!

$$M = \iint_R dx dy = \int_0^{\pi/2} \int_0^1 r dr d\theta = \int_0^{\pi/2} \frac{1}{2} d\theta = \frac{\pi}{4}$$



# 10.3 Calculus Review: Double Integrals

## ☑ Change of Variables in Double Integrals. Jacobian

- A change of variables in double integrals from  $x, y$  to  $u, v$

$$\iint_R f(x, y) dx dy = \iint_{R^*} f(x(u, v), y(u, v)) \left| \frac{\partial(x, y)}{\partial(u, v)} \right| du dv$$

- Jacobian: 
$$J = \frac{\partial(x, y)}{\partial(u, v)} = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial x}{\partial v} \\ \frac{\partial y}{\partial u} & \frac{\partial y}{\partial v} \end{vmatrix} = \frac{\partial x}{\partial u} \frac{\partial y}{\partial v} - \frac{\partial x}{\partial v} \frac{\partial y}{\partial u}$$

- Polar coordinates:  $x = r \cos \theta, y = r \sin \theta$

$$J = \frac{\partial(x, y)}{\partial(r, \theta)} = \begin{vmatrix} \frac{\partial x}{\partial r} & \frac{\partial x}{\partial \theta} \\ \frac{\partial y}{\partial r} & \frac{\partial y}{\partial \theta} \end{vmatrix} = \begin{vmatrix} \cos \theta & -r \sin \theta \\ \sin \theta & r \cos \theta \end{vmatrix} = r$$

$$\iint_R f(x, y) dx dy = \iint_{R^*} f(r \cos \theta, r \sin \theta) r dr d\theta$$

# 10.3 Calculus Review: Double Integrals

☑ **Ex. 1 Evaluate the double integral over the square  $R$**

$$\iint_R (x^2 + y^2) dx dy$$

$$J = \frac{\partial(x, y)}{\partial(u, v)} = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial x}{\partial v} \\ \frac{\partial y}{\partial u} & \frac{\partial y}{\partial v} \end{vmatrix}$$

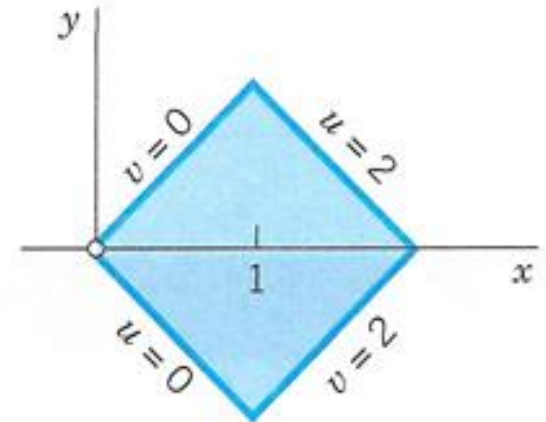
**Sol)** Transformation  $x + y = u, x - y = v$   $\left( x = \frac{1}{2}(u+v), y = \frac{1}{2}(u-v) \right)$

**Q : solve it**

$$J = \frac{\partial(x, y)}{\partial(u, v)} = \begin{vmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} & -\frac{1}{2} \end{vmatrix} = -\frac{1}{2}$$

$$\iint_R f(x, y) dx dy = \iint_{R^*} f(x(u, v), y(u, v)) \left| \frac{\partial(x, y)}{\partial(u, v)} \right| du dv$$

$$\Rightarrow \therefore \iint_R (x^2 + y^2) dx dy = \int_0^2 \int_0^2 \frac{1}{2} (u^2 + v^2) \frac{1}{2} du dv = \frac{8}{3}$$



**Region  $R$  in Example 1**

# 10.3 Calculus Review: Double Integrals

## ☑ Ex.2 Double Integrals in Polar Coordinates.

- Let  $f(x, y) = 1$  be the mass density in the region, Find the total mass, the center of gravity, and the moments of inertia  $I_x$ ,  $I_y$ ,  $I_0$ .

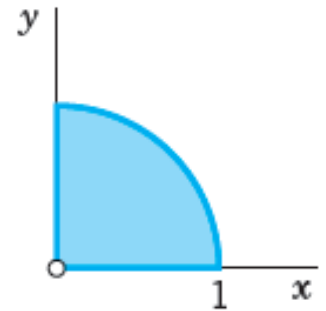
Sol)

$$J = \frac{\partial(x, y)}{\partial(r, \theta)} = \begin{vmatrix} \cos \theta & -r \sin \theta \\ \sin \theta & r \cos \theta \end{vmatrix} = r, \quad \iint_R f(x, y) dx dy = \iint_{R^*} f(r \cos \theta, r \sin \theta) r dr d\theta$$

$$M = \iint_R dx dy = \int_0^{\pi/2} \int_0^1 r dr d\theta = \int_0^{\pi/2} \frac{1}{2} d\theta = \frac{\pi}{4}$$

$$\bar{x} = \frac{4}{\pi} \int_0^{\pi/2} \int_0^1 r \cos \theta r dr d\theta = \frac{4}{\pi} \int_0^{\pi/2} \frac{1}{3} \cos \theta d\theta = \frac{4}{3\pi} = 0.4244$$

$$\bar{y} = \frac{4}{3\pi}$$



$$\bar{x} = \frac{1}{M} \iint_R x f(x, y) dx dy, \quad \bar{y} = \frac{1}{M} \iint_R y f(x, y) dx dy$$

# 10.3 Calculus Review: Double Integrals

## ☑ Ex.2 Double Integrals in Polar Coordinates.

- Let  $f(x, y) = 1$  be the mass density in the region, Find the total mass, the center of gravity, and the moments of inertia  $I_x$ ,  $I_y$ ,  $I_0$ .

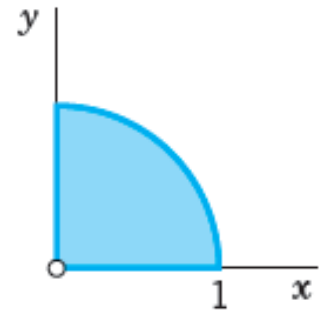
Sol)

$$I_x = \int_R \int y^2 dx dy \frac{4}{\pi} = \int_0^{\pi/2} \int_0^1 r^2 \sin^2 \theta r dr d\theta = \int_0^{\pi/2} \frac{1}{4} \sin^2 \theta d\theta$$

$$= \int_0^{\pi/2} \frac{1}{8} (1 - \cos 2\theta) d\theta = \frac{1}{8} \left( \frac{\pi}{2} - 0 \right) = \frac{\pi}{16} = 0.1963$$

$$I_y = \frac{\pi}{16}$$

$$I_0 = I_x + I_y = \frac{\pi}{8}$$



$$I_x = \iint_R y^2 f(x, y) dx dy, \quad I_y = \iint_R x^2 f(x, y) dx dy$$

# 10.4 Green's Theorem in the Plane

## ✓ Theorem 1 Green's Theorem in the Plane

- Let  $R$  be a closed bounded region in the  $xy$ -plane whose boundary  $C$  consists of finitely many smooth curves.
- Let  $F_1(x,y)$  and  $F_2(x,y)$  be functions that are continuous and have continuous partial derivatives  $\frac{\partial F_1}{\partial y}$  and  $\frac{\partial F_2}{\partial x}$  everywhere in some domain containing  $R$ . Then

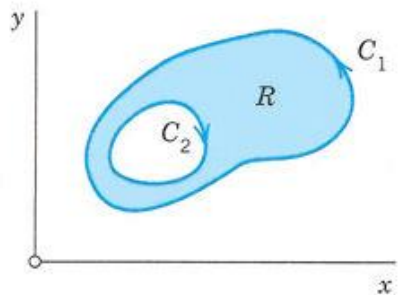
$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

Here we integrate along the entire boundary  $C$  of  $R$  in such a sense that  **$R$  is on the left** as we advance in the direction of integration.

- Vectorial form  $\left( \text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ F_1 & F_2 & F_3 \end{vmatrix} = \left[ \frac{\partial F_3}{\partial y} - \frac{\partial F_2}{\partial z}, \frac{\partial F_1}{\partial z} - \frac{\partial F_3}{\partial x}, \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right] \right)$

$$\mathbf{F} = [F_1, F_2] = F_1 \mathbf{i} + F_2 \mathbf{j}$$

$$\Rightarrow \iint_R (\text{curl } \mathbf{F}) \cdot \mathbf{k} dx dy = \oint_C \mathbf{F} \cdot d\mathbf{r}$$



Region  $R$  whose boundary  $C$  consists of two parts

# 10.4 Green's Theorem in the Plane $\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$

## ☑ Ex. 1 Verification of Green's Theorem in the Plane

$F_1 = y^2 - 7y$ ,  $F_2 = 2xy + 2x$  and  $C$  the circle  $x^2 + y^2 = 1$ .

---

$$1) \iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \iint_R [(2y + 2) - (2y - 7)] dx dy = 9 \iint_R dx dy = 9\pi$$

(Circular disk  $R$  has area  $\pi$ .)

2) We must orient  $C$  counterclockwise  $\Rightarrow \mathbf{r}(t) = [\cos t, \sin t]$ ,  $\mathbf{r}'(t) = [-\sin t, \cos t]$

$$F_1 = y^2 - 7y = \sin^2 t - 7 \sin t, \quad F_2 = 2xy + 2x = 2 \cos t \sin t + 2 \cos t$$

$$\begin{aligned} \Rightarrow \oint_C (F_1 x' + F_2 y') dt &= \int_0^{2\pi} \left[ (\sin^2 t - 7 \sin t)(-\sin t) + 2(\cos t \sin t + \cos t)(\cos t) \right] dt \\ &= \int_0^{2\pi} (-\sin^3 t + 7 \sin^2 t + 2 \cos^2 t \sin t + 2 \cos^2 t) dt \\ &= 0 + 7\pi - 0 + 2\pi = 9\pi \end{aligned}$$



# 10.4 Green's Theorem in the Plane

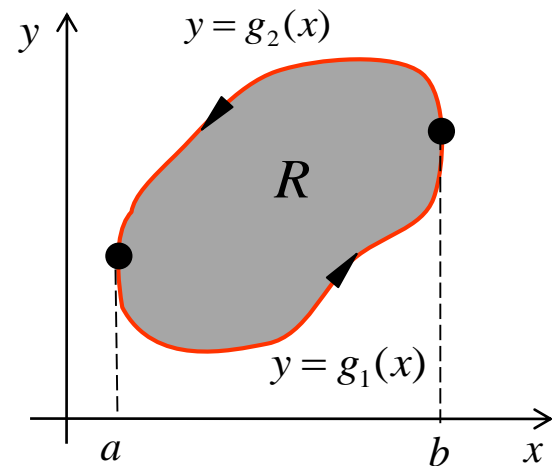
## ✓ Proof of Green's Theorem

$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

$$\oint_C F_1 dx + F_2 dy = \iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dA$$

**Proof)**  $R: g_1(x) \leq y \leq g_2(x), a \leq x \leq b$

$$\begin{aligned} -\iint_R \frac{\partial F_1}{\partial y} dA &= -\int_a^b \int_{g_1(x)}^{g_2(x)} \frac{\partial F_1}{\partial y} dy dx \\ &= -\int_a^b [F_1(x, g_2(x)) - F_1(x, g_1(x))] dx \\ &= \int_a^b F_1(x, g_1(x)) dx - \int_a^b F_1(x, g_2(x)) dx \\ &= \int_a^b F_1(x, g_1(x)) dx + \int_b^a F_1(x, g_2(x)) dx \\ &= \oint_C F_1(x, y) dx \end{aligned}$$



# 10.4 Green's Theorem in the Plane

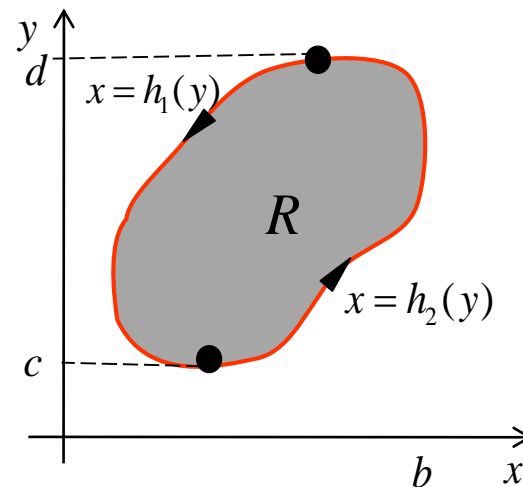
## ✓ Proof of Green's Theorem

$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

$$\oint_C F_1 dx + F_2 dy = \iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dA$$

**Proof)**  $R: h_1(y) \leq x \leq h_2(y), \quad c \leq y \leq d$

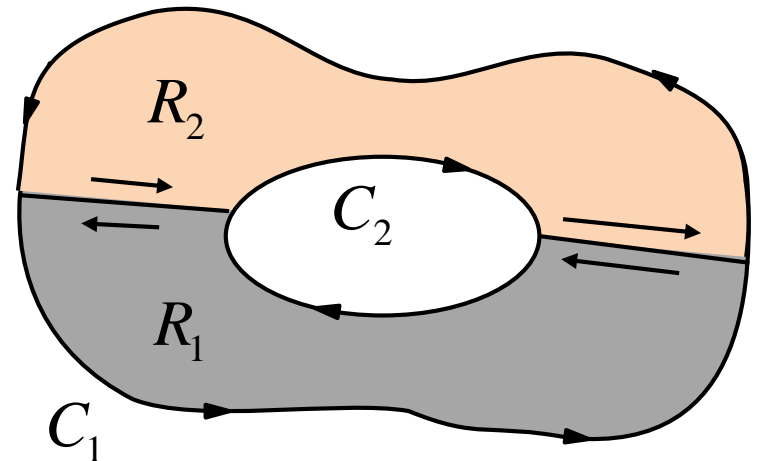
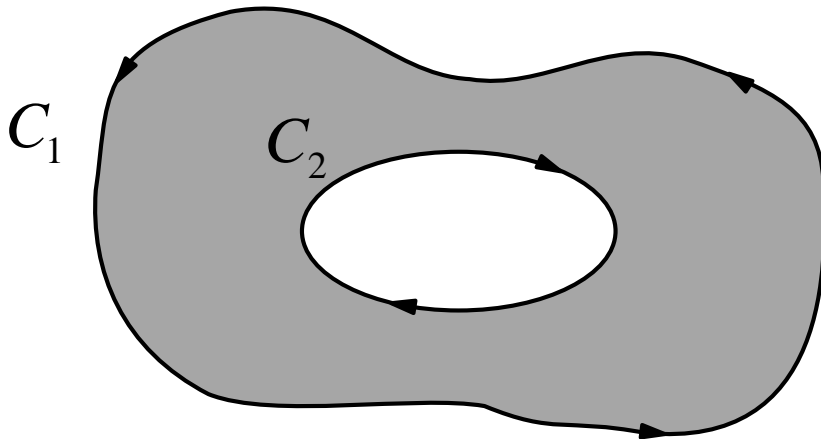
$$\begin{aligned} \iint_R \frac{\partial F_2}{\partial x} dA &= \int_c^d \int_{h_1(y)}^{h_2(y)} \frac{\partial F_2}{\partial x} dx dy \\ &= \int_c^d [F_2(h_2(y), y) - F_2(h_1(y), y)] dy \\ &= \int_c^d F_2(h_2(y), y) dy - \int_c^d F_2(h_1(y), y) dy \\ &= \int_c^d F_2(h_2(y), y) dy + \int_d^c F_2(h_1(y), y) dy \\ &= \oint_C F_2(x, y) dy \end{aligned}$$



# 10.4 Green's Theorem in the Plane $\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$

## Region with Holes

$$\begin{aligned} \iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dA &= \iint_{R_1} \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dA + \iint_{R_2} \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dA \\ &= \oint_{C_1} F_1 dx + F_2 dy + \oint_{C_2} F_1 dx + F_2 dy \\ &= \oint_C F_1 dx + F_2 dy \quad (C=C_1 \cup C_2) \end{aligned}$$



# 10.4 Green's Theorem in the Plane $\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$

## ☑ Some Applications of Green's Theorem

- **Ex. 2** Area of a Plane Region as a Line Integral Over the Boundary

$$\begin{array}{l}
 F_1 = 0, \quad F_2 = x \quad \Rightarrow \quad \iint_R dx dy = \overset{\text{R의 넓이 (=A)}}{\oint_C} x dy \\
 F_1 = -y, \quad F_2 = 0 \quad \Rightarrow \quad \iint_R dx dy = -\oint_C y dx
 \end{array}
 \quad \Rightarrow \quad A = \frac{1}{2} \oint_C (x dy - y dx)$$

- **Ex. 3** Area of a Plane Region in Polar Coordinates

Polar coordinates  $x = r \cos \theta, y = r \sin \theta$

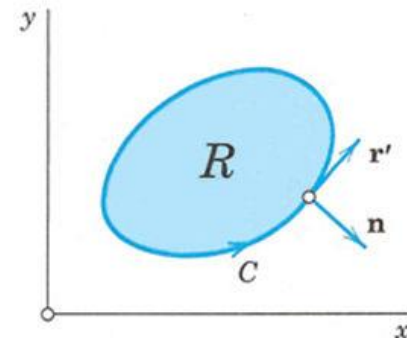
$$\Rightarrow dx = \cos \theta dr - r \sin \theta d\theta, \quad dy = \sin \theta dr + r \cos \theta d\theta$$

$$\begin{aligned}
 A &= \frac{1}{2} \oint_C (x dy - y dx) \\
 &= \frac{1}{2} \oint_C \left[ (r \cos \theta)(\sin \theta dr + r \cos \theta d\theta) - (r \sin \theta)(\cos \theta dr - r \sin \theta d\theta) \right] = \frac{1}{2} \oint_C r^2 d\theta
 \end{aligned}$$

# 10.4 Green's Theorem in the Plane $\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$

✓ **Ex. 4 Transformation of a Double Integral of the Laplacian of a Function ( $\nabla^2 w$ ) into a Line Integral of Its Normal Derivative ( $\frac{\partial w}{\partial n}$ )**

$w(x,y)$  is continuous and has continuous first and second partial derivatives in a domain of the  $xy$ -plane containing a region  $R$  of the type indicated in Green's theorem.



We set  $F_1 = -\frac{\partial w}{\partial y}, \quad F_2 = \frac{\partial w}{\partial x}$

$$1. \quad \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} = \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} = \nabla^2 w \Rightarrow \iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \iint_R \nabla^2 w dx dy$$

$$2. \quad \oint_C (F_1 dx + F_2 dy) = \oint_C \left( F_1 \frac{dx}{ds} + F_2 \frac{dy}{ds} \right) ds = \oint_C \left( -\frac{\partial w}{\partial y} \frac{dx}{ds} + \frac{\partial w}{\partial x} \frac{dy}{ds} \right) ds$$

$$\mathbf{r}' \cdot \mathbf{n} = \begin{bmatrix} \frac{dx}{ds} \\ \frac{dy}{ds} \end{bmatrix} \cdot \begin{bmatrix} -\frac{dy}{ds} \\ \frac{dx}{ds} \end{bmatrix} = 0$$

here,  $\frac{\partial w}{\partial x} \frac{dy}{ds} - \frac{\partial w}{\partial y} \frac{dx}{ds} = \begin{bmatrix} \frac{\partial w}{\partial x} & \frac{\partial w}{\partial y} \end{bmatrix} \cdot \begin{bmatrix} \frac{dy}{ds} \\ -\frac{dx}{ds} \end{bmatrix} = (\text{grad } w) \cdot \mathbf{n} = \frac{\partial w}{\partial n}$

$$D_{\mathbf{u}} f(x, y) = \nabla f(x, y) \cdot \mathbf{u}$$

$$= \oint_C \frac{\partial w}{\partial n} ds$$

$$\therefore \iint_R \nabla^2 w dx dy = \oint_C \frac{\partial w}{\partial n} ds$$

$$F_1 = -\frac{\partial w}{\partial y}, \quad F_2 = \frac{\partial w}{\partial x}$$

# 10.4 Green's Theorem in the Plane

☑ **Ex. 4** Transformation of a Double Integral of the Laplacian of a Function ( $\nabla^2 w$ ) into a Line Integral of Its Normal Derivative ( $\frac{\partial w}{\partial n}$ )

$$\iint_R \nabla^2 w dx dy = \iint_R \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} dx dy = \iint_R \frac{\partial}{\partial x} \left( \frac{\partial w}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{\partial w}{\partial y} \right) dx dy$$

$$= \iint_R \frac{\partial}{\partial x} \left( \frac{\partial w}{\partial x} \right) - \frac{\partial}{\partial y} \left( -\frac{\partial w}{\partial y} \right) dx dy = \iint_R \left( -\frac{\partial w}{\partial y} dx + \frac{\partial w}{\partial x} dy \right) \quad \iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \iint_C (F_1 dx + F_2 dy)$$

$$= \iint_C \left( -\frac{\partial w}{\partial y} \frac{dx}{ds} + \frac{\partial w}{\partial x} \frac{dy}{ds} \right) ds = \iint_C \left[ \frac{\partial w}{\partial x}, \frac{\partial w}{\partial y} \right] \left[ \frac{dy}{ds}, -\frac{dx}{ds} \right] ds = \iint_C (\text{grad } w) \cdot \mathbf{n} ds$$

$$= \iint_C \frac{\partial w}{\partial n} ds$$

$$\therefore \iint_R \nabla^2 w dx dy = \iint_C \frac{\partial w}{\partial n} ds$$

"결국 앞 페이지의  $F_1, F_2$ 는 과정을 쉽게 하기 위해 도입한 것이지, 위 식이 성립하는데 어떤 전제조건도 되지 않는다. 즉, 본 식은 일반적으로 어느 scalar  $w$ 에 대해서 성립한다."

# Example Flow of a Compressible Fluid.

비압축성 유체(Incompressible fluid)라고 가정하면,

## ☑ Continuity Equation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{V}) = 0 \quad \xrightarrow{(\rho = \text{const})} \quad \nabla \cdot \mathbf{V} = 0 \quad \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \right)$$

(divergence)

## ☑ Velocity Potential

$$\mathbf{V} = \text{grad } \phi \quad \mathbf{V} = u\mathbf{i} + v\mathbf{j} + w\mathbf{k} = \frac{\partial \phi}{\partial x} \mathbf{i} + \frac{\partial \phi}{\partial y} \mathbf{j} + \frac{\partial \phi}{\partial z} \mathbf{k}$$

$$+ \nabla \cdot \mathbf{V} = 0 \quad \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \right)$$

$$\parallel \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} = \nabla^2 \phi = 0$$

# Example Flow of a Compressible Fluid.

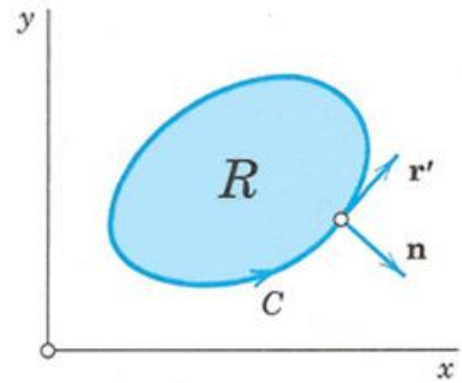
$$\therefore \iint_R \nabla^2 w dx dy = \oint_C \frac{\partial w}{\partial n} ds$$

## ☑ Physical Meaning

- Incompressible fluid when continuity equation is satisfied,

$$\nabla^2 \phi = 0$$

$$\therefore \iint_R \nabla^2 \phi dx dy = 0$$



C의 normal 방향으로의 유체의 속도

$$\oint_C \frac{\partial \phi}{\partial n} ds = 0$$

경계 C를 통해 단위 시간당 들어오고 나온 유체의 양=0



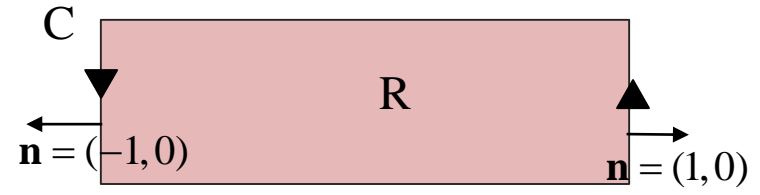
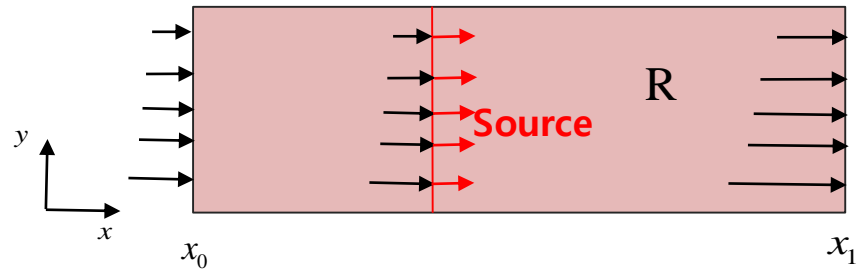
# Example Flow of a Compressible Fluid.

## Physical Meaning

- Incompressible fluid but continuity equation is **NOT** satisfied, ex) a source to add flux x direction, no flux in y direction  $\frac{\partial \phi}{\partial y} = \frac{\partial^2 \phi}{\partial y^2} = 0$

속도  $u$ 의 변화량

$$u(x_0, y) = \frac{\partial \phi}{\partial x}(x_0, y) \quad \frac{\partial u}{\partial x} = \frac{\partial^2 \phi}{\partial x^2} \quad u(x_1, y) = \frac{\partial \phi}{\partial x}(x_1, y)$$



경계를 통해 단위 시간당 빠져나가는 유체의 양

$$\oint_C \frac{\partial \phi}{\partial n} ds = \int -\frac{\partial \phi}{\partial x} \Big|_{x_0} + \frac{\partial \phi}{\partial x} \Big|_{x_1} dy = \int -u(x_0, y) + u(x_1, y) dy$$

$$\iint_R \nabla^2 \phi dx dy = \int \int_{x_0}^{x_1} \frac{\partial^2 \phi}{\partial x^2} dx dy = \int \frac{\partial \phi}{\partial x} \Big|_{x_0}^{x_1} dy = \int u(x_1, y) - u(x_0, y) dy$$

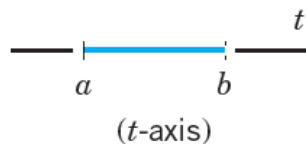
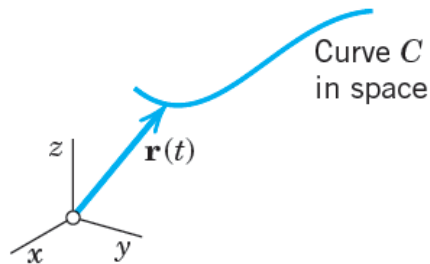
속도의 변화량의 적분

양 경계에서의 단위시간당 속도차 = 생성되는 유체의 양

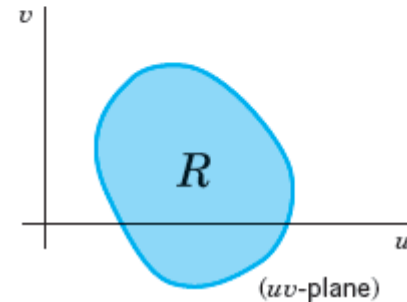
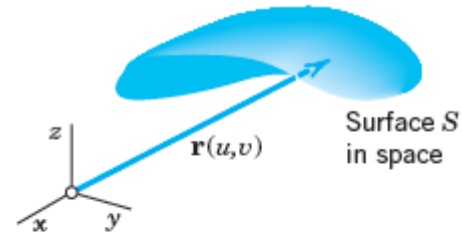
# 10.5 Surfaces for Surface Integrals

## ☑ Representation of Surfaces: $z = f(x, y)$ or $g(x, y, z) = 0$

- Curve  $C$ :  $r = \mathbf{r}(t)$ , where  $a \leq t \leq b$
- Surface  $S$ :  $\mathbf{r}(u, v) = [x(u, v), y(u, v), z(u, v)] = x(u, v) \mathbf{i} + y(u, v) \mathbf{j} + z(u, v) \mathbf{k}$  where  $(u, v)$  varies in some region  $R$  of the  $uv$ -plane



Parametric representation of a curve

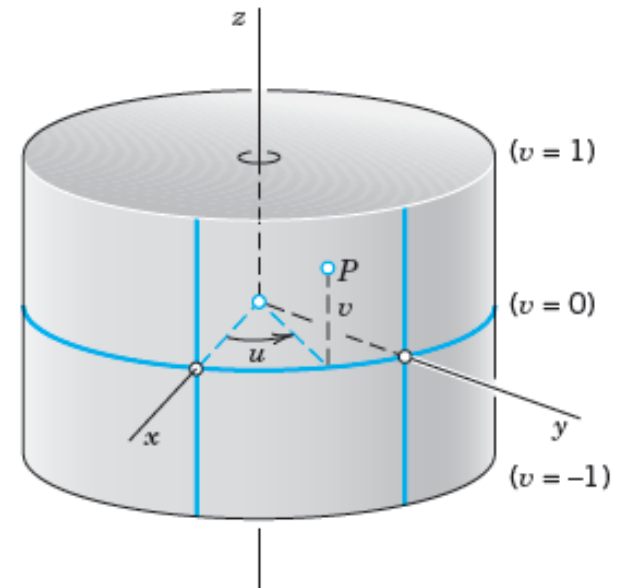


Parametric representation of a surface

# 10.5 Surfaces for Surface Integrals

## ☑ Ex. 1 Parametric Representation of a Cylinder

- The circular cylinder  $x^2 + y^2 = a^2$ ,  $-1 \leq z \leq 1$ , has radius  $a$ , height 2, and the  $z$ -axis as axis
- Parametric representation:  
$$\mathbf{r}(u, v) = [a \cos u, a \sin u, v] = a \cos u \mathbf{i} + a \sin u \mathbf{j} + v \mathbf{k}$$
- The parameters  $u, v$  vary in the rectangle  $R : 0 \leq u \leq 2\pi, -1 \leq v \leq 1$  in the  $uv$ -plane
- The components of  $\mathbf{r}$  are  $x = a \cos u, y = a \sin u, z = v$
- The curves  $u = \text{const}$  are vertical straight lines.
- The curves  $v = \text{const}$  are parallel circles.



*“cylinder surface를  $u, v$  사각형 구간으로 변환해야 2차원 적분이 쉽다.”*

Parametric representation of a cylinder

# 10.5 Surfaces for Surface Integrals

## ☑ Ex. 2 Parametric Representation of a Sphere

A sphere  $x^2 + y^2 + z^2 = a^2$  can be represented in the form

$$\mathbf{r}(u, v) = a \cos v \cos u \mathbf{i} + a \cos v \sin u \mathbf{j} + a \sin v \mathbf{k}$$

where the parameters  $u, v$  vary in the rectangle

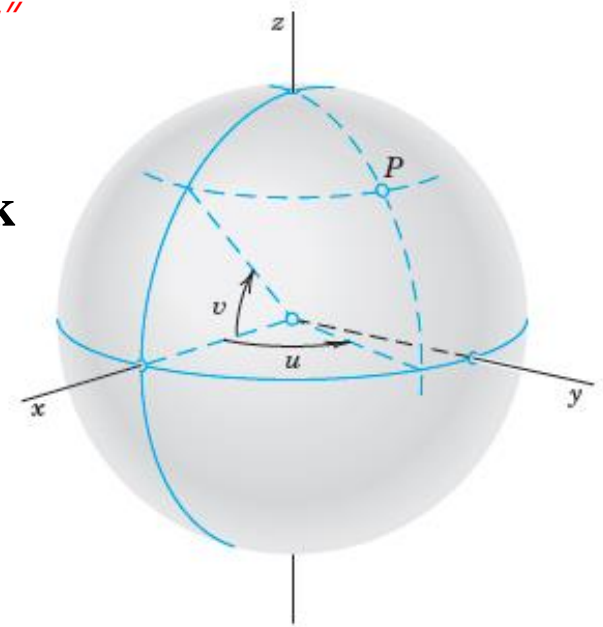
$$R: 0 \leq u \leq 2\pi, \quad -\frac{\pi}{2} \leq v \leq \frac{\pi}{2} \quad \text{"}u, v \text{ 사각형 구간"}$$

Another parametric representation is

$$\mathbf{r}(u, v) = a \cos u \sin v \mathbf{i} + a \sin u \sin v \mathbf{j} + a \cos v \mathbf{k}$$

where

$$R: 0 \leq u \leq 2\pi, \quad 0 \leq v \leq \pi$$



Parametric representation of a sphere

# 10.5 Surfaces for Surface Integrals

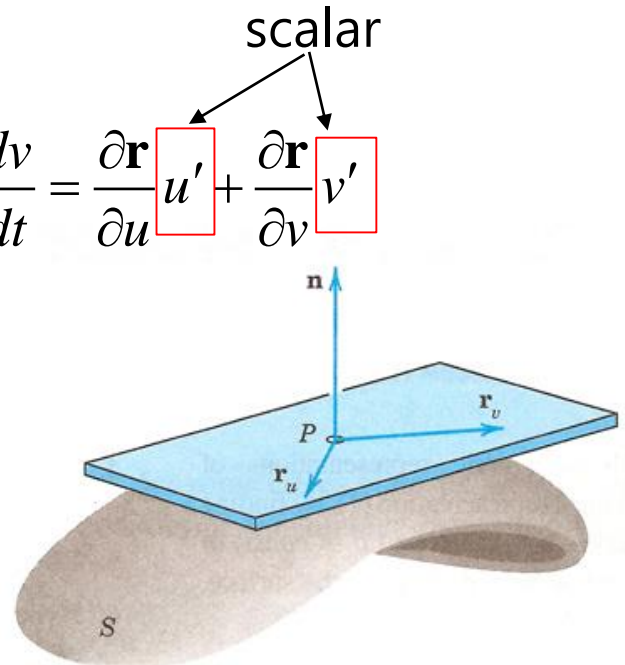
## ☑ Tangent Plane and Surface Normal

- **Tangent Plane:** A Plane which is formed by the tangent vectors of all the curves on a surface  $S$  through a point  $P$  of  $S$
- **Normal Vector:** A vector perpendicular to the tangent plane
- $S: \mathbf{r} = \mathbf{r}(u, v)$  and  $C: \tilde{\mathbf{r}}(t) = \mathbf{r}(u(t), v(t))$

✓ Tangent vector: 
$$\tilde{\mathbf{r}}'(t) = \frac{d\tilde{\mathbf{r}}}{dt} = \frac{\partial \mathbf{r}}{\partial u} \frac{du}{dt} + \frac{\partial \mathbf{r}}{\partial v} \frac{dv}{dt} = \frac{\partial \mathbf{r}}{\partial u} \boxed{u'} + \frac{\partial \mathbf{r}}{\partial v} \boxed{v'}$$

✓  $\frac{\partial \mathbf{r}}{\partial u}$ : tangent vector along  $u$  direction at  $P$  of a curve  $\mathbf{r}(u)$  when  $v = \text{const}$  like  $\mathbf{r}'(t)$

✓  $\frac{\partial \mathbf{r}}{\partial v}$ : tangent vector along  $v$  direction at  $P$  of a curve  $\mathbf{r}(v)$  when  $u = \text{const}$  like  $\mathbf{r}'(t)$



Tangent plane and normal vector

# 10.5 Surfaces for Surface Integrals

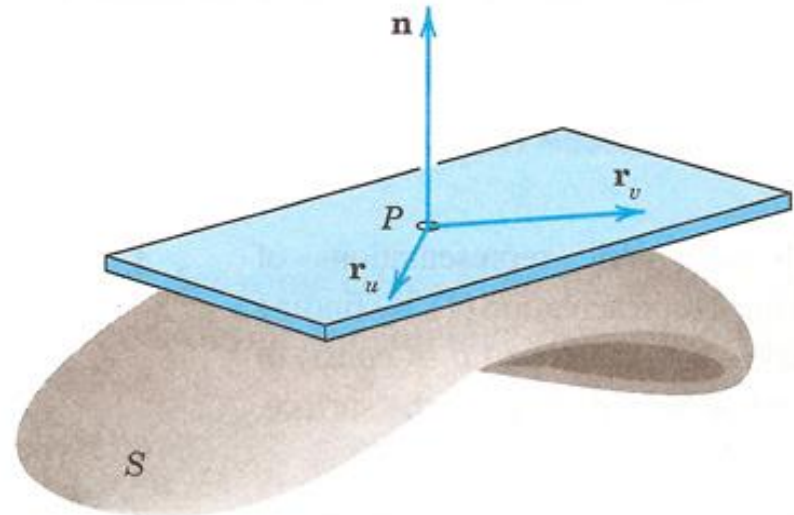
## ☑ Tangent Plane and Surface Normal

- **Tangent Plane:** A Plane which is formed by the tangent vectors of all the curves on a surface  $S$  through a point  $P$  of  $S$
- **Normal Vector:** A vector perpendicular to the tangent plane
- **Normal vector:**

$$\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v \neq \mathbf{0}$$

- **Unit normal vector:**

$$\mathbf{n} = \frac{1}{|\mathbf{N}|} \mathbf{N} = \frac{1}{|\mathbf{r}_u \times \mathbf{r}_v|} \mathbf{r}_u \times \mathbf{r}_v$$



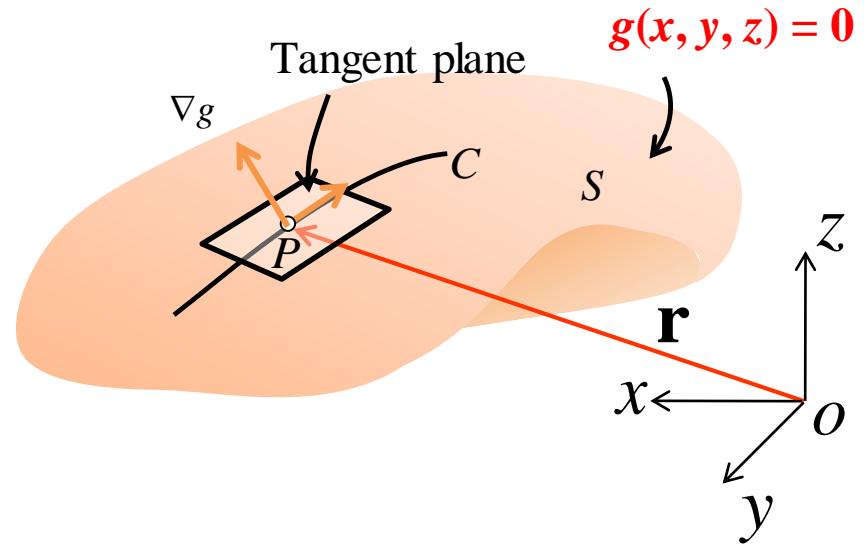
Tangent plane and normal vector

# 10.5 Surfaces for Surface Integrals

## ☑ Tangent Plane (접평면) and Surface Normal (곡면 법선)

- $S$  is represented by  $g(x, y, z) = 0$
- $S$  is a smooth surface if its surface normal depends continuously on the point of  $S$
- $S$  is piecewise smooth if it consists of finitely many smooth portions.

$$\mathbf{n} = \frac{1}{|\text{grad } g|} \text{grad } g$$



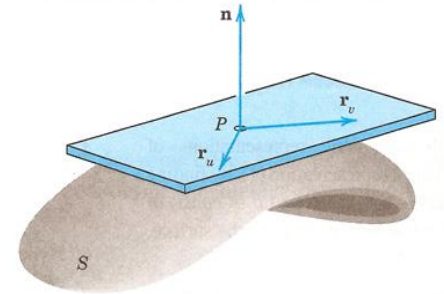
Normal vector for surface  $g(x, y, z) = 0$

# 10.5 Surfaces for Surface Integrals

## ☑ Theorem 1 Tangent Plane and Surface Normal

- If a surface  $S$  is given by  $\mathbf{r}(u,v)=[x(u,v), y(u,v), z(u,v)]$  with continuous  $\mathbf{r}_u$  and  $\mathbf{r}_v$  satisfying  $\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v$  at every point of  $S$ ,
- then  $S$  has at every point  $P$  a unique tangent plane passing through  $P$  and spanned by  $\mathbf{r}_u$  and  $\mathbf{r}_v$ ,
- and a unique normal whose direction depends continuously on the points of  $S$ . A normal vector is given by  $\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v$  and the corresponding unit normal vector by

$$\mathbf{n} = \frac{1}{|\mathbf{N}|} \mathbf{N} = \frac{1}{|\mathbf{r}_u \times \mathbf{r}_v|} \mathbf{r}_u \times \mathbf{r}_v$$



## ☑ Ex. 4 Unit Normal Vector of a Sphere

The sphere  $g(x,y,z) = x^2 + y^2 + z^2 - a^2 = 0$  has the unit normal vector

$$\mathbf{n}(x, y, z) = \frac{1}{|\text{grad } g|} \text{grad } g = \left[ \frac{x}{a}, \frac{y}{a}, \frac{z}{a} \right] = \frac{x}{a} \mathbf{i} + \frac{y}{a} \mathbf{j} + \frac{z}{a} \mathbf{k}$$



$$\int_C \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r} = \int_a^b \mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$$

## ☑ Surface Integral

$$S : \mathbf{r}(u, v) = [x(u, v), y(u, v), z(u, v)] = x(u, v)\mathbf{i} + y(u, v)\mathbf{j} + z(u, v)\mathbf{k}$$

- Normal vector:  $\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v \neq \mathbf{0}$

- Unit normal vector:  $\mathbf{n} = \frac{1}{|\mathbf{N}|} \mathbf{N} = \frac{1}{|\mathbf{r}_u \times \mathbf{r}_v|} \mathbf{r}_u \times \mathbf{r}_v$

- Surface integral over S:  $\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) dudv$

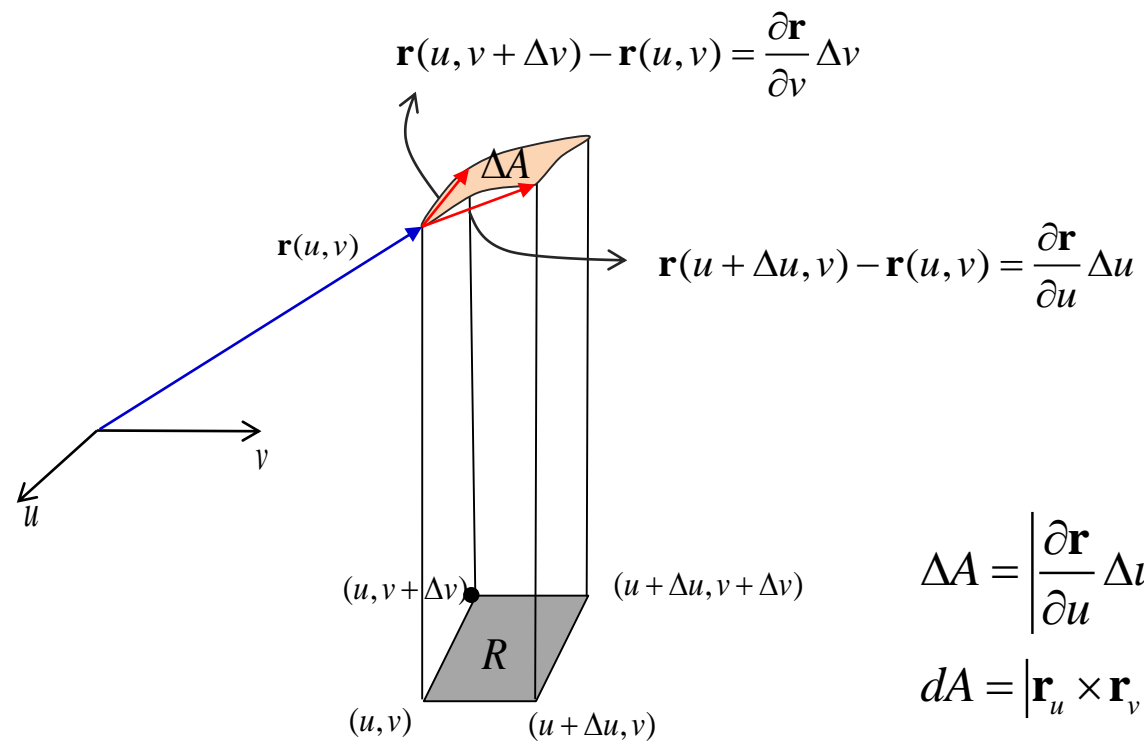
$|\mathbf{N}| = |\mathbf{r}_u \times \mathbf{r}_v|$ : the area of the parallelogram with sides  $\mathbf{r}_u$  and  $\mathbf{r}_v$   
(평행사변형)

$dA = |\mathbf{N}| dudv$

$$\therefore \mathbf{n} dA = \mathbf{n} |\mathbf{N}| dudv = \mathbf{N} dudv$$

# 10.6 Surface Integrals

$$\mathbf{n}dA = \mathbf{n}|\mathbf{N}|dudv = \mathbf{N}dudv ?$$



$$\Delta A = \left| \frac{\partial \mathbf{r}}{\partial u} \Delta u \times \frac{\partial \mathbf{r}}{\partial v} \Delta v \right| = \left| \frac{\partial \mathbf{r}}{\partial u} \times \frac{\partial \mathbf{r}}{\partial v} \right| \Delta u \Delta v$$

$$dA = |\mathbf{r}_u \times \mathbf{r}_v| dudv, \quad \mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v$$

$$\therefore dA = |\mathbf{N}| dudv$$

# 10.6 Surface Integrals

## ☑ Surface Integral (면적분)

$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) du dv$$

$\mathbf{F} \cdot \mathbf{n}$  : the normal component of  $\mathbf{F}$

When  $\mathbf{F} = \rho \mathbf{v}$  (density x velocity vector of the flow)

⇒ flux across  $S$  = mass of fluid crossing  $S$  per unit time

- In components

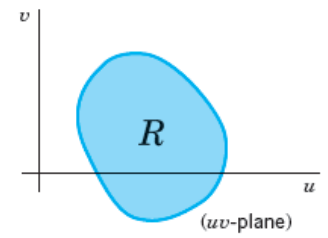
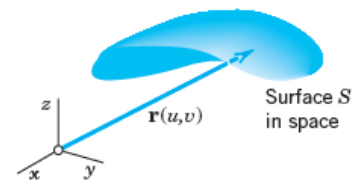
Here,  $\alpha, \beta, \gamma$  are the angles between  $\mathbf{n}$  and the coordinate axes.

$$\mathbf{F} = [F_1, F_2, F_3], \quad \mathbf{N} = [N_1, N_2, N_3], \quad \mathbf{n} = [\cos \alpha, \cos \beta, \cos \gamma]$$

$$\begin{aligned} \iint_S \mathbf{F} \cdot \mathbf{n} dA &= \iint_S (F_1 \cos \alpha + F_2 \cos \beta + F_3 \cos \gamma) dA & \cos \alpha &= \frac{\mathbf{n} \cdot \mathbf{i}}{|\mathbf{n}| |\mathbf{i}|} = \mathbf{n} \cdot \mathbf{i} = n_1 \\ &= \iint_R (F_1 N_1 + F_2 N_2 + F_3 N_3) du dv & \cos \beta &= \frac{\mathbf{n} \cdot \mathbf{j}}{|\mathbf{n}| |\mathbf{j}|} = \mathbf{n} \cdot \mathbf{j} = n_2 \\ & & \cos \gamma &= \frac{\mathbf{n} \cdot \mathbf{k}}{|\mathbf{n}| |\mathbf{k}|} = \mathbf{n} \cdot \mathbf{k} = n_3 \end{aligned}$$

$$\cos \alpha dA = dydz, \quad \cos \beta dA = dzdx, \quad \cos \gamma dA = dxdy$$

$$= \iint_S (F_1 dydz + F_2 dzdx + F_3 dxdy)$$



# 10.6 Surface Integrals

## ☑ Ex. 1 Flux Through a Surface

$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) du dv$$

- Compute the flux of water through the parabolic cylinder:  $S : y = x^2, 0 \leq x \leq 2, 0 \leq z \leq 3$   
velocity vector:  $\mathbf{v} = \mathbf{F} = [3z^2, 6, 6xz]$  (m/sec)  
 $\mathbf{F} = \rho \mathbf{v}$ , the density  $\rho = 1 \text{ gm/cm}^3 = 1 \text{ ton/m}^3$

**Sol)** Representation  $S: \mathbf{r} = [u, u^2, v]$  ( $0 \leq u \leq 2, 0 \leq v \leq 3$ )

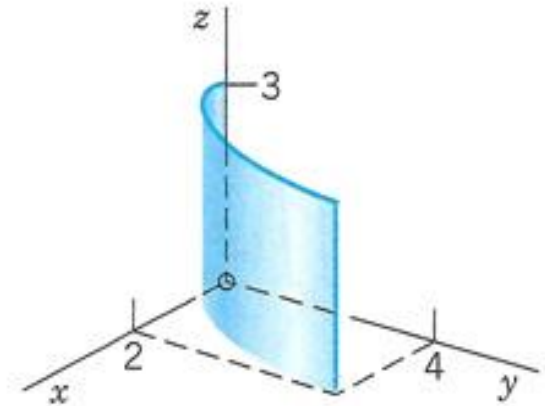
By differentiation and by the definition of the cross product

$$\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v = [1, 2u, 0] \times [0, 0, 1] = [2u, -1, 0]$$

$$\therefore \mathbf{F}(S) \cdot \mathbf{N} = 6uv^2 - 6$$

By integration

$$\begin{aligned} \iint_S \mathbf{F} \cdot \mathbf{n} dA &= \int_0^3 \int_0^2 (6uv^2 - 6) du dv = \int_0^3 (3u^2v^2 - 6u) \Big|_{u=0}^2 dv \\ &= \int_0^3 (12v^2 - 12) dv = (4v^3 - 12v) \Big|_{v=0}^3 = 72 \left[ \frac{\text{m}^3}{\text{sec}} \right] \end{aligned}$$



$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) du dv$$

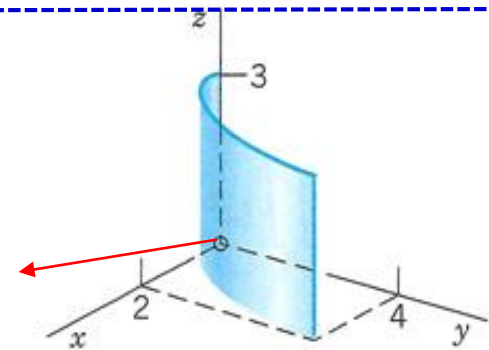
# 10.6 Surface Integrals

## ✓ Ex. 1 Flux Through a Surface

- Compute the flux of water through the parabolic cylinder:  $S: y=x^2, 0 \leq x \leq 2, 0 \leq z \leq 3$
- velocity vector:  $\mathbf{v} = \mathbf{F} = [3z^2, 6, 6xz]$  (m/sec)
- $\mathbf{F} = \rho \mathbf{v}$ , the density  $\rho = 1 \text{ gm/cm}^3 = 1 \text{ ton/m}^3$

**Sol)** Representation  $S: \mathbf{r} = [u, u^2, v]$  ( $0 \leq u \leq 2, 0 \leq v \leq 3$ )

$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_S (F_1 dy dz + F_2 dz dx + F_3 dx dy)$$



$$\mathbf{N} = |\mathbf{N}| \mathbf{n} = |\mathbf{N}| [\cos \alpha, \cos \beta, \cos \gamma] = [2u, -1, 0], \quad \cos \alpha > 0, \cos \beta < 0, \cos \gamma = 0$$

$$-\pi/2 < \alpha < 0 \Rightarrow \cos \alpha > 0, \quad \pi/2 < \beta < \pi \Rightarrow \cos \beta < 0, \quad \gamma = \pi/2 \Rightarrow \cos \gamma = 0$$

$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \int_0^3 \int_0^4 3z^2 dy dz - \int_0^2 \int_0^3 6 dz dx = \int_0^3 4(3z^2) dy dz - \int_0^2 6 \cdot 3 dx = 72$$

# 10.6 Surface Integrals

## ☑ Ex. 2 Surface Integral

$\mathbf{F} = [x^2, 0, 3y^2]$ ,  $x + y + z = 1$ . Evaluate  $\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) du dv$

Sol) Representation S  $\Rightarrow$  Representation R (곡면 S의 xy-plane으로의 투영)

$$x = u, y = v, \Rightarrow z = 1 - x - y = 1 - u - v$$

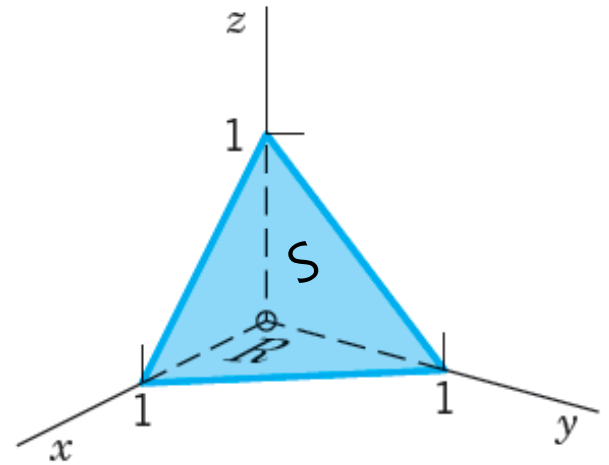
R  $\mathbf{r}(u, v) = [u, v, 1 - u - v]$

$$0 \leq u \leq 1 - v, 0 \leq v \leq 1$$

$$\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v = [1, 0, -1] \times [0, 1, -1] = [1, 1, 1]$$

$$\mathbf{F}(S) \cdot \mathbf{N} = [u^2, 0, 3v^2] \cdot [1, 1, 1] = u^2 + 3v^2$$

$$\begin{aligned} \iint_S \mathbf{F} \cdot \mathbf{n} dA &= \iint_R (u^2 + 3v^2) du dv = \int_0^1 \int_0^{1-v} (u^2 + 3v^2) du dv \\ &= \int_0^1 \left[ \frac{1}{3} (1-v)^3 + 3v^2 (1-v) \right] dv = \frac{1}{3} \end{aligned}$$



# 10.6 Surface Integrals

## ☑ Orientation (방향) of Surfaces

- The value of the integral depends on the choice of the unit normal vector  $\mathbf{n}$ .
- **An oriented surface  $S$  (방향을 가진 곡면, 유향곡면):** a surface  $S$  on which we have chosen one of the two possible unit normal vectors in a continuous fashion
- If we change the orientation of  $S$ , this means that we replace  $\mathbf{n}$  with  $-\mathbf{n}$ .

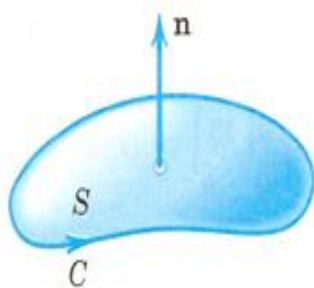
## ☑ Theorem 1 Change of Orientation in a Surface Integral

The replacement of  $\mathbf{n}$  by  $-\mathbf{n}$  corresponds to the multiplication of the integral by  $-1$

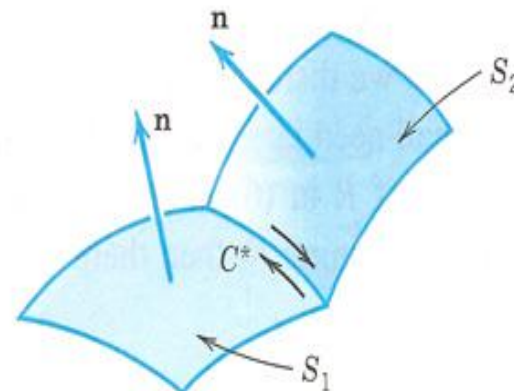
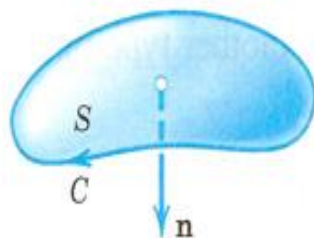
# 10.6 Surface Integrals

## ☑ Orientation of Piecewise Smooth Surfaces

- $S$  is **orientable** (방향을 가질 수 있는) if the positive normal direction can be continued in a unique and continuous way to the entire surface.
- For a smooth orientable surface  $S$  with boundary curve  $C$  we may associate each of the **two possible orientations of  $S$**  with **an orientation of  $C$** .
- A **piecewise smooth surface** is orientable (방향을 가질 수 있는) if we can orient each smooth piece of  $S$  so that along each curve  $C^*$  which is a common boundary of two pieces  $S_1$  and  $S_2$ .
- The positive direction of  $C^*$  relative to  $S_1$  is opposite to the direction of  $C^*$  relative to  $S_2$ .



(A) Smooth surface



(B) Piecewise smooth surface

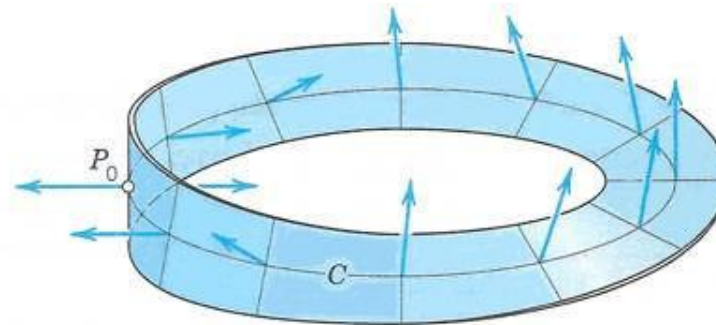
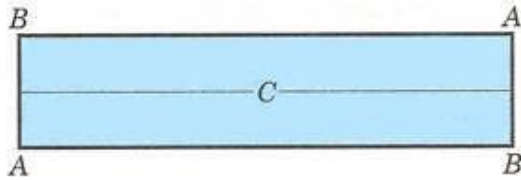
Orientation of a surface



# 10.6 Surface Integrals

## ☑ Nonorientable (방향을 가질 수 없는) Surfaces

- A sufficiently small piece of a smooth surface is always orientable. This may not hold for entire surfaces. Ex. Möbius strip



Möbius strip

$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) du dv$$

## 10.6 Surface Integrals

### ☑ Surface Integrals Without Regard to Orientation

- Another type of surface integral disregarding the orientation

$$\iint_S G(\mathbf{r}) dA = \iint_R G(\mathbf{r}(u, v)) |\mathbf{N}(u, v)| du dv$$

Here  $dA = |\mathbf{N}| du dv = |\mathbf{r}_u \times \mathbf{r}_v| du dv$  is the element of area of  $S$ .

- Mean value theorem for surface integrals

If  $R$  is simply connected and  $G(\mathbf{r})$  is continuous in a domain containing  $R$ , then there is a point in  $R$  such that

$$\iint_S G(\mathbf{r}) dA = G(\mathbf{r}(u_0, v_0)) A \quad (\text{A: Area of } S)$$

- Area of A:  $A(S) = \iint_S dA = \iint_R |\mathbf{r}_u \times \mathbf{r}_v| du dv$

# 10.6 Surface Integrals

## ☑ Ex. 4 Area of a Sphere (구의 겉넓이)

For a sphere  $\mathbf{r}(u, v) = [a \cos v \cos u, a \cos v \sin u, a \sin v]$ ,

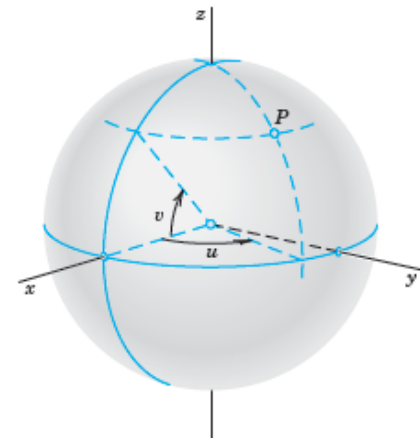
**Sol)**  $0 \leq u \leq 2\pi, -\pi/2 \leq v \leq \pi/2$ , we obtain by direct calculation

$$\mathbf{r}_u \times \mathbf{r}_v = \left[ a^2 \cos^2 v \cos u, a^2 \cos^2 v \sin u, a^2 \cos v \sin v \right]$$

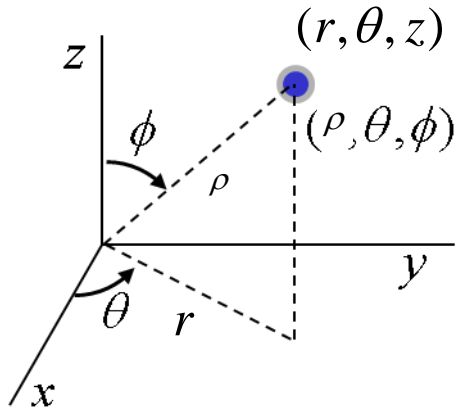
Using  $\cos^2 u + \sin^2 u = 1, \cos^2 v + \sin^2 v = 1$

$$|\mathbf{r}_u \times \mathbf{r}_v| = a^2 \left( \cos^4 v \cos^2 u + \cos^4 v \sin^2 u + \cos^2 v \sin^2 v \right)^{1/2} = a^2 |\cos v|$$

$$\therefore A(S) = a^2 \int_{-\pi/2}^{\pi/2} \int_0^{2\pi} |\cos v| du dv = 2\pi a^2 \int_{-\pi/2}^{\pi/2} \cos v dv = 4\pi a^2$$



# 10.6 Surface Integrals



Spherical coordinates

Spherical  $\rightarrow$  Cylindrical

$$r = \rho \sin \phi \quad \theta = \theta \quad z = \rho \cos \phi$$

Spherical  $\rightarrow$  Cartesian

$$x = r \sin \phi \cos \theta \quad y = r \sin \phi \sin \theta \quad z = r \cos \phi$$

Cartesian  $\rightarrow$  Spherical

$$r = \sqrt{x^2 + y^2 + z^2} \quad \theta = \tan^{-1}\left(\frac{y}{x}\right) \quad \phi = \cos^{-1}\left(\frac{z}{\sqrt{x^2 + y^2 + z^2}}\right)$$

# 10.6 Surface Integrals

$$\iint_S G(\mathbf{r})dA = \iint_R G(\mathbf{r}(u,v))|\mathbf{N}(u,v)|dudv$$

## ☑ Representations $z = f(x, y)$

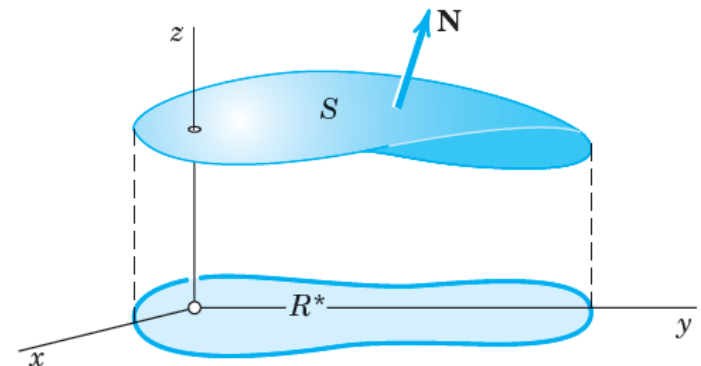
- If a surface  $S$  is given by  $z = f(x, y)$

$$|\mathbf{N}| = |\mathbf{r}_u \times \mathbf{r}_v| = |[1, 0, f_u] \times [0, 1, f_v]| = |[-f_u, -f_v, 1]| = \sqrt{1 + f_u^2 + f_v^2}$$

- Surface integral: 
$$\iint_S G(\mathbf{r})dA = \iint_{R^*} G(x, y, f(x, y))\sqrt{1 + \left(\frac{\partial f}{\partial x}\right)^2 + \left(\frac{\partial f}{\partial y}\right)^2} dx dy$$

Here,  $R^*$ : projection of  $S$  into the  $xy$ -plane

- Area: 
$$A(S) = \iint_{R^*} \sqrt{1 + \left(\frac{\partial f}{\partial x}\right)^2 + \left(\frac{\partial f}{\partial y}\right)^2} dx dy$$

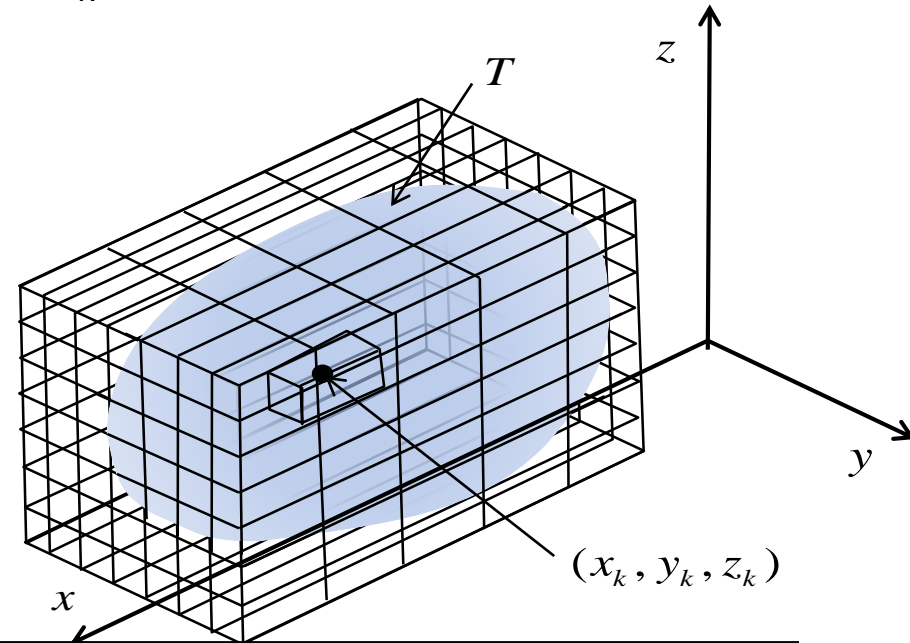


# 10.7 Triple Integrals. Divergence Theorem of Gauss

## ✓ Triple integral for an integral of a function $f(x, y, z)$

- We subdivide  $T$  by planes parallel to the coordinate planes.
- We consider those boxes of the subdivision that lie entirely inside  $T$ , and number them from 1 to  $n$ .
- In each such box we choose an arbitrary point, say,  $(x_k, y_k, z_k)$  in box  $k$ .
- The maximum length of all edges of those  $n$  boxes approaches zero as  $n$  approaches infinity.
- The volume of box  $k$  we denote by  $\Delta V_k$ . We now form the sum

$$J_n = \sum_{k=1}^n f(x_k, y_k, z_k) \Delta V_k$$



# 10.7 Triple Integrals. Divergence Theorem of Gauss

## ☑ Theorem 1 Divergence Theorem of Gauss (발산이론)

Let  $T$  be a closed bounded region in space whose boundary is a piecewise smooth orientable surface  $S$ . Let  $\mathbf{F}(x,y,z)$  be a vector function that is continuous and has continuous first partial derivatives in some domain containing  $T$ . Then

$$\iiint_T \operatorname{div} \mathbf{F} dV = \iint_S \mathbf{F} \cdot \mathbf{n} dA$$

In components of  $\mathbf{F}=[F_1, F_2, F_3]$  and of the outer unit normal vector  $\mathbf{n}=[\cos \alpha, \cos \beta, \cos \gamma]$  of  $S$ , formula becomes

$$\iiint_T \left( \frac{\partial F_1}{\partial x} + \frac{\partial F_2}{\partial y} + \frac{\partial F_3}{\partial z} \right) dx dy dz = \iint_S (F_1 \cos \alpha + F_2 \cos \beta + F_3 \cos \gamma) dA = \iint_S (F_1 dy dz + F_2 dz dx + F_3 dx dy)$$

# 10.7 Triple Integrals. Divergence Theorem of Gauss

**Proof)**

$$\begin{aligned}\iiint_T \left( \frac{\partial F_1}{\partial x} + \frac{\partial F_2}{\partial y} + \frac{\partial F_3}{\partial z} \right) dx dy dz &= \iint_S (F_1 \cos \alpha + F_2 \cos \beta + F_3 \cos \gamma) dA \\ &= \iint_S (F_1 dy dz + F_2 dz dx + F_3 dx dy)\end{aligned}$$

This equation is true if and only if the integrals of each component on both sides are equal

$$(3) \quad \iiint_T \frac{\partial F_1}{\partial x} dx dy dz = \iint_S F_1 \cos \alpha dA = \iint_S F_1 dy dz$$

$$(4) \quad \iiint_T \frac{\partial F_2}{\partial y} dx dy dz = \iint_S F_2 \cos \beta dA = \iint_S F_2 dx dz$$

$$(5) \quad \iiint_T \frac{\partial F_3}{\partial z} dx dy dz = \iint_S F_3 \cos \gamma dA = \iint_S F_3 dx dy$$





# 10.7 Triple Integrals. Divergence Theorem of Gauss

**Proof continued)**

$$(5) \iiint_T \frac{\partial F_3}{\partial z} dx dy dz = \iint_S F_3 \cos \gamma dA$$

$$\iiint_T \frac{\partial F_3}{\partial z} dx dy dz = \iint_{\bar{R}} \left[ \int_{g(x,y)}^{h(x,y)} \frac{\partial F_3}{\partial z} dz \right] dx dy$$

$$= \iint_{\bar{R}} F_3[x, y, h(x, y)] dx dy - \iint_{\bar{R}} F_3[x, y, g(x, y)] dx dy$$

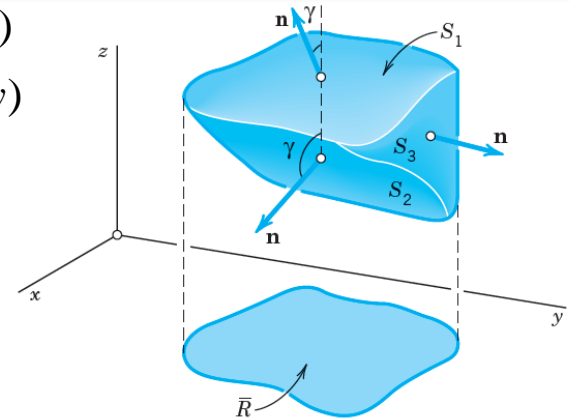
We can decide the sign of the integral because  $\cos \gamma < 0$  on  $S_2$ , and  $\cos \gamma > 0$  on  $S_1$

$$\iint_S F_3 \cos \gamma dA = \iint_S F_3 dx dy = + \iint_{\bar{R}} F_3[x, y, h(x, y)] dx dy - \iint_{\bar{R}} F_3[x, y, g(x, y)] dx dy$$

Therefore, we prove (5). In the same manner, (3), (4) can be proven.

$$S_1 : h(x, y)$$

$$S_2 : g(x, y)$$



$$\iiint_T \frac{\partial F_3}{\partial z} dx dy dz = \iint_S F_3 \cos \gamma dA$$

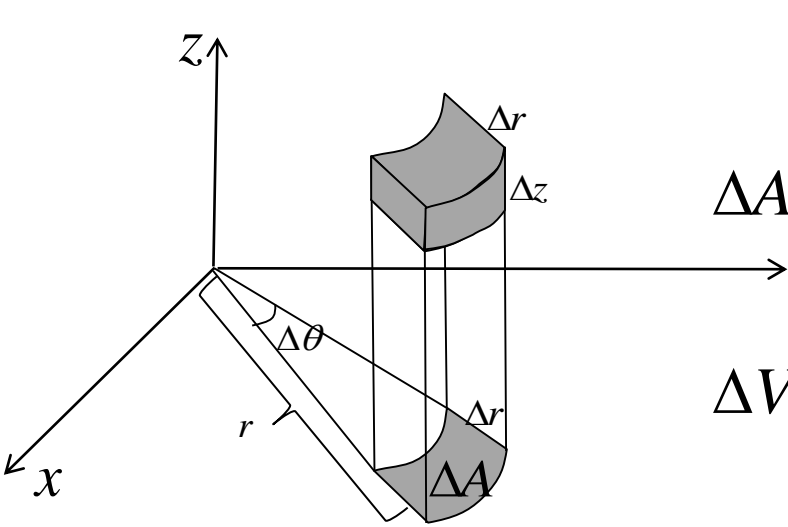
# 10.7 Triple Integrals. Divergence Theorem of Gauss

☑ **Ex. 1 Evaluation of a Surface Integral by the Divergence Theorem**

Evaluate  $I = \iiint_S (x^3 dydz + x^2 ydzdx + x^2 z dxdy)$  where  $S$  is the closed surface consisting of the cylinder  $x^2 + y^2 = a^2$  ( $0 \leq z \leq b$ ) and the circular disks  $z = 0$  and  $z = b$  ( $x^2 + y^2 \leq a^2$ ).

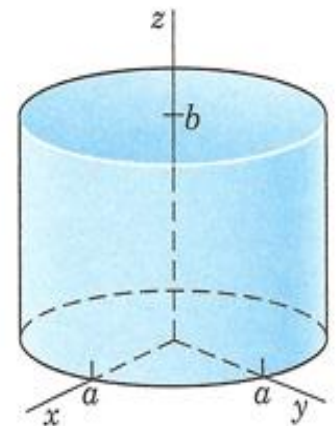
**Sol)**  $F_1 = x^3, F_2 = x^2 y, F_3 = x^2 z \Rightarrow \operatorname{div} \mathbf{F} = 3x^2 + x^2 + x^2 = 5x^2$

Polar coordinates ( $dxdydz = r dr d\theta dz$ )



$$\Delta A = (r \Delta \theta) \cdot \Delta r$$

$$\Delta V = \Delta A \Delta z = r \Delta r \Delta \theta \Delta z$$



**Surface S in Example 1**

# 10.7 Triple Integrals. Divergence Theorem of Gauss

## ☑ Ex. 1 Evaluation of a Surface Integral by the Divergence Theorem

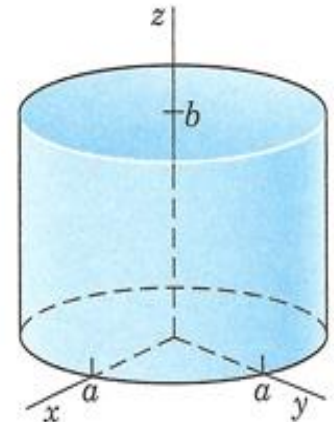
Evaluate  $I = \iiint_S (x^3 dydz + x^2 ydzdx + x^2 z dxdy)$  where  $S$  is the closed surface consisting of the cylinder  $x^2 + y^2 = a^2$  ( $0 \leq z \leq b$ ) and the circular disks  $z = 0$  and  $z = b$  ( $x^2 + y^2 \leq a^2$ ).

---

**Sol)**  $F_1 = x^3$ ,  $F_2 = x^2 y$ ,  $F_3 = x^2 z \Rightarrow \operatorname{div} \mathbf{F} = 3x^2 + x^2 + x^2 = 5x^2$

Polar coordinates ( $dxdydz = r dr d\theta dz$ )

$$\begin{aligned} I &= \iiint_T 5x^2 dx dy dz = \int_{z=0}^b \int_{\theta=0}^{2\pi} \int_{r=0}^a (5r^2 \cos^2 \theta) r dr d\theta dz \\ &= 5 \int_{z=0}^b \int_{\theta=0}^{2\pi} \frac{a^4}{4} \cos^2 \theta d\theta dz = 5 \int_{z=0}^b \frac{a^4 \pi}{4} dz = \frac{5\pi}{4} a^4 b \end{aligned}$$



Surface  $S$  in Example 1

# 10.7 Triple Integrals. Divergence Theorem of Gauss

## ☑ Coordinate Invariance of the Divergence (발산의 좌표계 불변)

- Mean value theorem for triple integrals

For any continuous function  $f(x, y, z)$  in a bounded and simply connected region  $T$  there is a point  $Q:(x_0, y_0, z_0)$  in  $T$  such that

$$\iiint_T f(x, y, z) dV = f(x_0, y_0, z_0) V(T) \quad (V(T) = \text{volume of } T)$$

set  $f = \text{div}\mathbf{F}$   $\Rightarrow$   $\text{div}\mathbf{F}(x_0, y_0, z_0) = \frac{1}{V(T)} \iiint_T \text{div}\mathbf{F} dV = \frac{1}{V(T)} \iint_{S(T)} \mathbf{F} \cdot \mathbf{n} dA$

- Choose a point  $P:(x_1, y_1, z_1)$  in  $T$  and let  $T$  shrink down onto  $P$  such that maximum distance  $d(T)$  of the points of  $T$  from  $P$  goes to zero.
- Then  $Q:(x_0, y_0, z_0)$  must approach  $P$ .

$$\text{div}\mathbf{F}(P) = \lim_{d(T) \rightarrow 0} \frac{1}{V(T)} \iint_{S(T)} \mathbf{F} \cdot \mathbf{n} dA$$

# 10.7 Triple Integrals. Divergence Theorem of Gauss

## ☑ Theorem 2 Invariance of the Divergence

- The divergence of a vector function  $F$  with continuous first partial derivatives in a region  $T$  is independent of the particular choice of Cartesian coordinates. For any  $P$  in  $T$  it is given by

$$\operatorname{div}\mathbf{F}(P) = \lim_{d(T) \rightarrow 0} \frac{1}{V(T)} \iint_{S(T)} \mathbf{F} \cdot \mathbf{n} dA$$

⇒ *Definition of the divergence*

# 10.8 Further Applications of the Divergence Theorem

## ☑ Ex. 1 Fluid Flow. Physical Interpretation of the Divergence

- An intuitive interpretation of the divergence of a vector
  - The flow of an incompressible fluid of constant density  $\rho = 1$  which is steady (does not vary with time).
  - Such a flow is determined by the field of its velocity vector  $\mathbf{v}(P)$  at any point  $P$ .
  - Let  $S$  be the boundary surface of a region  $T$  in space, and  $\mathbf{n}$  be the outer unit normal vector of  $S$ .
- ✓ The total mass of fluid that flows across  $S$  from  $T$  to the outside per unit time

$$\iint_S \mathbf{v} \cdot \mathbf{n} dA$$

- ✓ The average flow out of  $T$ :  $\frac{1}{V} \iint_S \mathbf{v} \cdot \mathbf{n} dA$

# 10.8 Further Applications of the Divergence Theorem

## ☑ Ex. 1 Fluid Flow. Physical Interpretation of the Divergence

- The flow is steady and the fluid is incompressible

⇒ the amount of fluid flowing outward must be continuously supplied.

$\frac{1}{V} \iint_S \mathbf{v} \cdot \mathbf{n} dA \neq 0 \Rightarrow$  there must be sources in  $T$ , that is, points where fluid is produced or disappears.

- Let  $T$  shrink down to a fixed point  $P$  in  $T$ , we obtain the source intensity at  $P$

$$\operatorname{div} \mathbf{v}(P) = \lim_{d(T) \rightarrow 0} \frac{1}{V(T)} \iint_{S(T)} \mathbf{v} \cdot \mathbf{n} dA$$

⇒ The divergence of the velocity vector  $\mathbf{v}$  of a steady incompressible flow is the source intensity (생성 강도) of the flow at the corresponding point.

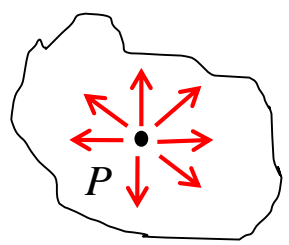
- If no sources in  $T$   $\iint_S \mathbf{v} \cdot \mathbf{n} dA = 0$



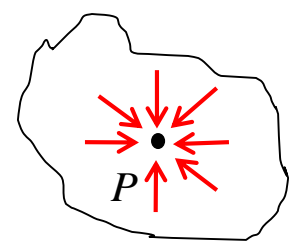
# [Reference] Source & Sink

$\nabla \cdot \mathbf{F} = 0$  : incompressible flow

$\nabla \cdot \mathbf{F} \neq 0$  : compressible flow



**Source**  
: Net outward flow  
( $\text{div } \mathbf{F}(P) > 0$ )

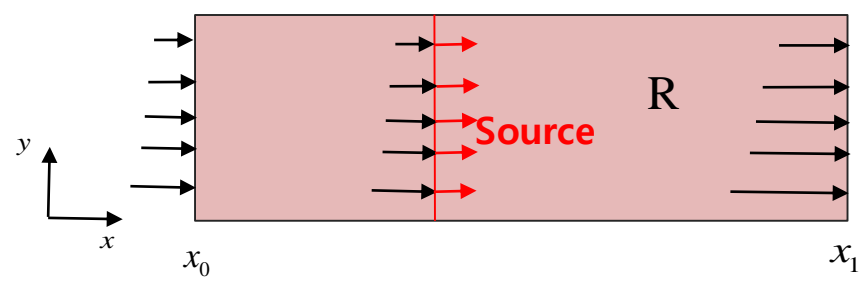


**Sink**  
: Net inward flow  
( $\text{div } \mathbf{F}(P) < 0$ )

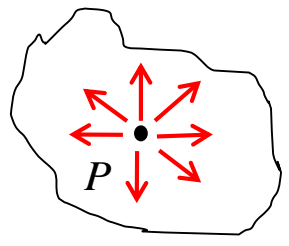
Generate a body shape by using Source and Sink

속도  $u$ 의 변화량

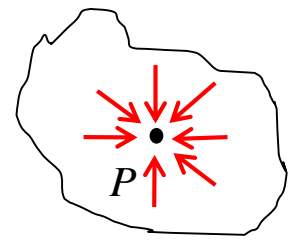
$$u(x_0, y) = \frac{\partial \phi}{\partial x}(x_0, y) \quad \frac{\partial u}{\partial x} = \frac{\partial^2 \phi}{\partial x^2} \quad u(x_1, y) = \frac{\partial \phi}{\partial x}(x_1, y)$$



# [Reference] Source & Sink



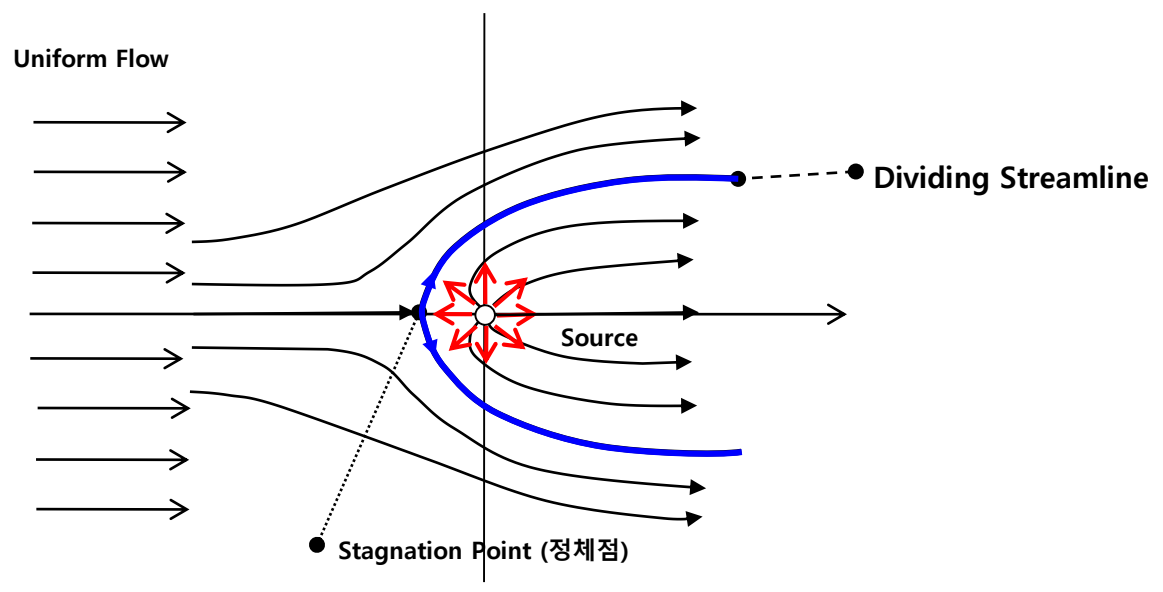
**Source**  
: Net outward flow  
( $\text{div } \mathbf{F}(P) > 0$ )



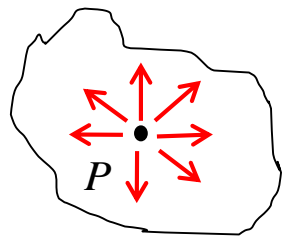
**Sink**  
: Net inward flow  
( $\text{div } \mathbf{F}(P) < 0$ )

Generate a body-like shape by using Source and Sink

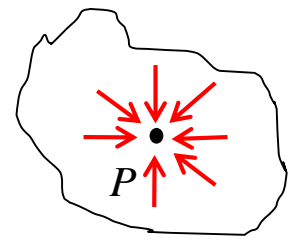
Half Body: Uniform Flow + Source



# [Reference] Source & Sink



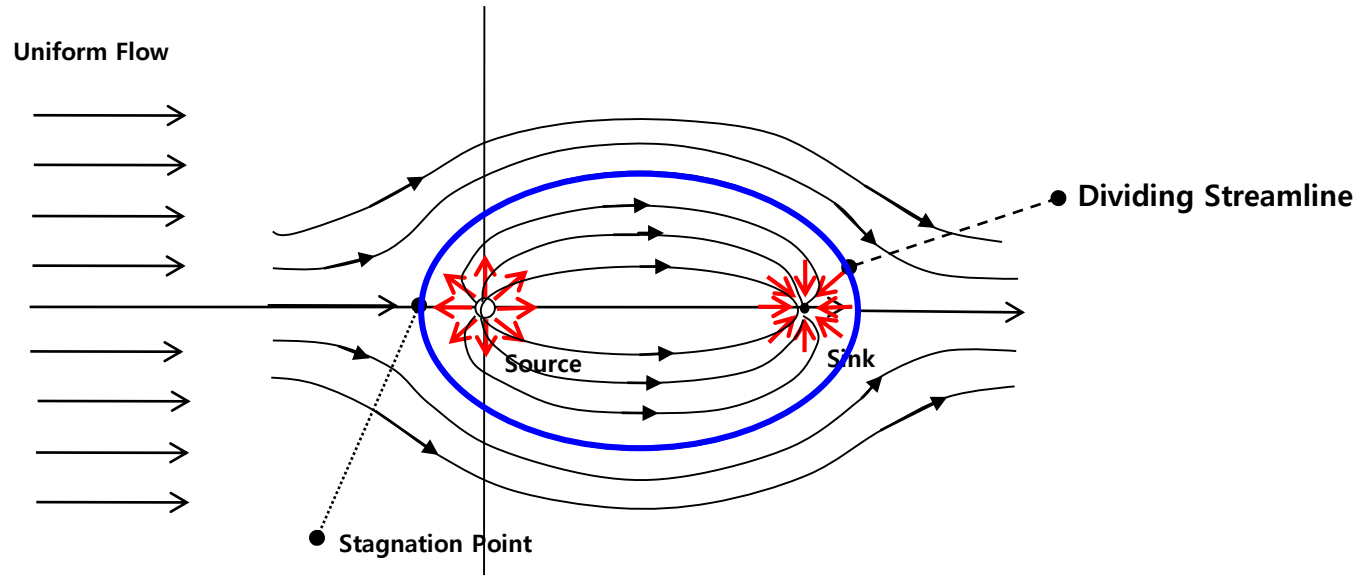
**Source**  
: Net outward flow  
( $\text{div } \mathbf{F}(P) > 0$ )



**Sink**  
: Net inward flow  
( $\text{div } \mathbf{F}(P) < 0$ )

Generate a body-like shape by using Source and Sink

Rankine Ovoid: Uniform Flow + Source + Sink



# 10.8 Further Applications of the Divergence Theorem

## ☑ Potential Theory. Harmonic Functions (조화함수)

- Laplace's equation: 
$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = 0$$
- Potential theory: The theory of solutions of Laplace's equation
- Harmonic function  
: A solution of Laplace's equation with continuous second-order partial derivatives

### ☑ Theorem 1 A Basic Property of Harmonic Functions

Let  $f(x, y, z)$  be a harmonic function in some domain  $D$  in space. Let  $S$  be any piecewise smooth closed orientable surface in  $D$  whose entire region it encloses belongs to  $D$ . Then the integral of the normal derivative of  $f$  taken over  $S$  is zero.

# 10.8 Further Applications of the Divergence Theorem

## ✓ Ex. 4 Green's Theorems

Let  $f$  and  $g$  be scalar functions such that  $\mathbf{F} = f \text{ grad } g$  satisfies the assumptions of the divergence theorem in some region  $T$ . Then

$$\begin{aligned} \text{div } \mathbf{F} &= \text{div} (f \text{ grad } g) = \text{div} \left[ \left[ f \frac{\partial g}{\partial x}, f \frac{\partial g}{\partial y}, f \frac{\partial g}{\partial z} \right] \right] \\ &= \left( \frac{\partial f}{\partial x} \frac{\partial g}{\partial x} + f \frac{\partial^2 g}{\partial x^2} \right) + \left( \frac{\partial f}{\partial y} \frac{\partial g}{\partial y} + f \frac{\partial^2 g}{\partial y^2} \right) + \left( \frac{\partial f}{\partial z} \frac{\partial g}{\partial z} + f \frac{\partial^2 g}{\partial z^2} \right) = f \nabla^2 g + \text{grad } f \bullet \text{grad } g \end{aligned}$$

Divergence theory

$$\iiint_T \text{div } \mathbf{F} dV = \iint_S \mathbf{F} \bullet \mathbf{n} dA \rightarrow \mathbf{F} \bullet \mathbf{n} = \mathbf{n} \bullet \mathbf{F} = \mathbf{n} \bullet (f \text{ grad } g) = (\mathbf{n} \bullet \text{grad } g) f$$

- Green's first formula:

$$\mathbf{n} \bullet \text{grad } g = \frac{\partial g}{\partial n} \text{ (directional derivative)} \Rightarrow \iiint_T (f \nabla^2 g + \text{grad } f \bullet \text{grad } g) dV = \iint_S f \frac{\partial g}{\partial n} dA$$

- For  $\mathbf{F} = g \text{ grad } f \Rightarrow \iiint_T (g \nabla^2 f + \text{grad } g \bullet \text{grad } f) dV = \iint_S g \frac{\partial f}{\partial n} dA$

- Green's second formula:  $\iiint_T (f \nabla^2 g - g \nabla^2 f) dV = \iint_S \left( f \frac{\partial g}{\partial n} - g \frac{\partial f}{\partial n} \right) dA$

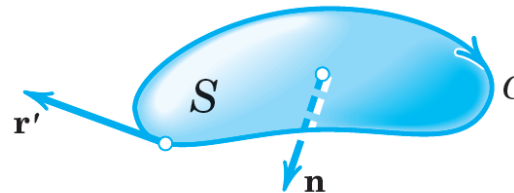
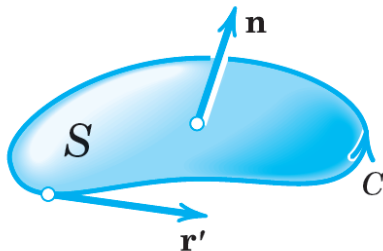
# 10.9 Stokes's Theorem

## ☑ Theorem 1 Stokes's Theorem

- $S$ : a piecewise smooth oriented surface in space  
the boundary of  $S$  be a piecewise smooth simple closed curve  $C$ .
- $F(x,y,z)$ : a continuous vector function that has continuous first partial derivatives in a domain in space containing  $S$ .

$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot d\mathbf{r} = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds$$

- ✓ Here  $\mathbf{n}$ : a unit normal vector of  $S$
- ✓  $\mathbf{r}' = d\mathbf{r}/ds$  is the unit tangent vector
- ✓  $s$ : the arc length of  $C$



# 10.9 Stokes's Theorem

## ☑ Theorem 1 Stokes's Theorem

- In components, formula becomes

$$\iint_R \left[ \left( \frac{\partial F_3}{\partial y} - \frac{\partial F_2}{\partial z} \right) N_1 + \left( \frac{\partial F_1}{\partial z} - \frac{\partial F_3}{\partial x} \right) N_2 + \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) N_3 \right] dudv = \oint_{\bar{C}} (F_1 dx + F_2 dy + F_3 dz)$$

- Here

$$\mathbf{F} = [F_1, F_2, F_3], \quad \mathbf{N} = [N_1, N_2, N_3], \quad \mathbf{n}dA = \mathbf{N}dudv, \quad \mathbf{r}' ds = [dx, dy, dz]$$

- $R$  is the region with boundary curve  $\bar{C}$  in the  $uv$ -plane corresponding to  $S$  represented by  $\mathbf{r}(u, v)$ .

# 10.9 Stokes's Theorem

☑ Green's Theorem: Double Integrals  $\Leftrightarrow$  Line Integrals

$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

☑ Gauss's Theorem (Divergence Theorem): Triple Integrals  $\Leftrightarrow$  Surface Integrals

$$\iiint_T \operatorname{div} \mathbf{F} dV = \iint_S \mathbf{F} \cdot \mathbf{n} dA$$

☑ Stokes's Theorem: Surface Integrals  $\Leftrightarrow$  Line Integrals  
(Generalization of Green's Theorem in the Plane)

$$\iint_S (\operatorname{curl} \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot d\mathbf{r} = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds$$



# 10.9 Stokes's Theorem

## ☑ Ex. 1 Verification of Stokes's Theorem

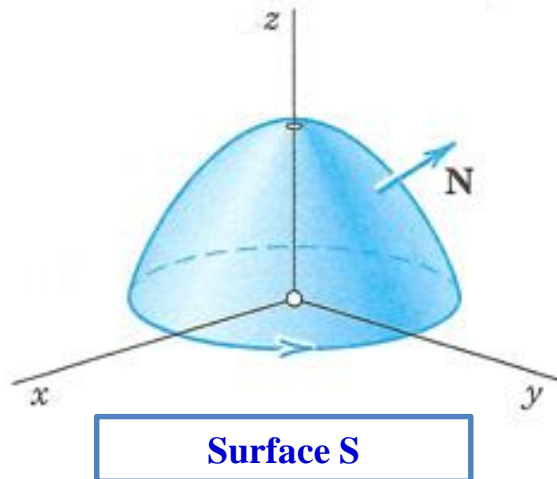
Let us first get used to it by verifying it for  $\mathbf{F} = [y, z, x]$  and  $S$  the paraboloid  $z = f(x,y) = 1 - (x^2 + y^2), z \geq 0$

Case 1. The curve  $C$  is the circle  $\mathbf{r}(s) = [\cos s, \sin s, 0]$

Its unit tangent vector:  $\mathbf{r}'(s) = [-\sin s, \cos s, 0]$

The function  $F$  on  $C$ :  $\mathbf{F}(\mathbf{r}(s)) = [\sin s, 0, \cos s]$

$$\therefore \oint_C \mathbf{F} \cdot d\mathbf{r} = \int_0^{2\pi} \mathbf{F}(\mathbf{r}(s)) \cdot \mathbf{r}'(s) ds = \int_0^{2\pi} [(\sin s)(-\sin s + 0 + 0)] ds = -\pi$$



$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds$$

# 10.9 Stokes's Theorem

## ☑ Ex. 1 Verification of Stokes's Theorem

Let us first get used to it by verifying it for  $\mathbf{F} = [y, z, x]$  and  $S$  the paraboloid  $z = f(x, y) = 1 - (x^2 + y^2), z \geq 0$

Case 2. The surface integral

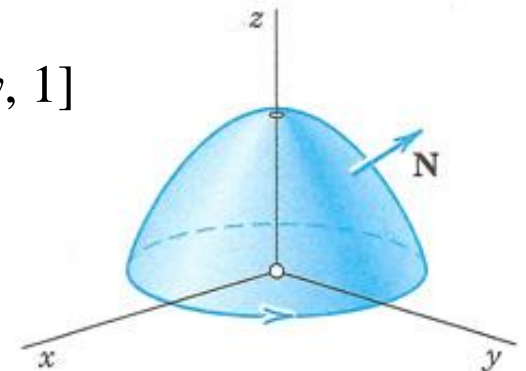
$$F_1 = y, F_2 = z, F_3 = x \Rightarrow \text{curl } \mathbf{F} = \text{curl}[F_1, F_2, F_3] = \text{curl}[y, z, x] = [-1, -1, -1]$$

A normal vector of  $S$ :  $\mathbf{N} = \text{grad}(z - f(x, y)) = [2x, 2y, 1]$

$$(\text{curl } \mathbf{F}) \cdot \mathbf{N} = -2x - 2y - 1$$

$$\therefore \iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \iint_R (\text{curl } \mathbf{F}) \cdot \mathbf{N} dx dy = \iint_R (-2x - 2y - 1) dx dy$$

$$= \int_{\theta=0}^{2\pi} \int_{r=0}^1 (-2r(\cos \theta + \sin \theta) - 1) r dr d\theta = \int_{\theta=0}^{2\pi} \left( -\frac{2}{3}(\cos \theta + \sin \theta) - \frac{1}{2} \right) d\theta = 0 + 0 - \frac{1}{2}(2\pi) = -\pi$$



# 10.9 Stokes's Theorem

## ✓ Proof

$$\iint_R \left[ \left( \frac{\partial F_3}{\partial y} - \frac{\partial F_2}{\partial z} \right) N_1 + \left( \frac{\partial F_1}{\partial z} - \frac{\partial F_3}{\partial x} \right) N_2 + \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) N_3 \right] dudv = \oint_{\bar{C}} (F_1 dx + F_2 dy + F_3 dz)$$

- If the integrals of each component on both sides are equal

$$\iint_R \left( \frac{\partial F_1}{\partial z} N_2 - \frac{\partial F_1}{\partial y} N_3 \right) dudv = \oint_{\bar{C}} F_1 dx$$

$$\iint_R \left( -\frac{\partial F_2}{\partial z} N_1 + \frac{\partial F_2}{\partial x} N_3 \right) dudv = \oint_{\bar{C}} F_2 dx$$

$$\iint_R \left( \frac{\partial F_3}{\partial y} N_1 - \frac{\partial F_3}{\partial x} N_2 \right) dudv = \oint_{\bar{C}} F_3 dx$$

# 10.9 Stokes's Theorem

## ✓ Proof

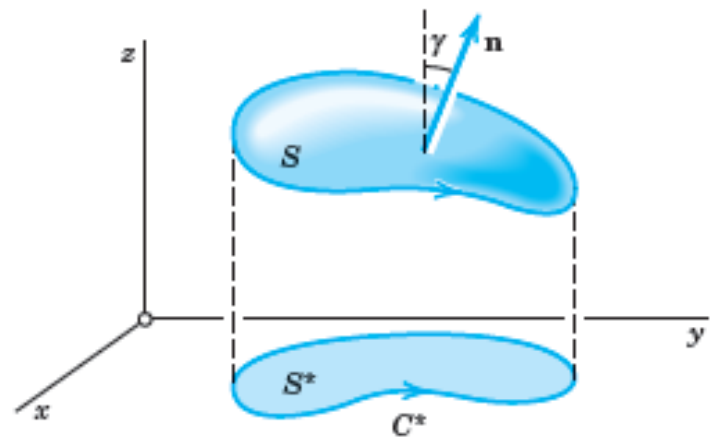
$$\iint_R \left( \frac{\partial F_1}{\partial z} N_2 - \frac{\partial F_1}{\partial y} N_3 \right) dudv = \oint_{\tilde{C}} F_1 dx$$

$$z = f(x, y)$$

$$u = x, v = y$$

$$\mathbf{r}(u, v) = \mathbf{r}(x, y) = [x, y, f(x, y)]$$

$$\mathbf{N} = \mathbf{r}_u \times \mathbf{r}_v = \mathbf{r}_x \times \mathbf{r}_y = [-f_x, -f_y, 1]$$



$$= \iint_{S^*} \left( \frac{\partial F_1}{\partial z} (-f_y) - \frac{\partial F_1}{\partial y} \right) dx dy$$

Green Theorem

$$\oint_{C^*} F_1 dx = \iint_{S^*} -\frac{\partial F_1}{\partial y} dx dy$$



$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

meanwhile, by chain rule,  $-\frac{\partial F_1(x, y, f(x, y))}{\partial y} = -\frac{\partial F_1(x, y, z)}{\partial y} - \frac{\partial F_1(x, y, z)}{\partial z} \frac{\partial f}{\partial y}$

$$\therefore \oint_{C^*} F_1 dx = \iint_{S^*} -\frac{\partial F_1}{\partial y} dx dy = \iint_{S^*} \left( \frac{\partial F_1}{\partial z} (-f_y) - \frac{\partial F_1}{\partial y} \right) dx dy = f_y$$

# 10.9 Stokes's Theorem

## ☑ Ex 2 Green's Theorem in the Plane ( $z = 0$ ) as a Special Case of Stokes's Theorem

- $\mathbf{F} = [F_1, F_2]$ : continuously differentiable in a domain in the  $xy$ -plane containing a simply connected bounded closed region  $S$  whose boundary  $C$  is a piecewise smooth simple closed curve.

$$\therefore (\text{curl } \mathbf{F}) \cdot \mathbf{n} = (\text{curl } \mathbf{F}) \cdot \mathbf{k} = \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y}$$

$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds = \oint_C (F_1 dx + F_2 dy + F_3 dz)$$

$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \iint_S \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dA = \oint_C (F_1 dx + F_2 dy)$$

- The same as Green Theorem

Green Theorem

$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

# 10.9 Stokes's Theorem

$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds = \oint_C (F_1 dx + F_2 dy + F_3 dz)$$

## ✓ Example 1

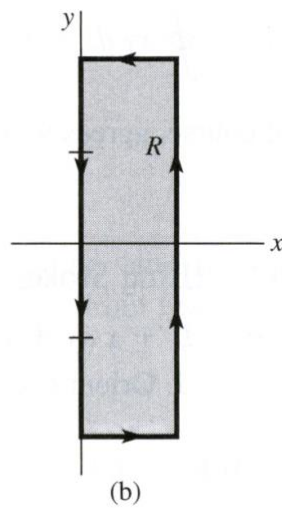
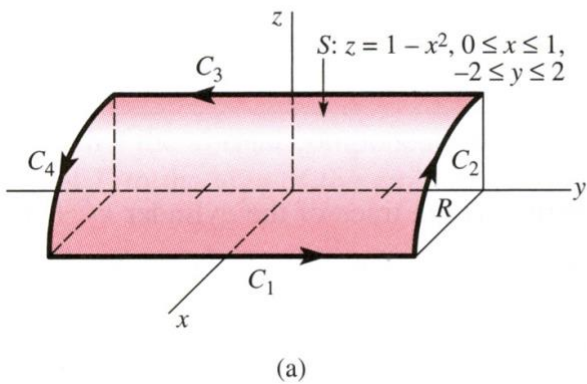
### Verifying Stokes's Theorem

Let  $S$  be the part of the cylinder

$$z = 1 - x^2 \text{ for } 0 \leq x \leq 1, -2 \leq y \leq 2.$$

Verify Stokes's theorem if

$$\mathbf{F} = xy\mathbf{i} + yz\mathbf{j} + xz\mathbf{k}$$



**Solution)** 1) Surface Integral

$$\mathbf{F} = xy\mathbf{i} + yz\mathbf{j} + xz\mathbf{k}$$

$$\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xy & yz & xz \end{vmatrix} = -y\mathbf{i} - z\mathbf{j} - x\mathbf{k}$$

$$g(x, y, z) = z + x^2 - 1 = 0$$

$$\mathbf{N} = \nabla g = 2x\mathbf{i} + \mathbf{k}$$

$$\begin{aligned} \iint_S (\text{curl } \mathbf{F} \cdot \mathbf{n}) dA &= \iint_R (\text{curl } \mathbf{F}) \cdot \mathbf{N} dx dy \\ &= \int_0^1 \int_{-2}^2 (-2xy - x) dy dx \\ &= \int_0^1 \left[ -xy^2 - xy \right]_{-2}^2 dx \\ &= \int_0^1 (-4x) dx = -2 \end{aligned}$$

# 10.9 Stokes's Theorem

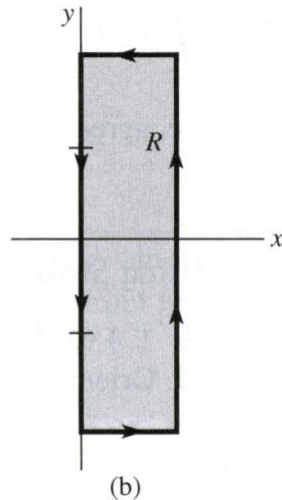
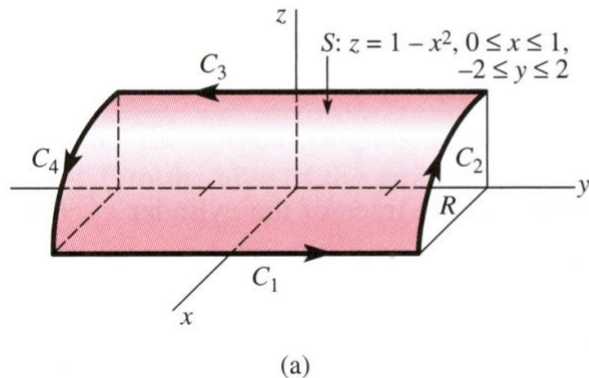
$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds = \oint_C (F_1 dx + F_2 dy + F_3 dz)$$

## ✓ Example 1

### Verifying Stokes's Theorem

Let  $S$  be the part of the cylinder  $z=1-x^2$  for  $0 \leq x \leq 1$ ,  $-2 \leq y \leq 2$ .

Verify Stokes' theorem if  $\mathbf{F} = xy\mathbf{i} + yz\mathbf{j} + xz\mathbf{k}$ .



**Solution)** 2) Line Integral

$$\oint_C = \int_{C_1} + \int_{C_2} + \int_{C_3} + \int_{C_4}$$

$$C_1 : x = 1, z = 0, dx = 0, dz = 0$$

$$\int_{C_1} 1 \cdot y \cdot 0 + y \cdot 0 dy + 1 \cdot 0 \cdot 0 = 0$$

$$C_2 : y = 2, z = 1 - x^2, dy = 0, dz = -2x dx$$

$$\int_{C_2} 2x dx + 2(1 - x^2) \cdot 0 + x(1 - x^2)(-2x dx)$$

$$= \int_1^0 (2x - 2x^2 + 2x^4) dx = -\frac{11}{15}$$

$$C_3 : x = 0, z = 1, dx = 0, dz = 0$$

$$\int_{C_3} 0 + y dy + 0 = \int_2^{-2} y dy = 0$$

$$C_4 : y = -2, z = 1 - x^2, dy = 0, dz = -2x dx$$

$$\int_{C_4} -2x dx - 2(1 - x^2) \cdot 0 + x(1 - x^2)(-2x) dx$$

$$= \int_0^1 (-2x - 2x^2 + 2x^4) dx = -\frac{19}{15}$$

$$\therefore \oint_C xy dx + yz + xz dz = 0 - \frac{11}{15} + 0 - \frac{19}{15} = -2$$

# 10.9 Stokes's Theorem

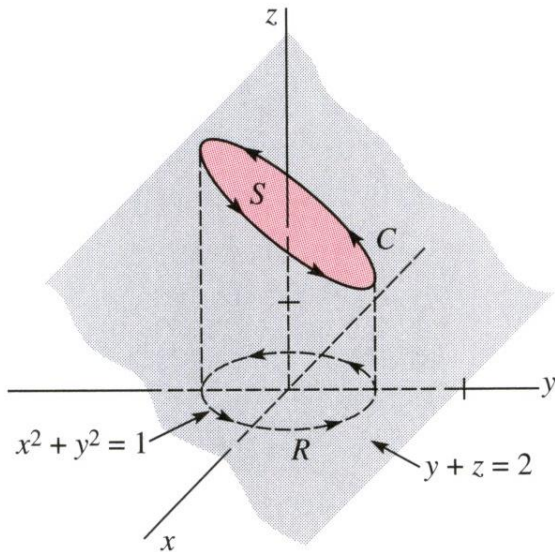
$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds = \oint_C (F_1 dx + F_2 dy + F_3 dz)$$

## ✓ Example 2

### Using Stokes's Theorem

Evaluate  $\oint_C z dx + x dy + y dz$ ,  
where  $C$  is the trace of the cylinder  
 $x^2 + y^2 = 1$  in the plane  $y + z = 2$ .

Orient  $C$  counterclockwise as viewed  
from above. See the Figure below



Solution)

$$\mathbf{F} = z\mathbf{i} + x\mathbf{j} + y\mathbf{k}$$

$$\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ z & x & y \end{vmatrix} = \mathbf{i} + \mathbf{j} + \mathbf{k}$$

$$g(x, y, z) = y + z - 2 = 0$$

$$\mathbf{N} = \nabla g = \mathbf{j} + \mathbf{k}$$

$$\begin{aligned} \oint_C \mathbf{F} \cdot d\mathbf{r} &= \iint_S (\text{curl } \mathbf{F} \cdot \mathbf{n}) dA \\ &= \iint_R (\text{curl } \mathbf{F}) \cdot \mathbf{N} dx dy \\ &= \iint_R [(\mathbf{i} + \mathbf{j} + \mathbf{k}) \cdot (\mathbf{j} + \mathbf{k})] dA \\ &= \iint_R 2 dA = 2\pi \end{aligned}$$

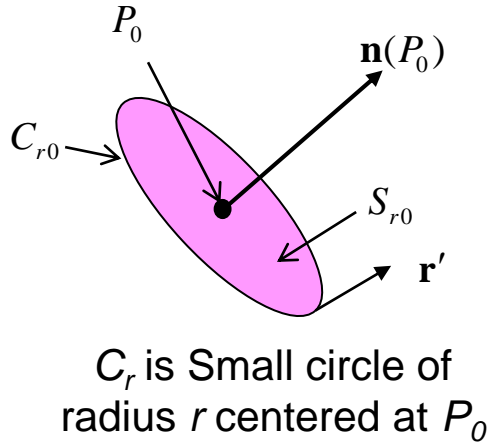


# 10.9 Stokes's Theorem

$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds = \oint_C \mathbf{F} \cdot d\mathbf{r}$$

## Ex. 4) Physical Interpretation of Curl

Mean value theorem for surface integrals



$C_r$  is Small circle of radius  $r$  centered at  $P_0$

$$\oint_{C_{r_0}} \mathbf{F} \cdot \mathbf{r}'(s) ds = \iint_{S_{r_0}} (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = (\text{curl } \mathbf{F}) \cdot \mathbf{n}(P^*) A_{r_0}$$

$P^*$  is a suitable point of  $S_{r_0}$ .

$$(\text{curl } \mathbf{F}) \cdot \mathbf{n}(P^*) = \frac{1}{A_{r_0}} \oint_{C_{r_0}} \mathbf{F} \cdot \mathbf{r}' ds$$

In case of a fluid motion with velocity vector  $\mathbf{F} = \mathbf{v}$ ,

$$\oint_{C_{r_0}} \mathbf{v} \cdot \mathbf{r}' ds \quad : \text{circulation of the flow around } C_{r_0}.$$

If we now let  $r_0$  approach zero.  $(\text{curl } \mathbf{v}) \cdot \mathbf{n}(P) = \lim_{r_0 \rightarrow 0} \frac{1}{A_{r_0}} \oint_{C_{r_0}} \mathbf{v} \cdot \mathbf{r}' ds$

The component of the curl in the positive normal direction

$\Rightarrow$  **specific circulation** (circulation per unit area) of the flow in the surface at the corresponding point

# Summary

☑ Green's Theorem

$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

$$\therefore \iint_R \nabla^2 \phi dx dy = \oint_C \frac{\partial \phi}{\partial n} ds$$

$$\iint_R \nabla^2 \phi dx dy = \int \int_{x_0}^{x_1} \frac{\partial^2 \phi}{\partial x^2} dx dy = \int \frac{\partial \phi}{\partial x} \Big|_{x_0}^{x_1} dy = \int u(x_1, y) - u(x_0, y) dy$$

속도의 변화량의 적분      양 경계에서의 단위시간당 속도차  
= 생성되는 유체의 양

경계를 통해 단위 시간당 빠져나가는 유체의 양

$$\oint_C \frac{\partial \phi}{\partial n} ds = \int -\frac{\partial \phi}{\partial x} \Big|_{x_0} + \frac{\partial \phi}{\partial x} \Big|_{x_1} dy = \int -u(x_0, y) + u(x_1, y) dy$$

▪ Surface Integral

$$\iint_S \mathbf{F} \cdot \mathbf{n} dA = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot \mathbf{N}(u, v) du dv$$

▪ Divergence Theorem of Gauss

$$\iiint_T \text{div } \mathbf{F} dV = \iint_S \mathbf{F} \cdot \mathbf{n} dA$$

$$\iiint_T \nabla^2 \phi dV = \iint_S \frac{\partial \phi}{\partial n} dA$$

$$\iiint_T \left( \frac{\partial F_1}{\partial x} + \frac{\partial F_2}{\partial y} + \frac{\partial F_3}{\partial z} \right) dx dy dz = \iint_S (F_1 \cos \alpha + F_2 \cos \beta + F_3 \cos \gamma) dA = \iint_S (F_1 dy dz + F_2 dz dx + F_3 dx dy)$$

Green's first formula

$$\iiint_T (f \nabla^2 g + \text{grad } f \cdot \text{grad } g) dV = \iint_S f \frac{\partial g}{\partial n} dA$$

Green's second formula

$$\iiint_T (f \nabla^2 g - g \nabla^2 f) dV = \iint_S \left( f \frac{\partial g}{\partial n} - g \frac{\partial f}{\partial n} \right) dA$$

# Summary

**Green's Theorem**

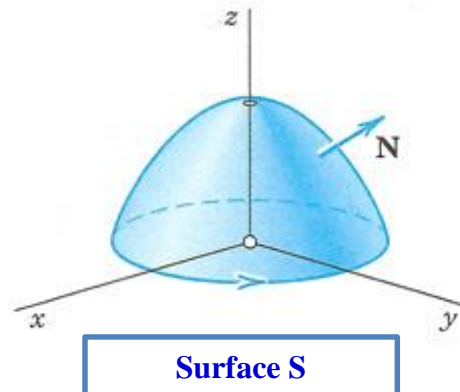
$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

$$\Rightarrow \iint_R (\text{curl } \mathbf{F}) \cdot \mathbf{k} dx dy = \oint_C \mathbf{F} \cdot d\mathbf{r}$$

**Stokes's Theorem**

$$\iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{n} dA = \iint_R (\text{curl } \mathbf{F}) \cdot \mathbf{N} dx dy = \oint_C \mathbf{F} \cdot d\mathbf{r} = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds$$

$$\iint_R \left[ \left( \frac{\partial F_3}{\partial y} - \frac{\partial F_2}{\partial z} \right) N_1 + \left( \frac{\partial F_1}{\partial z} - \frac{\partial F_3}{\partial x} \right) N_2 + \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) N_3 \right] dudv = \oint_C (F_1 dx + F_2 dy + F_3 dz)$$



# Summary

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## ☑ Green's Theorem: Double Integrals $\Leftrightarrow$ Line Integrals

$$\iint_R \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \oint_C (F_1 dx + F_2 dy)$$

## ☑ Gauss's Theorem (Divergence Theorem): Triple Integrals $\Leftrightarrow$ Surface Integrals

$$\iiint_T \operatorname{div} \mathbf{F} dV = \iint_S \mathbf{F} \cdot \mathbf{n} dA$$

## ☑ Stokes's Theorem: Surface Integrals $\Leftrightarrow$ Line Integrals (Generalization of Green's Theorem in the Plane)

$$\iint_S (\operatorname{curl} \mathbf{F}) \cdot \mathbf{n} dA = \oint_C \mathbf{F} \cdot d\mathbf{r} = \oint_C \mathbf{F} \cdot \mathbf{r}'(s) ds$$