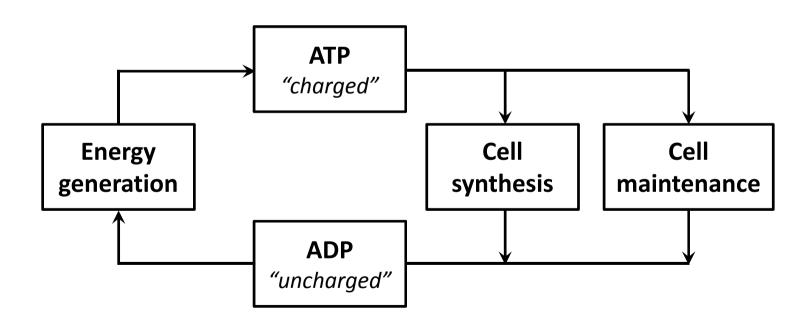
# **Bacterial energetics**

# Today's lecture

- Bacterial energetics overview
- Gibbs free energy of reaction
- Correlating reaction energetics and yield coefficient

#### **Bacterial energetics**

 Microorganisms carry out redox reactions to obtain energy for growth and cell maintenance



#### **Energetics and growth: thoughts**

- Bacterial cells grow more rapidly when:
  - More energy is obtained by oxidation of (an e<sup>-</sup> equivalent of) an e<sup>-</sup> donor
  - More energy is obtained by reduction of (an e<sup>-</sup> equivalent of) an e<sup>-</sup> acceptor
  - Conditions are favorable...
    - for rapid utilization of substrates
    - abundance of e<sup>-</sup> donor, e<sup>-</sup> acceptor, nutrients, etc.
    - low concentration of inhibiting compounds

## **Energetics and growth: math**

$$Y_n = Y - b \frac{X_a}{-dS/dt}$$

- $-Y_n \uparrow$  when  $Y \uparrow$ : favorable  $e^-$  donor and acceptor
- $-Y_n \uparrow$  when  $X_a << -dS/dt$ : favorable conditions for substrate utilization

<sup>\*</sup> We will discuss about the -dS/dt term in forthcoming lectures!

# Gibbs free energy: standard conditions

- "Standard" free energy
  - $-\Delta G^0$ , free energy at 25°C, 1 atm, and unit activity for any chemicals involved
  - $-\Delta G^{0\prime}$ , standard free energy adjusted to pH=7

ex) 
$$\frac{1}{4}O_2 + H^+ + e^- = \frac{1}{2}H_2O$$
  
 $\Delta G^0$  is for  $\{O_2\} = P_{O_2} = 1$  atm  
 $\{H^+\} = 1 \text{ (pH = 0)}$   
 $\{H_2O\} = 1$   
 $\Delta G^{0'}$  is for  $\{O_2\} = P_{O_2} = 1$  atm  
 $\{H^+\} = 10^{-7}$ )  
 $\{H_2O\} = 1$ 

 $\{H_2O\} = 1$  applies to any dilute aqueous solutions

# Free energy of formation, $\Delta G_f$

 Gibbs free energy that accompanies the formation of 1 mole of the substance from its component elements

# Gibbs free energy change of reaction

• Free energy change of reaction,  $\Delta G_r$ 

$$\sum (product \Delta G_f) - \sum (reactant \Delta G_f)$$

For a generic reaction written as

$$0 = \sum_{i=1}^{n} v_{ir} A_i$$

 $0 = \sum_{i=1}^{n} v_{ir} A_i$   $v_{ir} = \text{stoichiometric coefficient, (-) for reactants, (+) for}$ 

 $A_i$  = reaction constituent, reactants or products

 $\Delta G_r$  can be written as

$$\Delta G_r = \sum_{i=1}^n v_{ir} \Delta G_f$$

# Reaction free energy

**Q1:** Calculate the standard free energy adjusted pH 7 for the half reaction of 2-chlorobenzoate formation as given below.

$$\frac{1}{28}HCO_3^-(aq) + \frac{3}{14}CO_2(g) + \frac{1}{28}Cl^-(aq) + \frac{29}{28}H^+(aq) + e^- \rightarrow$$

$$\frac{1}{28}C_6H_4ClCOO^-(aq) + \frac{13}{28}H_2O(l)$$

Use the following values of free energy of formation (in textbook Appendix A):

Species	HCO <sub>3</sub> -(aq)	CO <sub>2</sub> (g)	Cl <sup>-</sup> (aq)	H <sup>+</sup> (aq, 10 <sup>-7</sup> )	C <sub>6</sub> H <sub>4</sub> CICOO <sup>-</sup> (aq)	H <sub>2</sub> O(I)
ΔG <sub>f</sub> <sup>0</sup> ′ @ 25°C (kJ/mole)	-586.85	-394.36	-31.35	-39.87	-237.9	-237.18

$$\frac{1}{28}HCO_3^-(aq) + \frac{3}{14}CO_2(g) + \frac{1}{28}Cl^-(aq) + \frac{29}{28}H^+(aq) + e^- \rightarrow \frac{1}{28}C_6H_4ClCOO^-(aq) + \frac{13}{28}H_2O(l)$$

Species	HCO <sub>3</sub> -(aq)	CO <sub>2</sub> (g)	Cl <sup>-</sup> (aq)	H <sup>+</sup> (aq, 10 <sup>-7</sup> )	C <sub>6</sub> H <sub>4</sub> ClCOO <sup>-</sup> (aq)	H <sub>2</sub> O(I)
$\Delta G_f^{0'}$ @ 25°C (kJ/mole)	-586.85	-394.36	-31.35	-39.87	-237.9	-237.18

$$\Delta G_r = \sum_{i=1}^n v_{ir} \Delta G_f$$

 $v_{ir}$  = stoichiometric coefficient, (-) for reactants, (+) for products

$$\Delta G_r^{0'} = \left(\frac{1}{28} \times (-586.85) + \frac{3}{14} \times (-394.36) + \frac{1}{28} \times (-31.35) + \frac{29}{28} \times (-39.87)\right) + \left\{\frac{1}{28} \times (-237.9) + \frac{13}{28} \times (-237.18)\right\}$$

$$= 29.26 \, kJ/e^- \, eq$$

# Reaction free energy

**Q2:** Calculate the standard free energy adjusted pH 7 for overall energy reaction with ethanol as an e<sup>-</sup> donor and oxygen as an e<sup>-</sup> acceptor. Use the half reactions listed in Table 2.2 and 2.3.

$$R_d$$
: O-5  $\Delta G_r^{0'} = 31.18 \, kJ/e^- \, eq$ 

R<sub>a</sub>: I-14 
$$\Delta G_r^{0'} = -78.72 \, kJ/e^- \, eq$$

$$R_{e} = R_{a} - R_{d}$$

$$\Delta G_{r}^{0'}(R_{e}) = \Delta G_{r}^{0'}(R_{a}) - \Delta G_{r}^{0'}(R_{d})$$

$$R_{a}: \frac{1}{4}O_{2} + H^{+} + e^{-} = \frac{1}{2}H_{2}O$$

$$= -78.72 - 31.18$$

$$-R_{d}: \frac{1}{12}C_{2}H_{5}OH + \frac{1}{4}H_{2}O = \frac{1}{6}CO_{2} + H^{+} + e^{-}$$

$$= -109.90 kJ/e^{-} eq$$

R<sub>e</sub>: 
$$\frac{1}{12}C_2H_5OH + \frac{1}{4}O_2 = \frac{1}{6}CO_2 + \frac{1}{4}H_2O$$

#### Reaction free energy: general conditions

For nonstandard conditions,

$$\Delta G_r = \Delta G_r^0 + RT \sum_{i=1}^n v_{ir} ln a_i$$

 $a_i$  = activity of constituent  $A_i$  R = gas constant,  $8.314 \times 10^{-3} \ kJ/mole - K$ T = absolute temperature, K

#### **Caution:**

- $v_{ir}$  is negative for reactants and positive for products
- $\Delta G_r^{~0}$  is for standard conditions -- pH=0 From  $\Delta G_r^{~0}$ ', we can calculate  $\Delta G_r^{~0}$  by:  $\Delta G_r^{~0} = \Delta G_r^{~0}$ ' RT $v_{H^+}ln[10^{-7}]$

# Reaction free energy

**Q3:** Calculate the free energy of reaction for aerobic ethanol degradation at the following conditions:  $T = 20^{\circ}C$ , pH = 5.0,  $[C_2H_5OH] = 2 \times 10^{-3} M$ ,  $P_{CO2} = 3 \times 10^{-4} atm$ ,  $P_{O2} = 0.21 atm$ .

#### From Q2,

$$\Delta G_r^{0'} = -109.90 \ kJ/e^- \ eq$$

$$R_e: \quad \frac{1}{12}C_2H_5OH + \frac{1}{4}O_2 = \frac{1}{6}CO_2 + \frac{1}{4}H_2O$$

$$\Delta G_r^0 = \Delta G_r^{0'} - RTv_{H^+}ln[10^{-7}] = G_r^{0'} - 0 = G_r^{0'}$$

$$\Delta G_r = \Delta G_r^0 + RT \sum_{i=1}^n v_{ir} ln a_i$$

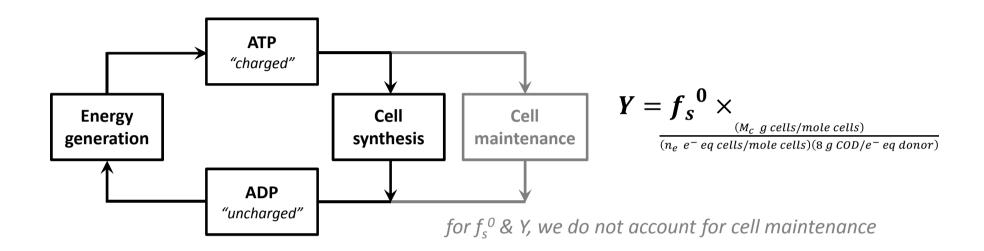
$$= -109.90 \, kJ/e^- \, eq + (8.314 \times 10^{-3} \, kJ/mole - K) \times (293 \, K)$$

$$\times \left\{ -\frac{1}{12} ln(2 \times 10^{-3}) - \frac{1}{4} ln(0.21) + \frac{1}{6} ln(3 \times 10^{-4}) + \frac{1}{4} ln(1) \right\}$$

$$=-110.98 \, kJ/e^- \, eq$$

 $a_{H_2O} = 1$  for aqueous solutions; you may omit the water term

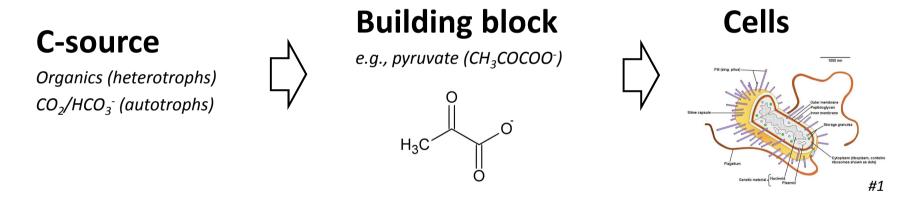
## Deriving $f_s^0$ or Y by thermodynamic principles



- To determine  $f_s^0$  or Y we consider the energy balance for cell synthesis
  - energy is needed (ATP→ADP) to synthesize cells [1]
  - energy reaction  $(R_e)$  supplies the required energy (ADP $\rightarrow$ ATP) [2]
  - At steady state,energy required for [1] = energy supplied by [2]

#### Two steps of <u>cell synthesis</u>, the efficiency

 We conceptualize the cell synthesis mechanism into two steps



- 1) Carbon source is metabolized to form a building block
- 2) The building block is synthesized to a cell
- We should consider that bacteria are not 100% efficient engines -- each step involves energy loss!

# $\Delta G_p$ (C-source $\rightarrow$ pyruvate), $\Delta G_{pc}$ (pyruvate $\rightarrow$ cells)

• Energy required to convert carbon source to pyruvate,  $\Delta G_p$  (heterotrophic bacteria, ammonia as N source):

```
\Delta G_p = 35.09 - \Delta G_c^{0\prime}
(in kJ/e^- eq)
35.09 = reaction free energy for formation of pyruvate from CO<sub>2</sub>
<math display="block">\Delta G_c^{0\prime} = reaction free energy for formation of carbon source from CO<sub>2</sub>
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• Energy required to convert pyruvate to cells,  $\Delta G_{pc}$  = 18.8 kJ/e<sup>-</sup> eq

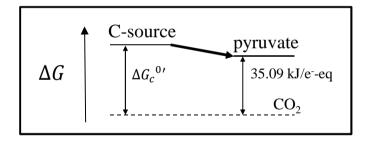
(estimated value for a cell formula of  $C_5H_7O_2N$  using  $NH_4^+$  as a N source)

# $\Delta G_S$ (C-source $\rightarrow$ cells)

• Energy required for cell synthesis from the carbon source,  $\Delta G_s$ :

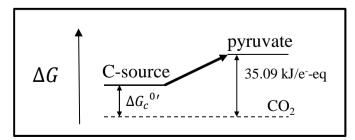
if  $\Delta G_p < 0$  (C-source is at higher energy state than pyruvate)

$$\Delta G_{S} = \varepsilon \Delta G_{p} + \frac{\Delta G_{pc}}{\varepsilon}$$



if  $\Delta G_p > 0$  (C-source is at lower energy state than pyruvate)

$$\Delta G_{S} = \frac{\Delta G_{p}}{\varepsilon} + \frac{\Delta G_{pc}}{\varepsilon}$$



 $\varepsilon$  = energy transfer efficiency

#### **Energy balance of overall reaction**

- The energy obtained by an energy reaction is used to synthesize cells
- Energy obtained = Energy used (at steady state)
- Keep in mind that bacteria cannot use 100% of the energy available by an energy reaction (energy transfer efficiency,  $\varepsilon$ )
- Therefore we write

$$A\varepsilon\Delta G_r + \Delta G_s = 0$$

 $A = e^-$  equivalent of  $e^-$  donor used for energy production per  $e^-$  equivalent of cells formed  $\Delta G_r =$  reaction free energy for energy reaction  $= \Delta G_a - \Delta G_d$  (per  $e^-$ -eq)  $\Delta G_S =$  energy required for cell synthesis from the carbon source (per  $e^-$ -eq)

# Deriving $f_s^0$ or Y by thermodynamic principles

• Solving for 
$$A$$
: 
$$A = -\frac{\Delta G_p/\varepsilon^n + \Delta G_{pc}/\varepsilon}{\varepsilon \Delta G_r} \qquad n = -1 \text{ for } \Delta G_p < 0$$

$$n$$
 = -1 for  $\Delta G_p < 0$   
+1 for  $\Delta G_p > 0$ 

• From A, we can calculate  $f_s^0$  and  $f_e^0$  as:

$$f_s^0 = \frac{1}{1+A}$$
  $f_e^0 = 1 - f_s^0 = \frac{A}{1+A}$ 

- Energy transfer efficiency, ε
  - 55-70% under optimal conditions
  - Use 0.6 for ordinary cases

#### Deriving $f_s^0$ or Y by thermodynamic principles

**Q4:** Estimate  $f_s^0$  and Y for aerobic oxidation of acetate assuming  $\varepsilon$ =0.4 and 0.6 at standard conditions except for a pH of 7.0. Ammonia is available for cell synthesis.

From O-1, 
$$\Delta G_c^{\ 0'}=27.40\ kJ/e^-\ eq$$
 
$$\Delta G_p=35.09-27.40=7.69\ kJ/e^-\ eq$$
 
$$\Delta G_r=\Delta G_a-\Delta G_d=-78.72-27.40=-106.12\ kJ/e^-\ eq$$
 
$$\Delta G_d=27.40\ kJ/e^-\ eq, \quad \Delta G_a=-78.72\ kJ/e^-\ eq \ (from I-14)$$

$$\Delta G_p > 0 \rightarrow n = +1$$

$$A = -\frac{\frac{\Delta G_p}{\varepsilon^n} + \frac{\Delta G_{pc}}{\varepsilon}}{\varepsilon \Delta G_r} = -\frac{\frac{7.69}{\varepsilon^{+1}} + \frac{18.8}{\varepsilon}}{-106.12\varepsilon}$$

$$\epsilon = 0.4 : A = 1.56$$

$$\epsilon = 0.6 : A = 0.69$$

$$f_s^0 = \frac{1}{1+A}$$

$$f_s^0 = 0.39, Y = 0.28 \text{ g cells/g COD}$$

$$f_s^0 = 0.59, Y = 0.42 \text{ g cells/g COD}$$

# References

#1) https://cronodon.com/BioTech/Bacteria.html