

# More Complex Brayton Cycles

**TABLE 6.9**

**Results of Brayton Cycle Cases of Examples 6.7 through 6.14**

| Parameter                                                          | Ex. 6.7 | Ex. 6.8 | Ex. 6.9 | Ex. 6.10A | Ex. 6.10B | Ex. 6.11 | Ex. 6.12                                                          | Ex. 6.13                                                          | Ex. 6.14                                                          |
|--------------------------------------------------------------------|---------|---------|---------|-----------|-----------|----------|-------------------------------------------------------------------|-------------------------------------------------------------------|-------------------------------------------------------------------|
| $\beta = \left( \frac{p_2 p_4}{p_3 p_1} \right)^{\gamma-1/\gamma}$ | 1.0     | 1.0     | 1.05    | 1.0       | 1.0       | 1.0      | 1.0                                                               | 1.0                                                               | 1.0                                                               |
| Component isentropic efficiency ( $\eta_s$ )                       | 1.0     | 0.9     | 0.9     | 1.0       | 0.9       | 1.0      | 1.0                                                               | 1.0                                                               | 1.0                                                               |
| Regenerator effectiveness ( $\xi$ )                                | —       | —       | —       | 0.95      | 0.95      | 0.95     | —                                                                 | —                                                                 | —                                                                 |
| Pressure ratio ( $r_p$ )                                           | 4       | 4       | 4       | 4         | 4         | 8        | 4                                                                 | 4                                                                 | 4                                                                 |
| Intercooling                                                       | —       | —       | —       | —         | —         | —        | $\frac{p'_1}{p_1} = \frac{1}{2} \frac{p_2}{p_1}$<br>$T_1'' = T_1$ | —                                                                 | $\frac{p'_1}{p_1} = \frac{1}{2} \frac{p_2}{p_1}$<br>$T_1'' = T$   |
| Reheat                                                             | —       | —       | —       | —         | —         | —        | —                                                                 | $\frac{p'_3}{p_4} = \frac{1}{2} \frac{p_3}{p_4}$<br>$T_3'' = T_3$ | $\frac{p'_3}{p_4} = \frac{1}{2} \frac{p_3}{p_4}$<br>$T_3'' = T_3$ |
| Turbine work ( $\dot{W}_T/\dot{m}$ ) Btu/lb MJ/kg                  | 925.9   | 833.3   | 776.5   | 925.9     | 833.3     | 1229.4   | 925.9                                                             | 1052.5                                                            | 1052.5                                                            |
| Compressor work ( $\dot{W}_c/\dot{m}$ ) Btu/lb MJ/kg               | 2.150   | 1.935   | 1.803   | 2.150     | 1.935     | 2.855    | 2.150                                                             | 2.444                                                             | 2.444                                                             |
| Net work ( $\dot{W}_{NET}/\dot{m}$ ) Btu/lb MJ/kg                  | 458.7   | 509.7   | 509.7   | 458.7     | 509.7     | 801.9    | 395.96                                                            | 458.7                                                             | 395.96                                                            |
| Heat in ( $\dot{Q}_R/\dot{m}$ ) Btu/lb MJ/kg                       | 1.066   | 1.184   | 1.184   | 1.066     | 1.184     | 1.862    | 0.920                                                             | 1.066                                                             | 0.920                                                             |
| Cycle thermal efficiency ( $\eta_{th}$ )(%)                        | 467.2   | 323.6   | 266.9   | 467.2     | 323.6     | 427.5    | 529.9                                                             | 593.8                                                             | 656.5                                                             |
|                                                                    | 1.084   | 0.752   | 0.620   | 1.084     | 0.752     | 0.993    | 1.23                                                              | 1.378                                                             | 1.524                                                             |
|                                                                    | 1103.0  | 1052.9  | 1052.9  | 934.9     | 844.4     | 1205.7   | 1364.5                                                            | 1630.1                                                            | 1890.8                                                            |
|                                                                    | 2.560   | 2.45    | 2.45    | 2.172     | 1.961     | 2.800    | 3.169                                                             | 3.786                                                             | 4.391                                                             |
|                                                                    | 42.3    | 30.7    | 25.3    | 50.0      | 38.3      | 35.46    | 38.8                                                              | 36.4                                                              | 34.7                                                              |

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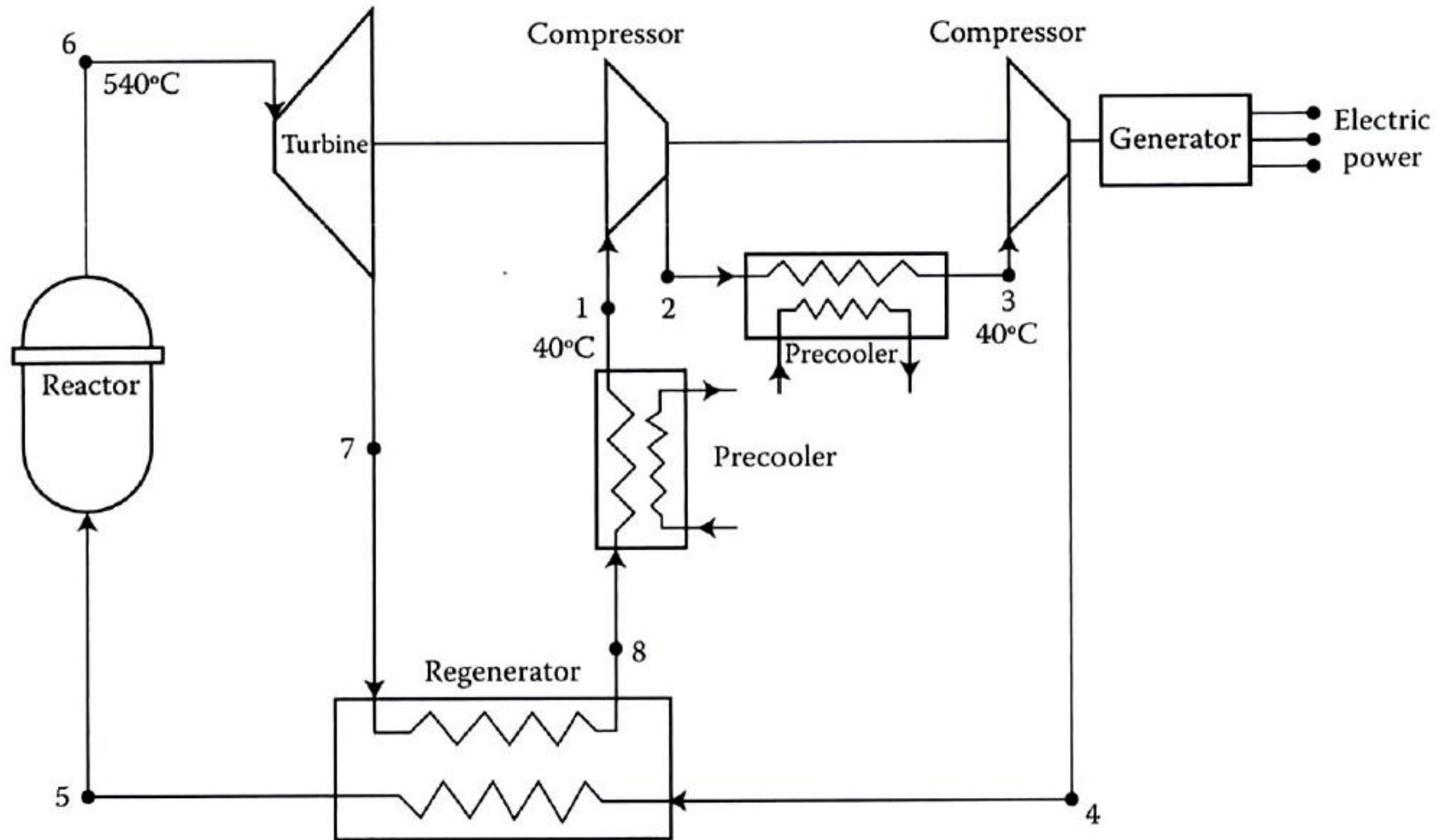
A gas-cooled reactor is designed to heat helium gas to a maximum temperature of 540°C. The helium flows through a gas turbine, generating work to run the compressors and an electric generator, and then through a regenerative heat exchanger and two stages of compression with pre-cooling to 40°C before entering each compressor. Each compressor and the turbine have an isentropic efficiency of 85%, and the exchanger drop factor  $\beta$  is equal to 1.05. Each compression stage has a pressure ratio ( $r_p$ ) of 1.27. The heat exchanger effectiveness ( $\xi$ ) is 0.90.

Determine the cycle thermal efficiency. The Brayton cycle system is illustrated in Figure 6.42. The pressure drop factor  $\beta$  is defined as

$$\beta \equiv \left( \frac{P_4}{P_6} \cdot \frac{P_7}{P_1} \cdot \frac{P_2}{P_3} \right)^{\gamma-1/\gamma} = 1.05$$

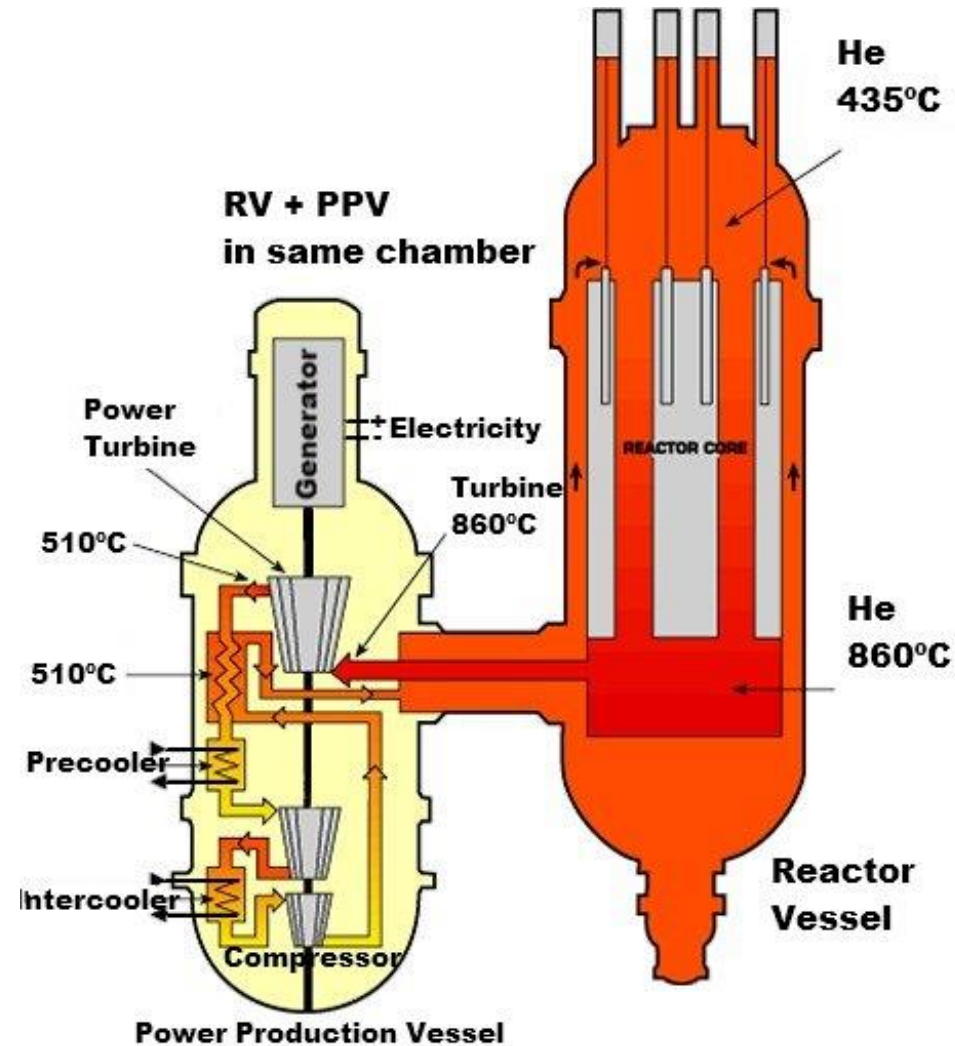
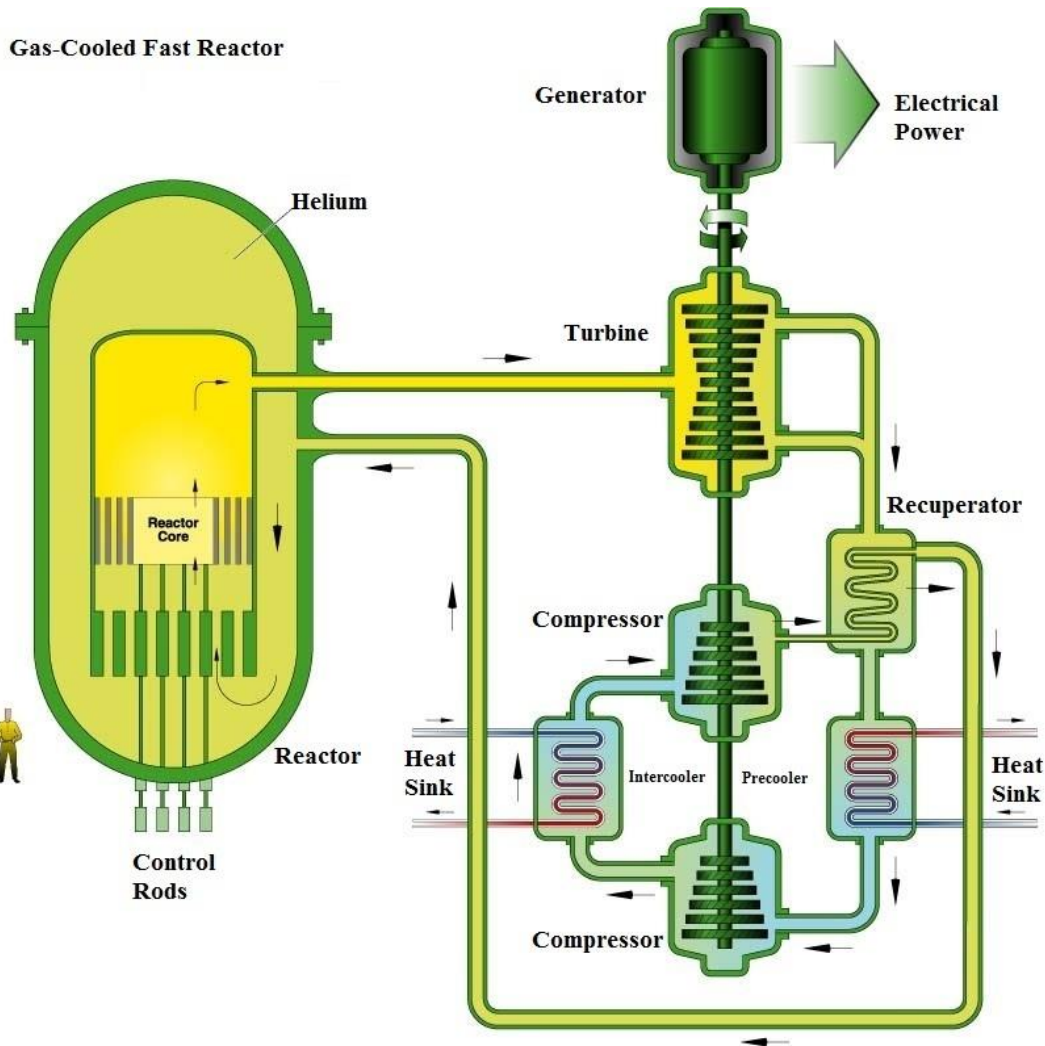
*Answer:*  $\eta_{th} = 13.8\%$

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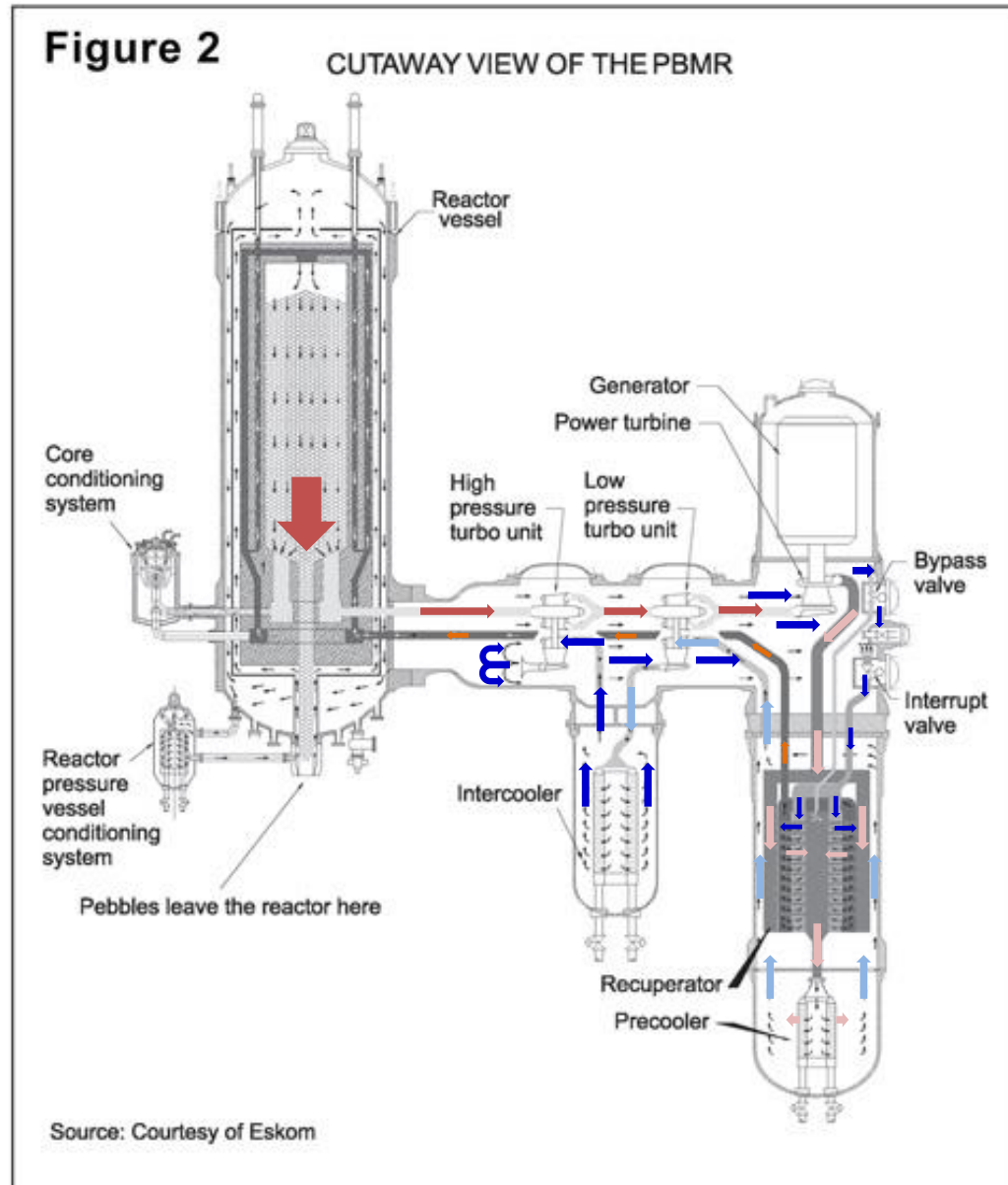
# Simple Brayton Cycle

## ❖ Brayton Cycle



# Simple Brayton Cycle

## ❖ Brayton Cycle



## ❖ Contents of lecture

- Chapter 1 Principal Characteristics of Power Reactors

- Will be replaced by the lecture note
- Introduction to Nuclear Systems

Nuclear system

- Chapter 4 Transport Equations for Single-Phase Flow (up to energy equation)

- Chapter 6 Thermodynamics of Nuclear Energy Conversion Systems:

Nonflow and Steady Flow : First- and Second-Law Applications

- Chapter 7 Thermodynamics of Nuclear Energy Conversion Systems :

Nonsteady Flow First Law Analysis

Thermodynamics

- Chapter 3 Reactor Energy Distribution

- Chapter 8 Thermal Analysis of Fuel Elements

Heat transport  
Conduction  
heat transfer