

# Electromagnetics:

Flow of EM Power and the Poynting Vector  
Normal Incidence at a Plane Conducting Boundary  
(8-5, 8-6)

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# Energy Flow of EM Waves (1)

For static constitutive parameters:  $\epsilon, \mu$  &  $\sigma$

Maxwell's equations:

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$$

$$\nabla \cdot \mathbf{D} = \rho$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\mathbf{D} = \epsilon \mathbf{E} = \epsilon_0 \mathbf{E} + \mathbf{P}$$

$$\mathbf{B} = \mu \mathbf{H} = \mu_0 \mathbf{H} + \mu_0 \mathbf{M}$$

$$\begin{aligned} \nabla \cdot (\mathbf{E} \times \mathbf{H}) &= \mathbf{H} \cdot (\nabla \times \mathbf{E}) - \mathbf{E} \cdot (\nabla \times \mathbf{H}) \\ &= \mathbf{H} \cdot \left(-\frac{\partial \mathbf{B}}{\partial t}\right) - \mathbf{E} \cdot \left(\mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}\right) \end{aligned}$$

$$\mathbf{H} \cdot \frac{\partial \mathbf{B}}{\partial t} = \mathbf{H} \cdot \frac{\partial (\mu \mathbf{H})}{\partial t} = \frac{\mu}{2} \frac{\partial (\mathbf{H} \cdot \mathbf{H})}{\partial t} = \frac{\partial}{\partial t} \left( \frac{1}{2} \mu H^2 \right)$$

$$\mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t} = \mathbf{E} \cdot \frac{\partial (\epsilon \mathbf{E})}{\partial t} = \frac{\epsilon}{2} \frac{\partial (\mathbf{E} \cdot \mathbf{E})}{\partial t} = \frac{\partial}{\partial t} \left( \frac{1}{2} \epsilon E^2 \right)$$

$$\mathbf{E} \cdot \mathbf{J} = \mathbf{E} \cdot (\sigma \mathbf{E}) = \sigma E^2$$

$$\rightarrow \nabla \cdot (\mathbf{E} \times \mathbf{H}) = -\frac{\partial}{\partial t} \left( \frac{1}{2} \epsilon E^2 + \frac{1}{2} \mu H^2 \right) - \sigma E^2$$

$$\rightarrow \oint_S (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{s} = -\frac{\partial}{\partial t} \int_V \left( \frac{1}{2} \epsilon E^2 + \frac{1}{2} \mu H^2 \right) dv - \int_V \sigma E^2 dv$$

# Energy Flow of EM Waves (2)

Poynting theorem & Poynting vector:

$$\rightarrow \oint_S (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{s} = -\frac{\partial}{\partial t} \int_V \left( \frac{1}{2} \epsilon E^2 + \frac{1}{2} \mu H^2 \right) dv - \int_V \sigma E^2 dv$$

*Negative rate of the temporal change* (points to  $-\frac{\partial}{\partial t}$ )  
*Stored energy in E-field* (points to  $\frac{1}{2} \epsilon E^2$ )  
*Stored energy in H-field* (points to  $\frac{1}{2} \mu H^2$ )  
*Ohmic power dissipation* (points to  $\sigma E^2$ )  
*Poynting vector: Power flow per unit area* (points to  $\mathbf{E} \times \mathbf{H}$ )

$$\mathbf{P} = \mathbf{E} \times \mathbf{H}$$

$$\oint_S \mathbf{P} \cdot d\mathbf{s} = -\frac{\partial}{\partial t} \int_V (w_e + w_m) dv - \int_V p_\sigma dv$$

*Poynting's theorem*

$w_e$  : Electric energy density

$w_m$  : Magnetic energy density

$p_\sigma$  : Ohmic power density

# Instantaneous and Average Power Densities

Complex notation for time-harmonic **E** & **H**:

$$\mathbf{E}(\mathbf{r}, t) = \frac{1}{2} [\mathbf{E}(\mathbf{r})e^{j\omega t} + c.c.] = \text{Re}[\mathbf{E}(\mathbf{r})e^{j\omega t}] \quad \rightarrow \text{Re}(\mathbf{A}) = \frac{1}{2} (\mathbf{A} + \mathbf{A}^*)$$
$$\mathbf{H}(\mathbf{r}, t) = \frac{1}{2} [\mathbf{H}(\mathbf{r})e^{j\omega t} + c.c.] = \text{Re}[\mathbf{H}(\mathbf{r})e^{j\omega t}] \quad \rightarrow \text{Re}(\mathbf{B}) = \frac{1}{2} (\mathbf{B} + \mathbf{B}^*)$$

For product operations:

$$\mathbf{E}(\mathbf{r}, t) \times \mathbf{H}(\mathbf{r}, t), \mathbf{E}(\mathbf{r}, t) \cdot \mathbf{D}(\mathbf{r}, t), \dots \rightarrow \text{Re}(\mathbf{A}) \times \text{Re}(\mathbf{B}), \text{Re}(\mathbf{A}) \cdot \text{Re}(\mathbf{D}), \dots$$

$$\begin{aligned} \text{Re}(\mathbf{A}) \times \text{Re}(\mathbf{B}) &= \frac{1}{2} (\mathbf{A} + \mathbf{A}^*) \times \frac{1}{2} (\mathbf{B} + \mathbf{B}^*) = \frac{1}{4} (\mathbf{A} \times \mathbf{B}^* + \mathbf{A}^* \times \mathbf{B} + \mathbf{A} \times \mathbf{B} + \mathbf{A}^* \times \mathbf{B}^*) \\ &= \frac{1}{2} \text{Re}(\mathbf{A} \times \mathbf{B}^* + \mathbf{A} \times \mathbf{B}) \end{aligned}$$

For a power density (Poynting vector):

*Instantaneous:*  $\rightarrow \mathbf{P} = \mathbf{E}(\mathbf{r}, t) \times \mathbf{H}(\mathbf{r}, t) = \frac{1}{2} \text{Re}[\mathbf{E}(\mathbf{r}) \times \mathbf{H}^*(\mathbf{r}) + \mathbf{E}(\mathbf{r}) \times \mathbf{H}(\mathbf{r})e^{j2\omega t}]$

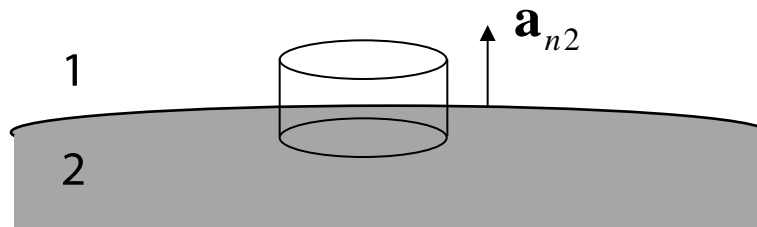
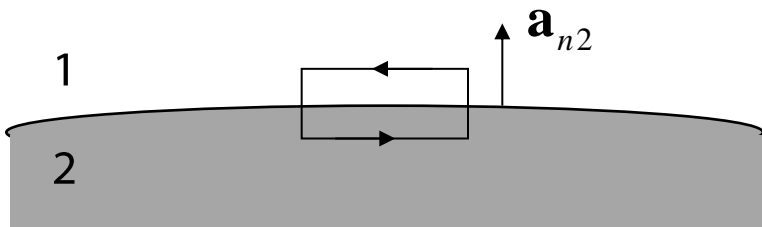
*Time-average:*  $\rightarrow \mathbf{P}_{av} = \frac{1}{2} \text{Re}[\mathbf{E}(\mathbf{r}) \times \mathbf{H}^*(\mathbf{r})]$

$\rightarrow$  Zero  
if time-averaged!

# Electromagnetic Boundary Conditions

Continuity conditions:

$$\begin{aligned} \nabla \times \mathbf{E} + \frac{\partial \mathbf{B}}{\partial t} = 0 &\rightarrow \oint_C \mathbf{E} \cdot d\mathbf{l} = - \int_S \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s} \rightarrow E_{1t} = E_{2t} \\ &\rightarrow \mathbf{a}_{n2} \times (\mathbf{E}_1 - \mathbf{E}_2) = 0 \\ \nabla \times \mathbf{H} - \frac{\partial \mathbf{D}}{\partial t} = \mathbf{J} &\rightarrow \oint_C \mathbf{H} \cdot d\mathbf{l} = \int_S \left( \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \right) \cdot d\mathbf{s} \\ &\rightarrow \mathbf{a}_{n2} \times (\mathbf{H}_1 - \mathbf{H}_2) = \mathbf{J}_s \\ \nabla \cdot \mathbf{D} = \rho &\rightarrow \mathbf{a}_{n2} \cdot (\mathbf{D}_1 - \mathbf{D}_2) = \rho_s \\ \nabla \cdot \mathbf{B} = 0 &\rightarrow B_{1n} = B_{2n} \rightarrow \mathbf{a}_{n2} \cdot (\mathbf{B}_1 - \mathbf{B}_2) = 0 \end{aligned}$$



# Interface between a Dielectric and a Perfect Conductor

A perfect conductor:  $\sigma = \infty$

→ No fields exist in the interior, i.e.  $E = D = B = H = 0$ ,  
for time-varying fields!

$$\nabla \times \mathbf{E} + \frac{\partial \mathbf{B}}{\partial t} = 0 \quad \rightarrow \quad \mathbf{a}_{n2} \times (\mathbf{E}_1 - \mathbf{E}_2) = 0$$

$$\nabla \times \mathbf{H} - \frac{\partial \mathbf{D}}{\partial t} = \mathbf{J} \quad \rightarrow \quad \mathbf{a}_{n2} \times (\mathbf{H}_1 - \mathbf{H}_2) = \mathbf{J}_s$$

$$\nabla \cdot \mathbf{D} = \rho \quad \rightarrow \quad \mathbf{a}_{n2} \cdot (\mathbf{D}_1 - \mathbf{D}_2) = \rho_s$$

$$\nabla \cdot \mathbf{B} = 0 \quad \rightarrow \quad \mathbf{a}_{n2} \cdot (\mathbf{B}_1 - \mathbf{B}_2) = 0$$

→

$$E_{1t} = 0, \quad E_{2t} = 0$$

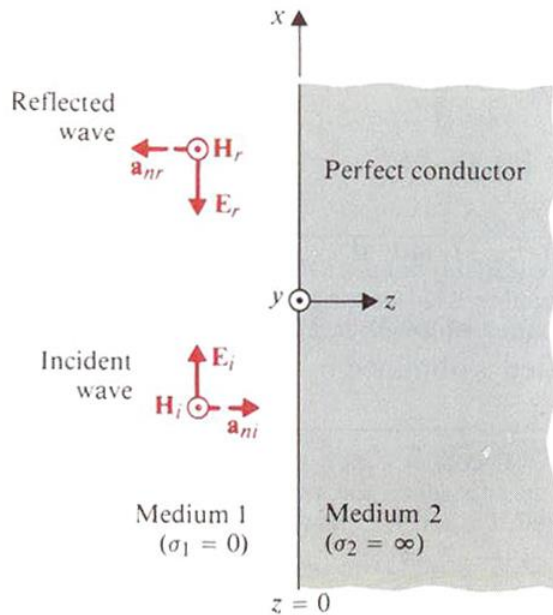
$$\mathbf{a}_{n2} \times \mathbf{H}_1 = \mathbf{J}_s, \quad H_{2t} = 0$$

$$\mathbf{a}_{n2} \cdot \mathbf{D}_1 = \rho_s, \quad D_{2n} = 0$$

$$B_{1n} = 0, \quad B_{2n} = 0$$

→ Any charges or currents the perfect conductor may have  
exist on the "surface" only!

# Normal Incidence at a Plane Conducting Boundary (1)



D. K. Cheng, Field and Wave Electromagnetics, 2nd ed., Addison-Wesley, 1989.

In medium 1 ( $z < 0$ ):

$$\mathbf{E}_i(z) = \mathbf{a}_x E_{i0} e^{-j\beta_1 z}$$

$$\mathbf{H}_i(z) = \mathbf{a}_y \frac{E_{i0}}{\eta_1} e^{-j\beta_1 z} \quad \leftarrow \text{Intrinsic impedance}$$

$$\mathbf{E}_r(z) = \mathbf{a}_x E_{r0} e^{+j\beta_1 z}$$

$$\mathbf{H}_r(z) = \mathbf{a}_y H_{r0} e^{+j\beta_1 z}$$

$$\rightarrow \mathbf{E}_1(z) = \mathbf{E}_i(z) + \mathbf{E}_r(z)$$

$$\rightarrow \mathbf{H}_1(z) = \mathbf{H}_i(z) + \mathbf{H}_r(z)$$

In medium 2 ( $z > 0$ ):

$$\rightarrow \mathbf{E}_2(z) = 0 \quad \text{for a perfect conductor}$$

$$\rightarrow \mathbf{H}_2(z) = 0 \quad (\sigma = \infty)$$

# Normal Incidence at a Plane Conducting Boundary (2)

For tangential components of E-fields:

$$\mathbf{a}_{n2} \times (\mathbf{E}_1 - \mathbf{E}_2) = 0$$

$$\rightarrow \mathbf{E}_1(z=0) = \mathbf{a}_x (E_{i0} + E_{r0}) = \mathbf{E}_2(z=0) = 0$$

$$\rightarrow E_{r0} = -E_{i0}$$

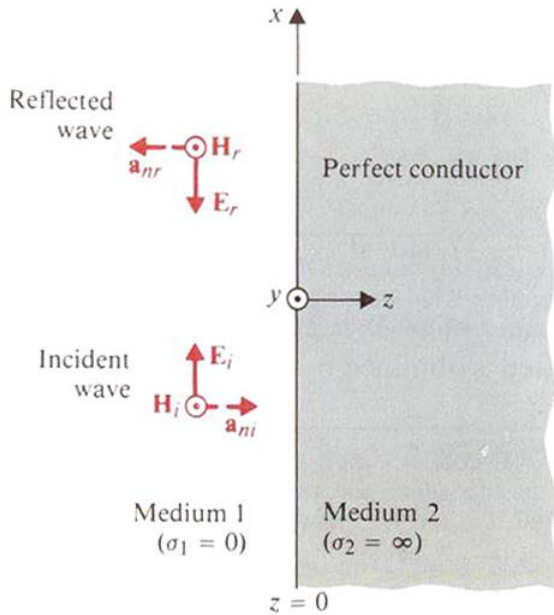
$$\begin{aligned} \rightarrow \mathbf{E}_1(z) &= \mathbf{a}_x E_{i0} (e^{-j\beta_1 z} - e^{+j\beta_1 z}) \\ &= -\mathbf{a}_x j2E_{i0} \sin \beta_1 z \end{aligned}$$

Recall: 
$$\mathbf{H} = -\frac{1}{j\omega\mu} (\nabla \times \mathbf{E})$$

$$\rightarrow \mathbf{H}_r(z) = \frac{1}{\eta_1} \mathbf{a}_{nr} \times \mathbf{E}_r = \frac{1}{\eta_1} (-\mathbf{a}_z) \times \mathbf{E}_r$$

$$= -\mathbf{a}_y \frac{1}{\eta_1} E_{r0} e^{+\beta_1 z} = \mathbf{a}_y \frac{E_{i0}}{\eta_1} e^{+\beta_1 z}$$

$$\begin{aligned} \rightarrow \mathbf{H}_1(z) &= \mathbf{H}_i(z) + \mathbf{H}_r(z) = \mathbf{a}_y \frac{E_{i0}}{\eta_1} (e^{-i\beta_1 z} + e^{+i\beta_1 z}) \\ &= \mathbf{a}_y 2 \frac{E_{i0}}{\eta_1} \cos \beta_1 z \end{aligned}$$



D. K. Cheng, Field and Wave Electromagnetics, 2nd ed., Addison-Wesley, 1989.



# Normal Incidence at a Plane Conducting Boundary (3)

$$\rightarrow \mathbf{E}_1(z) = -\mathbf{a}_x j2E_{i0} \sin \beta_1 z$$

$$\rightarrow \mathbf{H}_1(z) = \mathbf{a}_y 2 \frac{E_{i0}}{\eta_1} \cos \beta_1 z$$

$$\rightarrow \mathbf{E}_1(z, t) = \text{Re}[\mathbf{E}_1(z)e^{j\omega t}]$$

$$= \mathbf{a}_x 2E_{i0} \sin \beta_1 z \sin \omega t$$

$$\rightarrow \mathbf{H}_1(z, t) = \text{Re}[\mathbf{H}_1(z)e^{j\omega t}]$$

$$= \mathbf{a}_y 2 \frac{E_{i0}}{\eta_1} \cos \beta_1 z \cos \omega t$$

→ *Standing wave*

*Poynting vector:*  $\mathbf{E}_1 \times \mathbf{H}_1 = ?$

