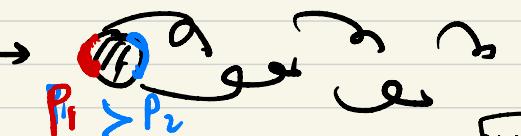
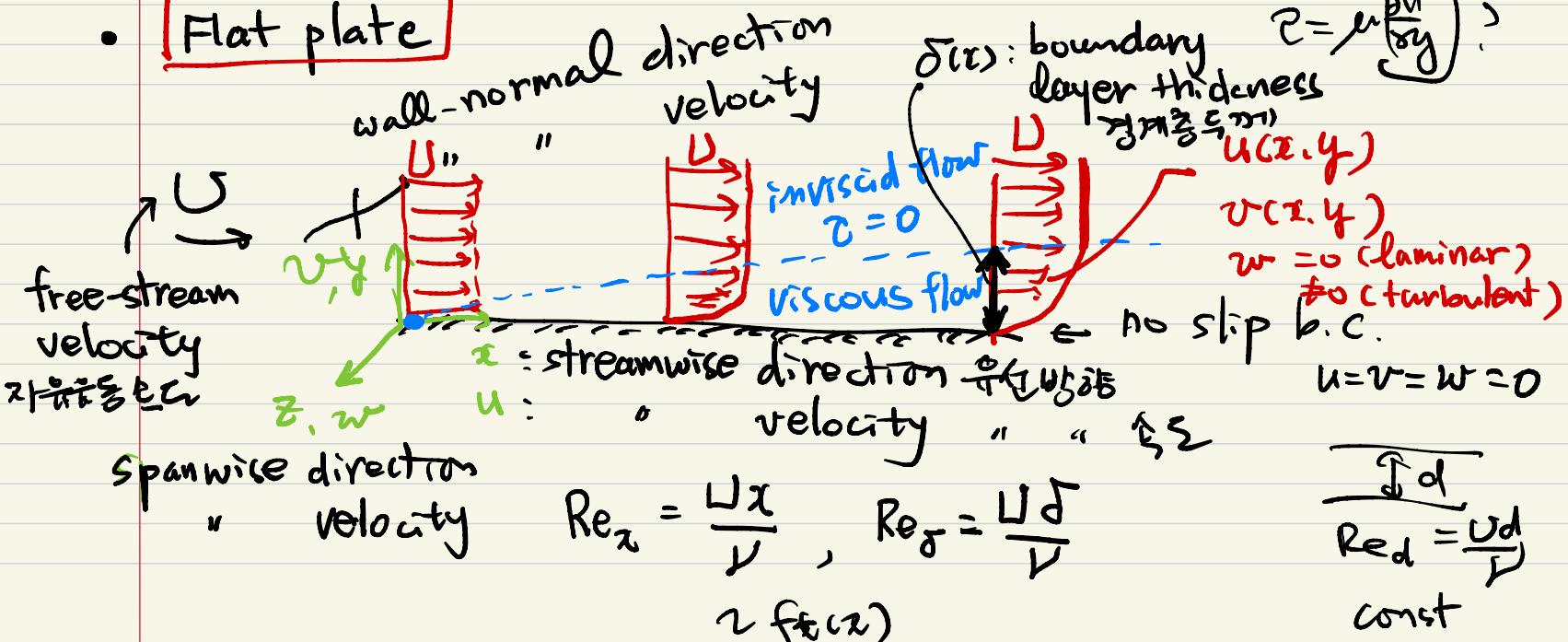


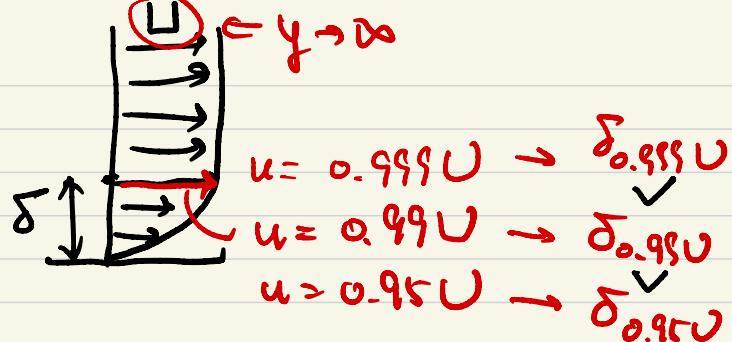
④ Reynolds number and geometry effects

two types: ① streamlined body → 

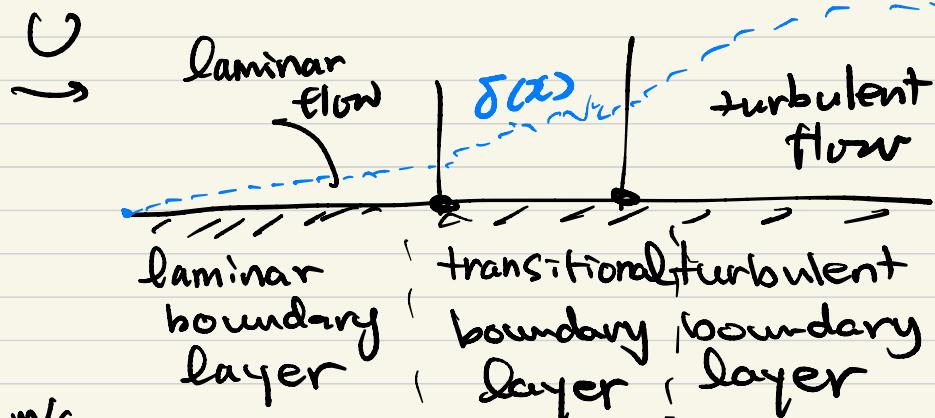
② bluff body → 

• Flat plate





δ ?



$U = 10 \text{ m/s}$

\rightarrow air δ ?

3 m

$Re_x = \frac{Ux}{\nu} = \frac{10 \times 3}{1.5 \times 10^{-5}} = 2 \times 10^6 \rightarrow \delta_{\text{laminar}} = \frac{5.0 \times 3}{\sqrt{2 \times 10^6}} \approx 1 \text{ cm}$

"thin"!

δ_{turb} $= \frac{0.16 \times 3}{(2 \times 10^6)^{1/7}} \approx 6 \text{ cm}$

Blasius (1908)

$$\frac{\delta}{x} = \begin{cases} \frac{5.0}{\sqrt{Re_x}} & \text{laminar} \\ \frac{0.16}{Re_x^{1/7}} & \text{turbulent} \end{cases} \rightarrow \delta \sim \sqrt{x}$$

- flow around slender bodies

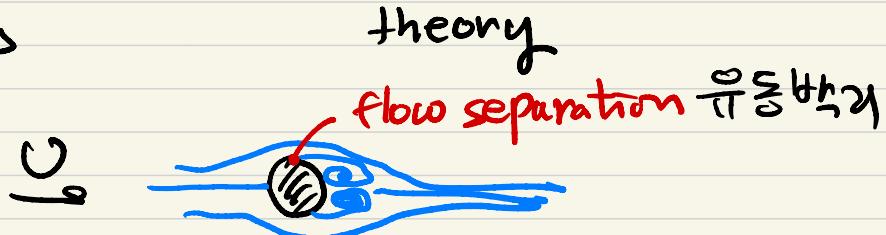


Plates) thin boundary
airfoils ↑ layer

- flow around bluff bodies



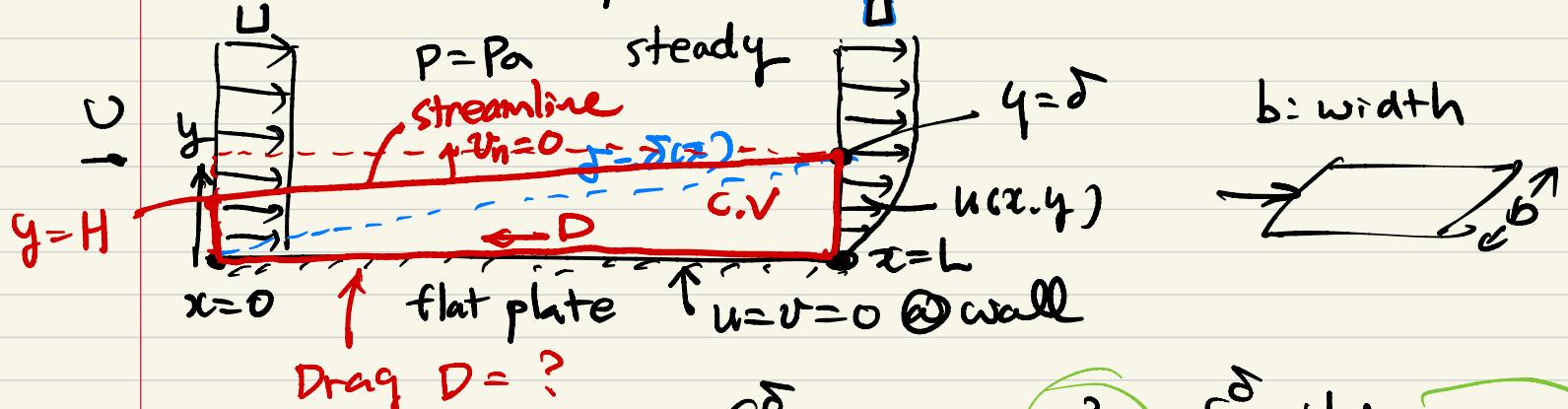
↑
theory
Stokes flow



$U \uparrow$ $Re_d = \frac{Ud}{\nu} \uparrow$ theory fails.

experiment
computational fluid
dynamics (CFD)

7.2 Momentum-integral estimates



$$\text{continuity: } UH = \int_0^H u dy \rightarrow U^2 H = \int_0^H u U dy$$

$$\begin{aligned} x\text{-mtn: } \sum F_x &= -D = b \iint_{C.S.} \rho u (\nabla \cdot \underline{v}) dA = b \left(\int_0^H \rho u^2 dy - \int_0^H \rho U^2 dy \right) \\ &= \rho b \left(\int_0^H u^2 dy - \int_0^H u U dy \right) \end{aligned}$$

$$\therefore D = \rho b \int_0^H (uU - u^2) dy = \rho b U^2 \int_0^H \frac{u}{U} \left(1 - \frac{u}{U} \right) dy$$

$\equiv \Phi(x)$



$$\delta = \int_0^y \frac{U}{U} \left(1 - \frac{U}{U}\right) dy$$

: momentum thickness $\frac{\delta U^2}{2}$

$$D(x) = \rho b U^2 \delta(x) \rightarrow \frac{dD}{dx} = \rho b U^2 \frac{d\delta}{dx}$$

|||

$$\int_0^x \tau_w dx \cdot b \Rightarrow \frac{dP}{dx} = \tau_w \cdot b$$

\uparrow
wall shear stress
 $\tau_w = \mu \frac{du}{dy}|_{w=0}$

$$\tau_w = \mu \frac{du}{dy}|_{w=0}$$

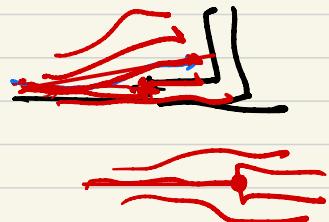
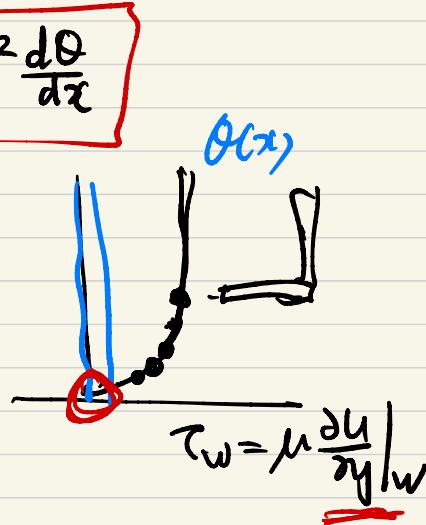
$$C_f = \frac{\tau_w}{\frac{1}{2} \rho U^2} = 2 \frac{d\delta}{dx}$$

skin-friction coefficient
 $C_f = \frac{2}{\delta}$

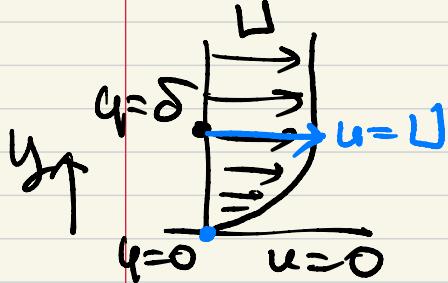
valid for
laminar &
turbulent flows

$$\frac{C_f}{2} = \frac{d\delta}{dx}$$

momentum-integral
relation for flat-plate
boundary layer flow



- von Karman's assumption on velocity profile



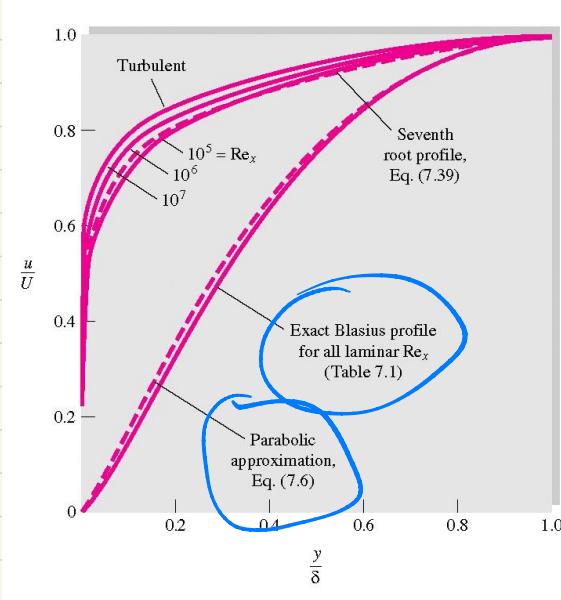
$$u = 0 \text{ @ } y = 0$$

$$u = U \text{ @ } y = \delta$$

$$\frac{\partial u}{\partial y} = 0 \text{ @ } y = \delta$$

$$u = a + b y + c y^2$$

$$u(x,y) = U \left(\frac{2y}{\delta} - \frac{y^2}{\delta^2} \right) \quad 0 \leq y \leq \delta$$



$$0 = \int_0^{\delta} \frac{\delta u}{\delta U} \left(1 - \frac{u}{U} \right) dy = \frac{2}{15} \delta$$

$$\tau_w = \mu \frac{\partial u}{\partial y} \Big|_{y=0} = \frac{\mu \cdot 2U}{\delta} \quad || \rightarrow \frac{\delta^2}{2} = 15 \frac{U^2}{C}$$

$$C U^2 \frac{d\delta}{dx} = \rho U^2 \cdot \frac{2}{15} \frac{d\delta}{dx}$$

$$\frac{\delta}{x} = 5.5 \sqrt{\frac{U}{U_x}} = \frac{5.5}{\sqrt{Re_x}}$$

$$\Rightarrow \delta \sim \sqrt{x}$$

$$\frac{\delta}{x} = \frac{5.0}{\sqrt{Re_x}}$$

Blasius

10% error

$$\frac{\theta}{x} = \frac{\theta}{\delta} \cdot \frac{\delta}{x} = \frac{2}{15} \cdot \frac{5.5}{\sqrt{Re_x}} = \frac{0.733}{\sqrt{Re_x}} \rightarrow \theta \sim \sqrt{x}$$

$$c_f = \frac{\frac{1}{2} \rho U^2}{\frac{1}{2} \rho U^2} = \frac{2 \mu U / \delta}{\frac{1}{2} \rho U^2} = \frac{4 \mu}{\rho U \delta} = \frac{x}{\delta} \cdot \frac{4 \mu}{\rho U^2} = \frac{0.73}{\sqrt{Re_x}} \rightarrow 10\% \text{ error}$$

$$\rightarrow c_f \sim x^{-\frac{1}{2}}$$

$$c_f = \frac{0.664}{\sqrt{Re_x}} \text{ Blasius}$$

