

INVISCID FLOW

Week 4

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Inviscid Flow

Basic Conservation Laws – Viscosity Coefficients

- Let's find a physical meaning of two parameters, λ and μ
- Consider a simple shear flow in an incompressible fluid where the velocity is defined as $u = u(y)$ and $v = w = 0$.

$$\sigma_{ij} = -p\delta_{ij} + \lambda\delta_{ij}\frac{\partial u_k}{\partial x_k} + \mu\left(\frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j}\right) \quad \Rightarrow \quad \begin{aligned} \sigma_{12} &= \sigma_{21} = \mu \frac{du}{dy} \\ \sigma_{11} &= \sigma_{22} = \sigma_{33} = -p \\ \sigma_{13} &= \sigma_{31} = \sigma_{23} = \sigma_{32} = 0 \end{aligned}$$

- from Newton's law of viscosity, the proportionality factor (μ) between the shear stress and the velocity gradient in a simple shear flow is the dynamic viscosity
 - Kinematic viscosity $\nu = \mu/\rho$

Basic Conservation Laws – Viscosity Coefficients

- λ is usually referred as a second viscosity coefficient
- Let's consider the average of normal stress components as

$$-\bar{p} = \frac{1}{3}(\sigma_{11} + \sigma_{22} + \sigma_{33})$$

- This is mechanical pressure, i.e., coming from hydrostatics and/or from the motion of a fluid
- Different from the thermodynamic pressure
- σ_{ii} = trace of σ

$$-\bar{p} = -p + \lambda \frac{\partial u_k}{\partial x_k} + \frac{2}{3} \mu \frac{\partial u_k}{\partial x_k} = -p + \left(\lambda + \frac{2}{3} \mu\right) \frac{\partial u_k}{\partial x_k}$$

- Difference between the thermodynamic pressure and the mechanical pressure is proportional to the divergence of the velocity vector

Basic Conservation Laws – Viscosity Coefficients

$$p - \bar{p} = \left(\lambda + \frac{2}{3} \mu\right) \frac{\partial u_k}{\partial x_k} = K \frac{\partial u_k}{\partial x_k} \quad K: \text{bulk viscosity}$$

- What is bulk viscosity?
 - mechanical pressure is a measure of the translational energy of the molecules only
 - thermodynamic pressure is a measure of the total energy, which includes vibrational and rotational modes of energy as well as the translational mode
 - in a flow field, it is possible to have energy transferred from one mode to another
 - bulk viscosity is a measure of this transfer of energy from the translational mode to the other modes
 - If the fluid is a monatomic gas, the only mode of molecular energy is the translational mode. Then, the mechanical pressure and thermodynamic pressure are the same: $\lambda = -\frac{2}{3} \mu$ Stoke's relation

Basic Conservation Laws – Navier-Stokes Equation

$$\rho \frac{\partial u_j}{\partial t} + \rho u_k \frac{\partial u_j}{\partial x_k} = \frac{\partial \sigma_{ij}}{\partial x_i} + \rho f_j \quad \sigma_{ij} = -p\delta_{ij} + \lambda \delta_{ij} \frac{\partial u_k}{\partial x_k} + \mu \left(\frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} \right)$$

- Momentum conservation eqn + Newtonian fluid constitutive eqn → Navier-Stokes Eqn

$$\begin{aligned} \frac{\partial \sigma_{ij}}{\partial x_i} &= \frac{\partial}{\partial x_i} \left[-p\delta_{ij} + \lambda \delta_{ij} \frac{\partial u_k}{\partial x_k} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] \\ &= -\frac{\partial p}{\partial x_j} + \frac{\partial}{\partial x_j} \left(\lambda \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] \end{aligned}$$

$$\rho \frac{\partial u_j}{\partial t} + \rho u_k \frac{\partial u_j}{\partial x_k} = -\frac{\partial p}{\partial x_j} + \frac{\partial}{\partial x_j} \left(\lambda \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] + \rho f_j$$

Basic Conservation Laws – Navier-Stokes Equation

- In incompressible (constant density) and constant viscosity flow,

$$\begin{aligned} \rho \frac{\partial u_j}{\partial t} + \rho u_k \frac{\partial u_j}{\partial x_k} &= -\frac{\partial p}{\partial x_j} + \frac{\partial}{\partial x_j} \left(\lambda \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] + \rho f_j \\ \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] &= \mu \left[\frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_i} \right) + \frac{\partial^2 u_j}{\partial x_i \partial x_i} \right] = \mu \frac{\partial^2 u_j}{\partial x_i \partial x_i} \end{aligned}$$

$$\Rightarrow \rho \frac{\partial u_j}{\partial t} + \rho u_k \frac{\partial u_j}{\partial x_k} = -\frac{\partial p}{\partial x_j} + \mu \frac{\partial^2 u_j}{\partial x_i \partial x_i} + \rho f_i$$

- If we can ignore the effect of viscosity,

$$\Rightarrow \rho \frac{\partial u_j}{\partial t} + \rho u_k \frac{\partial u_j}{\partial x_k} = -\frac{\partial p}{\partial x_j} + \rho f_i \quad \text{Euler Equation} \rightarrow \text{Inviscid Flow}$$

Basic Conservation Laws – Energy Equations

- The first term at RHS of energy conservation eqn,

$$\rho \frac{\partial e}{\partial t} + \rho u_k \frac{\partial e}{\partial x_k} = \underbrace{\sigma_{ij} \frac{\partial u_j}{\partial x_i}}_{\text{Work done by the surface stresses}} \frac{\partial q_j}{\partial x_j}$$

$$\sigma_{ij} \frac{\partial u_j}{\partial x_i} = \left[-p \delta_{ij} + \lambda \delta_{ij} \frac{\partial u_k}{\partial x_k} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] \frac{\partial u_j}{\partial x_i}$$

$$= \underbrace{-p \frac{\partial u_k}{\partial x_k}}_{\text{reversible transfer of energy due to compression}} + \underbrace{\lambda \left(\frac{\partial u_k}{\partial x_k} \right)^2 + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_j}{\partial x_i}}_{\text{Dissipation function, } \Phi}$$

Basic Conservation Laws – Energy Equations

$$\Phi = \lambda \left(\frac{\partial u_k}{\partial x_k} \right)^2 + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_j}{\partial x_i}$$

- This is a measure of the rate at which mechanical energy is being converted into thermal energy → Dissipation function
- For an incompressible flow,

$$\Phi = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_j}{\partial x_i}$$

$$= \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \left[\frac{1}{2} \left(\frac{\partial u_j}{\partial x_i} - \frac{\partial u_i}{\partial x_j} \right) + \frac{1}{2} \left(\frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} \right) \right]$$

$$= \frac{1}{2} \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)^2 \quad \rightarrow \text{Positive definite} \rightarrow \text{dissipation function}$$

always works to increase irreversibly the internal energy of an incompressible fluid

Basic Conservation Laws – Energy Equations

- Using the dissipation function and Fourier's law, the energy eqn becomes

$$\rho \frac{\partial e}{\partial t} + \rho u_k \frac{\partial e}{\partial x_k} = -p \frac{\partial u_k}{\partial x_k} + \frac{\partial}{\partial x_j} \left(k \frac{\partial T}{\partial x_j} \right) + \Phi$$

$$\Phi = \lambda \left(\frac{\partial u_k}{\partial x_k} \right)^2 + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_j}{\partial x_i}$$

Basic Conservation Laws – Governing Equations

- For newtonian fluids, in summary

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_k} (\rho u_k) = 0$$

$$\rho \frac{\partial u_j}{\partial t} + \rho u_k \frac{\partial u_j}{\partial x_k} = -\frac{\partial p}{\partial x_j} + \frac{\partial}{\partial x_j} \left(\lambda \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] + \rho f_j$$

$$\rho \frac{\partial e}{\partial t} + \rho u_k \frac{\partial e}{\partial x_k} = -p \frac{\partial u_k}{\partial x_k} + \lambda \left(\frac{\partial u_k}{\partial x_k} \right)^2 + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_j}{\partial x_i} + \frac{\partial}{\partial x_j} \left(k \frac{\partial T}{\partial x_j} \right)$$

$$p = p(\rho, T) \text{ e.g., } p = \rho RT \text{ for ideal gas}$$

$$e = e(\rho, T) \text{ e.g., } e = C_v T$$

- Seven unknowns: p , ρ , e , T , and u_j

Basic Conservation Laws – Boundary Conditions

- Navier-Stokes equations are, mathematically, a set of three elliptic, second-order PDEs. The appropriate type of boundary conditions are therefore Dirichlet or Neumann conditions on a closed boundary
 - Dirichlet condition: one prescribes the value of a variable at the boundary, e.g. $u(x) = \text{constant}$
 - Neumann condition: one prescribes the gradient normal to the boundary of a variable at the boundary, e.g. $\partial u / \partial n = \text{constant}$.
- Physically, this usually amounts to specifying the velocity on all solid boundaries.
 - No-slip condition except for a few special cases