Lecture Note #14 (Spring, 2022)

Industrial electrolysis

- 1. Industrial electrolysis
- 2. Electrochemical reactors
- 3. Redox-flow battery

Fuller & Harb (textbook), ch.14, Pletcher, ch.3, Oh, ch.11

Industrial electrochemistry

- Industrial electrolytic processes consume about 6% of US electricity

Industrial electrolysis

- to use electrical energy to convert raw materials into desired products - e.g. the production of aluminum, chloro-alkali process \rightarrow 90% of the electricity used in all electrolytic processes

- Chloro-alkali process

 $\begin{array}{lll} 2\text{CI}^{-}\rightarrow\text{CI}_{2}+2\text{e}^{-} & \text{E}^{0}=1.3595 \text{ V} \\ 2\text{H}_{2}\text{O}+2\text{e}^{-}\rightarrow\text{H}_{2}+2\text{OH}^{-} & \text{E}^{0}=-0.828 \text{ V} \\ \text{Standard potential for full cell}:2.188 \text{ V} \end{array}$

Fig. 14.1 : a diaphragm cell

Illustration 14.1



Figure 14.1 Diaphragm cell for the production of chlorine and caustic soda.





From Asahi Kasei

Chloro-alkali process







| Chlor-alkali industry9-13 | Extraction of chlorine and sodium hydroxide from NaCl | | | |
|---|--|--|--|--|
| Metal extraction | Aluminium (Hall–Heroult process)^{14–16} Sodium, magnesium, lithium (electrolysis of the fused salts) Electrolysis in aqueous solution (principally copper and zinc) | | | |
| Electrolysis in the preparation of inorganic compounds ¹⁷ | Strong oxidizing agents: KMnO₄, K₂Cr₂O₇, Na₂S₂O₈, F₂, NaClO₃. Active metal oxides: MnO₂, Cu₂O Hydrogen and oxygen by water electrolysis¹⁸⁻²⁰ | | | |
| Electro-organic synthesis ^{21–24} | Hydrodimerization of acrylonitrile (Monsanto process) Direct processes e.g. reduction Me₂CO→i-PrOH Indirect processes—an inorganic reagent is used as catalyst, being oxidized or reduced at the electrode to give a species that reacts with the organic compound e.g. Electrode(Pb): Cr³⁺→Cr₂O₇²⁻ Solution: Cr₂O₇²⁻ + anthracene→ anthraquinone + Cr³⁺ | | | |

Table 15.1. Industrial electrolysis and electrosynthesis

C. M. A. Brett, A. M. O. Brett, Electrochemistry, Oxford, 1994.



Figure 14.2 Transport in diaphragm separator of a chlor-alkali cell. (a) Movement of species and potential gradient. (b) Concentration profiles.

Performance measures

(1) Faradaic efficiency : the ratio of the product mass to the amount that could be obtained based on the current and Faraday's law

 η_f = mass of product / theoretical mass from Faraday's law = $m_i / (QM_i / nF) = \dot{m}_i / (IM_i / nF)$

m_i: mass of the product, Q: total charge passed during electrolysis, m_i: mass flow rate of the desired product, I: total current, M_i: molecular weight

- η_f for the Cl₂ reaction for a diaphragm cell ~0.96 or 96% to use electrical energy to convert raw materials into desired products - Lower η_f for side reactions, contaminants (that react with the desired products) (2) Space-time yield : the rate of production per volume of reactor \rightarrow reactor efficiency

 $Y = \dot{m}_i / V_R = \eta_f x (IM_i / nF) / V_R = \eta_f x (ia_r M_i / nF)$

 a_r (specific area for the reactor) \to area of the electrode at which the production takes place divided by volume of the reactor, \bm{V}_R : the reactor volume

- Y unit: kg·s⁻¹m⁻³
- ia_r: current per unit volume of the reactor

(3) Energy efficiency : the product of the faradaic efficiency and the ratio of the equilibrium potential to the cell potential

 $\eta_{energy} = \eta_f \mathbf{x} (\mathbf{E}^0 / \mathbf{E}_{cell})$

 E^0 / E_{cell} : voltage efficiency defined for an electrolytic cell (η_V)

- η_{energy} : the theoretical power required to complete the chemical conversion ($I_{Rx}E^{0}$) divided by the actual power used (IV_{cell}) $V_{cell} = E_{cell}$

Illustration 14.2, 14.3, 14.4

Voltage losses and the polarization curve

- Relationship between the potential of the cell and the current density for an electrolytic cell

 $E_{cell} = E_{cell}^{0} + |\eta_{s,anode}| + |\eta_{s,cathode}| + |\eta_{conc,anode}| + |\eta_{conc,cathode}| + |\eta_{ohmic}|$

 $η_s$: surface overpotential (E-E⁰) $η_{ohmic}$ = ih / κ = iR_Ω, h: a gap of distance

- For a diaphragm cell, $R_{\Omega}[\Omega \cdot m^{2}] = h_{a} / \kappa + h_{d}\tau / \kappa\epsilon_{d} + h_{c} / \kappa + R_{leads}$



T, tortuosity ε_{c}

ε_d, porosity





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Figure 5.4 Tortuous path through porous media





- Gas evolution \rightarrow increasing ohmic loss

$$\kappa_{eff} = \kappa (1 - \epsilon_g)^{3/2}$$

 ϵ_g : volume fraction of gas

For a diaphragm cell, $R_{\Omega}[\Omega \cdot m^{2}] = h_{a} / \kappa + h_{d}T / \kappa \epsilon_{d} + h_{c} / \kappa + R_{leads}$



Figure 14.5 Polarization in an operating diaphragm chlor-alkali cell.

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Figure 14.4 Evolution of gas on an electrode.

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Illustration 14.5

Dimensionally stable anode (DSA)

- One of the most significant advancements in industrial electrochemistry is the development of stable oxide electrodes or DSA. The first anodes for chloro-alkali were carbon and then graphite, both of which were consumed over time, increasing the electrode gap and requiring costly maintenance. Titanium is stable in the harsh environment of chloro-alkali cell, but forms a nonconducting oxide. The key innovation was the application of conductive oxides on Ti to produce a "nonconsumable," dimensionally stable electrode. Also, with titanium as a support, the electrode could be constructed in the form of meshes and expanded metals. The open structure allowed gases to be removed more easily, thus allowing the gap to be reduced.



From Wikipedia

Design of electrochemical reactors



Figure 14.6 Trade-off between size and efficiency is essential part of design.

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| Variable | Units | Description | Comments | |
|--|---|---|---|--|
| $\overline{\dot{m}_i}$ kg·s ⁻¹ metric tons·yr ⁻¹ | | Rate of production of desired material | Size scales with production rate | |
| i V _{cell} Nenersy | $A \cdot m^{-2}$ V become and a let | Current density Potential of an individual cell Energy efficiency | These three along with the <i>configuration</i> of the cell would be optimized simultaneously | |
| A | m ² | Total electrode area, sometimes referred to as the separator area | Follows directly from Faraday's law once <i>i</i> is established | |
| V_s | \mathbf{v} which is a set in the set of the set | Voltage of the DC power system | | |
| m | i <u>z</u> nociasti ustrifiant to ^s | Number of cells that are connected in series | Follows directly, $m = \frac{V_s}{V_{cell}}$ | |
| A _c | m ² | Area of individual electrodes | Cells may be placed in parallel | |

Table 14.1 Eight Key Variables for an Electrochemical Reactor

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Illustration 14.6

Electrical configurations

- Number of series connections is established from the system voltage (V_s) and potential of an individual cell (V_{cell})

number of cells in series = $m = V_s / V_{cell}$ (14.17)

- Two general methods for making electrical connections: monopolar and bipolar

(1) monopolar: a separate electrical connection is made to each electrode. Many electrode pairs can be combined in a single cell. All the anodes are at the same potential, as are all of the cathodes. The voltage between each anode and cathode pair is the same and equal to the cell voltage.

(2) bipolar: current in a bipolar stack flows straight through the stack. Failure of one cell results in failure of the entire stack. It is possible for a portion of the current to skip one or more cells and flow directly to another cell downstream, referred as a *bypass* or *shunt current*.

 \rightarrow standard in fuel cells and redox-flow batteries, but used less frequently in industrial electrolysis

Illustration 14.7





Flow configurations

- Industrial electrochemical reactors are usually flow reactors \rightarrow streams of reactants into and out of the reactor

- Two principal flow arrangements: parallel flow and series flow
- (1) Parallel flow: a lower pressure drop
- (2) Series flow: problem associated gas evolution
- \rightarrow hybrids of parallel and series possible







Figure 14.8 Basic flow arrangements. (a) Parallel flow. (b) Series flow.

Reactor volume

- Specific area of reactor (a_r)

- Cell pitch: the number of electrode pairs per unit length when the repeating units are stacked together

cell pitch = 1 / center to center distance between electrodes of the same type

 $a_r = electrode area / total volume$

= 2(length)(width) / [(length)(width)/cell pitch] = 2 x cell pitch

- the factor of 2 accounts for the two active faces of the electrode

Illustration 14.9

Scale up



Figure 14.9 One possible scale-up process from fundamental electrochemistry to prototype reactor.



Figure 14.10 Plate-and-frame system that is commercially available for process evaluation. Image provided by ElectroCell A/S.

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u = amount reacted / amount suppliedu: utilizationA_c: full size

Examples of industrial electrolytic processes

Synthesis of inorganic chemicals

- The largest electrolytic industry: chloro-alkali process \rightarrow chlorine, sodium hydroxide, (hydrogen) from a salt solution \rightarrow two types of cells dominated: diaphragm cell, mercury cell \rightarrow third type (new type): a membrane cell

- Production of chlorine and hydrogen from hydrochloric acid using diaphragm cell and membrane cell \rightarrow process converting byproduct HCl due to serious environmental concerns

- Other examples of industrial electrolysis: fluorine gas, strong oxidizing agents such as KMnO₄, H₂O₂, Na₂S₂O₈(sodium persulfate) \rightarrow recently, hydrogen peroxide(H₂O₂) has been produced in situ by electrolysis at the quantity needed for optimal use

- MnO₂ production by electrolysis for battery applications
- Hot issue: water electrolysis to produce hydrogen and oxygen gas at high purity

Chlor-Alkali Production by Process Type



Hydrogen Peroxide(과산화수소)



Global Hydrogen Peroxide Market



Market Share by Application (%)

Electrowinning of metals 전해제련

- The production of metals from ores by electrodeposition from a melt or solution

- The most important industrial electrowinning process: production of aluminum using Hall-Heroult process

$$2AI_2O_3 + 3C \rightarrow 4AI + 3CO_2$$

- Li, Mg, Na from a molten salt (typically chloride-based salts)
- Cu, Zn from aqueous solutions

Illustration 14.10



Figure 14.11 Hall–Héroult process for the production of aluminum.

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Hall-Heroult Cell

Cathode: $4AI^{3+} + 12e^{-} \rightarrow 4AI$ Anode: $6O^{2-} + 3C \rightarrow 3CO_2 + 12e^{-}$ Overall: $2AI_2O_3 + 3C \rightarrow 4AI + 3CO_2$



Electrorefining

- To purify the metal (rather than to recover the metal)
- Cu: Cu anode is dissolved and Cu is plated at the cathode \rightarrow active impurities are dissolved but not plated at the cathode \rightarrow high purity copper at the cathode (e.g. 99.999%)
- Ni, Co, Pb, Sn in aqueous solution
- Al in a molten salt electrolyte

Electrosynthesis of organic compounds

- Types of reactions: oxidation and reduction of functional groups, cleavage, substitutions (e.g. halogenation), additions (e.g. hydrogenation), coupling (e.g. dimerization), rearrangement

Reductions: Sn^{4+/}Sn²⁺, Cr³⁺/Cr²⁺, Ti⁴⁺/Ti³⁺, Zn²⁺/Zn, Na⁺/NaHg Oxidations: Ce³⁺/Ce⁴⁺, Cr³⁺/Cr⁶⁺, Mn²⁺/Mn³⁺, Mn²⁺/ Mn⁴⁺, Ni (OH)₂/NiOOH, I⁻/I₂,Br⁻/Br₂,Cl⁻/ClO⁻

- The most significant industrial process: production of adiponitrile, an intermediate in the production of Nylon

 \rightarrow cathode reaction: electro-hydro-dimerization of acrylonitrile, and oxygen is evolved at the anode (using aqueous sulfuric acid electrolyte)

 $\begin{array}{l} 2\text{CH}_2\text{CHCN}+2\text{H}^++2\text{e}^-\rightarrow\text{NC}(\text{CH}_2)_4\text{CN}\\ \text{H}_2\text{O}\rightarrow2\text{H}^++0.5\text{O}_2+2\text{e}^-\\ \text{Overall reaction: } 2\text{CH}_2\text{CHCN}+\text{H}_2\text{O}\rightarrow0.5\text{O}_2+\text{NC}(\text{CH}_2)_4\text{CN} \end{array}$

- Electrochemical synthesis of ethylene glycol

Illustration 14.11

Thermal management and cell operation



Figure 14.12 Process diagram for Zn electrowinning that emphasizes cooling of the electrolyte.

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energy balance

 $mC_p \frac{dT}{dt} = \sum_m \dot{n}_m H_{in,m} - \sum_p \dot{n}_p H_{out,p} + \dot{q} - \dot{W}$ $-\sum_i r_i \Delta H_{Rx,j}, \qquad (14.22)$

where

m = mass of the system, assumed constant [kg] $C_p = \text{average heat capacity of the system [J \cdot kg^{-1} \cdot K^{-1}]}$ $H_{out,p} = \text{enthalpy of outlet stream } p \text{ [J \cdot mol^{-1}]}$ $H_{in,m} = \text{enthalpy of inlet stream } m \text{ [J \cdot mol^{-1}]}$ $\dot{n}_m = \text{molar flowrate of inlet stream } m, \text{ [mol \cdot s^{-1}]}$ $\dot{n}_p = \text{molar flowrate of outlet stream } p, \text{ [mol \cdot s^{-1}]}$ $\dot{q} = \text{heat transferred to the system from the environment } [W]$ $\dot{W} = \text{Rate of work done by the system on the environment } [W]$ $r_i = \text{Rate of reaction of species } i \text{ [mol \cdot s^{-1}]}$

 $\Delta H_{Rx,j}$ = Heat of reaction *j* per mole of species *i* [J·mol⁻¹]

Electrolytic processes for a sustainable future

Electrolytic fuel generation

- Solar fuels such as hydrogen: Hydrogen production using photoelectrochemical cell (ch.15 in the textbook)

Water electrolysis

- A fuel cell in reverse \rightarrow three principal types of electrolyzers: alkaline, PEM(proton exchange membrane), solid oxide

- Alkaline electrolyzer: most commercial water electrolyzer

Cathode: $2H_2O + 2e^- \rightarrow H_2 + 2OH^-$ Anode: $2OH^- \rightarrow 0.5O_2 + H_2O + 2e^-$

- Water electrolysis as a function of T \rightarrow T $\uparrow \rightarrow$ potential \downarrow



Figure 14.13 Equilibrium and thermoneutral potentials assuming gaseous water.

- Voltage losses as a function of current density in a typical alkaline electrolyzer \rightarrow overpotentials for both the anodic and cathodic reactions are significant, ohmic losses become more important at the high current densities

- Commercial electrolyzers typically operate at below 2 V and current densities between 1000 and 3000 A-m²

(note at 25°C, E = 1.229 V, and thermoneutral potential is 1.481 V assuming liquid water)

- electrolyte: 25-30% KOH
- 60~100°C, >15 years

Illustration 14.13



Figure 14.14 Electrolysis of water at 40 °C. *Source:* Adapted from Ulleberg 2003.

- PEM(proton exchange membrane) electrolyzer: similar to PEM fuel cell Cathode: $2H^+ + 2e^- \rightarrow H_2$ Anode: $H_2O \rightarrow 0.5O_2 + 2H^+ + 2e^-$

- Solid oxide electrolyzer: similar to solid oxide fuel cell \rightarrow operate at high T and utilize a solid, ceramic O²⁻ conducting electrolyte

Cathode: $H_2O + 2e^- \rightarrow H_2 + O^{2-}$ Anode: $O^{2-} \rightarrow 0.5O_2 + 2e^-$

Electrolyser Systems



Table 1.Characterisation of the four types of water electrolysers.

Blue color: low technology maturity

| | Alkaline | PEM | AEM | Solid Oxide |
|---|--|--|---|---|
| Operating temperature | 70-90 °C | 50-80 °C | 40-60 °C | 700-850 °C |
| Operating pressure | 1-30 bar | < 70 bar | < 35 bar | 1 bar |
| Electrolyte | Potassium hydroxide (KOH) 5-7 molL ⁻¹ | PFSA membranes | DVB polymer support with | Yttria-stabilized Zirconia (YSZ) |
| | | | KOH or NaHCO3 1molL ⁻¹ | |
| Separator | ZrO ₂ stabilized with PPS mesh | Solid electrolyte (above) | Solid electrolyte (above) | Solid electrolyte (above) |
| Electrode / catalyst (oxygen side) | Nickel coated perforated stainless steel | Iridium oxide | High surface area Nickel or NiFeCo alloys | Perovskite-type (<i>e.g.</i> LSCF, LSM) |
| Electrode / catalyst (hydrogen side) | Nickel coated perforated stainless steel | Platinum nanoparticles on carbon black | High surface area nickel | Ni/YSZ |
| Porous transport layer anode | Nickel mesh (not always present) | Platinum coated sintered porous titanium | Nickel foam | Coarse Nickel-mesh or foam |
| Porous transport layer cathode | Nickel mesh | Sintered porous titanium or carbon cloth | Nickel foam or carbon Cloth | None |
| Bipolar plate anode | Nickel-coated stainless steel | Platinum-coated titanium | Nickel-coated stainless steel | None |
| Bipolar plate cathode | Nickel-coated stainless steel | Gold-coated titanium | Nickel-coated Stainless steel | Cobalt-coated stainless steel |
| Frames and sealing | PSU, PTFE, EPDM | PTFE, PSU, ETFE | PTFE, Silicon | Ceramic glass |

Source: IRENA (2020)

Water Electrolysis(수전해)





Other electrolysis processes

- Advantages over water electrolysis:

(1) Use of a waste stream to produce the desire fuel and perhaps other valuable products while simultaneously cleaning up the stream
(2) Reduction of the voltage, hence the energy, required for hydrogen production

- Hydrogen generation using the electrolysis of HCI and the electrolysis of $NH_3 \rightarrow H_2$ production + cleaning up the stream - $E^0_{cell} = 0.06$ V of electrolysis of $NH_3 \rightarrow$ lower than water electrolysis (1.229 V) \rightarrow hydrogen production from ammonia waste streams require less energy

- Urea-contaminated wastewater electrolysis ($E_{cell}^0 = 0.37 \text{ V}$)

 $NH_3 \rightarrow 3/2H_2$ (cathode) + $1/2N_2$ (anode) $CO(NH_2)_2 + H_2O \rightarrow 3H_2$ (cathode) + N_2 (anode) + CO_2

Wastewater treatment

- The use of electrochemical reactors in environment friendly ways to produce useful products while simultaneously cleaning up waste streams

- Another use of electrochemical technologies is for the cleanup of industrial effluent streams containing dilute concentrations of toxic materials: toxic metal ions, pharmaceutical residues

Illustration 14.14

Redox-flow batteries

- A battery in the sense that it is used to store and release energy \rightarrow it operates like a combination of fuel cell (discharge) and an electrolyzer (charge) \rightarrow the reactants and products in a flow battery are contained within the electrolyte, which circulates through the cells

- Vanadium redox-flow battery (VRB): two vanadium redox couples for the negative (V^{3+}/V^{2+}) and positive electrodes (VO_2^+/VO^{2+})

$$V^{3+} + e^{-} = V^{2+} (E^{0} = -0.26 V)$$

 $VO_{2}^{+} + 2H^{+} + e^{-} = VO^{2+} + H_{2}O (E^{0} = 1.00V)$

Illustration 14.14



Figure 14.16 Vanadium redox-flow battery. Reactions and transport are shown for discharging.



PV Magazine (Dec. 21, 2020)

- charge-discharge curve

 $E = E^{0} + (RT/2F) ln[(c^{2}_{V2+} c_{VO2}^{+}) / (c^{2}_{V3+} c_{VO}^{2+})]$



Illustration 14.15

Figure 14.17 Example of polarization curve for the vanadium redox-flow battery at a high state of charge.