3. Analyzing strain: Definitions and Concepts

3.1 Introduction

- Strain
 - The nature of deformations experienced by a real deformable body as a result of internal force or stress distributions will be studied.
 - Methods to measure or compute deformations will be established.

- Displacement
 - Movement of a point with respect to some convenient reference system of axes
 - Vector quantity: from A to A', (u_A, v_A)
 - Associated with a translation/rotation and change in size/shape
- Deformation

 $-\delta_{AB} = L_f - L_i$

- Change in any dimension associated with relative displacements (δ)

- Strain
 - A quantity used to measure the intensity of a deformation
 - Normal strain: rate of elongation or contraction of a line segment (ε)
 - Shear strain: change in angle between two lines that are orthogonal

in the undeformed state (γ)

• Average axial strain

$$\varepsilon_{avg} = \frac{\delta_n}{L}$$

• Axial strain at a point

$$\varepsilon(p) = \lim_{\Delta L \to 0} \frac{\Delta \delta_n}{\Delta L} = \frac{d \delta_n}{dL}$$





• Shearing Strain

$$\gamma_{avg} = \frac{\delta_s}{L} = \tan \phi \approx \phi$$
$$\gamma_{xy}(p) = \lim_{\Delta L \to 0} \frac{\Delta \delta_s}{\Delta L} = \frac{d\delta_s}{dL} = \frac{\pi}{2} - \theta^{2}$$

- Sign convention of strains
 Normal strain: tensile strain (+) compressive strain (-)
 - Shear strain: increased angle (-) decreased angel (+)



• Example problem 3-1

There is a bar which is of 1-in.-diameter and 8-ft-length. It has 0.5 in.-diameter in a 2-ft central portion. Axial strain in the central portion is 960 μ in./in., total elongation of the bar is 0.04032 in., and the diameter of the central portion is 0.49986 in. when an axial load is applied to the ends of the bar.

- The elongation of the central portion of the bar
- The axial strain in the end portions of the bar
- The diametral strain in the central portion of the bar
- Example problem 3-2 The shear force V produces an average shearing strain γ_{avg} of 1000 µrad.
 - Horizontal displacement of point A



3.3 The state of strain at a point

• State of strain

- Completely determined by defining 3 normal strains and 3 shear strains on the faces of a rectangular parallelepiped



3.4 The strain transformation equations for plane strain

• Normal strain

$$(OB')^{2} = (OC')^{2} + (C'B')^{2} - 2(OC')(C'B')\cos\left(\frac{\pi}{2} + \gamma_{xy}\right)$$

$$\rightarrow [(1 + \varepsilon_{n})dn]^{2} = [(1 + \varepsilon_{x})dx]^{2} + [(1 + \varepsilon_{y})dy]^{2}$$

$$- 2[(1 + \varepsilon_{x})dx][(1 + \varepsilon_{y})dy][-\sin\gamma_{xy}]$$

Substituti ng $dx = dn \cos\theta$ and $dy = dn \sin\theta$
 $(1 + \varepsilon_{n})^{2} dn^{2} = (1 + \varepsilon_{x})^{2} dn^{2} \cos^{2}\theta + (1 + \varepsilon_{y})^{2} dn^{2} \sin^{2}\theta$

$$+ 2dn^{2} \sin\theta \cos\theta(1 + \varepsilon_{x})(1 + \varepsilon_{y})\sin\gamma_{xy}$$

$$\rightarrow 1 + 2\varepsilon_{n} = (1 + 2\varepsilon_{x})\cos^{2}\theta + (1 + 2\varepsilon_{y})\sin^{2}\theta + 2\gamma_{xy}\sin\theta\cos\theta$$

$$\varepsilon_{n} = \varepsilon_{x}\cos^{2}\theta + \varepsilon_{y}\sin^{2}\theta + \gamma_{xy}\sin\theta\cos\theta$$

$$\rightarrow \varepsilon_{n} = \frac{\varepsilon_{x} + \varepsilon_{y}}{2} + \frac{\varepsilon_{x} - \varepsilon_{y}}{2}\cos2\theta + \frac{\gamma_{xy}}{2}\sin2\theta$$



3.4 The strain transformation equations for plane strain

• Shear strain

$$\gamma_{nt} = -(\varepsilon_x - \varepsilon_y)\sin 2\theta + \gamma_{xy}\cos 2\theta$$
$$\left(\text{c.f. } \tau_{nt} = -\frac{\sigma_x - \sigma_y}{2}\sin 2\theta + \tau_{xy}\cos 2\theta\right)$$

- Sign convention
- Tensile strains are positive; compressive strains are negative
- Shearing strains that decrease the angle between two lines are positive
- Angles measured counterclockwise from the x-axis are positive

3.4 The strain transformation equations for plane strain

• Example problem 3-4

 $\varepsilon_x = 800 \,\mu, \quad \varepsilon_y = -1000 \,\mu, \quad \text{and} \quad \gamma_{xy} = -600 \,\mu$ Determine $\varepsilon_n, \ \varepsilon_t, \text{ and } \ \gamma_{nt}$



3.5 Principal strains and maximum shear strain

$$\tan 2\theta_{p} = \frac{\gamma_{xy}}{\varepsilon_{x} - \varepsilon_{y}} \left(\text{c.f. } \tan 2\theta_{p} = \frac{2\tau_{xy}}{\sigma_{x} - \sigma_{y}} \right)$$
$$\varepsilon_{p1,p2} = \frac{\varepsilon_{x} + \varepsilon_{y}}{2} \pm \sqrt{\left(\frac{\varepsilon_{x} - \varepsilon_{y}}{2}\right)^{2} + \left(\frac{\gamma_{xy}}{2}\right)^{2}} \left(\text{c.f. } \sigma_{p1,p2} = \frac{\sigma_{x} + \sigma_{y}}{2} \pm \sqrt{\left(\frac{\sigma_{x} - \sigma_{y}}{2}\right)^{2} + \tau_{xy}^{2}} \right)$$
$$\gamma_{\text{max}} = 2\sqrt{\left(\frac{\varepsilon_{x} - \varepsilon_{y}}{2}\right)^{2} + \left(\frac{\gamma_{xy}}{2}\right)^{2}} \left(\text{c.f. } \tau_{\text{max}} = \sqrt{\left(\frac{\sigma_{x} - \sigma_{y}}{2}\right)^{2} + \tau_{xy}^{2}} \right)$$



3.5 Principal strains and maximum shear strain

• Example problem 3-5

 $\varepsilon_x = 1200 \,\mu, \quad \varepsilon_y = -600 \,\mu, \quad \text{and} \quad \gamma_{xy} = 900 \,\mu$

Determine principal strains and the maximum shear strain

3.6 Mohr's circle for plane strain

$$\left(\varepsilon_{n} - \frac{\varepsilon_{x} + \varepsilon_{y}}{2}\right)^{2} + \left(\frac{\gamma_{nt}}{2}\right)^{2} = \left(\frac{\varepsilon_{x} - \varepsilon_{y}}{2}\right)^{2} + \left(\frac{\gamma_{xy}}{2}\right)^{2}$$
$$R = \sqrt{\left(\frac{\varepsilon_{x} - \varepsilon_{y}}{2}\right)^{2} + \left(\frac{\gamma_{xy}}{2}\right)^{2}}$$



3.7 Strain measurement and rosette analysis

- Normal strain is not affected by the presence of the out-of-plane displacements: strains for a plane strain case are valid for a plane stress case

$$(A'B')^{2} = (L + \delta_{AB})^{2} = (L + du)^{2} + (dv)^{2} + (dw)^{2}$$
$$L^{2} + 2L\delta_{AB} + \delta_{AB}^{2} = L^{2} + 2Ldu + (du)^{2} + (dv)^{2} + (dw)^{2}$$

Neglecting the second - degree terms

 $\delta_{AB} = du$



3.7 Strain measurement and rosette analysis

- The electrical resistance strain gages are sensitive only to normal strains: shear strains are obtained by measuring normal strains in two or three different directions

$$\varepsilon_{a} = \varepsilon_{x} \cos^{2} \theta_{a} + \varepsilon_{y} \sin^{2} \theta_{a} + \gamma_{xy} \sin \theta_{a} \cos \theta_{a}$$
$$\varepsilon_{b} = \varepsilon_{x} \cos^{2} \theta_{b} + \varepsilon_{y} \sin^{2} \theta_{b} + \gamma_{xy} \sin \theta_{b} \cos \theta_{b}$$
$$\varepsilon_{c} = \varepsilon_{x} \cos^{2} \theta_{c} + \varepsilon_{y} \sin^{2} \theta_{c} + \gamma_{xy} \sin \theta_{c} \cos \theta_{c}$$

- The out-of-plane principal strain should be considered to obtain the maximum shear strains

$$\gamma_{\max} = \left(\varepsilon_{p\max} - \varepsilon_{p\min}\right) : \left(\varepsilon_{p1} - \varepsilon_{p2}\right), \quad \left(\varepsilon_{p1} - \varepsilon_{p3}\right), \quad \text{or} \quad \left(\varepsilon_{p3} - \varepsilon_{p2}\right)$$
$$\varepsilon_{p3} = -\frac{V}{1 - V} \left(\varepsilon_{x} + \varepsilon_{y}\right)$$





3.7 Strain measurement and rosette analysis

- Example problem 3-7
- Principal strains and the maximum shear strain with their orientations on a sketch

Poisson's ratio is 1/3.

 $\varepsilon_a = 1000 \,\mu$ $\varepsilon_b = 750 \,\mu$ $\varepsilon_c = -650 \,\mu$

