

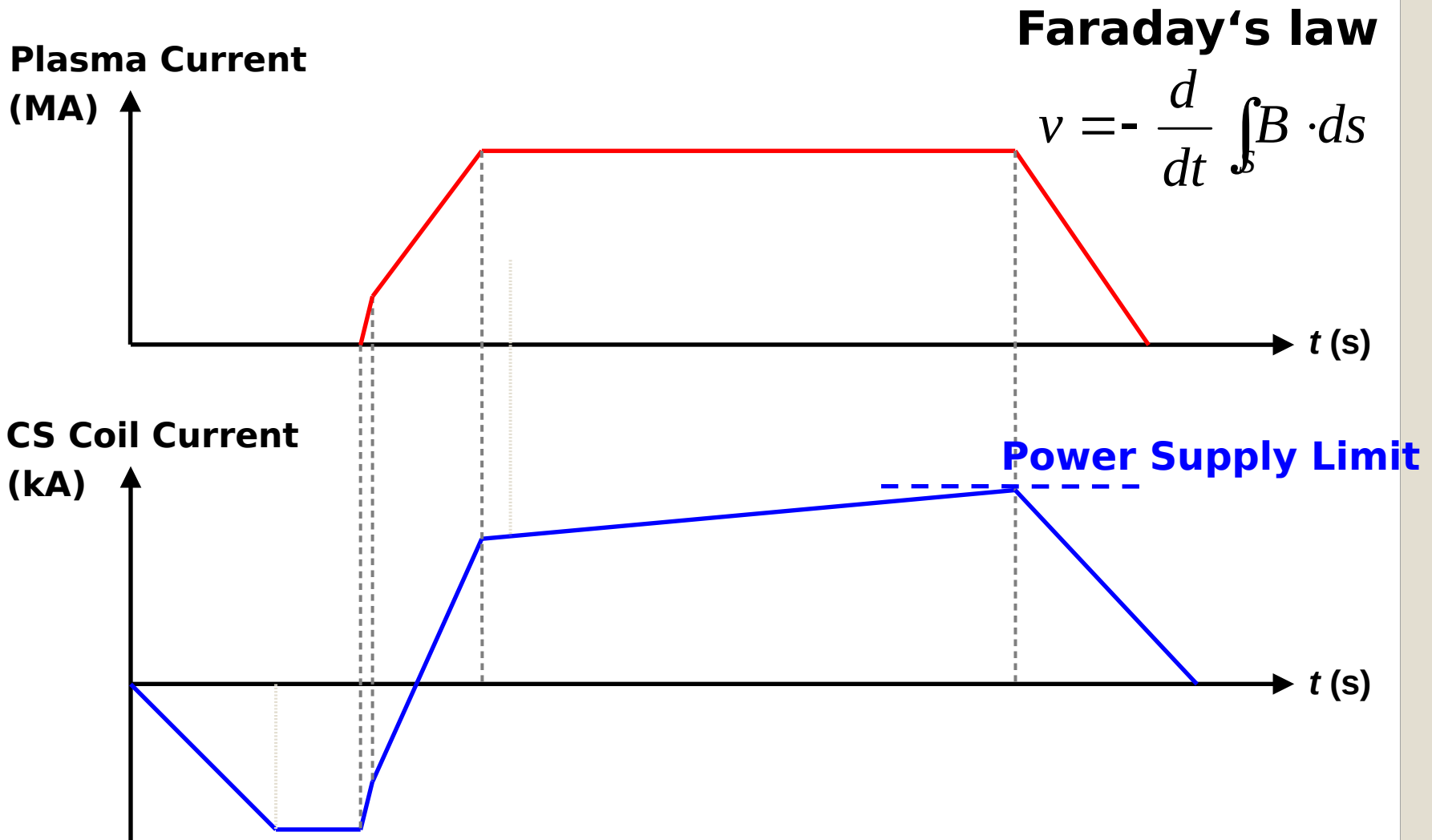
Fusion Reactor Technology 2

(459.761, 3 Credits)

Prof. Dr. Yong-Su Na

(32-206, Tel. 880-7204)

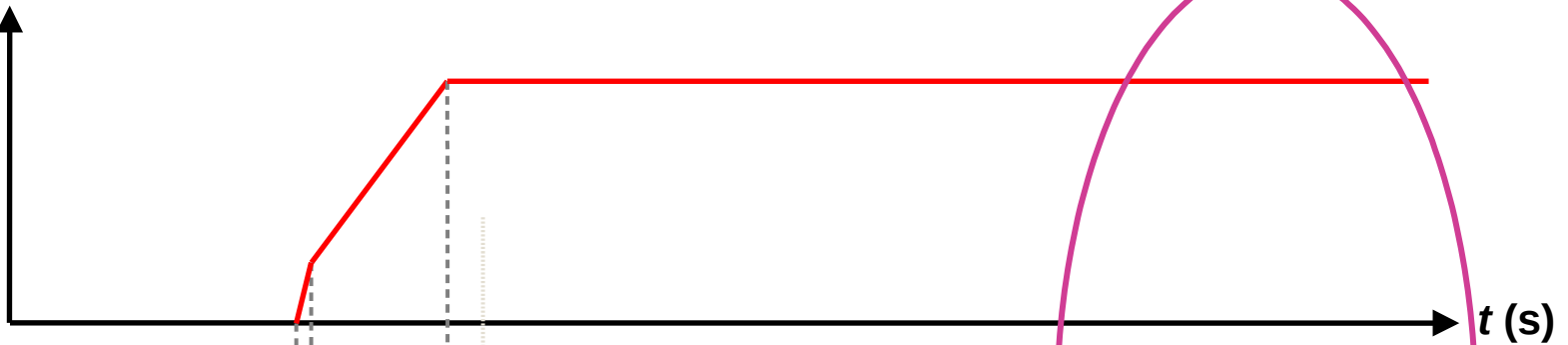
Pulsed Operation



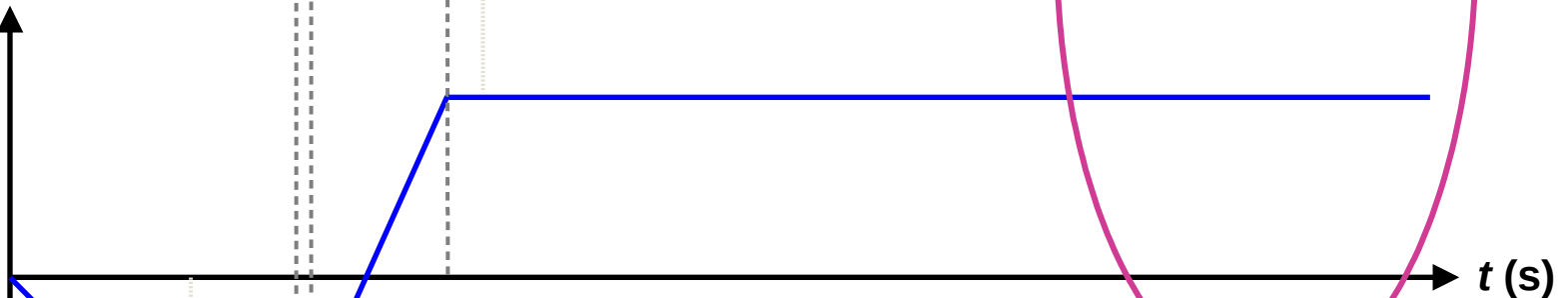
Inherent drawback of Tokamak!

Steady-State Operation

Plasma Current
(MA)



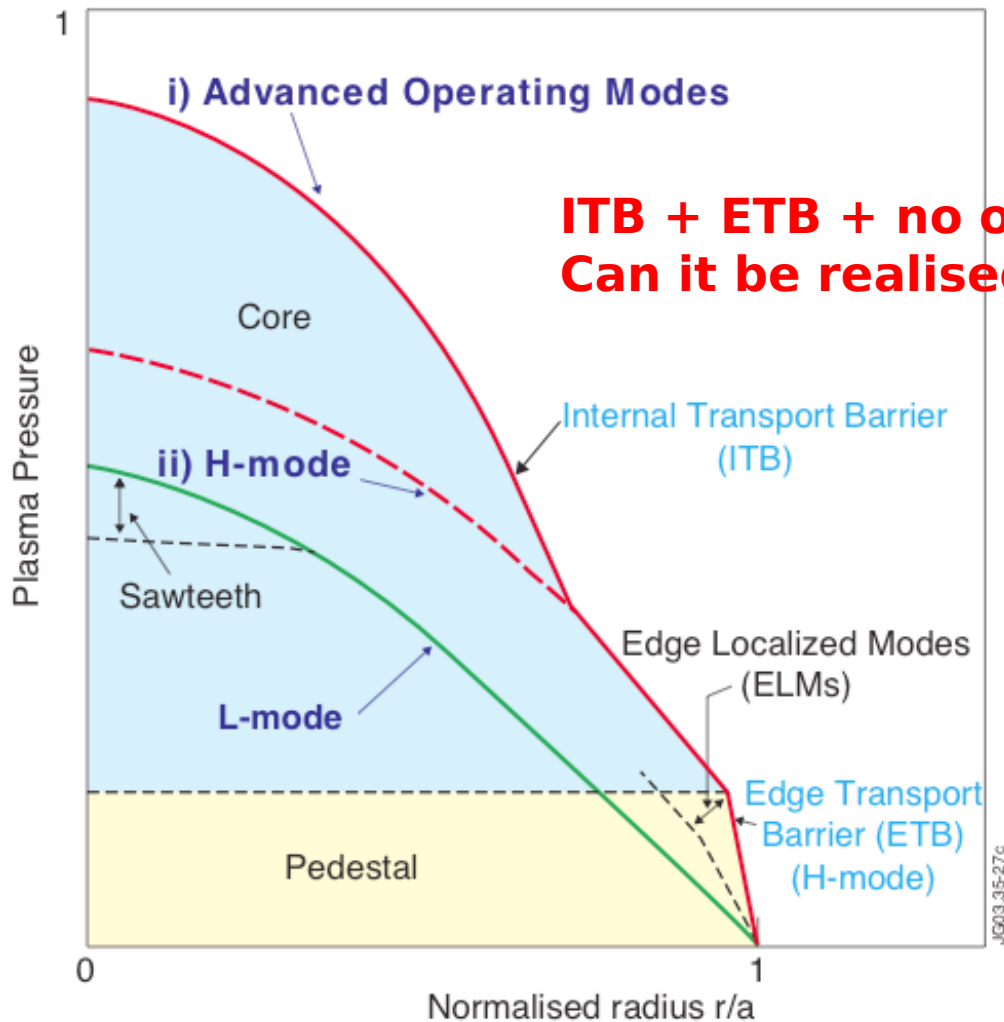
CS Coil Current
(kA)



$d/dt \sim 0$

**Steady-state operation
by self-generated and externally driven current**

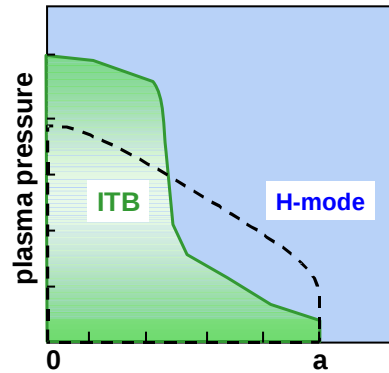
Tokamak Operation Modes



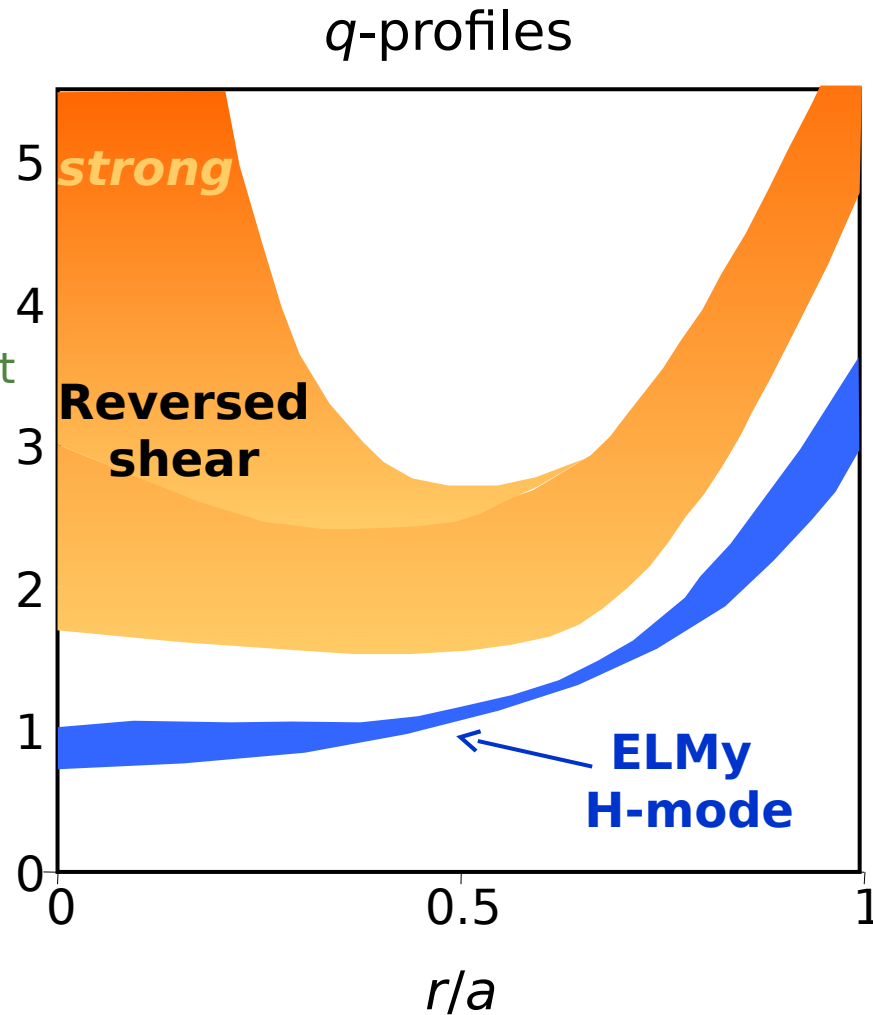
**ITB + ETB + no or mild ELM is our dream!
Can it be realised?**

JG03.35-27c

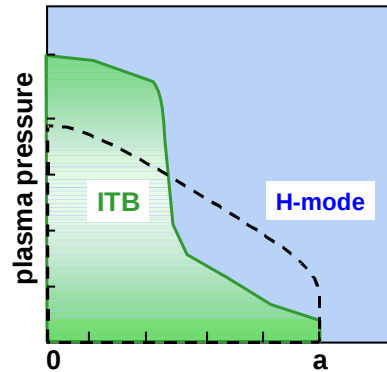
Advanced Operating Modes



- Good confinement
- Poor stability

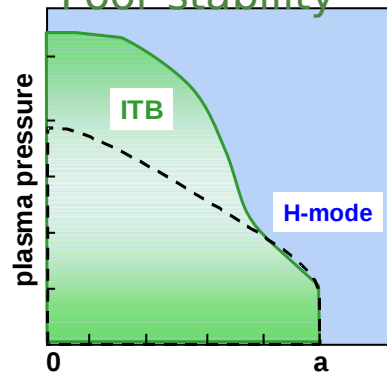


Advanced Operating Modes



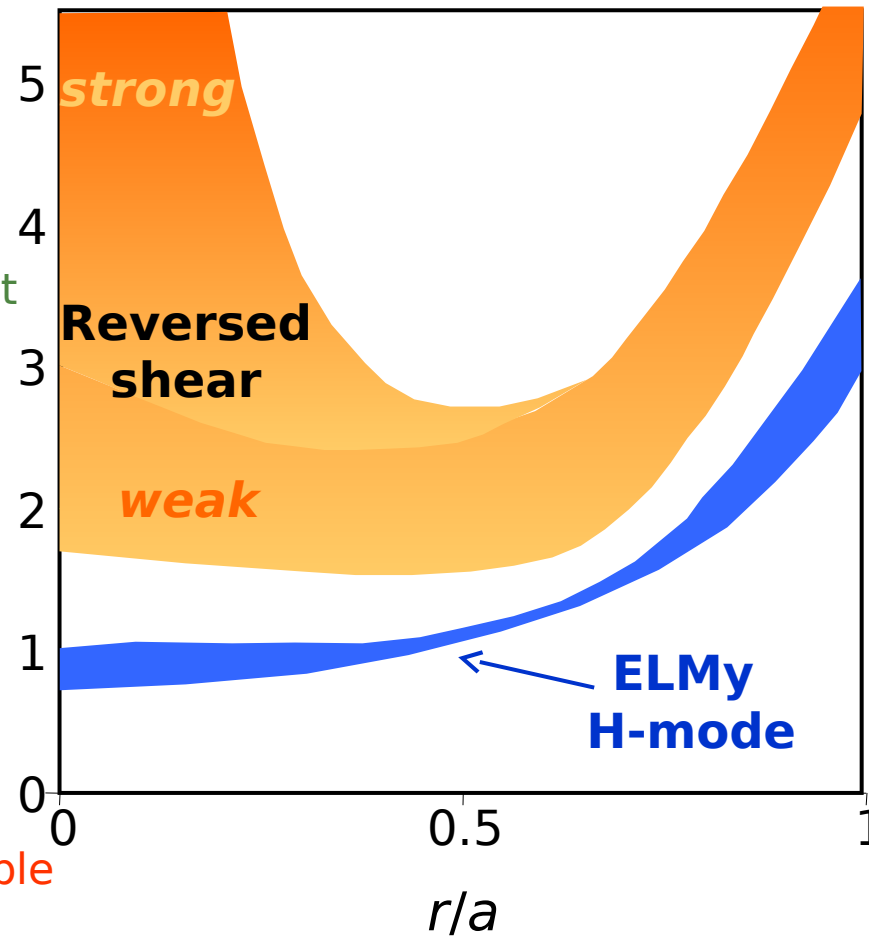
- Good confinement

- Poor stability

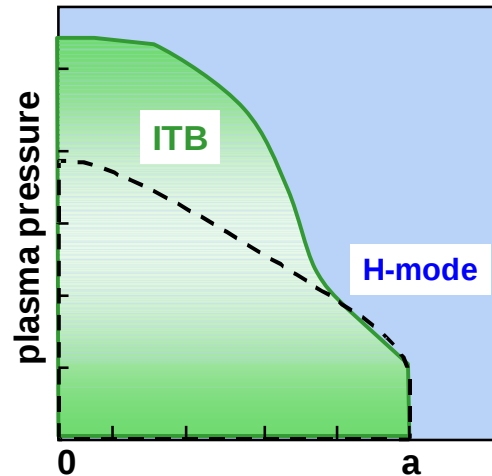
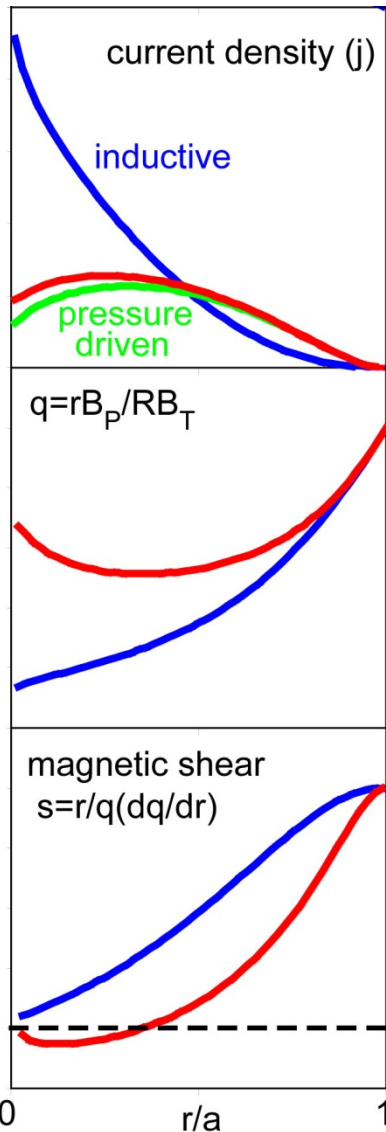


- Only "weak" RS plasmas are stable but they require a delicate active control

q -profiles



Reversed Shear Mode

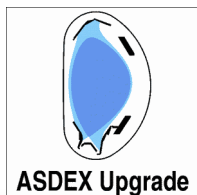
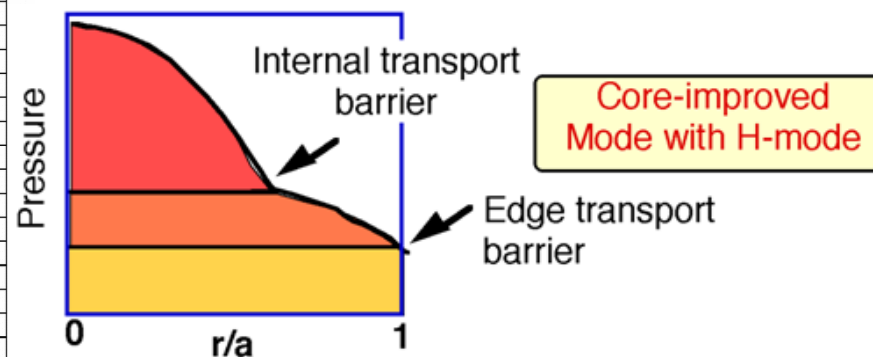
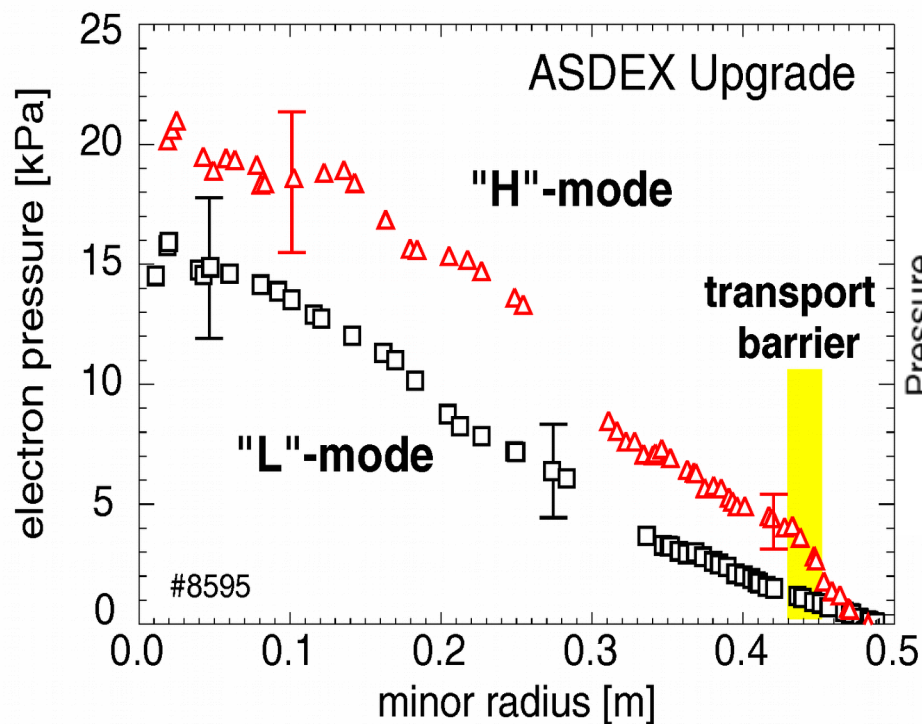


- Higher pressure gradient region in the core with steep edge pedestal
- Hollow current profile
- Reversed q -profile
- With negative magnetic shear

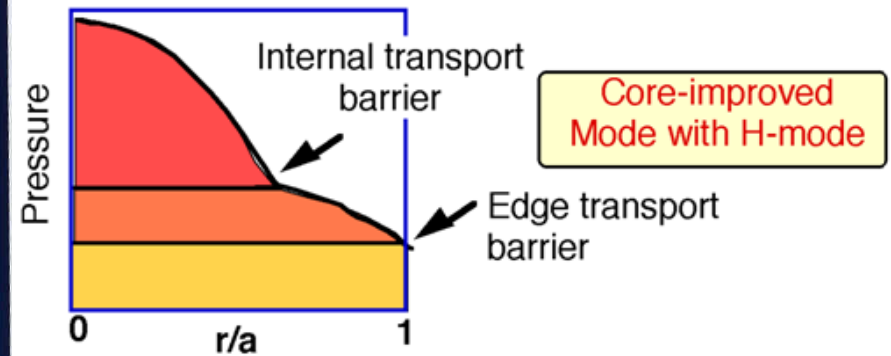
Reversed Shear Mode

H-mode

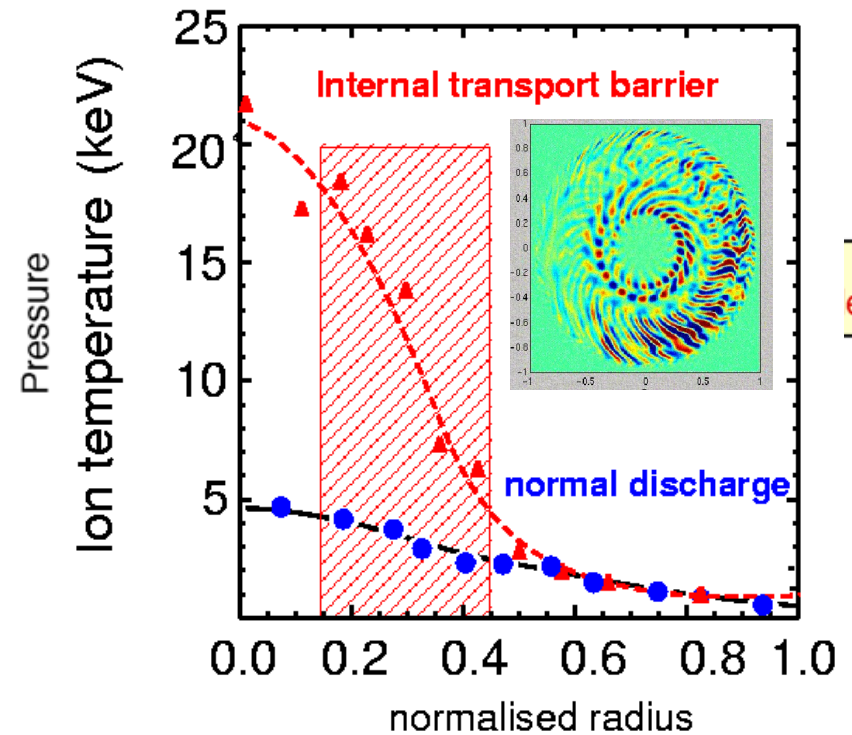
Reversed shear mode



Reversed Shear Mode



Reversed Shear Mode



e

Internal Transport Barrier

Tokamak operation in the high- β_p regime is a promising concept for a steady-state tokamak reactor [1,2].

LETTERS

6 JUNE 1994

Here the poloidal beta is defined as $\beta_p = 2\mu_0 \langle p \rangle / B_p^2$,

where $\langle p \rangle$ is the volume-averaged plasma pressure and B_p is the averaged poloidal magnetic field on the face.

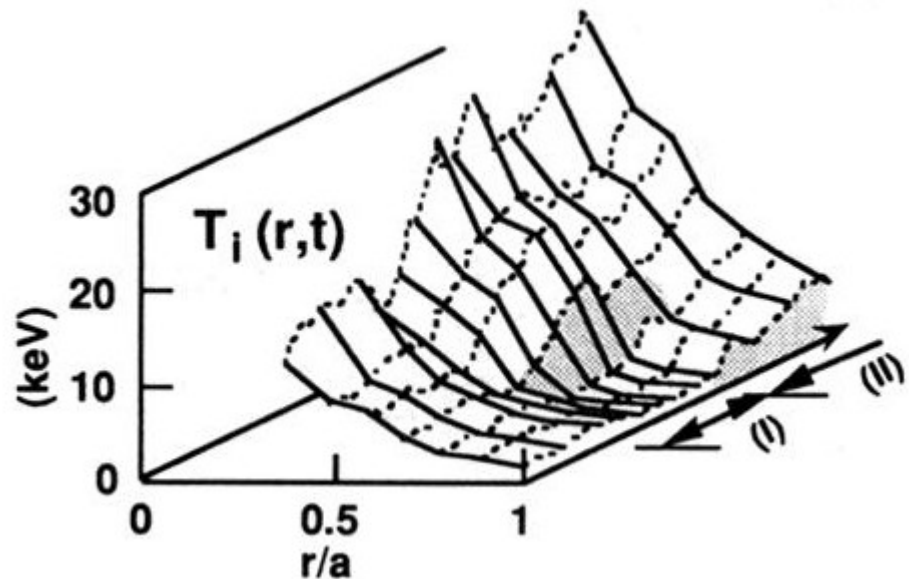
An energy confinement time, τ_E , more than that for L mode (for example, ITER89-P [3]) in the high- β_p regime to reduce the plasma current and hence to achieve efficient steady-state operation [4].

Improved confinement time was achieved in the high- β_p regime ($\beta_p = 1-2$) in JT-60U, where the confinement improvement factor, $\tau_E/\tau_{E,L}$, increased with $\epsilon\beta_p$ [5].

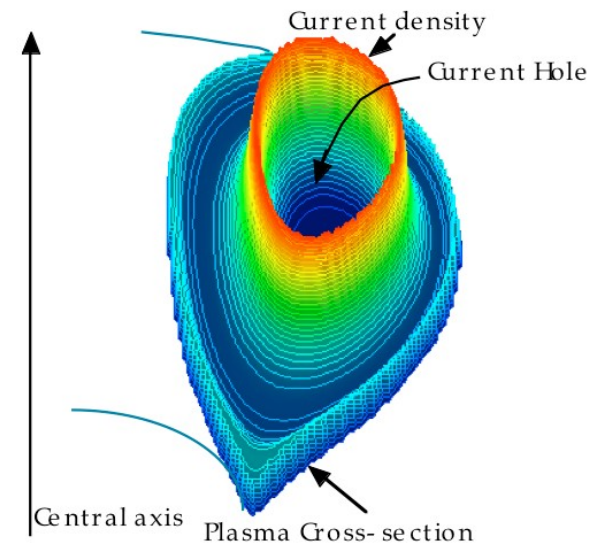
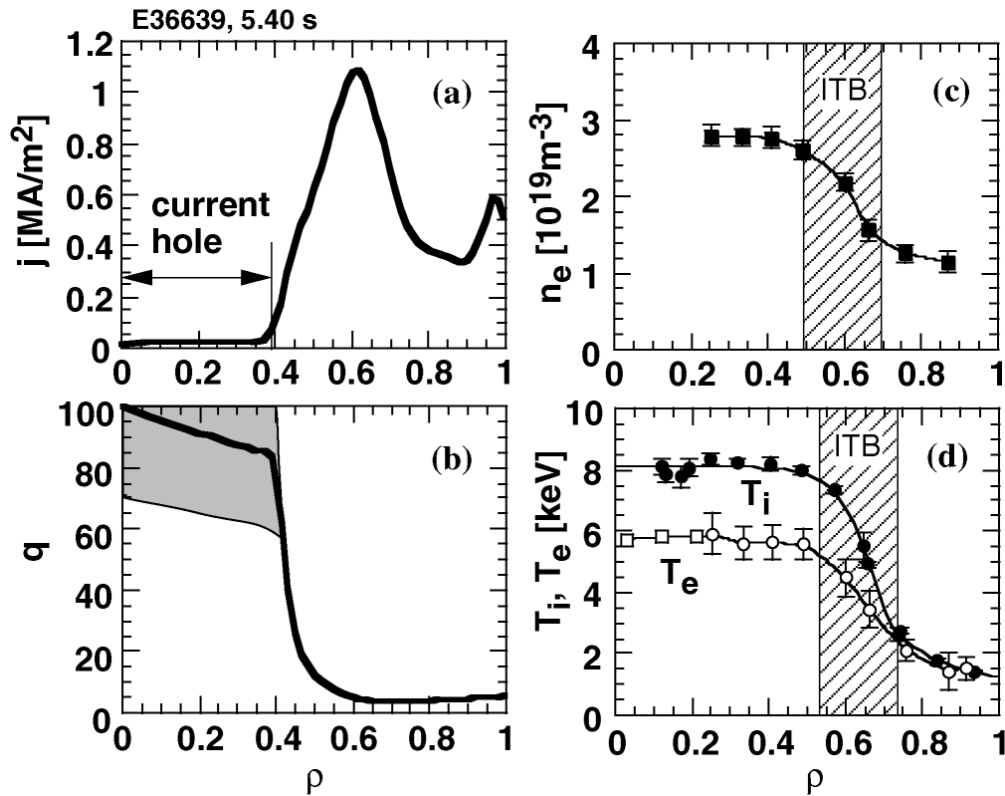
In this regime, the "high- β_p mode" is characterized by a bootstrap-current fraction of up to 58% at the center of the plasma, and a central ion temperature, $T_i(0)$, of 38 keV were achieved.

Recently the high- β_p mode regime was extended to a lower q regime ($q_{\text{eff}} \sim 4.3$; q_{eff} is the effective safety factor defined in Ref. [6]) by using current profile control to avoid sawteeth.

And high fusion performance was attained in this regime [7,8]. This Letter describes two distinctive features of this high- β_p mode: (1) the formation of an "internal" transport barrier near the $q=3$ rational surface and (2) the appearance of high poloidal plasma rotation velocity of ~ 50 km/s in the plasma interior.



Current Hole Regime



T. Fujita et al, PRL 87 245001 (2001)

Internal+Edge Transport Barrier

Internal Barriers

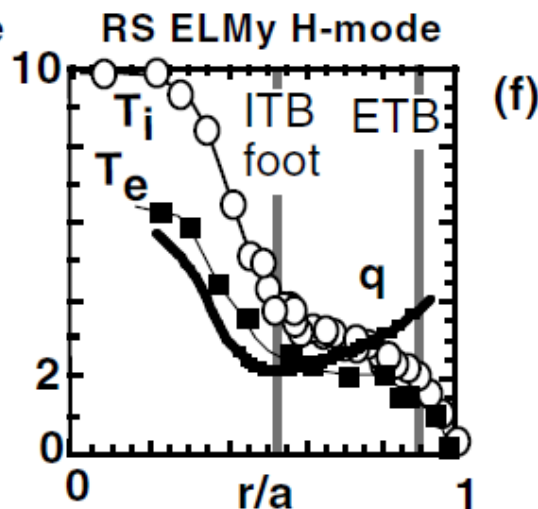
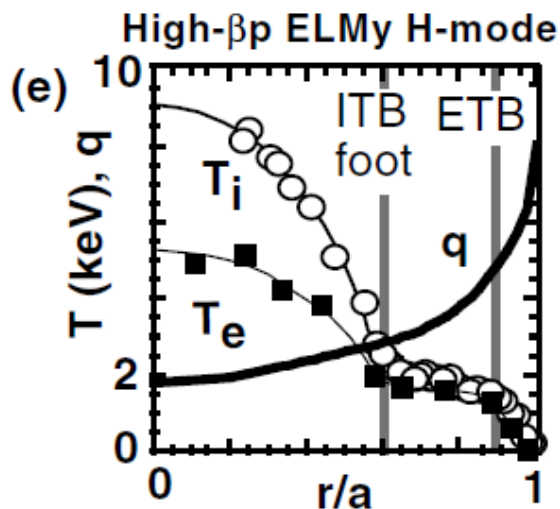
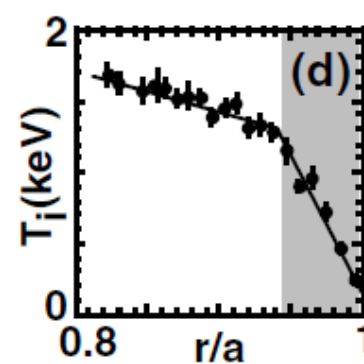
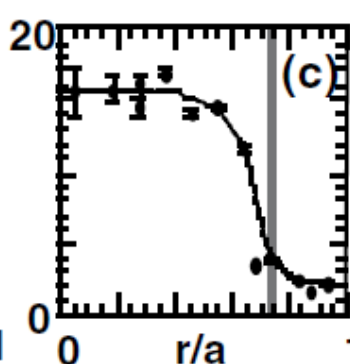
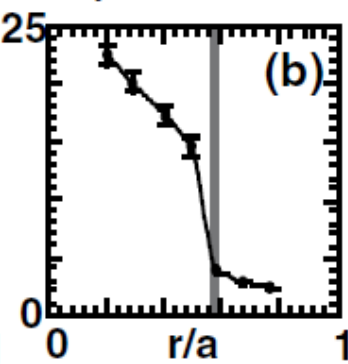
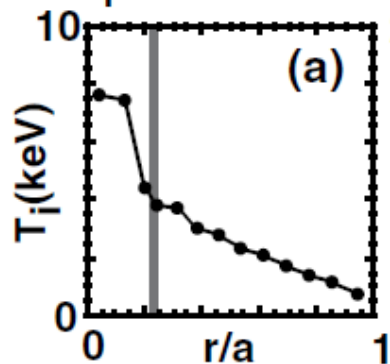
Edge Barrier

Central Pellet
q=1 surface

High- β_p mode
weak positive shear

Reverse Shear mode
negative shear

H-mode



ITB without reversed shear

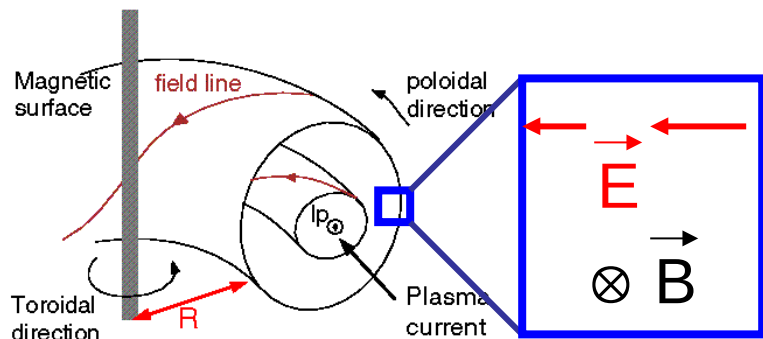
Turbulence Stabilisation

- Formation of internal transport barriers to improve confinement

- Reversed magnetic shear

- Rotation shear

} Stabilises turbulence

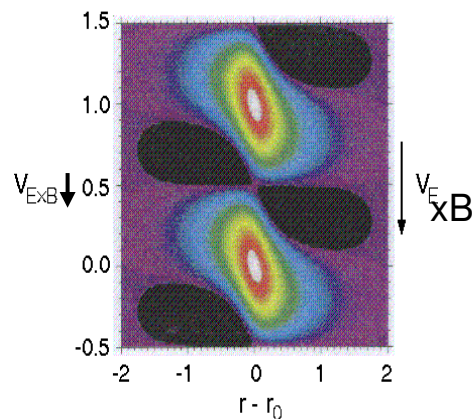
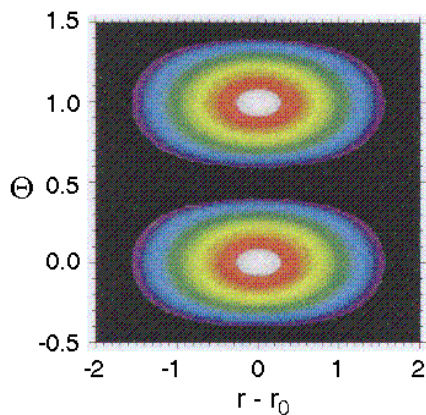


- One reason:

Losses of fast ions at the plasma edge

- sheared radial electric field
- sheared mean $E \times B$ rotation
- eddies get tilted and ripped apart

cause turbulence suppression!



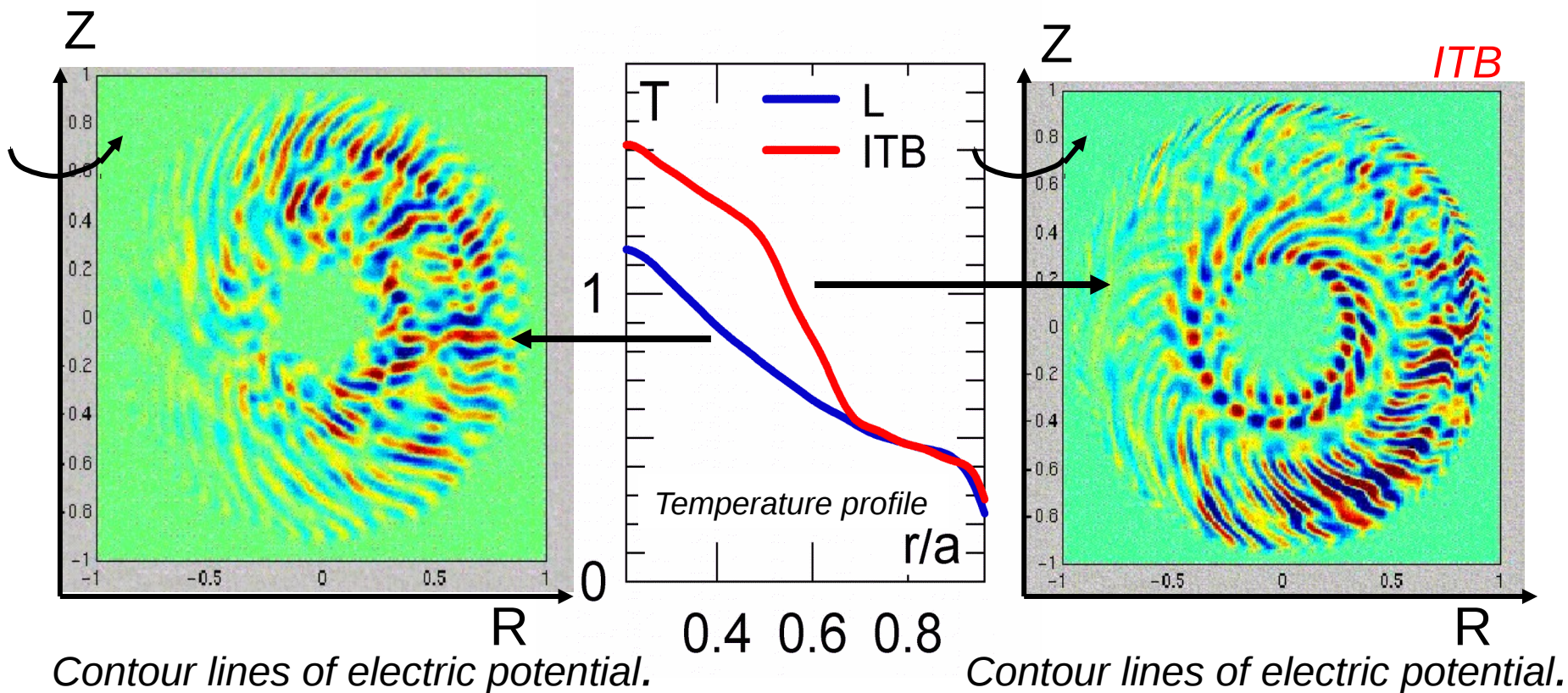
Turbulence Stabilisation

- Formation of internal transport barriers to improve confinement

- Reversed magnetic shear

- Rotation shear

} Stabilises turbulence



Turbulence Stabilisation

**Gyrokinetic Simulations
of Plasma Microinstabilities**

simulation by

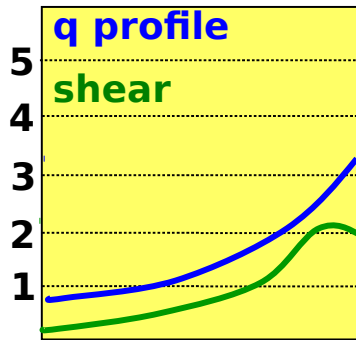
Zhihong Lin et al.

Science 281, 1835 (1998)

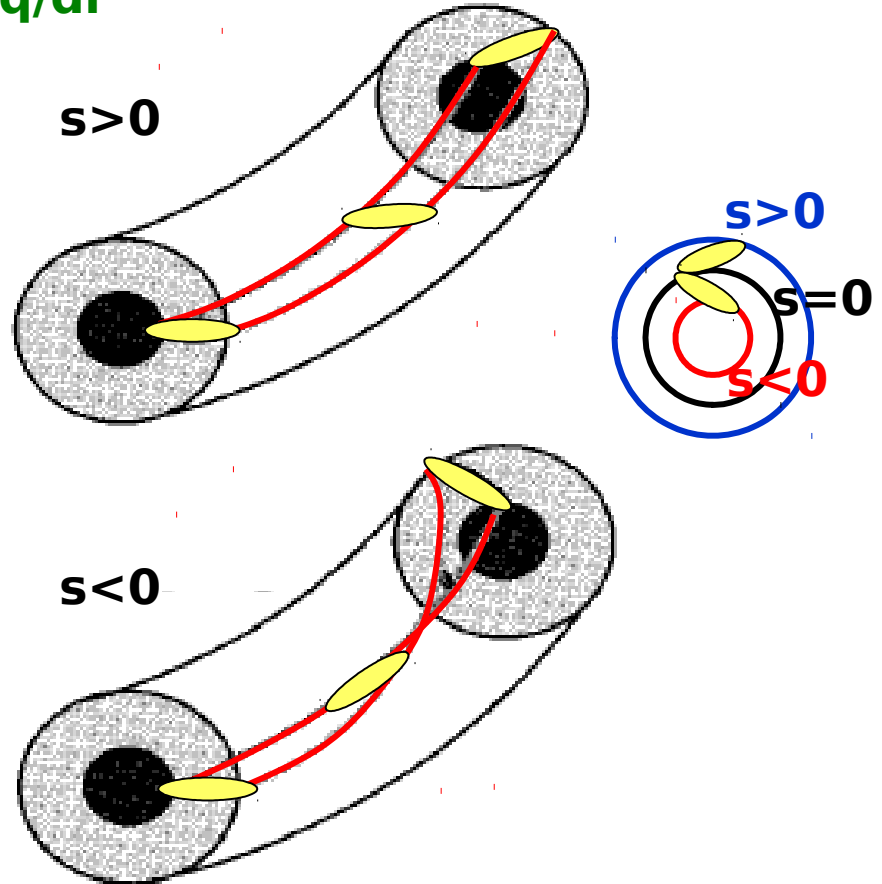
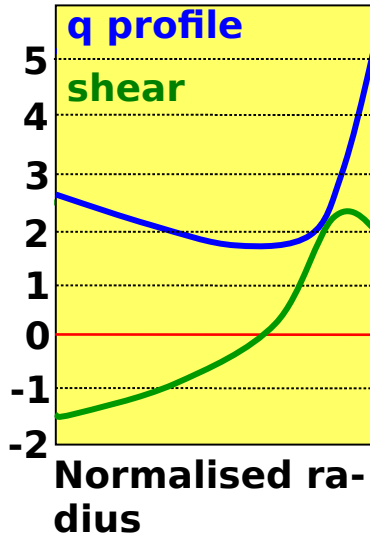
Turbulence Stabilisation

q & magnetic shear: $s = r/q \, dq/dr$

Standard scenario



Advanced tokamak scenario



Magnetic shear can twist plasma disturbances

Turbulence Stabilisation

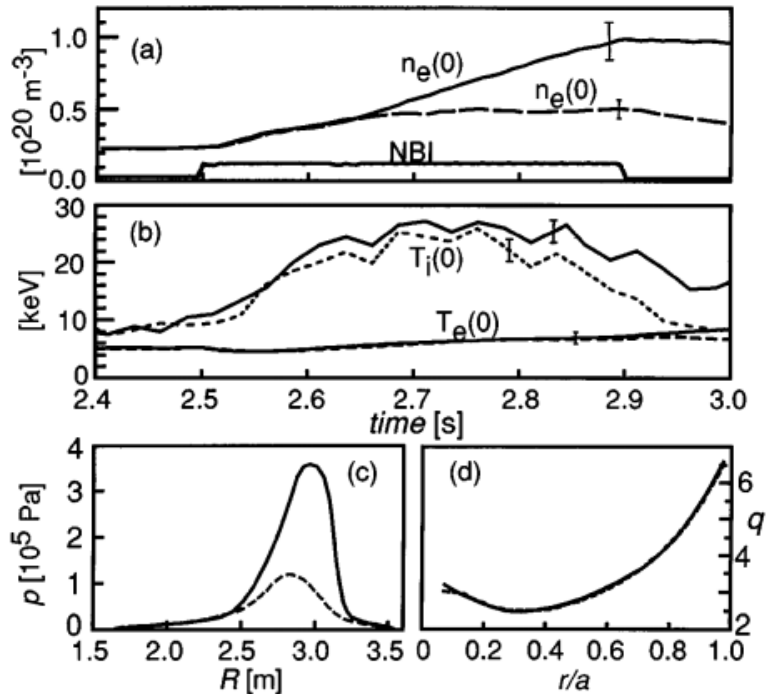


FIG. 1. Time evolution of central electron density (a) and temperatures (b) in ERS (solid line) and RS (dashed line) plasmas with 29 and 27 MW of balanced NBI, respectively. The bottom graphs show the radial profiles of the plasma pressure (c) at $t = 2.9 \text{ s}$, and the safety factor (d) at the bifurcation time ($t \approx 2.65 \text{ s}$).

E. Mazzucato et al, PRL 77 3145 (1996)

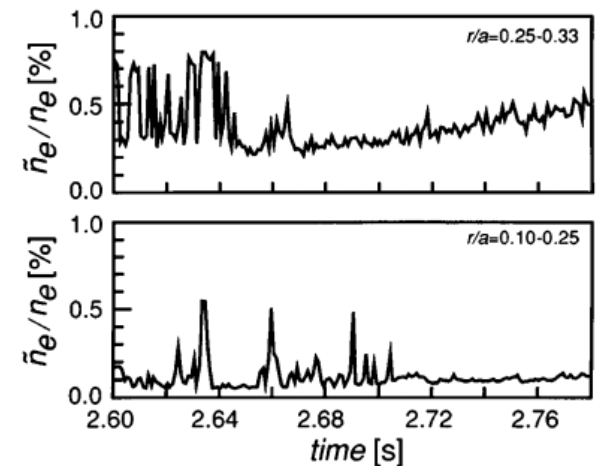


FIG. 3. Time evolution of density fluctuations in the ERS mode.

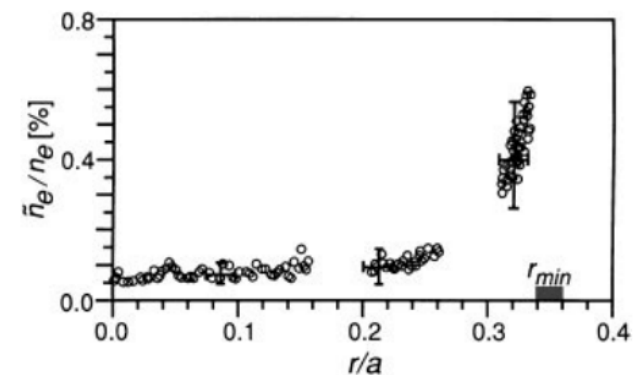
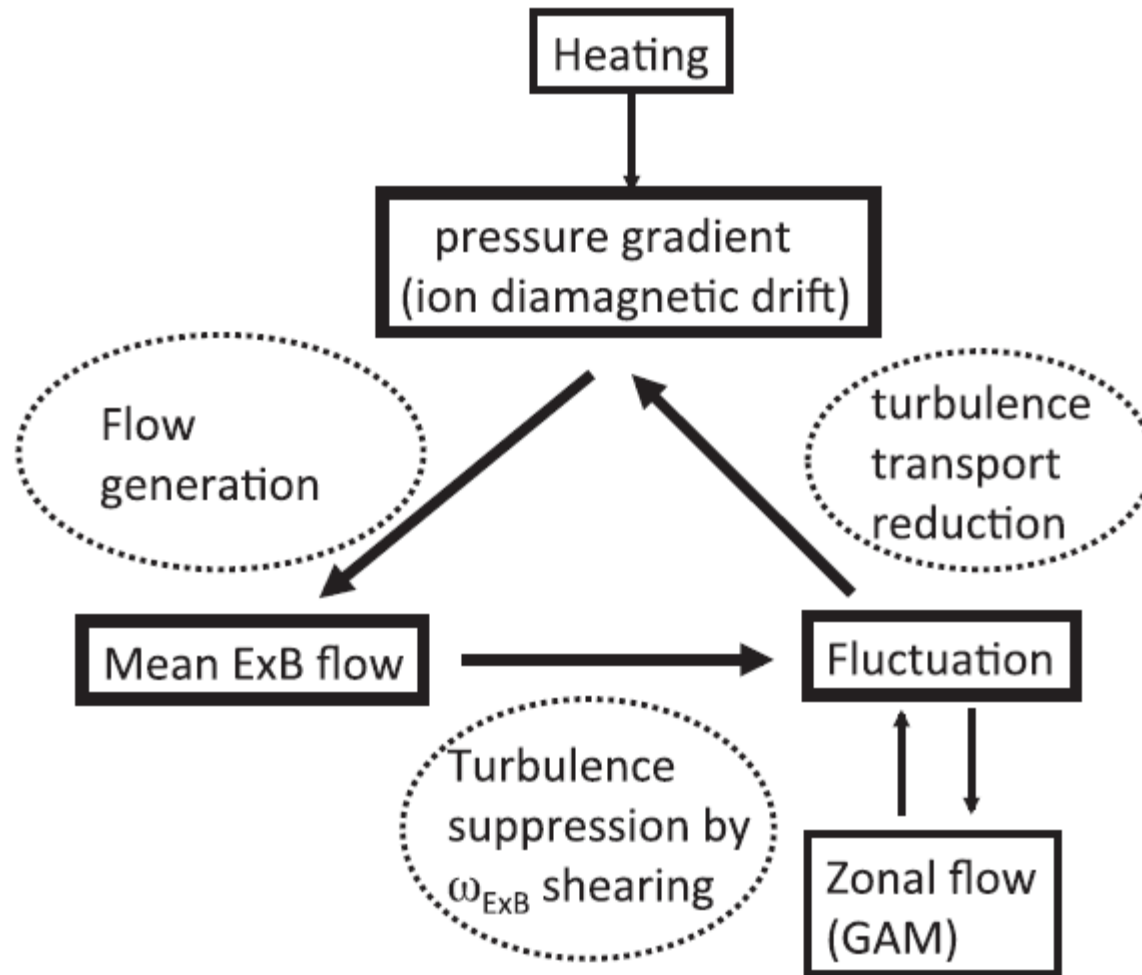


FIG. 4. Amplitude of density fluctuations in the ERS mode at $t = 2.72-2.78 \text{ s}$; r_{min} is the radial position with minimum q .

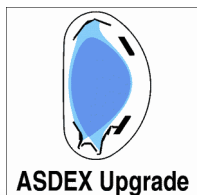
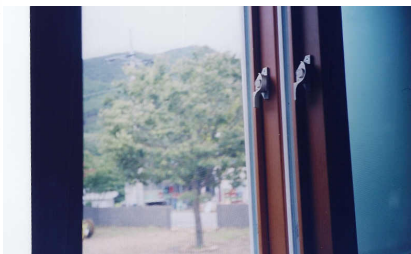
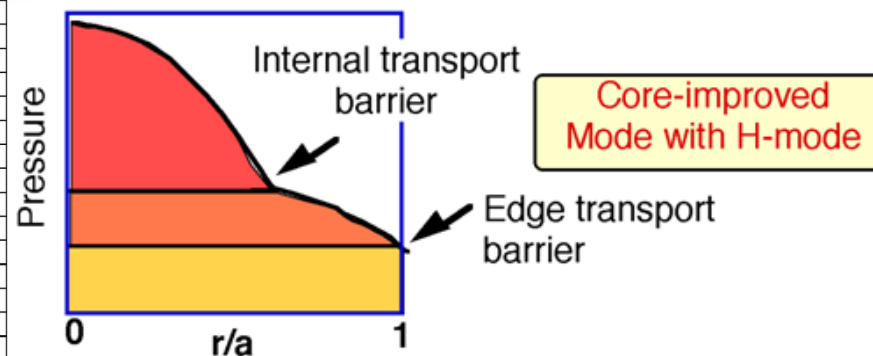
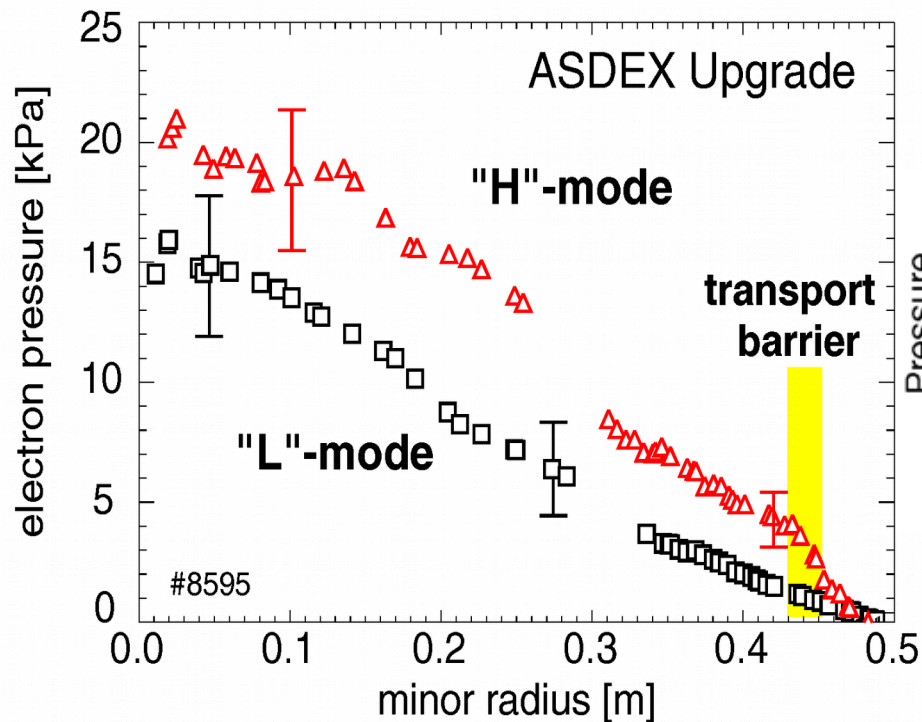
Turbulence Stabilisation



Reversed Shear Mode

H-mode

Reversed shear mode



Reversed Shear Mode

HW: How can one identify the ITBs (electron or ion or heat or particle or rotation) in the experiment?

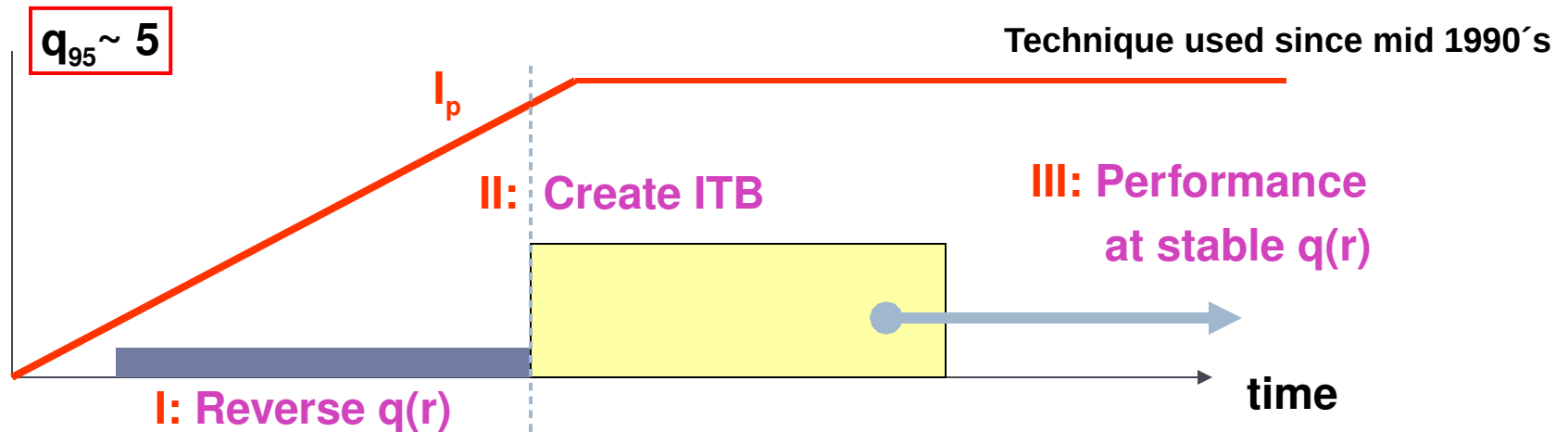
Explain any diagnostics or theories which can be used to identify them.

Find scalings of threshold power for ITB formation.

Reversed Shear Mode

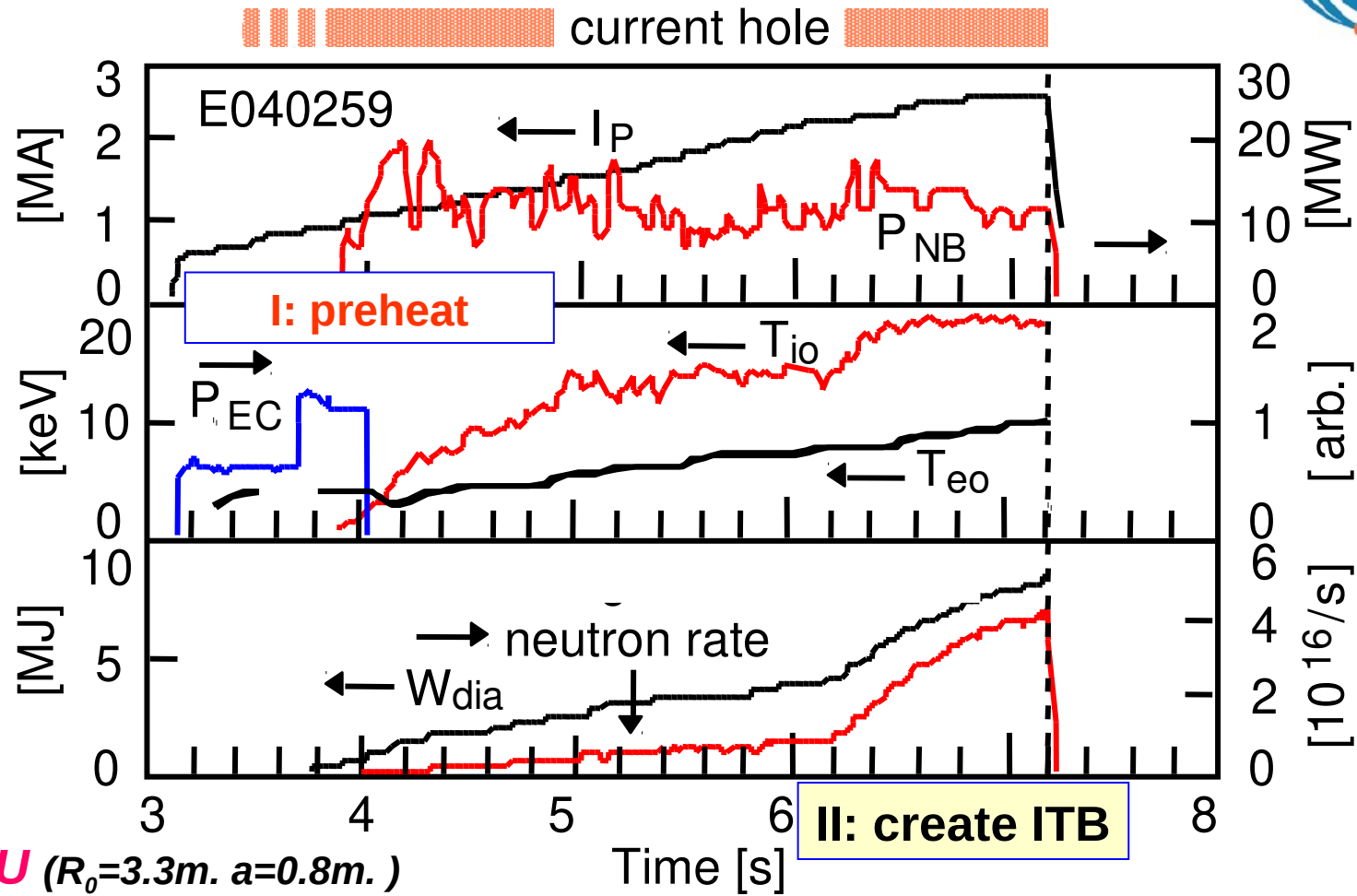
- Operation at lower plasma current: $f_{BS} \sim \beta_p \sim I_p^{-2}$
 - Confinement degradation: $\tau_E \sim H_{98}(y,2) I_p^{0.93}$
 - To get enough fusion power: $H_{98}(y,2) > 1$ (advanced)

Reversed Shear Scenario



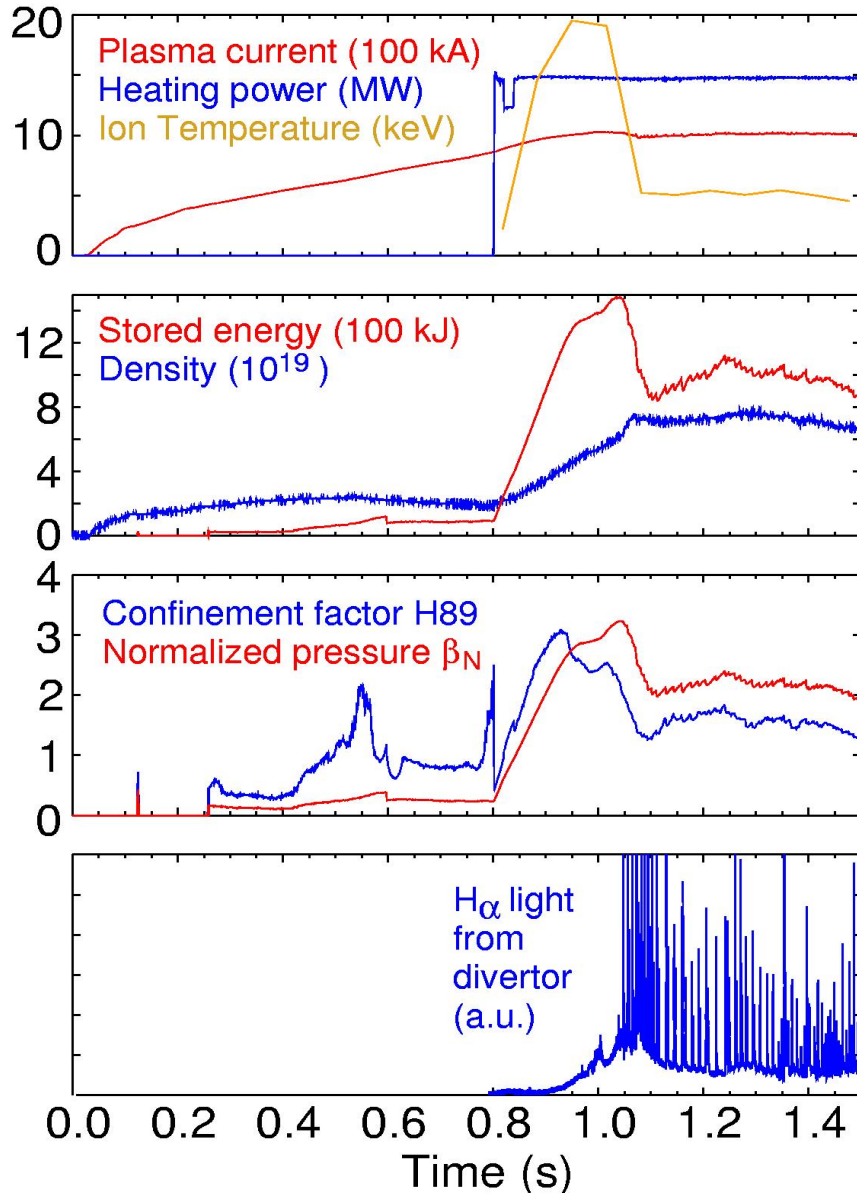
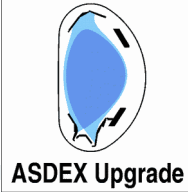
- I: Heat during current rise, external current drive (reversed q).
- II: Increase heating power to produce ITB (turbulence stabilised) and improve plasma confinement, try to increase pressure (β_N)
- III: Keep going
(e.g. ITER steady state scenario at 9 MA : $H_{98} \sim 1.6$, $\beta_N \sim 3.0$, 50% external current drive (73MW), 50% bootstrap fraction)

Reversed Shear Scenario



I: Form $q(r)$, II: create ITB, III: But discharge terminates (unstable)

Reversed Shear Scenario

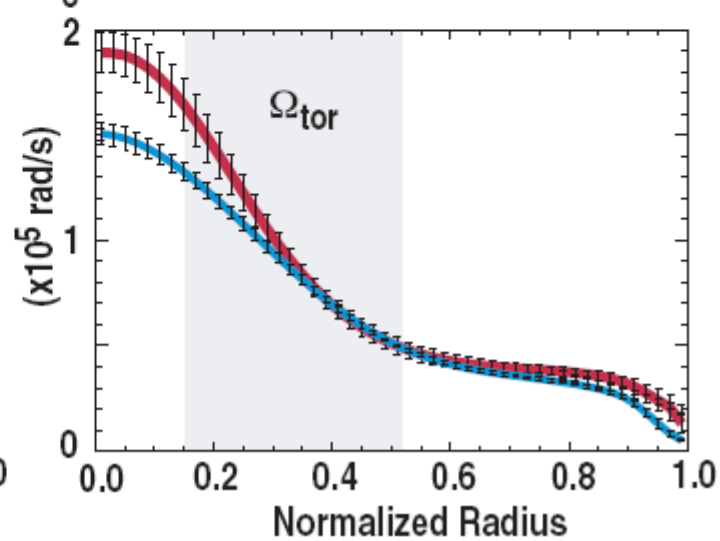
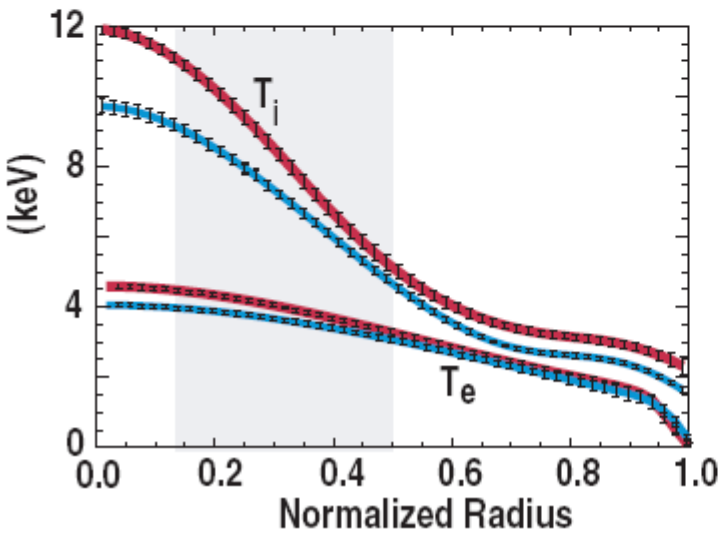
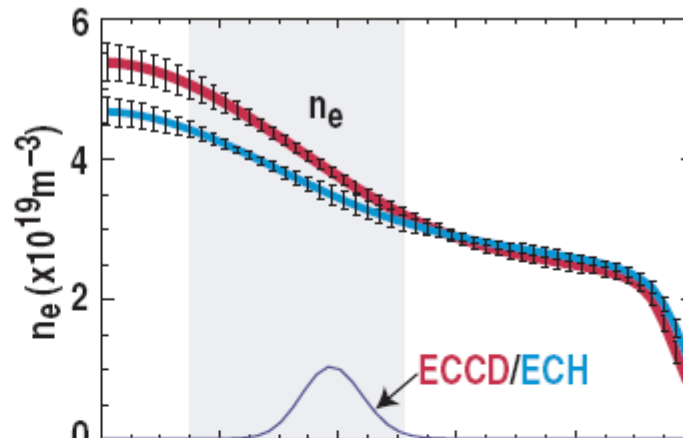
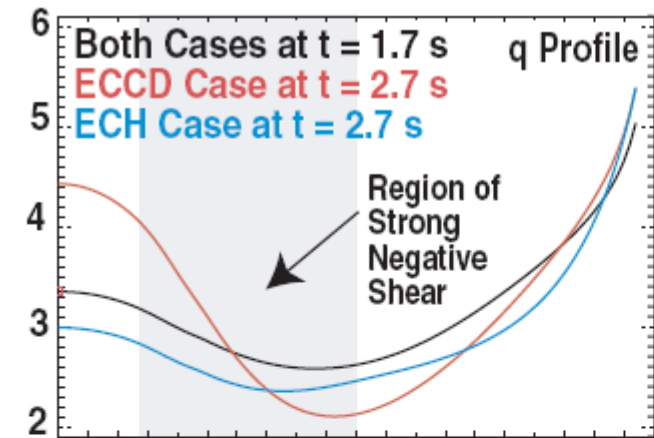


- Formation of an ITB at low n_e , with 15 MW NBI power
 $T_i > T_e$, high rotation shear
- ITBs are relatively short lived, only few τ_E
- Good, transient performance:
 $H_{89} \sim 3$, $\beta_N \sim 3$
- ITB not compatible with H-mode edge barrier and large ELMs

Reversed Shear Scenario

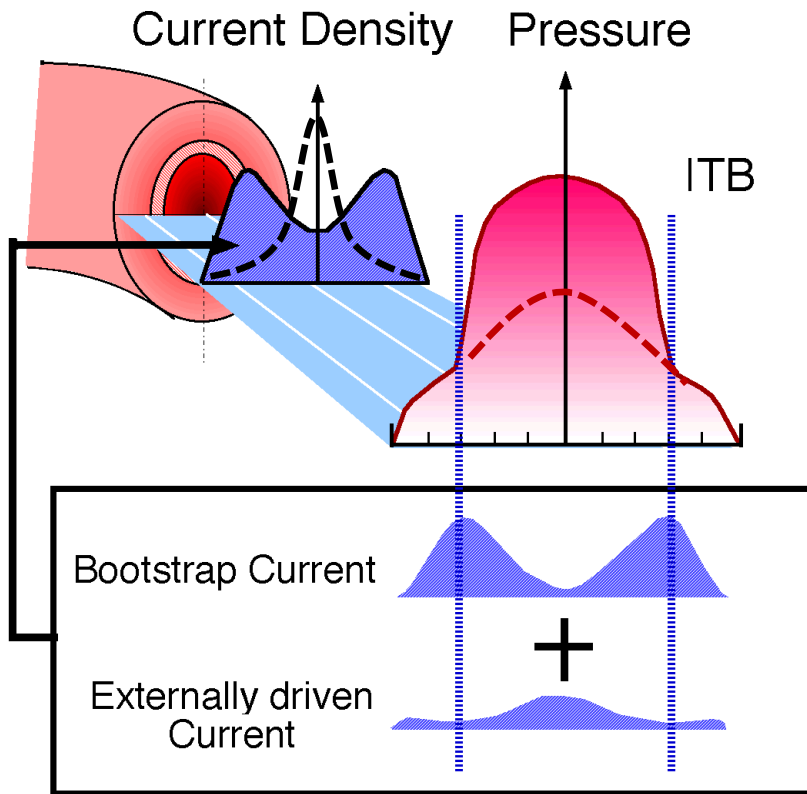


$(R_0 = 1.7 \text{ m}, a = 0.6 \text{ m})$



- weak RS
- $H_{98} = 1.37$
- $\beta_N = 2.62$
- $q_{95} = 5$
- „Weak“ ITBs

Current drive and current profile control



Non-monotonic current profile

Turbulence suppression

High pressure gradients

Large bootstrap current

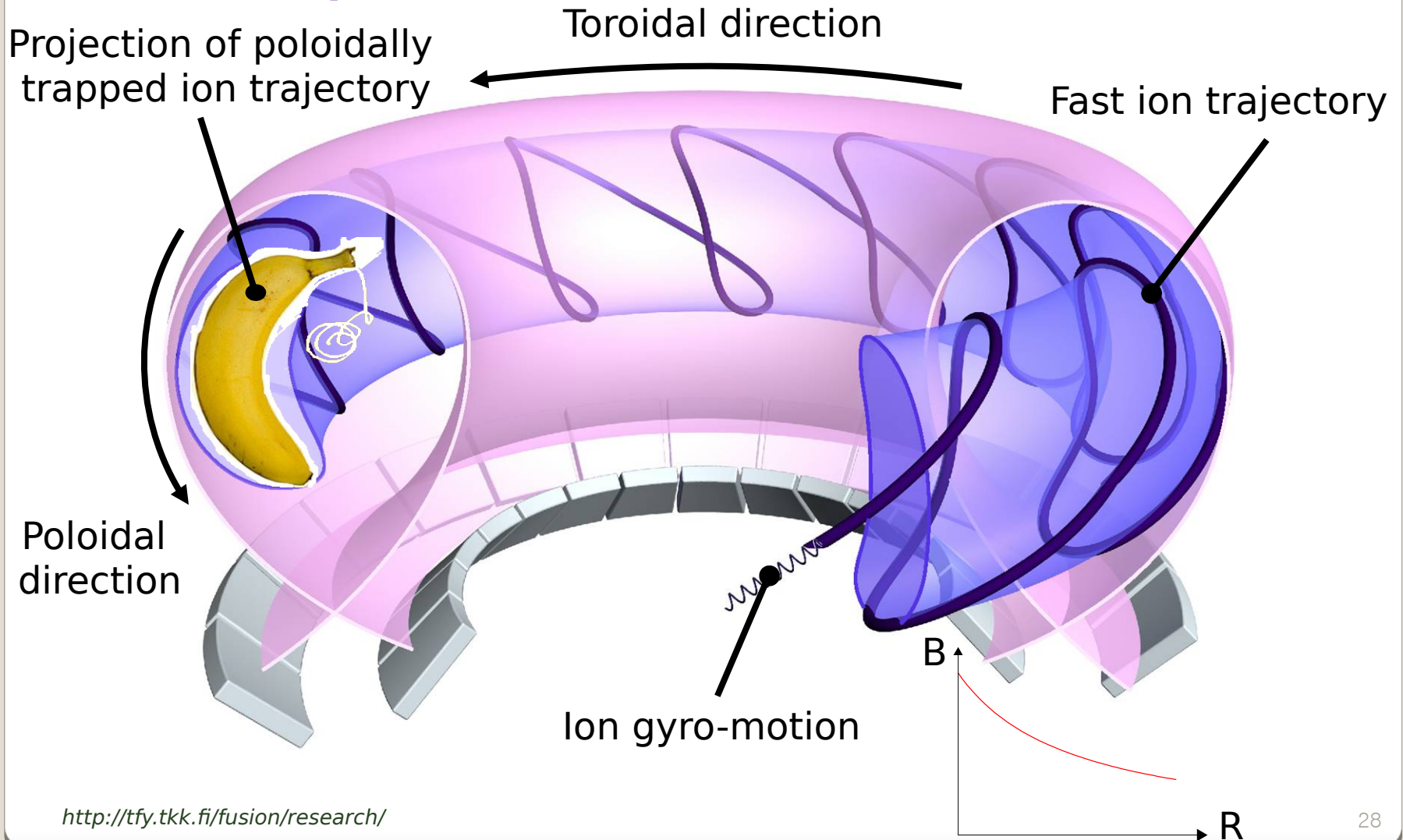
Non-inductive current drive

Does it make a closed loop?

Unfortunately, no!

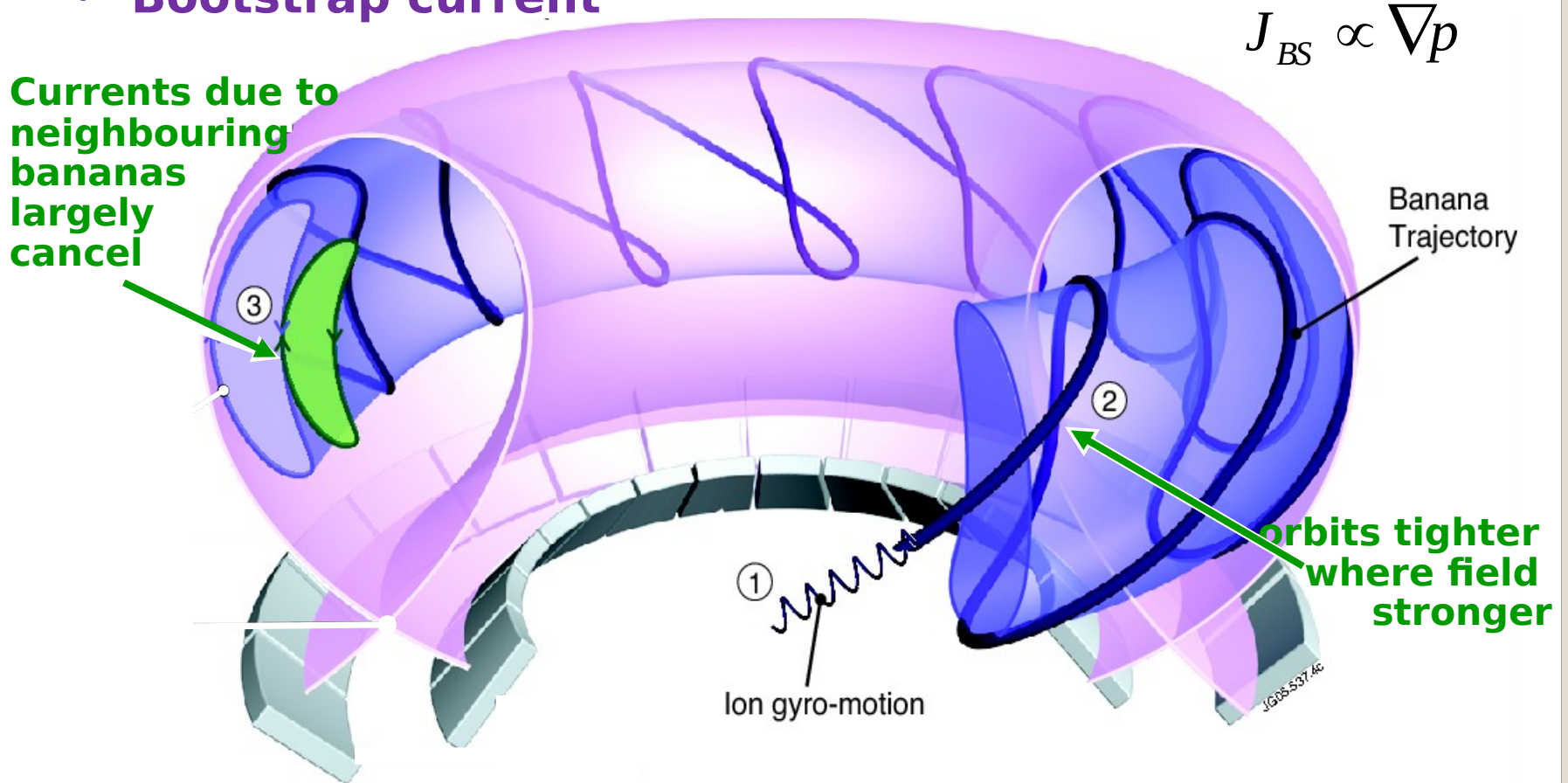
Current drive and current profile control

- **Bootstrap current**



Current drive and current profile control

- Bootstrap current



- More & faster particles on orbits nearer the core (green .VS. blue) lead to a net “banana current”.
- This is transferred to a helical bootstrap current via collisions.

Current drive and current profile control

- Bootstrap current

110

NATURE PHYSICAL SCIENCE VOL. 229 JANUARY 25 1971

HW. How can one measure bootstrap current?
Give examples of 100% bootstrap current drive.

Diffusion Driven Plasma Currents and Bootstrap Tokamak

by

R. J. BICKERTON, J. W. CONNOR & J. B. TAYLOR

UKAEA Research Group, Culham Laboratory, Abingdon, Berkshire

In toroidal systems of plasma confinement the intrinsic diffusion driven toroidal current modifies estimates of the maximum ratio of plasma pressure to magnetic field pressure. This intrinsic current may also make possible a type of Tokamak machine which operates in a steady state, unlike present pulsed designs.

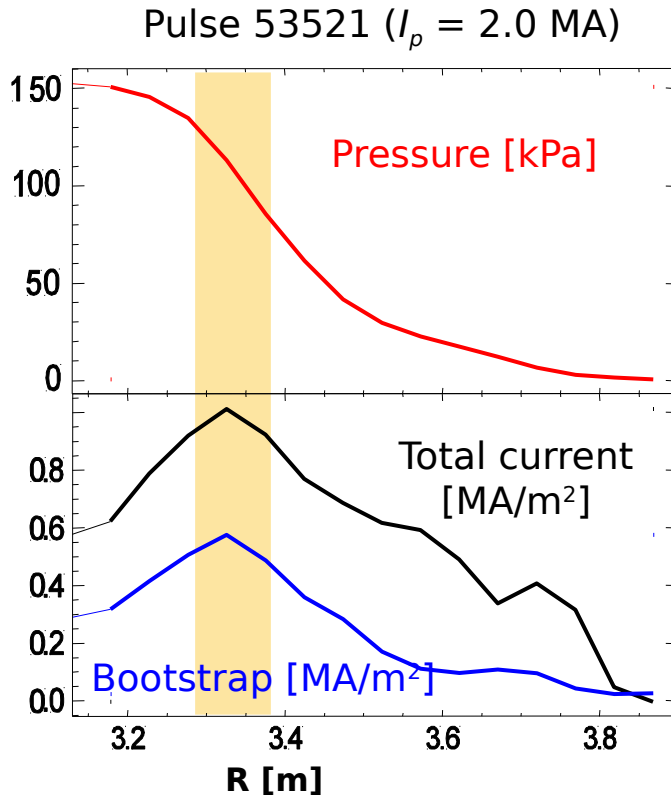
in what we call a “bootstrap” Tokamak. Such a machine could operate in a steady state, unlike present pulsed designs, because refuelling and thermonuclear reactions provide a continuous source of plasma to diffuse across the lines of force.

The existence of the intrinsic toroidal current is implicit in all calculations of toroidal diffusion and its value may be obtained easily from such calculations, so that only the result need be quoted here. For simplicity we consider the usual axisymmetric system with concentric magnetic surfaces $B_\phi = B_0/h$, $B_\theta = \Theta B_\phi$ with

$$\Theta = \epsilon \frac{t}{2\pi} \ll 1, \quad h = 1 + (r/R) \cos \theta, \quad \text{and } r, \theta, \phi$$

Current drive and current profile control

- Bootstrap current



Bootstrap current is not well aligned with the ITB foot.

→ q_{min} moves to the centre.

→ ITB lost finally.

Bickerton 1971 & Galeev 1970

Current drive and current profile control

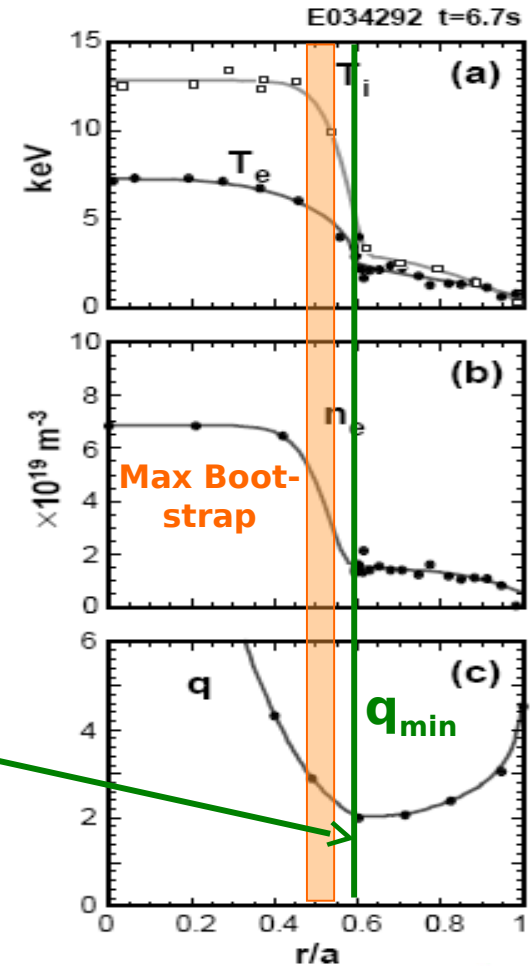
ITB foot location often correlated with q_{\min} radius



Pressure gradient and bootstrap current location

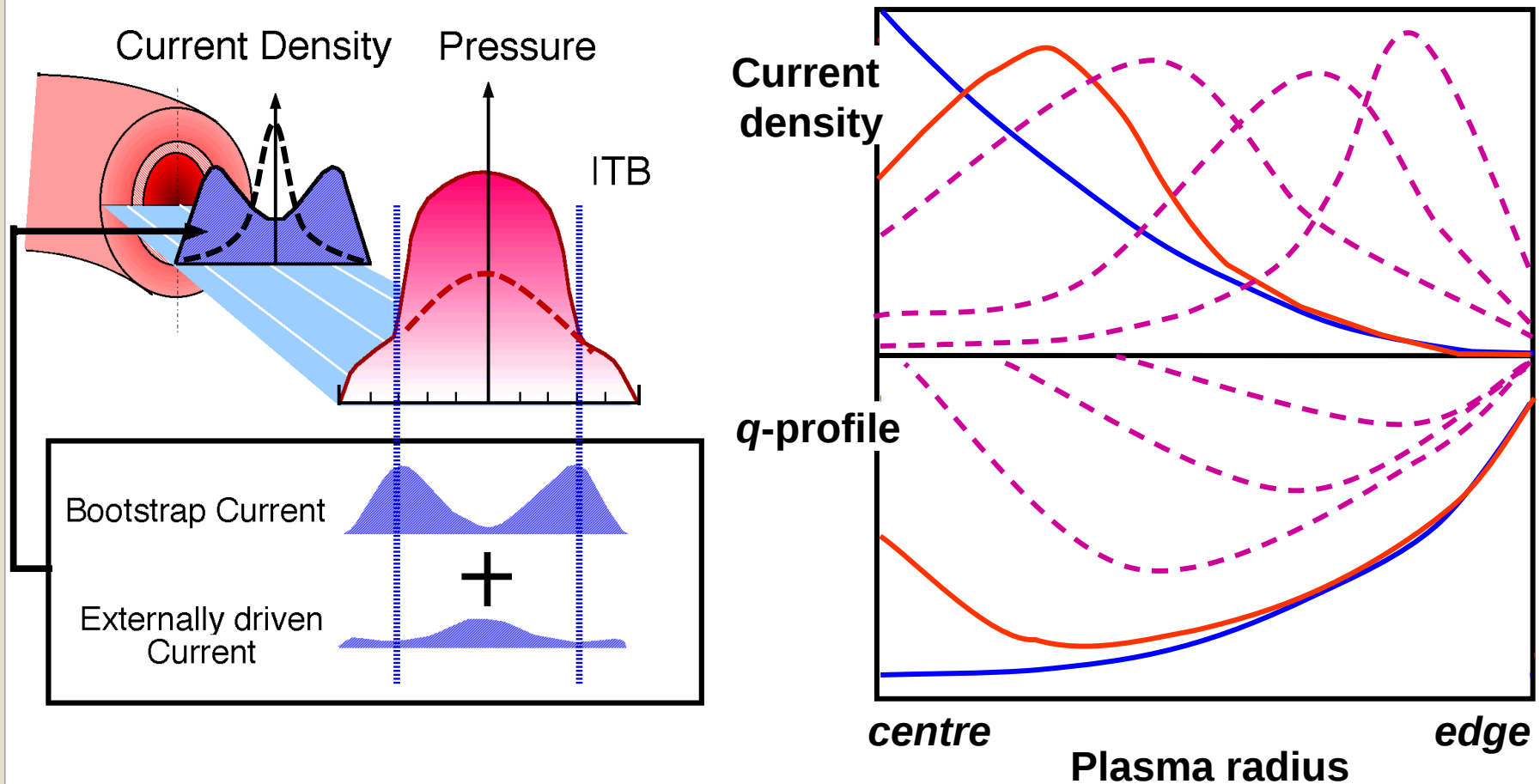
Current drive required to maintain the ITB in steady state (JT-60U)

- 100% bootstrap not likely:
need current drive at $r/a \sim 0.7$ for broad ITB



Sustainment of Non-monotonic Current Profile

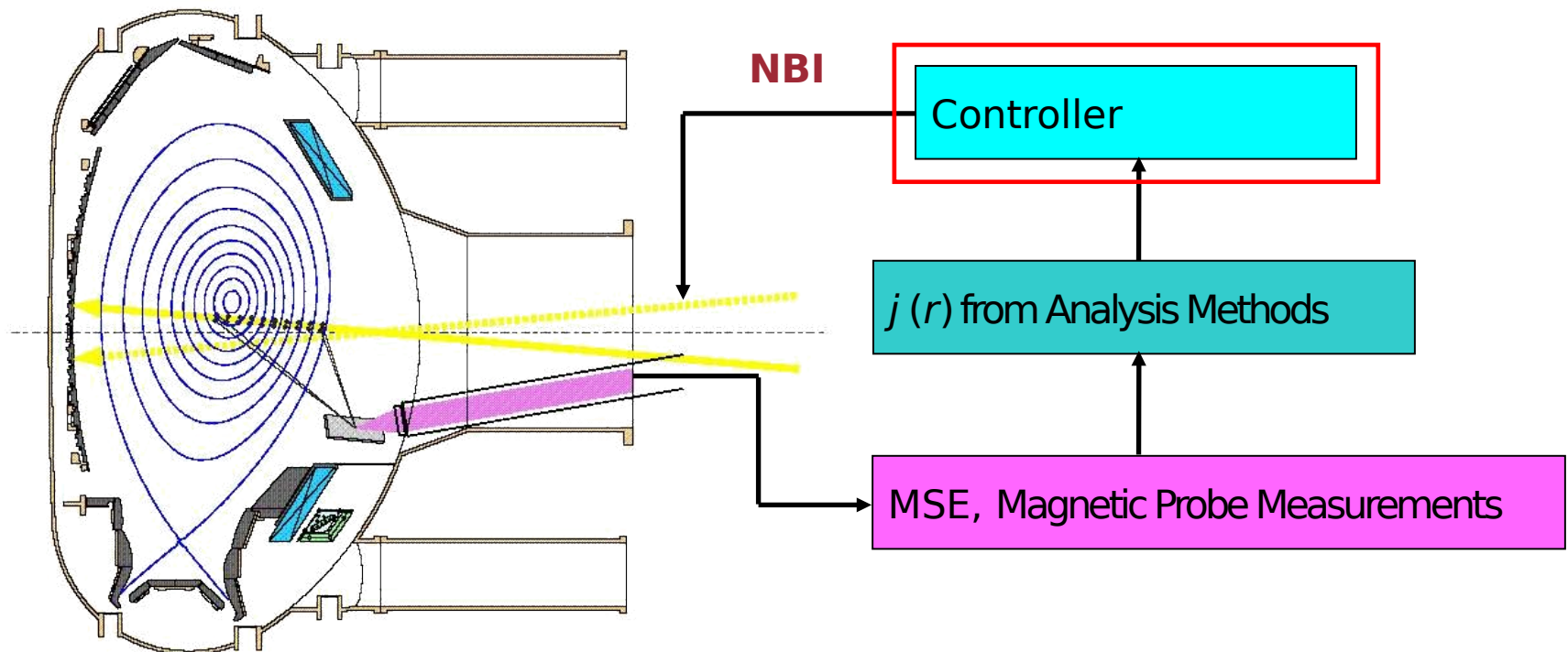
- Plasma current diffusion into the core from the edge



Current and pressure profile control !

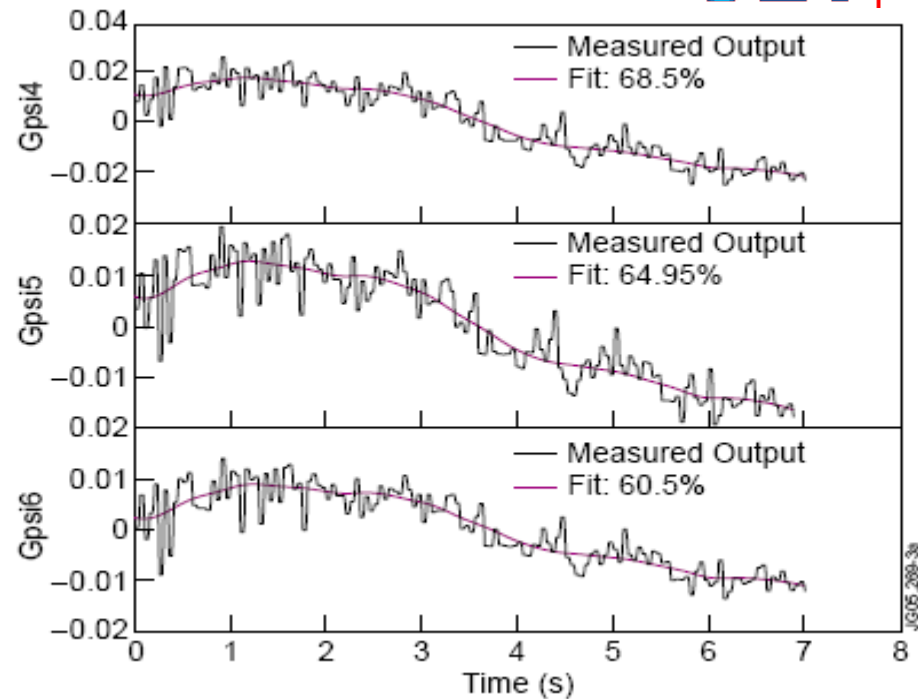
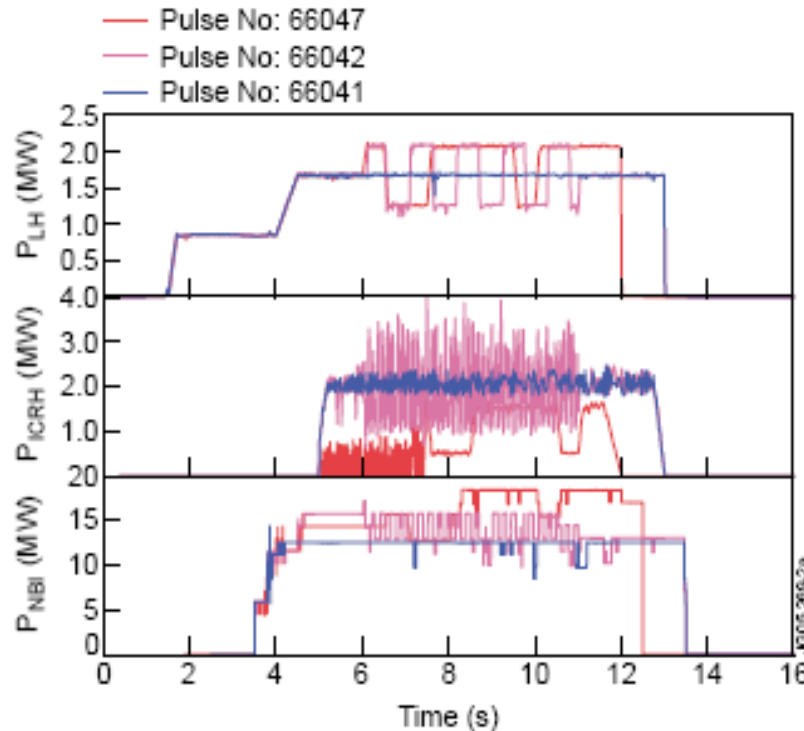
Reversed Shear Scenario

- Current density profile control at ASDEX Upgrade



RT Current and Pressure Profile Control

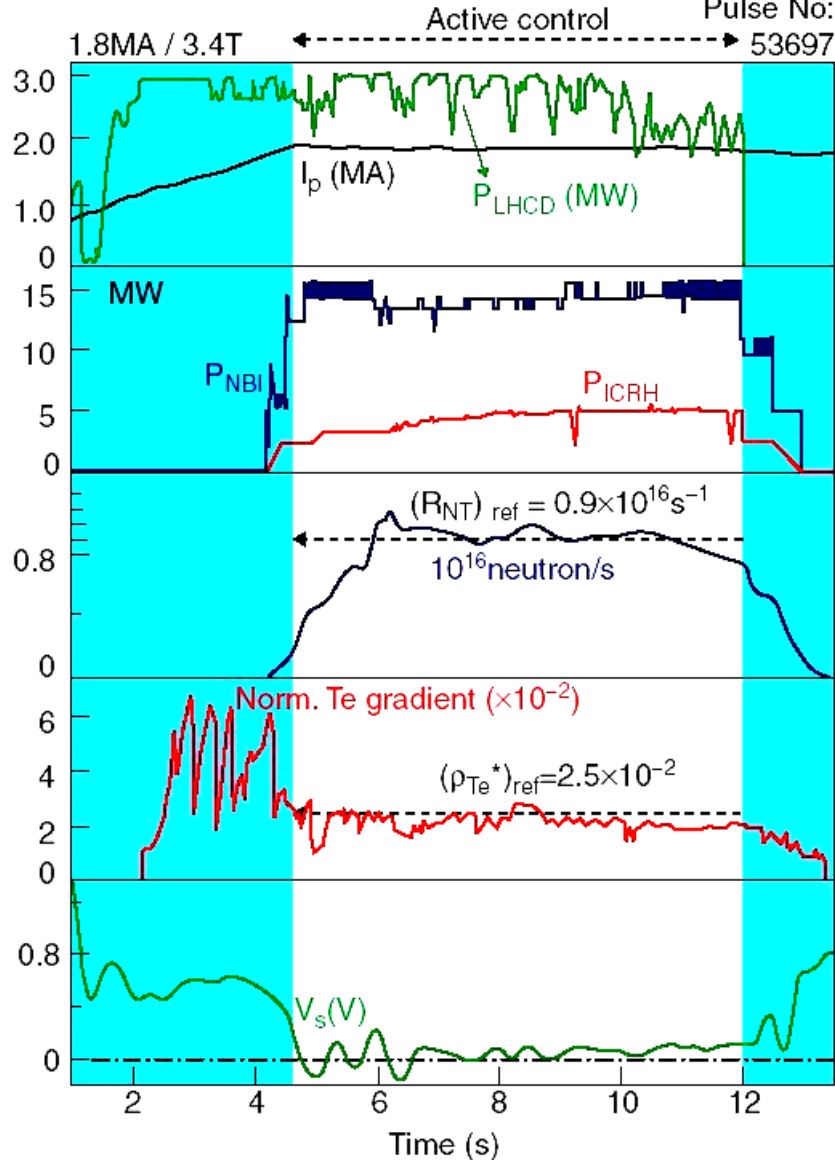
- Simultaneous control of distributed magnetic and kinetic parameters
- Dedicated experiments to identify controller coefficients



- Modulation combinations of actuators (NBI, LH, ICRH) to infer the coefficients of the state space model of the slow loop.
- Two control loops, 4 actuators (NBI, LH, ICRH, PF)

RT Current and Pressure Profile Control

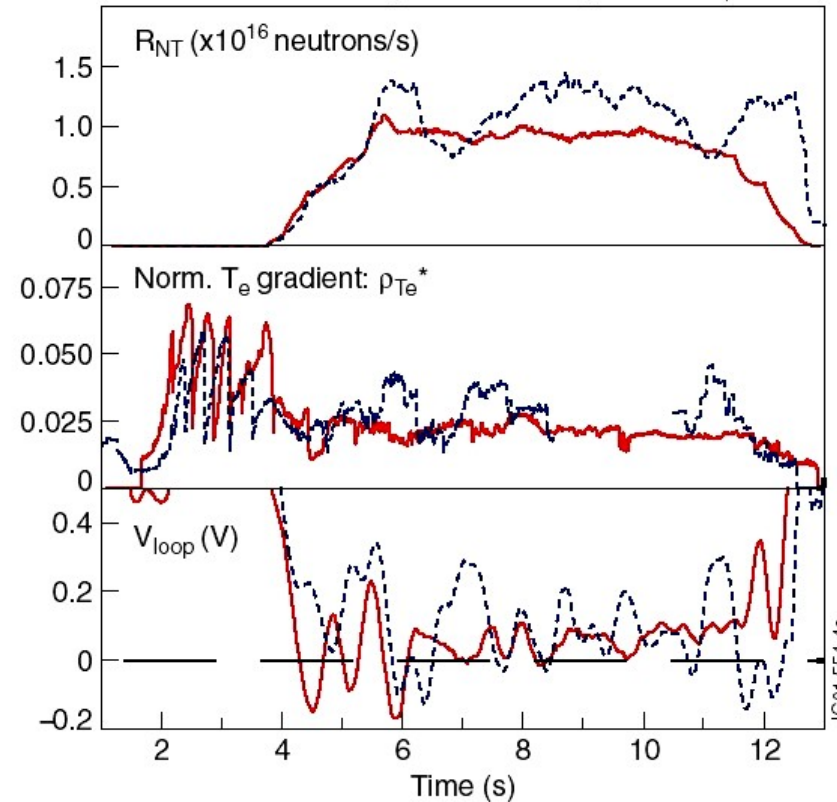
Pulse No: 53697



— Pulse No: 53697 (controlled)

--- Pulse No: 53521 (without control)

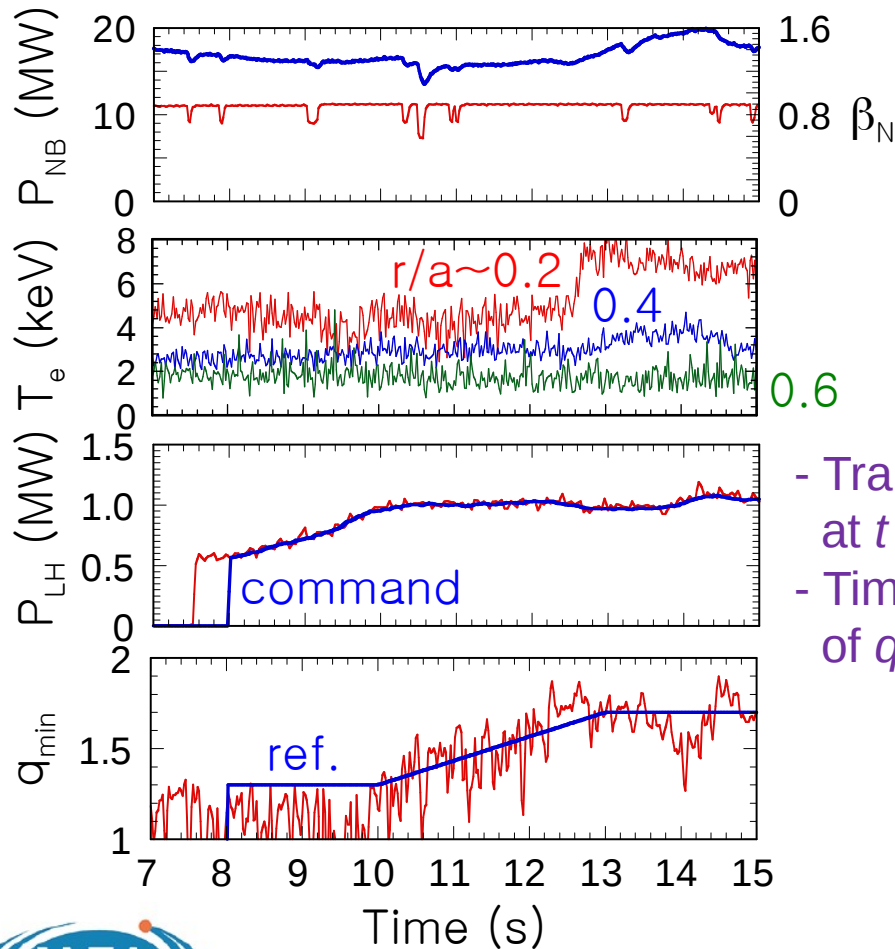
B₀ = 3.4T



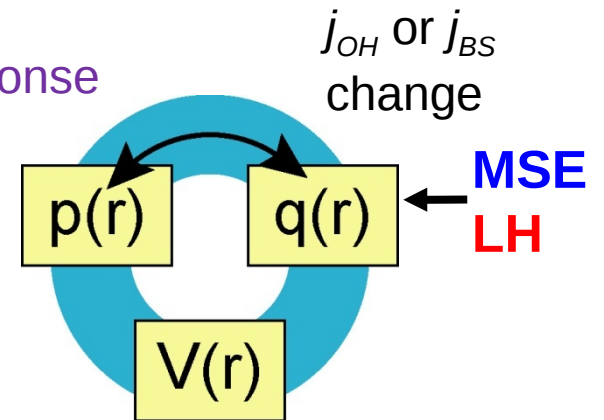
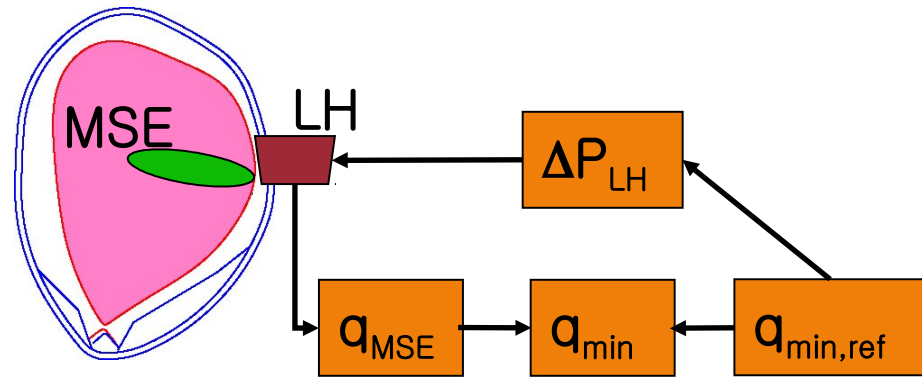
- Real time pressure profile and q-profile control to keep ITB steady

RT Current and Pressure Profile Control

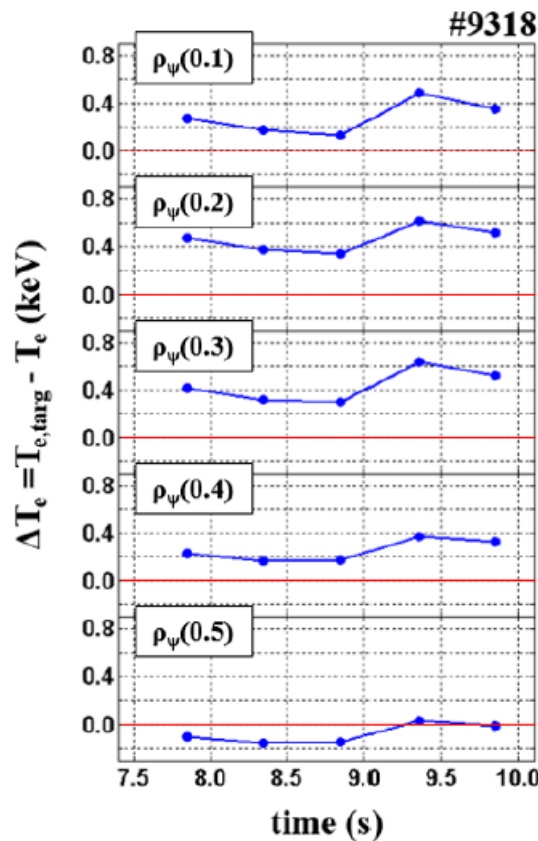
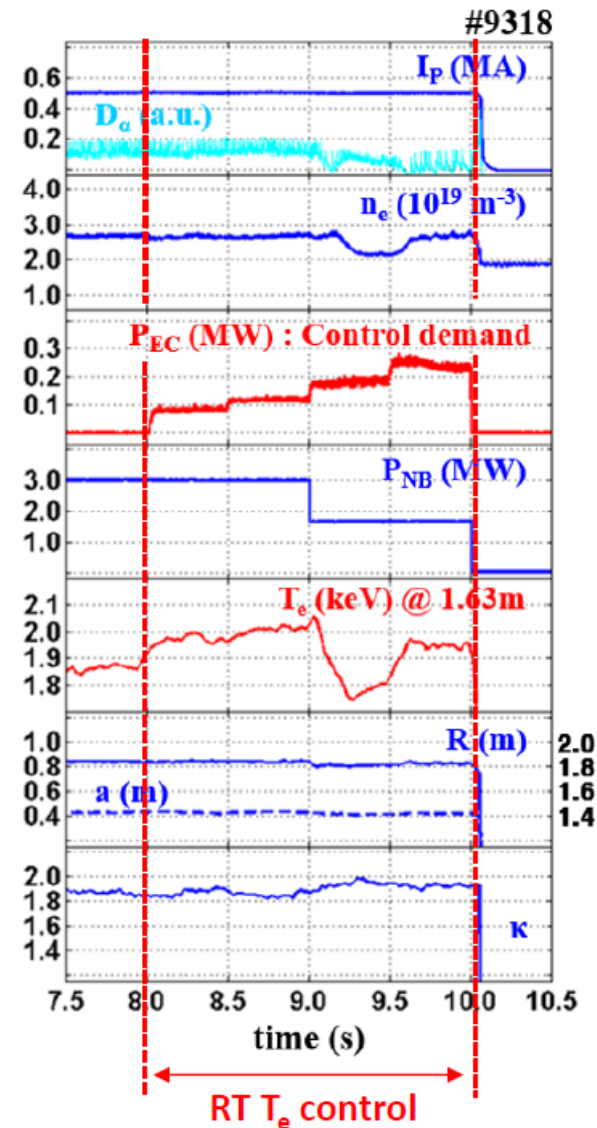
- JT60-U: Real time q_{min} control with MSE diagnostics and LHCD



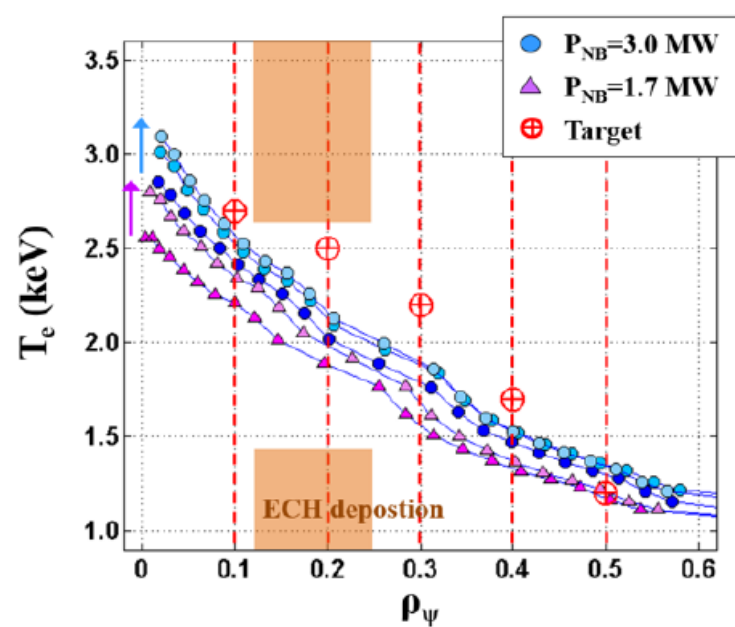
- Transport reduction at $t = 12.4$ s
- Time delay in response of q_{min}



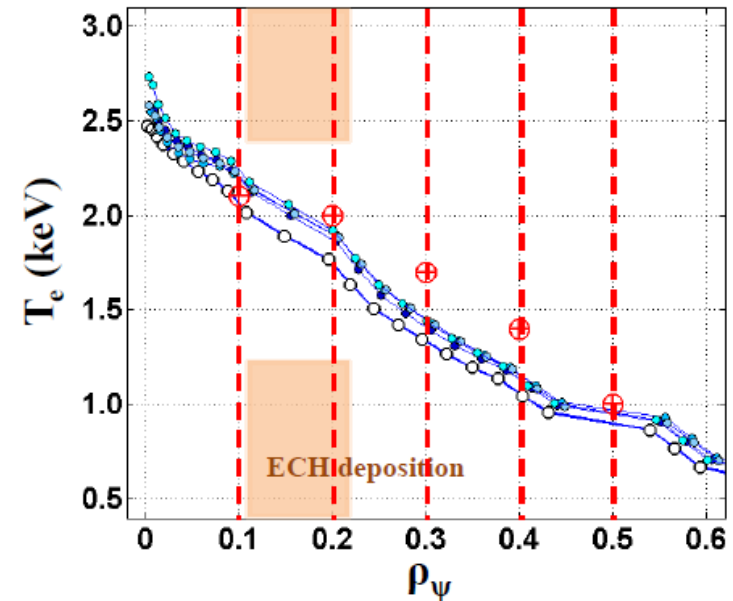
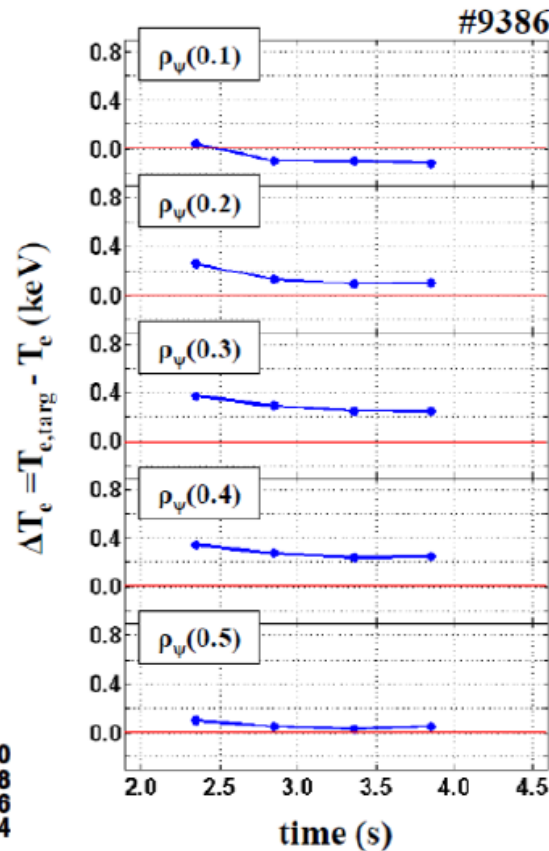
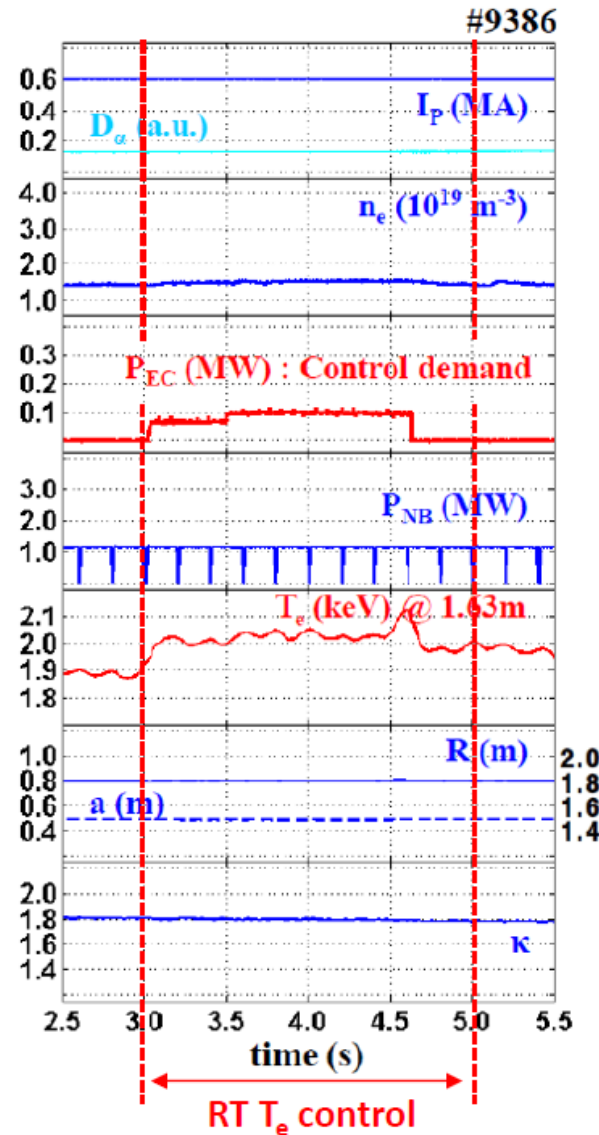
Experimental result of RT T_e control by ECH (H-mode)



✓ In **H-mode discharge**, T_e profile was controllable even in the presence of transient injection of P_{NB} with the model estimation, however T_e profile could not reach to the target due to limitation of EC source.



Experimental result of RT T_e control by ECH (L-mode)

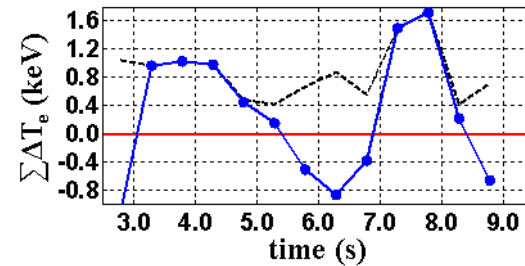
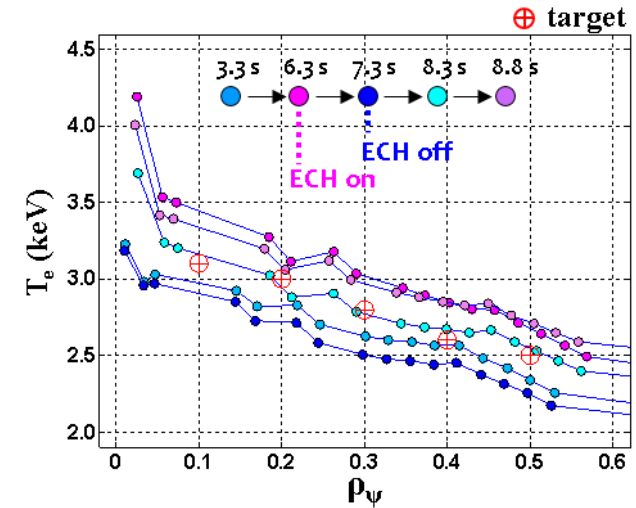
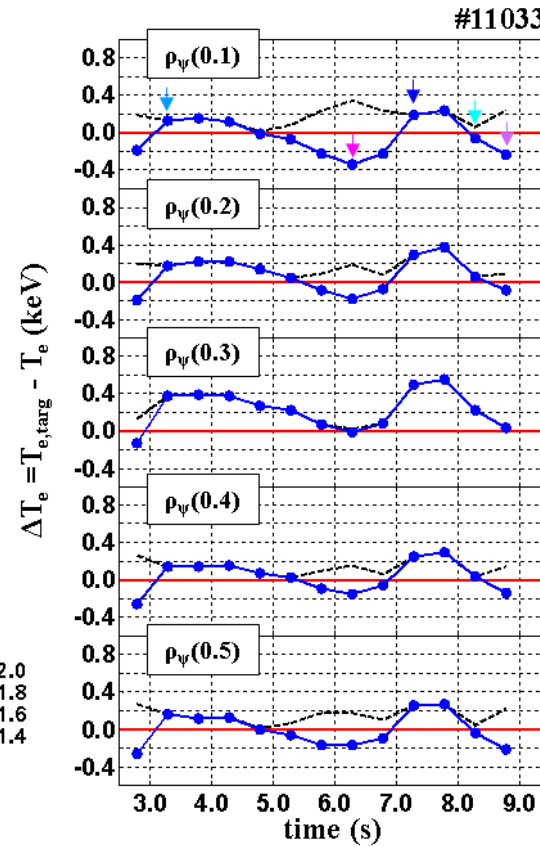
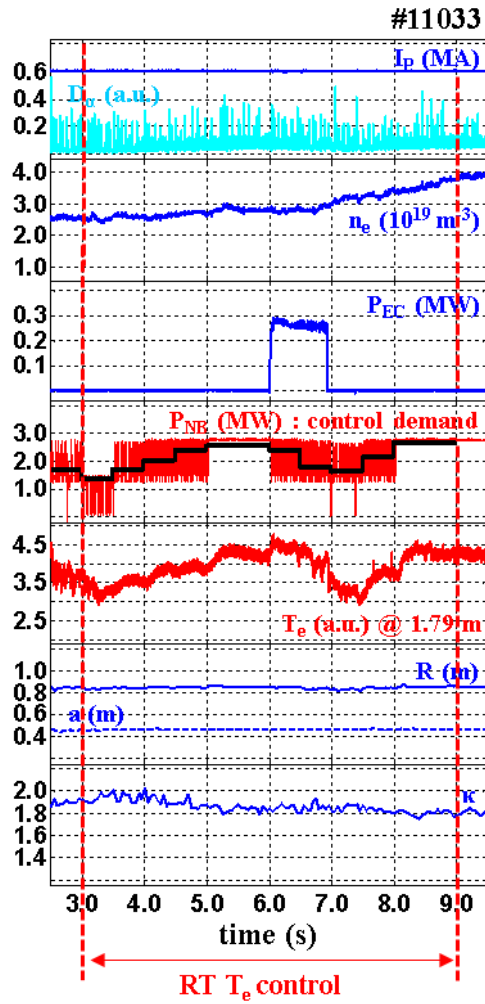


- ✓ In **L-mode discharge**, T_e profile was also controllable, however the control demand was stable right away to the 0.1 MW of P_{EC} based on the evaluation of SVD technique.

Experimental result of RT T_e control by NBI (H-mode)



Experimental result of real time T_e profile control (actuator: NBI)



➤ **In H-mode discharge, T_e profile was controllable by modulation of NBI power even in the presence of sudden injection of P_{EC} with the static system matrix estimation.**

Hyun-Seok Kim et al, IAEA FEC 2016

References

- *A. C. C. Sips*, Seminars