

# Reduction of Sludge Production

- Alternative to Energy Recovery from Waste Sludge

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# Introduction



## THE PROBLEM

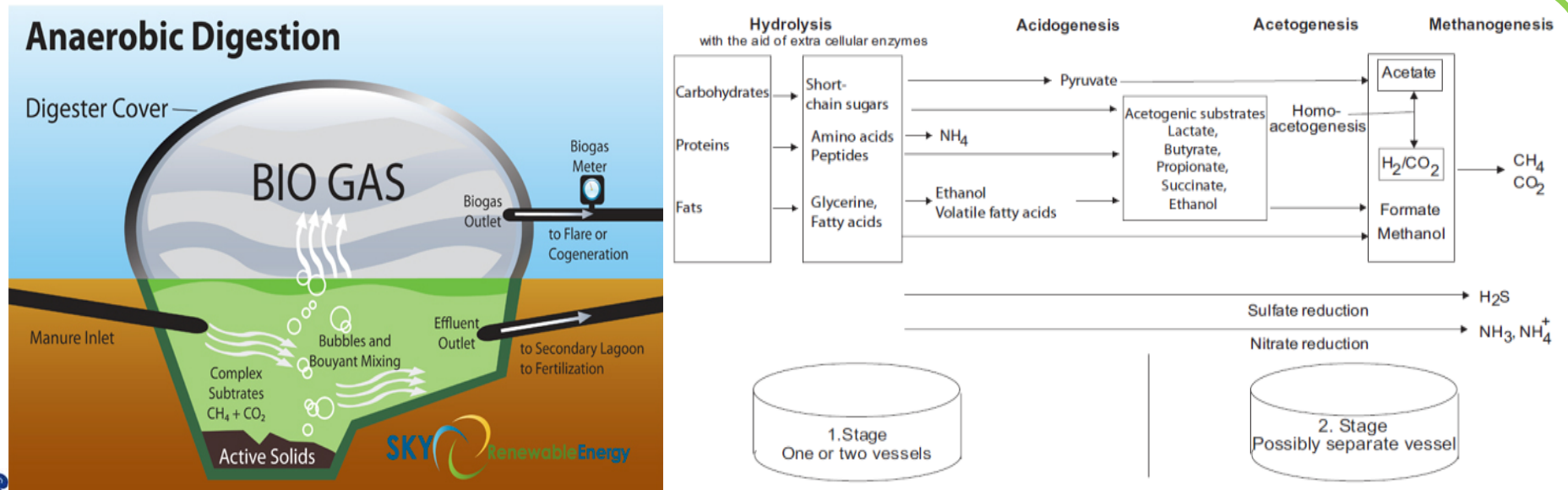
- Waste activated sludge (WAS) generation in Korea (KMOE, 2014) :
  - 3.5 Mil ton/year in 2013
  - steadily increase for the past 10 years with annual average of 4.66%
- Prevention of ocean dumping by London Treaty
  - ⇒ require appropriate alternatives
- WAS volume reduction methods :
  - anaerobic digestion
  - pretreatment for enhanced efficiency
- ⇒ require a relatively high amount of energy consumption

## SLUDGE



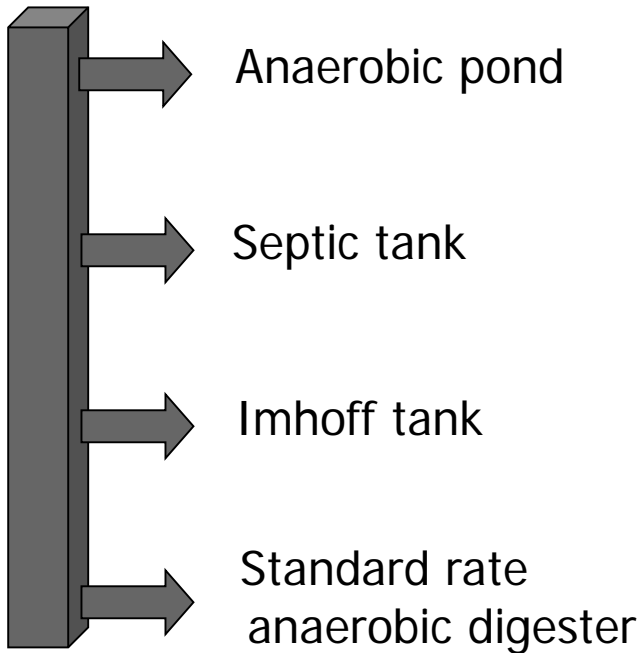
## ANAEROBIC DIGESTION

- Methane fermentation : hydrolysis, acidogenesis, acetogenesis, and methanation
- The individual phases : partly stand in syntrophic interrelation and place different requirements on the environment
- Two stages: the first 2 phases and the last 2 phases are linked closely with each other



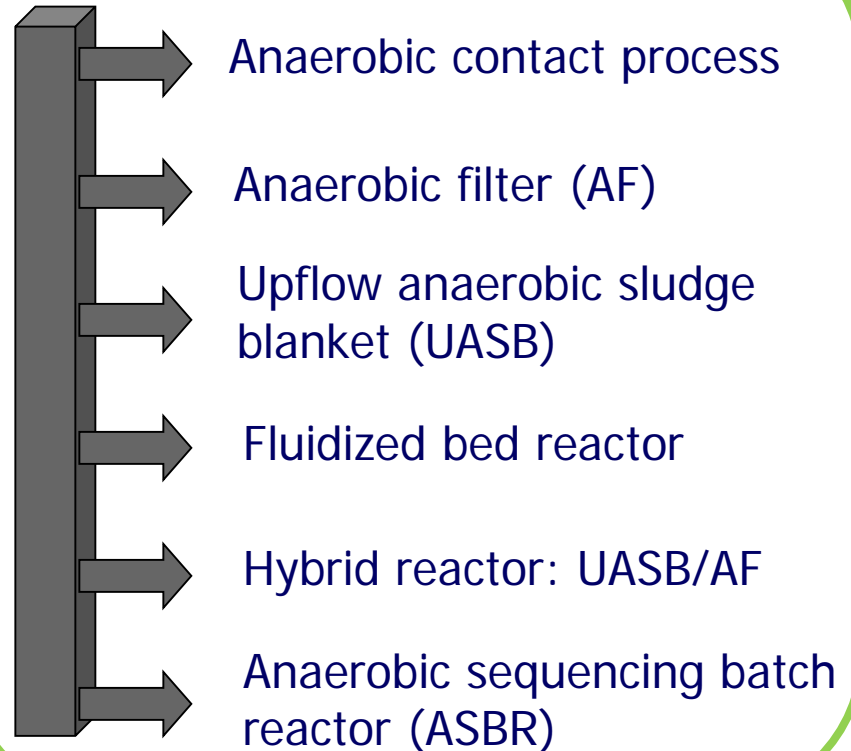
## Anaerobic Digestion Reactors

### ▪ Low-rate anaerobic reactors



Slurry type bioreactor, temperature, mixing, SRT or other environmental conditions are not regulated. Loading : 1-2 kg COD/m<sup>3</sup>-day

### ▪ High-rate anaerobic reactors



Able to retain very high concentration of active biomass in the reactor. Thus extremely high SRT could be maintained irrespective of HRT.  
Loading: 5-20 kg COD/m<sup>3</sup>-d

## BIOGAS COMPOSITION PRODUCED BY AD

- The gas components: specified to the plant and substrate and should be checked regularly on a long-term basis

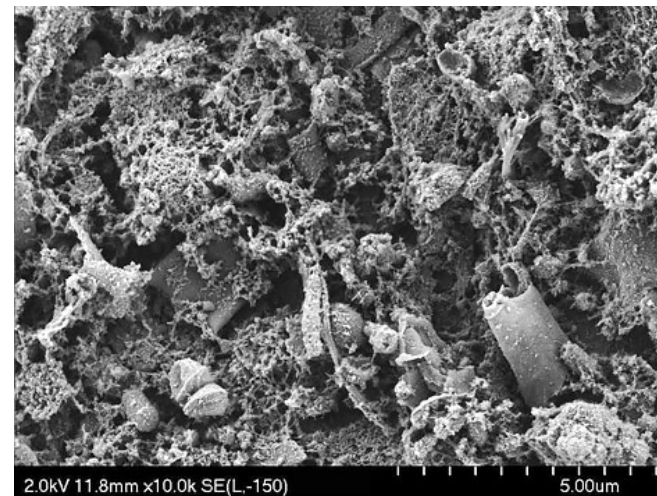
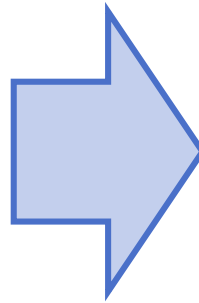
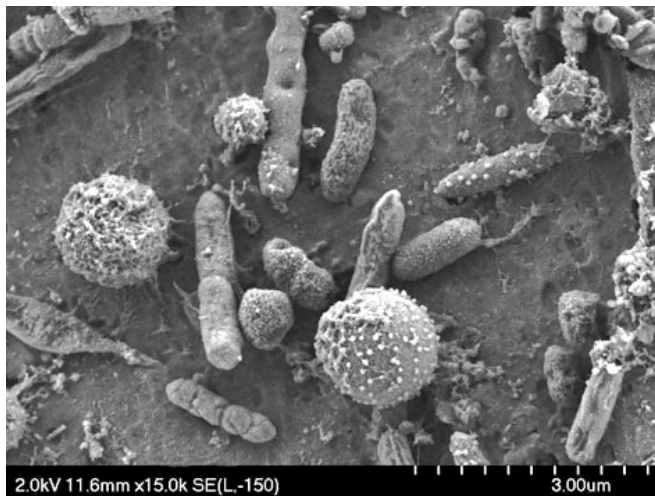
Component	Content	Effect
CO <sub>2</sub>	25–50% by vol.	Lowers the calorific value  Increases the methane number and the anti-knock properties of engines  Causes corrosion (low concentrated carbon acid), if the gas is wet  Damages alkali fuel cells
H <sub>2</sub> S	0–0.5% by vol.	Corrosive effect in equipment and piping systems (stress corrosion); many manufacturers of engines therefore set an upper limit of 0.05 by vol.%  SO <sub>2</sub> emissions after burners or H <sub>2</sub> S emissions with imperfect combustion– upper limit 0.1 by vol.%  Spoils catalysts
NH <sub>3</sub>	0–0.05% by vol.	NO <sub>x</sub> emissions after burners damage fuel cells  Increases the anti-knock properties of engines
Water vapor	1–5% by vol.	Causes corrosion of equipment and piping systems  Condensates damage instruments and plants  Risk of freezing of piping systems and nozzles
Dust	>5 µm	Blocks nozzles and fuel cells
N <sub>2</sub>	0–5% by vol.	Lowers the calorific value  Increases the anti-knock properties of engines
Siloxanes	0–50 mg Nm <sup>-3</sup>	Act like an abrasive and damages engines

# **Pretreatment Methods for Enhanced Biogas Production**



## P. L. McCarty at Stanford University

- Looking for a way to improve anaerobic digestion (in the late 1970s)
  - Primary Sludge (PS) : easily digested
  - Waste Activated Sludge (WAS) : only 1/3 can be digested
- Waste Activated Sludge : mostly consisted of microbial cells
  - Protection by cell walls, most cellular material is unavailable to anaerobic microbes.
- Pretreatment Methods : focused on 'Cell Lysis'
  - Volatile solids reduction (VSR) can be increased 2~3 times.
  - Biogas production can be doubled.





## Methods of Cell Lysis

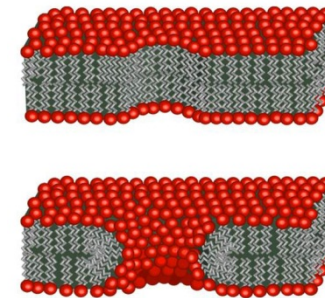
- High temperature (Hydrolysis)
  - Cambi™ by Cambi AS, Norway : 165°C at 6 bar for 20~30 min
  - Exelys™ by Veolia, France : 165°C at 9 bar for 30 min
- High Pressure
  - MicroSludge® by Paradigm Environment, Canada : homogenizer (60 bar)
- Physical Force
  - OpenCel® by OpenCel LLC, Atlanta : focused pulse
  - Ultrasound homogenizer
- Others : high or low pH, chemical oxidation, etc.



Cambi™



MicroSludge® Homogenizer



OpenCel® (pores on cell wall)

## Carbon source production from sludge using Cell Lysis

- Methanol alternatives as C source for denitrification
  - Reduced sludge production & reduced
  - Utilization as C source has 10 times its value making biogas
    - ⇒ Reduced greenhouse gas emission
    - ⇒ Reduced O&M cost

## Major Issues on Pretreatment of Sludge

- Cost can be higher than the benefit it can provide !!
  - Benefit (increased biogas production) should be greater than CAPEX + OPEX.
  - There are various unforeseeable and hidden costs.

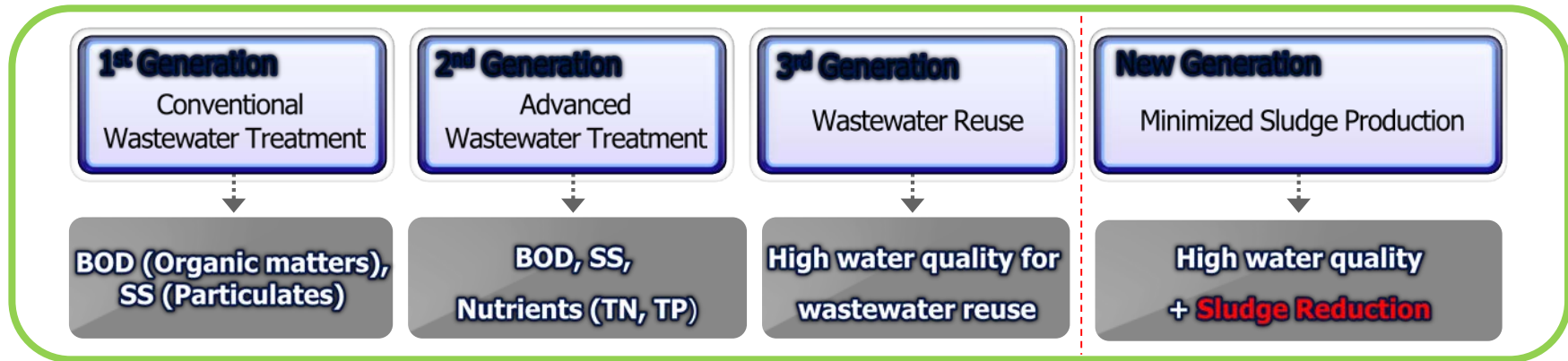


# Reduction of Sludge Production

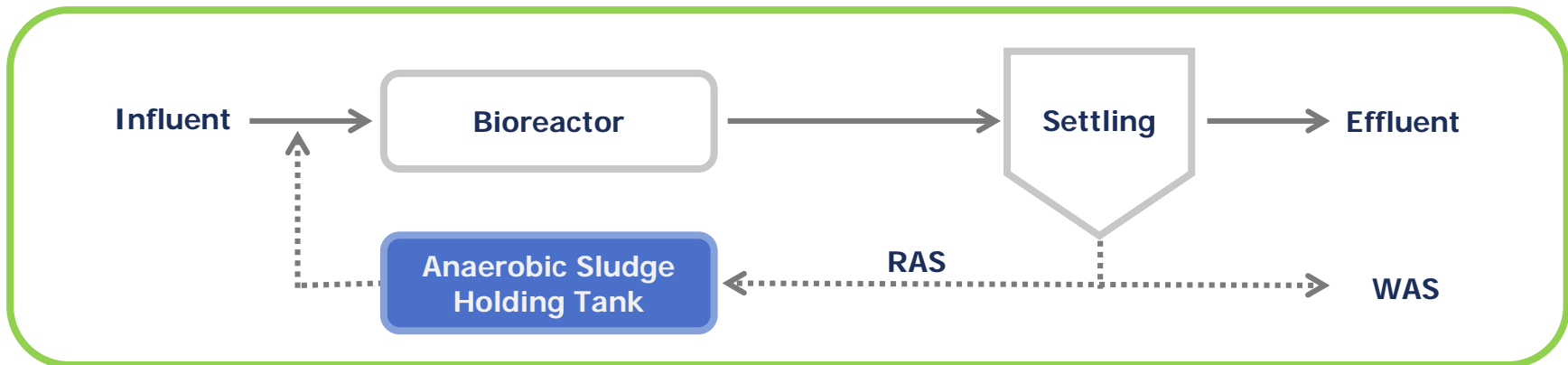


## Paradigm Shift

- New technology for source reduction during wastewater treatment by manipulating microbial growth kinetics



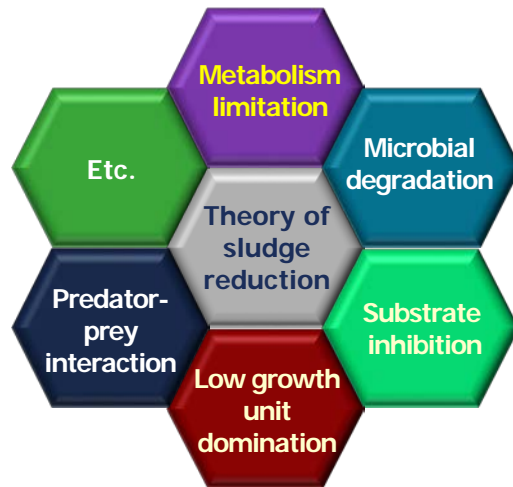
- Process Diagram



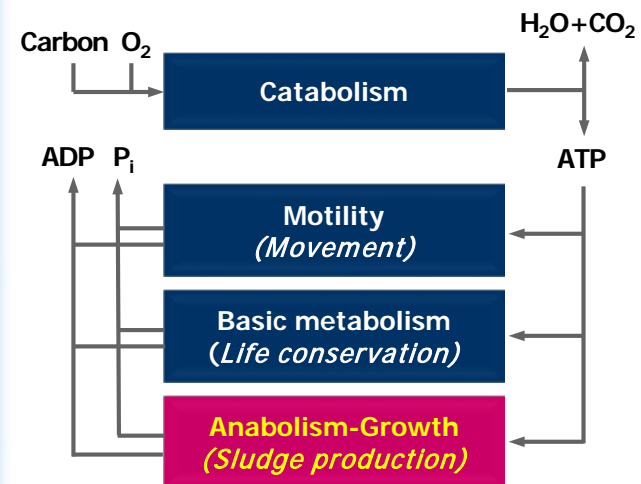
## PRINCIPLE OF SLUDGE REDUCTION

- The abrupt change in growth environments
  - “Uncoupling metabolism” most widely studied
  - Yield reduction while maintaining substrate uptake rate
  - The reduction of ATP production in microbial cells

### Possible Explanation



### Uncoupling Metabolism



## Determination of Optimal HRT of the Anaerobic SHT

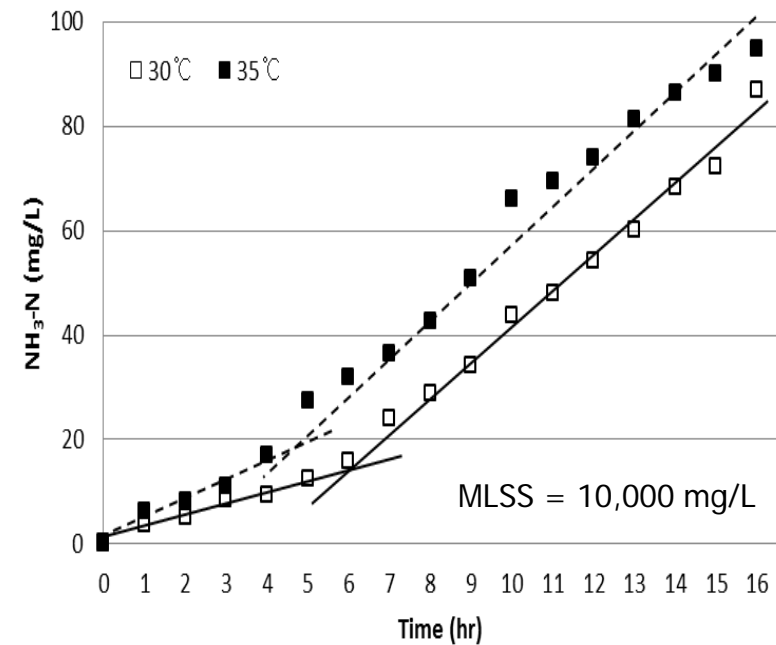
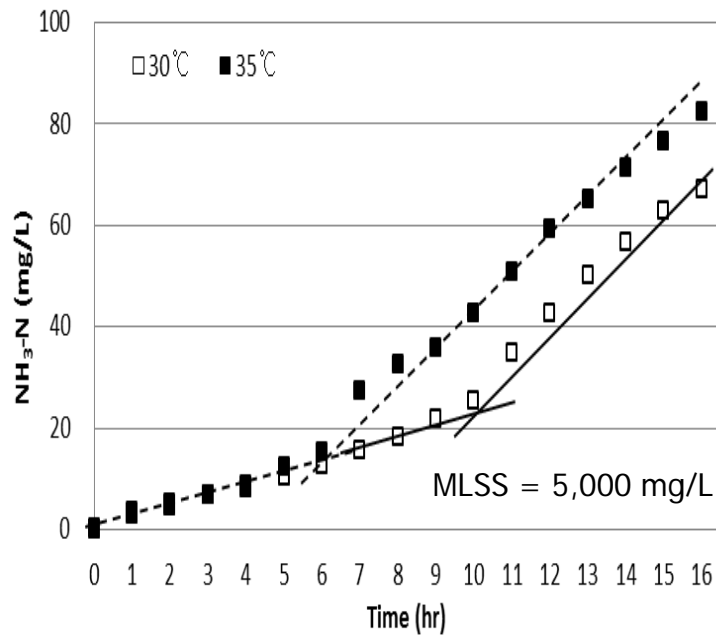
- Monitoring  $\text{NH}_3\text{-N}$  concentration while incubating anaerobically
  - in the same growth condition of SHT
  - no substrate addition during incubation
- Abrupt increase in  $\text{NH}_3$  release rate
  - considered as the start of endogenous phase
  - considered as optimal HRT of SHT



[Conditions for the incubation of sludge]

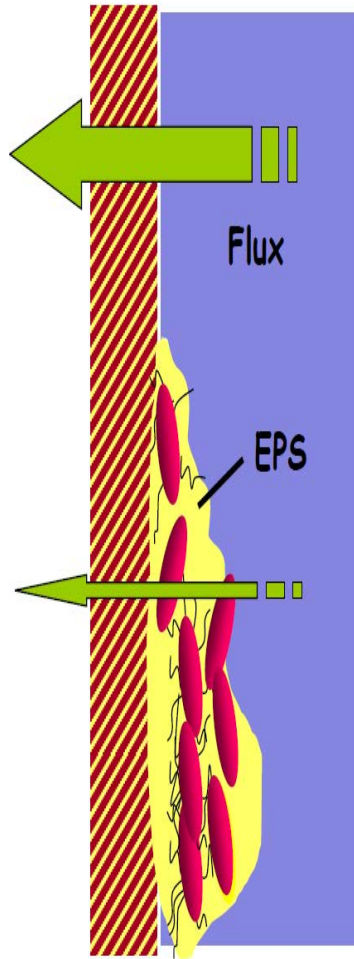
Incubation Condition	Exp. 1	Exp. 2	Exp. 3	Exp. 4
MLSS (mg/L)	5,000	5,000	10,000	10,000
Temp. (°C)	30	35	30	35

## Ammonia Concentration with Time



- Increase in the release rate = the increased degradation of microbial cells
- Optimal point : the start of full endogenous phase at each experimental as the optimal hydraulic retention time for SHT.

## / Membrane fouling by EPS



### Extracellular polymeric substances (EPS) ?

- EPS are metabolic products accumulating on the bacterial cell surface

### Importance...

- EPS is the main cause of membrane fouling
- Reduce water permeability and increase operation cost

### Composed of...

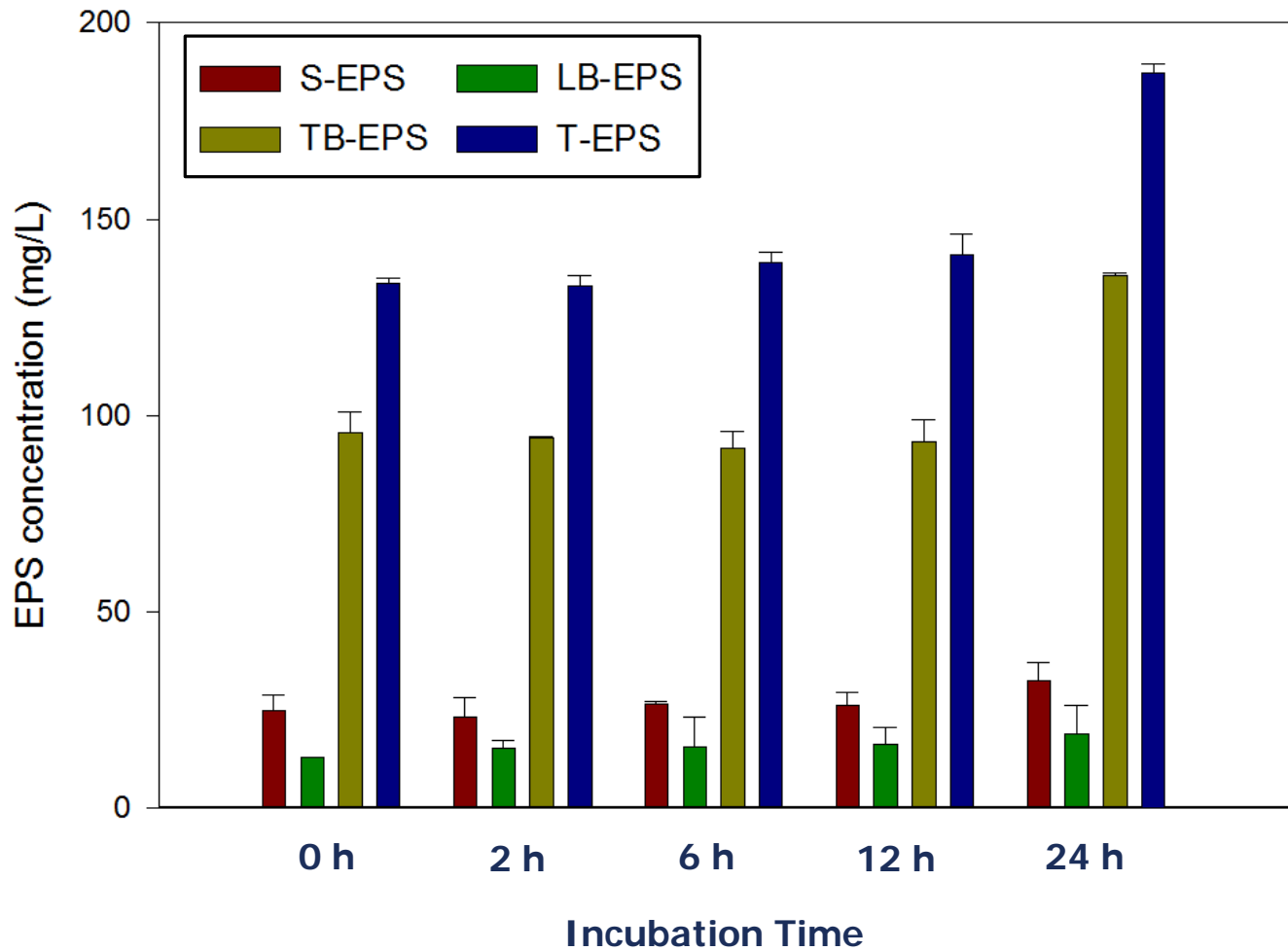
- polysaccharide, protein, humic substances, DNA etc.

### Divided into...

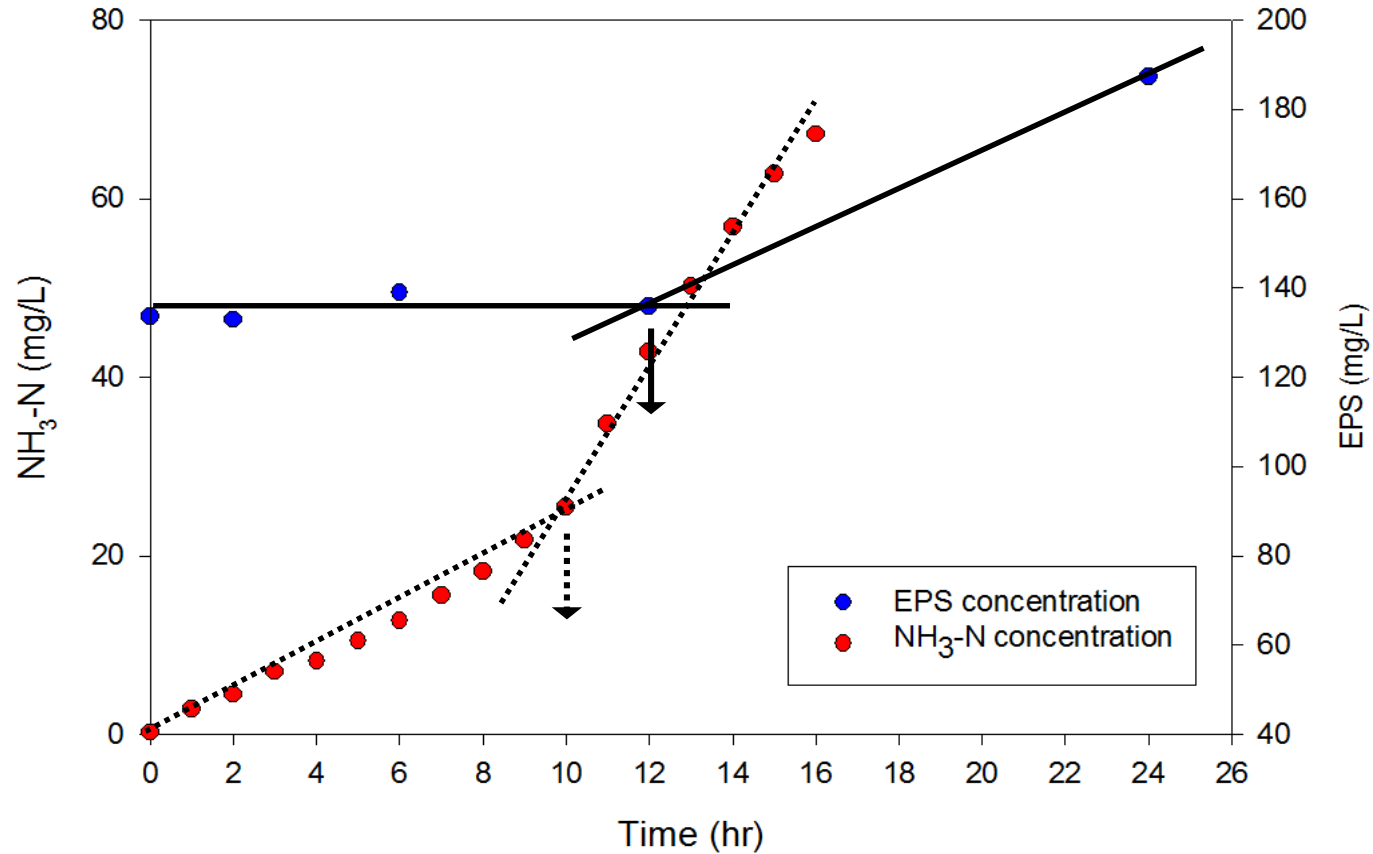
- Bound EPS
- Soluble EPS



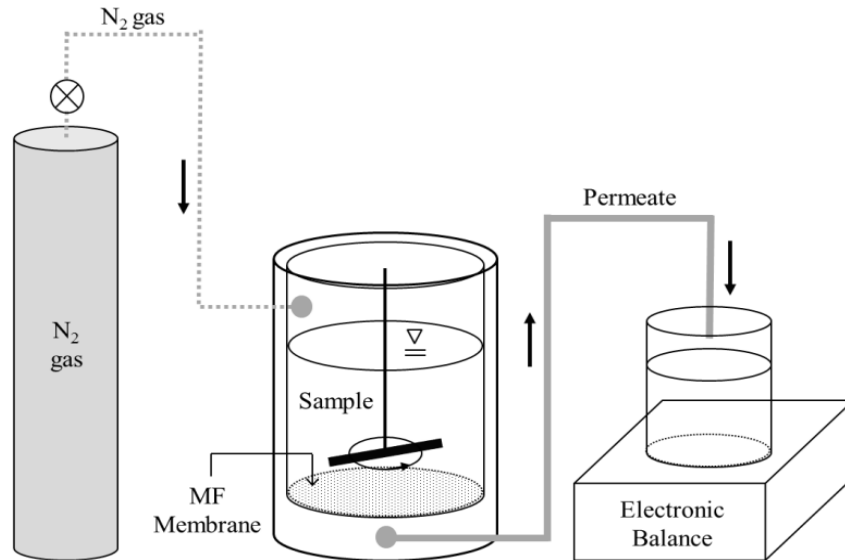
## / EPS concentrations with respect to anaerobic incubation time



## Comparison between EPS and ammonia release with incubation time



## Filterability test



### ➤ Experimental Conditions

- Flat sheet PVDF membrane
- Pore size: 0.1  $\mu\text{m}$
- Membrane area: 32  $\text{cm}^2$
- Filtration
  - Pressure : 0.5 bar
  - Volume : 150 ml-MLSS
- Backwashing
  - Pressure : 0.5 bar
  - Volume : 150 ml-DI water

### ➤ Reversibility of the membranes by backwashing after filtrations

$$IF_n = \frac{J_{p(n-1)} - J_{p(n)}}{J_{P(0)}}$$

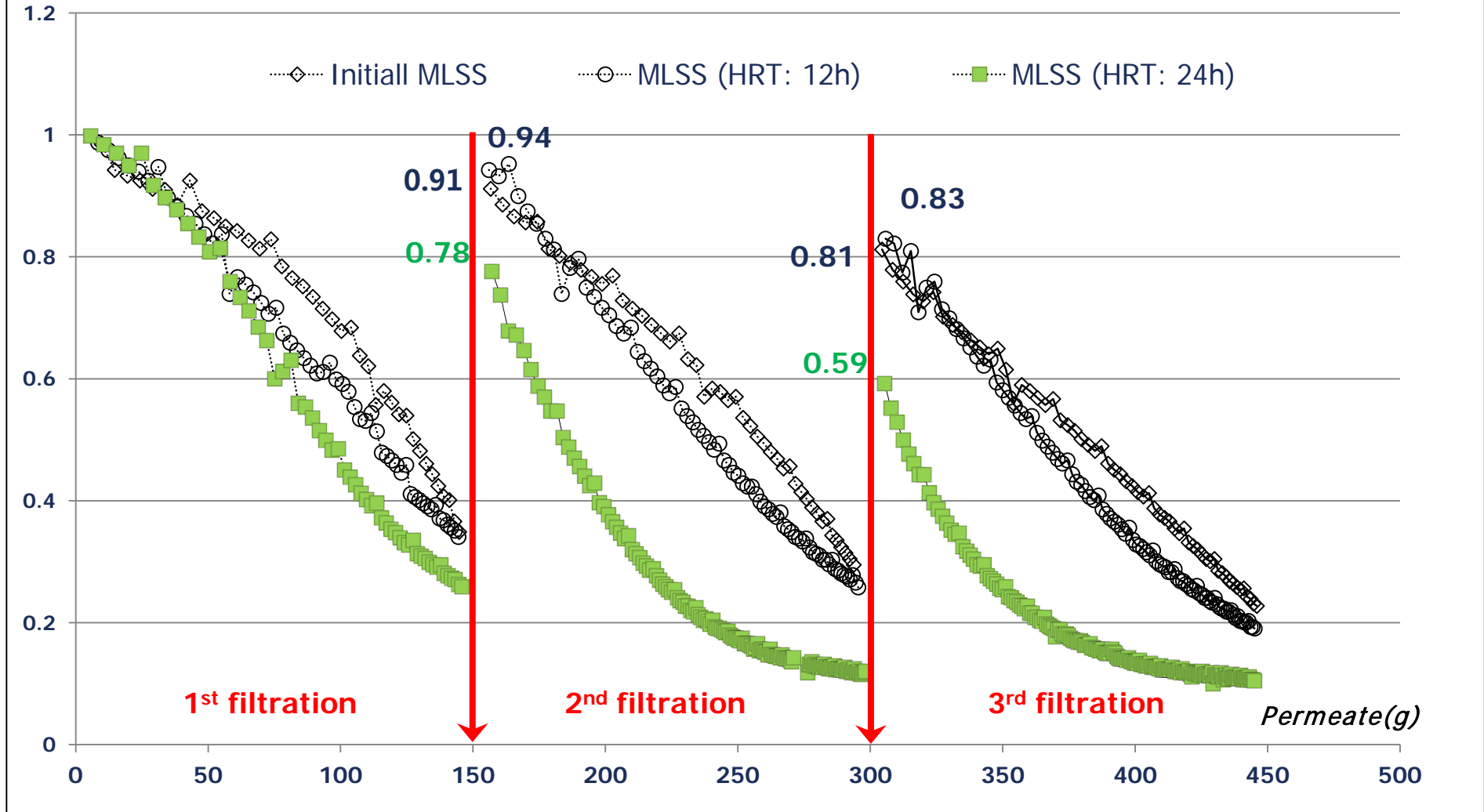
$$RF_n = \frac{J_{s(n+1)} - J_{e(n)}}{J_{P(0)}}$$

$$TF_n = IF_n + RF_n$$

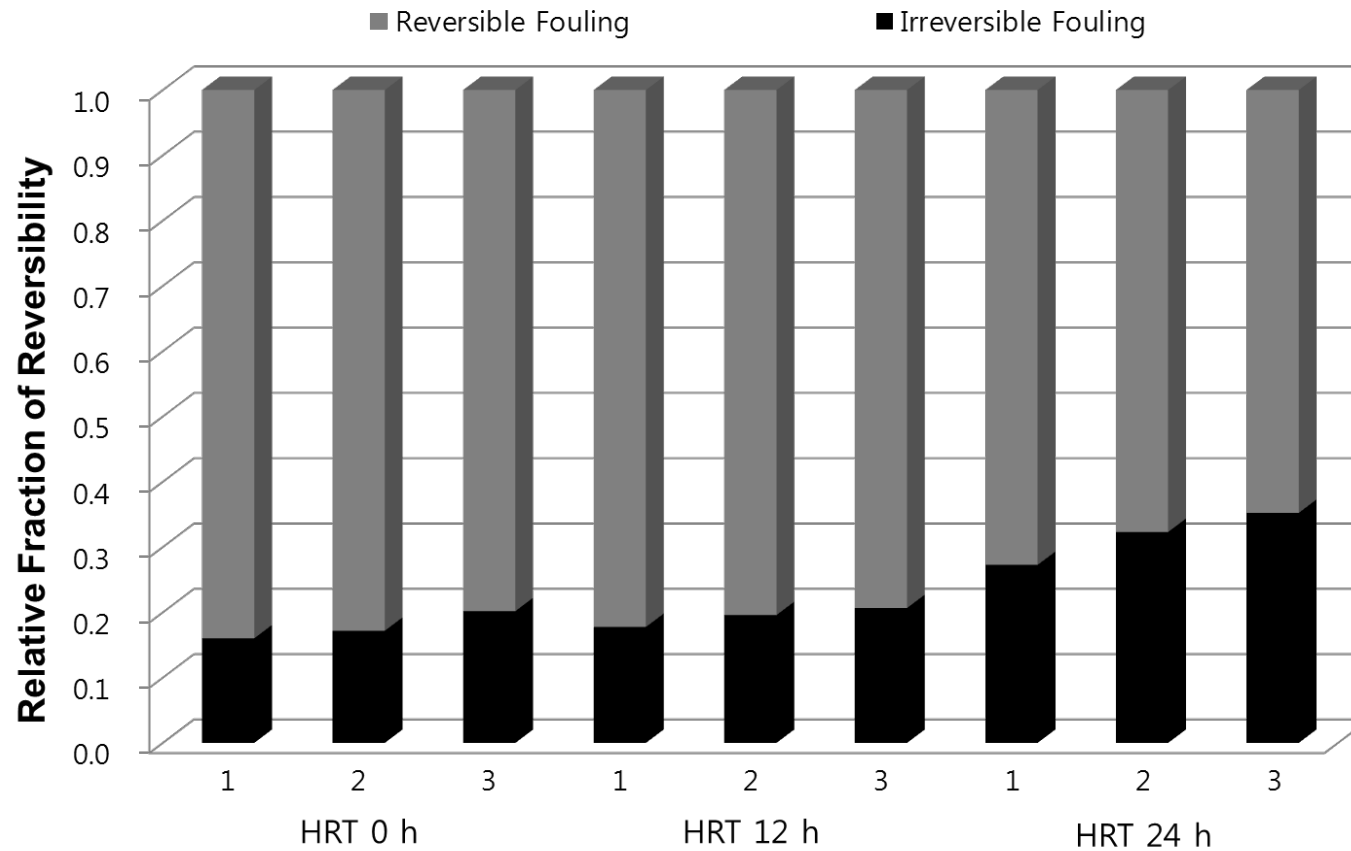
- $IF$ ,  $RF$  and  $TF$  : irreversible, reversible and total fouling, respectively.
- $n$  : the number of the filtration cycle
- $J_{p(n)}$ ,  $J_{s(n)}$  and  $J_{e(n)}$  : average flux of DI water after rinse, the starting and ending flux of the sludge sample, respectively.

# Determination of Optimal HRT of the Anaerobic SHT

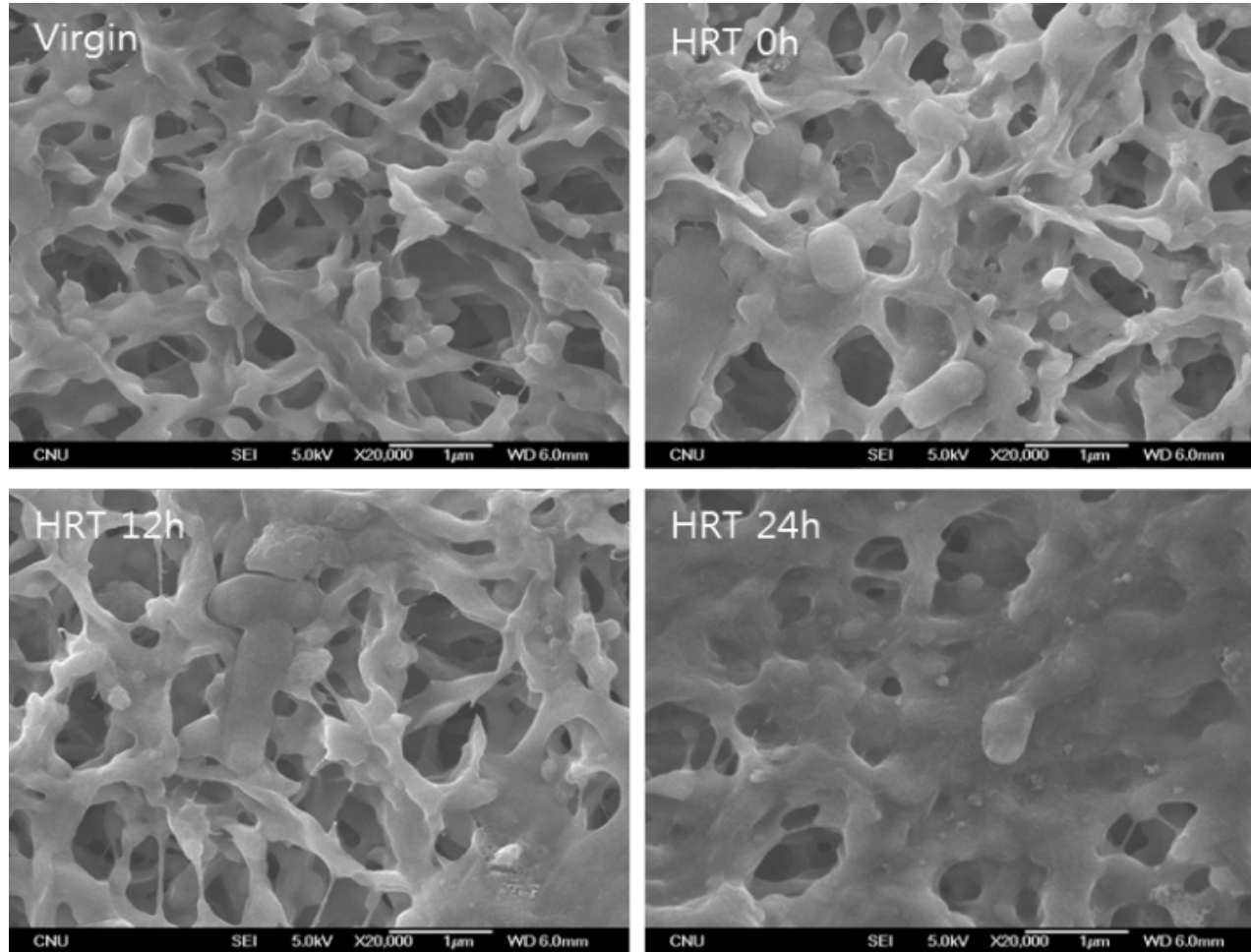
## Filtration curves of the sludge samples



## Relative fraction of fouling reversibility

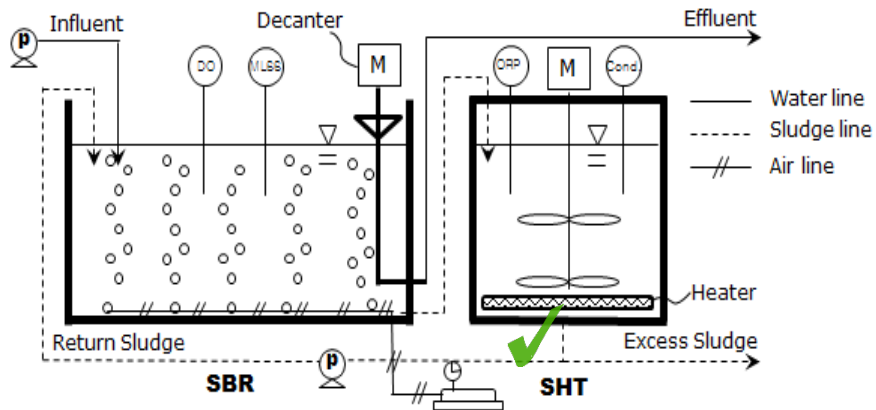


## SEM images of the membranes after 3 times filtration of the mixed liquor

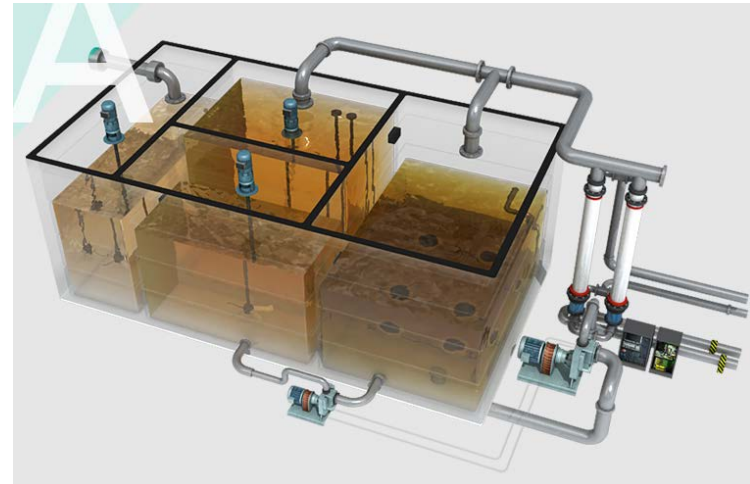
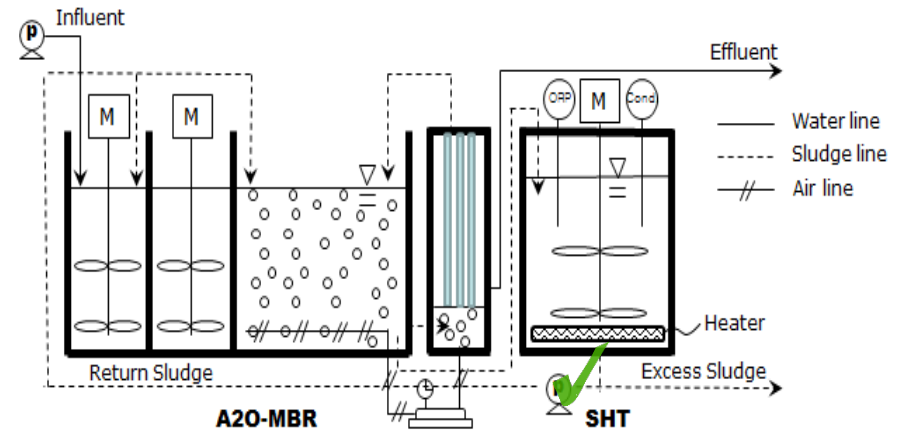


# Pilot Operation – SBR and MBR

## SBR system with SHT



## MBR system with SHT



Biological kinetic parameters

⇒ direct evidence of sludge yield reduction

Kinetic parameter estimation :

- SHT was operated in 4 different conditions  
(as in the experiments of HRT evaluation of SHT, Table 2)
- F/M ratio of 0.15
- For  $Y_H$  estimation

$$Y_H = \frac{\Delta \text{Biomass COD}}{\Delta \text{Soluble COD}}$$

- For  $b_H$  estimation (non-active biomass fraction,  $f'_p$  as 0.08)

$$b_H = \frac{b'_H}{1 - Y_H(1 - f'_p)}$$

- For Sludge production,  $P_{X,VSS}$

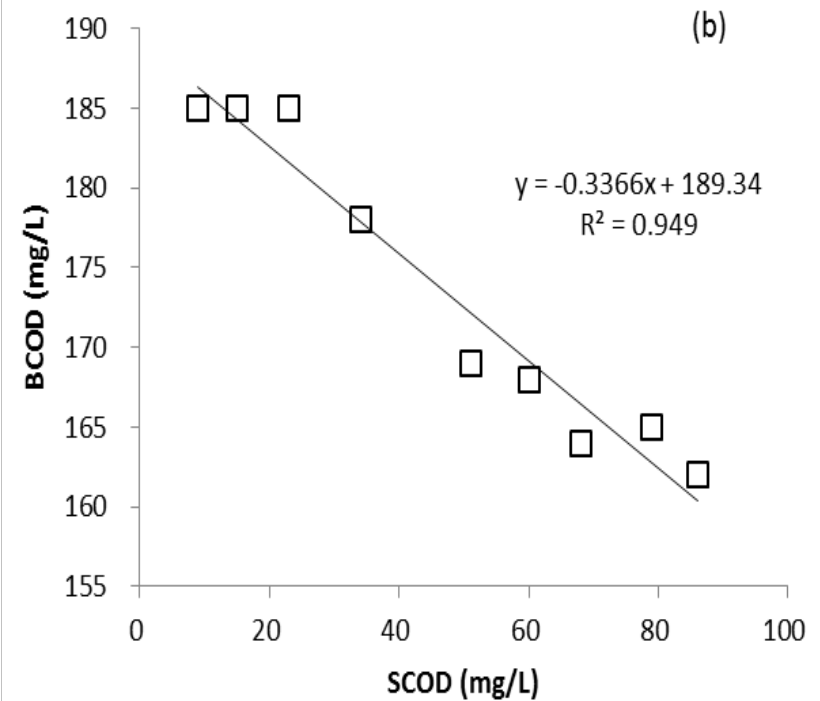
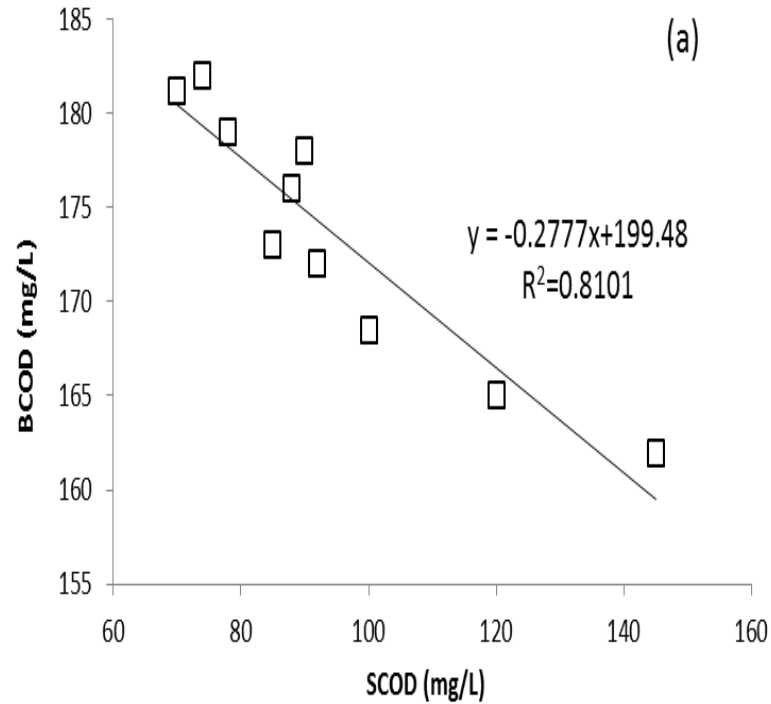
$$Y_{obs} = \frac{Y_H}{1 + b_H SRT}$$

$$P_{X,VSS} = Y_{obs}(Q)(S_0 - S)$$

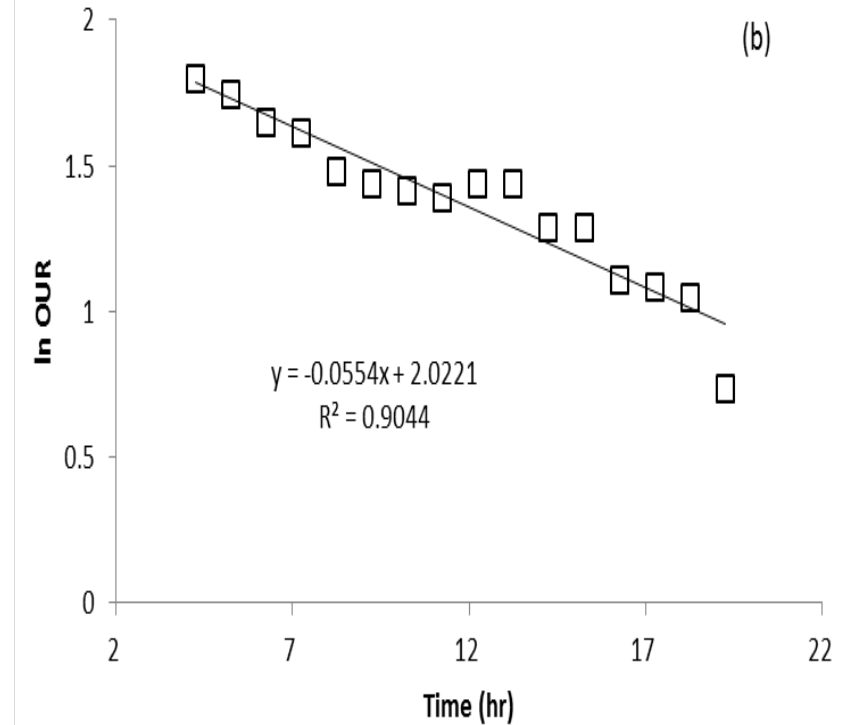
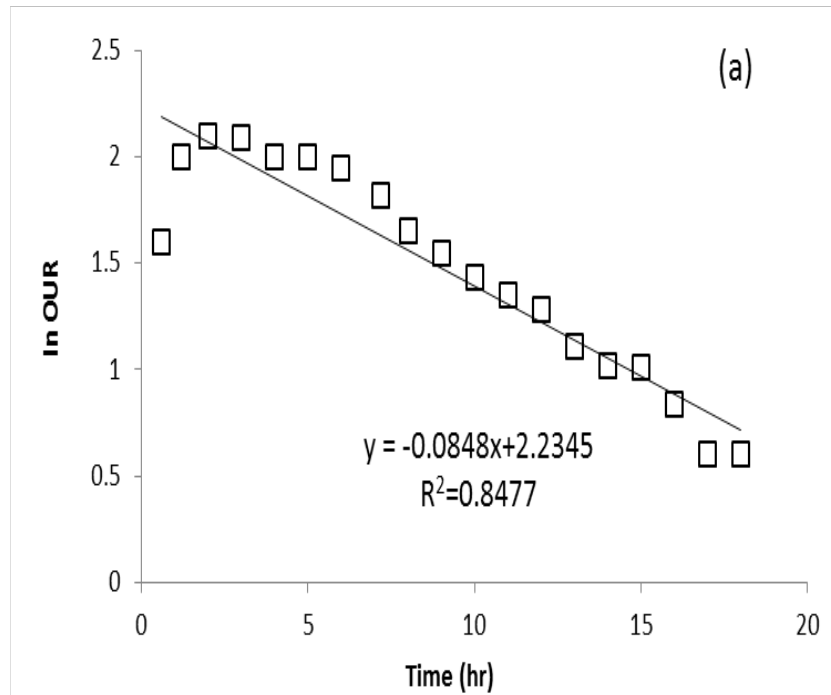




## Experimental results obtained for $Y_H$ estimation for (a) SBR and (b) MBR systems



## Experimental results obtained for $b_H$ estimation for (a) SBR and (b) MBR systems

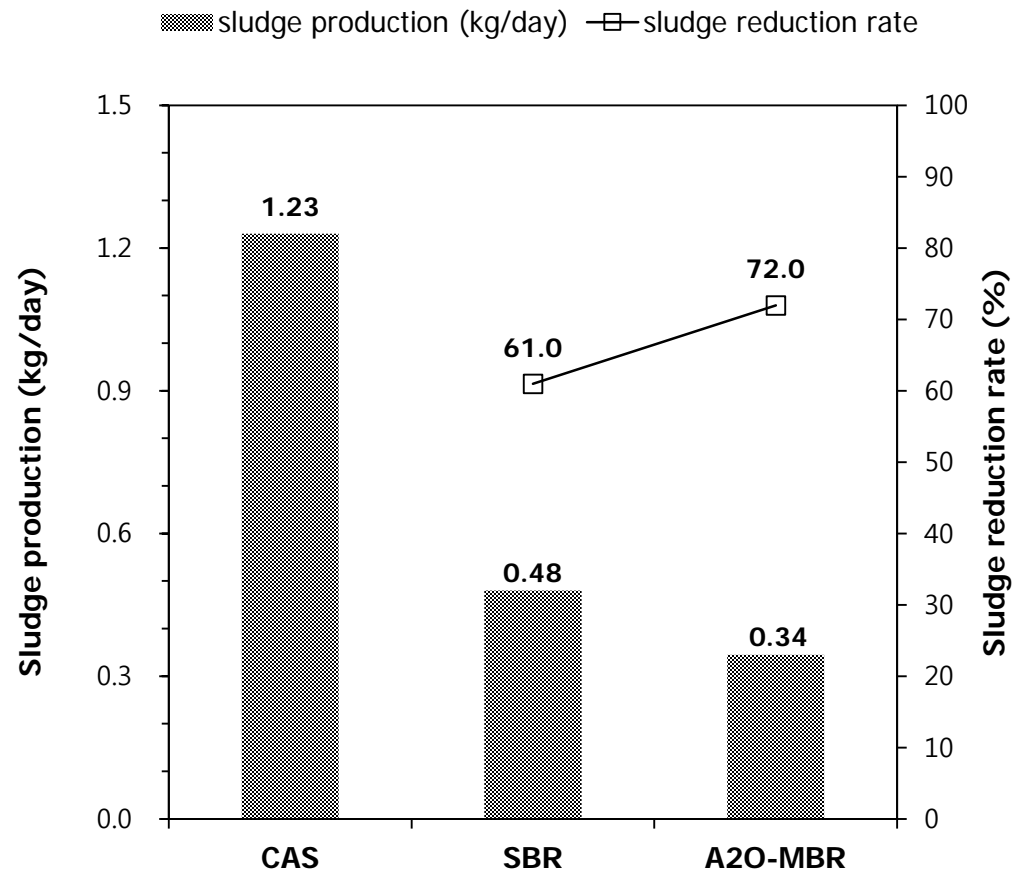


## Kinetic parameters estimated for the SBR and MBR systems operated with SHT

Conditions		SBR	MBR
SHT	MLSS (mg/L)	5,000	8,000
	Temp. (°C)	30±1	
SRT(day)		68.4	149.6
$Y_H$		0.28	0.34
$b_H$ (d <sup>-1</sup> )		0.11	0.080
$Y_{obs}$		0.032	0.026

Reference	Condition		Y <sub>obs</sub>	Units
Ozdemir and Yenigu (2013)	SRT (day)	10	0.310	kg MLVSS/ kg COD removed
		37	0.220	
		53	0.206	
		110	0.130	
Rensink and Rulkens (1997)	Conventional activated Sludge (23°C)		0.15 – 0.17	kg SS/ kg COD removed
Zhang (2000)	MBR with submerged membrane (suction mode) (20°C)		0.00–0.12	kg SS/ kg COD removed
	MBR with submerged membrane (gravitational mode) (20°C)		0.10–0.15	
Wei et al. (2003)	Conventional activated Sludge (20 °C)		0.17	kg SS/ kg COD removed

## Sludge production of MBR and SBR compared to conventional activated sludge (CAS)



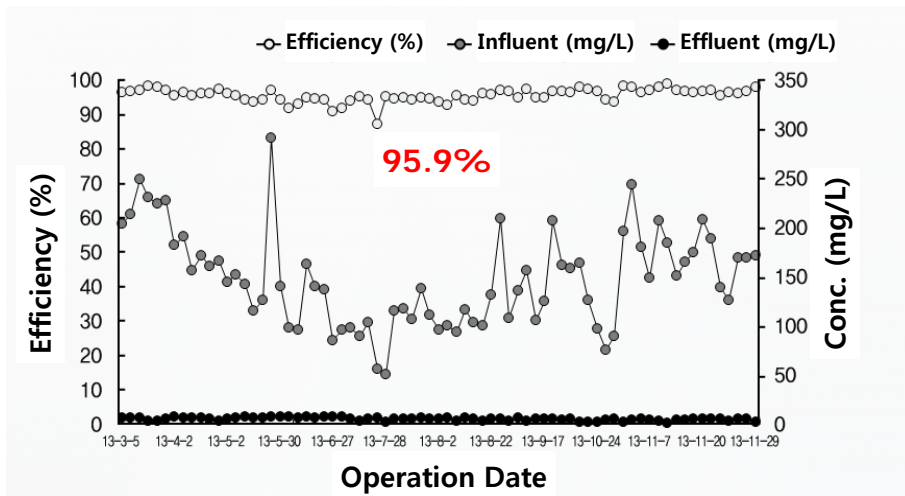
## Treatment Efficiency - SBR

Item	Influent (mg/L)	Effluent (mg/L)	Average efficiency (%)
COD <sub>Cr</sub>	89.4 ~ 310.8	4.6 ~ 7.4	95.7
SS	74 ~ 191	1.8 ~ 6.8	96.1
TN	19.8 ~ 41.1	7.8 ~ 13.3	65.4
TP	1.7 ~ 5.0	0.7 ~ 0.9	71.4

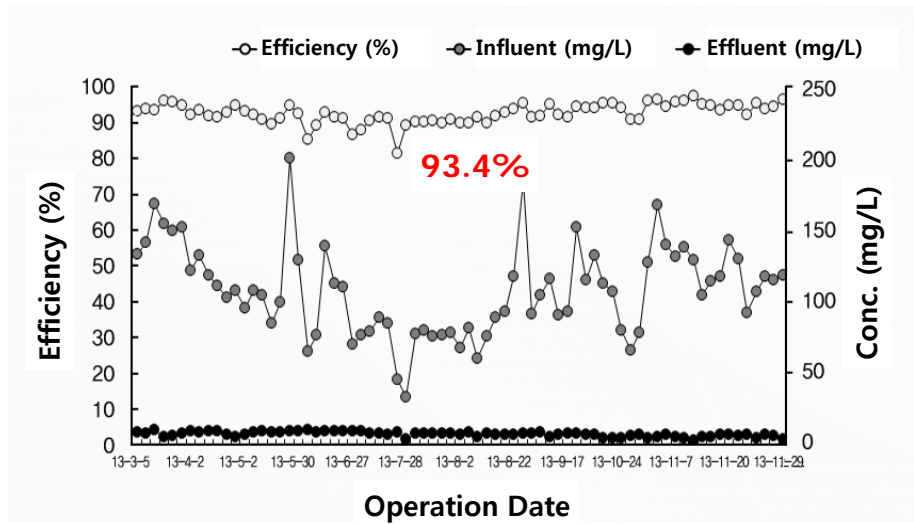


# Treatment Efficiency - MBR

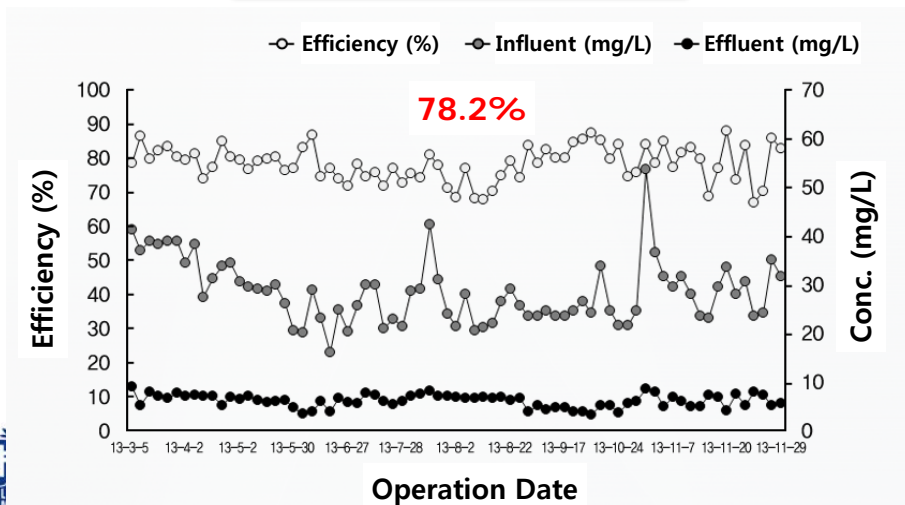
## BOD



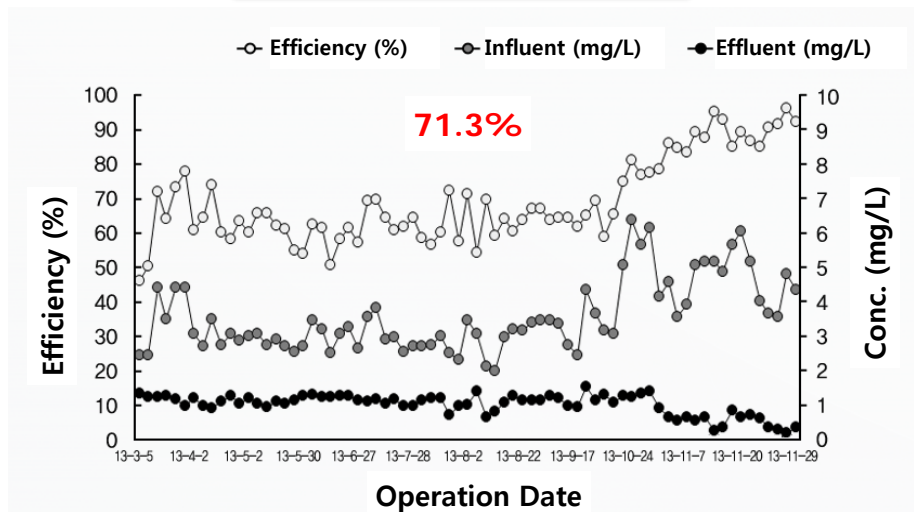
## COD



## T-N



## T-P



- ✓ **Sludge reduction rate by evaluating microbial kinetic parameters**  
: Pilot scale **SBR** and **MBR** systems operated with anaerobic side-stream SHT,  
by **61.0%** and **72.0%**, respectively.
- ✓ **Treated water quality**  
: not deterioration of the effluent water quality but phosphorus removal
- ✓ **SHT application for various processes with reduced WAS**  
: will contribute to minimize environmental and economic problems  
pertaining to the final disposal of sludge.
- ✓ **Reduction of sludge production can be**  
: an economic and efficient way with net energy gain compared to other  
pretreatment methods, and  
: a sustainable method to reduce sludge disposal cost.

*Thank You !*

*(Q & A)*

