

< Element Potential >

At equilibrium \Rightarrow minimum Gibbs Function G

$$G = \sum_i N_i g_i$$

Atom balance

$$\sum_i \eta_{ij} N_i = a_j = \text{total \# of moles of } j \text{ atoms in the system}$$

\Downarrow

number of j atoms in species i

eg.) $\text{CH}_4 + 2\text{CO}_2 \Rightarrow a_c = 1 \times 1 + 1 \times 2 = 3$. $\left(\begin{array}{l} \eta_{\text{CH}_4, c} = 1, \eta_{\text{CO}_2, c} = 1 \\ N_{\text{CH}_4} = 1, N_{\text{CO}_2} = 2. \end{array} \right)$

$$G = G(T, p, N_i)$$

$$dG_{(T,p)} = \sum_i g_i dN_i$$

T, p constant.

$$\sum_i \eta_{ij} dN_i = da_j = 0 \quad (\text{atom conservation})$$

⊙ Method of Lagrange Multipliers.

\rightarrow We will have j eqns (j constraints)

eg.) $\text{CH}_4 + 2\text{CO}_2$

there are 3 constraints (C, H, O) from atom balance

multiplier λ_j represents j th constraint to drop out N_i .

$$\text{at equilibrium } dG_{T,p} = 0 = dG_{T,p} - \sum_j \lambda_j \underbrace{\sum_i \eta_{ij} dN_i}_{= da_j = 0}$$

$$\Rightarrow \sum_i (g_i - \sum_j \eta_{ij} \lambda_j) dN_i = 0.$$

at equilibrium, coef. for dN_i should be 0

$$\therefore g_i = \sum_j \eta_{ij} \lambda_j$$

$\lambda_j \equiv$ element potential for the j atoms

For an ideal gas.

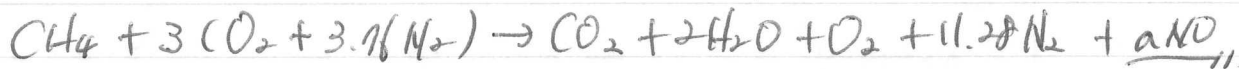
$$g_i(T, P_i) = g_i(T, P) + \hat{R}T \ln X_i = \sum_j \nu_{ij} \lambda_j$$

$$\therefore \ln X_i = - \frac{g_i(T, P)}{\hat{R}T} + \sum_j \nu_{ij} \left(\frac{\lambda_j}{\hat{R}T} \right)$$

To get X_i , we need λ_j .

* \Rightarrow These can be derived using dominant species assumption, then, using the element potentials (λ_j), mole fractions of minor product species can be estimated.

ex) Calculate the equilibrium NO mole fraction in the product of the combustion of a lean methane/air mixture ($\phi = 2/3$) at 1500 K, 1 bar.



To estimate X_{NO} , we need element potential of N and O.

$$X_{\text{N}_2} = \frac{11.28}{1+2+1+11.28} = 0.738 \quad \therefore \text{NO is minor species}$$

$$X_{\text{O}_2} = 0.0654$$

$$\ln X_{\text{N}_2} = - \frac{g_{\text{N}_2}(1500\text{K}, 1\text{bar})}{\underbrace{8.314}_{=\hat{R}} \times 1500} + 2 \times \frac{\lambda_{\text{N}}}{8.314 \times 1500}$$

$$\ln X_{\text{O}_2} = - \frac{g_{\text{O}_2}(1500\text{K}, 1\text{bar})}{8.314 \times 1500} + 2 \times \frac{\lambda_{\text{O}}}{8.314 \times 1500}$$

$$g_i = \underbrace{\left(h_i(T) - h_i(T_{\text{ref}}) \right)}_{\text{on NIST-JANAF table}} + \underbrace{\Delta_f H_i(T_{\text{ref}})}_{\text{on NIST-JANAF table}} - T \underbrace{S_i(T, 1\text{bar})}_{\text{on NIST-JANAF table}}$$

on NIST-JANAF table

$$g_{N_2} = -324.4 \text{ kJ/mol}$$

$$g_{O_2} = -346.5 \text{ kJ/mol}$$

$$g_{NO} = -264.0 \text{ kJ/mol}$$

$$\left(\begin{array}{l} \lambda_N = -13.15 \times \hat{R}T \\ \lambda_O = -15.26 \times \hat{R}T \end{array} \right)$$

$$\underline{X_{NO} = \exp\left(\frac{-g_{NO} + \lambda_N + \lambda_O}{\hat{R}T}\right) = \boxed{1.14 \times 10^{-4}} \text{, minor product.}}$$