

## Solution Technique (Chapter 11)

- Inversion
- Direct Method
  - Cramer's Rule
  - Gauss Elimination
  - LU factorization, Cholesky's method
- Indirect Method
  - Inverse Iteration
    - Jacobi method : total steps
    - Gauss-Seidel method : single step

### Inversion

$$\underline{K}\underline{U} = \underline{P}, \quad \underline{U} = \underline{K}^{-1}\underline{P}$$

Inefficient method since it requires the evaluation of a number of determinants of high order in calculation of  $\underline{K}^{-1}$

### Gauss Elimination

Characteristics of matrix calculation does not change even after row- and column-calculations.

A systematic procedure for making a triangular matrix  
Or for eliminating variables one by one

- 1) forwarding
- 2) backwarding (back-substitution)

$$\underline{K} \underline{U} = \underline{P}$$

$$\begin{bmatrix} & & & \\ & & & \\ & & & \\ & & & \end{bmatrix} \begin{bmatrix} \\ \\ \\ \end{bmatrix} = \begin{bmatrix} \\ \\ \\ \end{bmatrix}$$

⇓ Elimination (forwarding)

$$\begin{bmatrix} & & & \\ & & & \\ & & & \\ \underline{0} & & & \end{bmatrix} \begin{bmatrix} \\ \\ \\ \end{bmatrix} = \begin{bmatrix} \\ \\ \\ \end{bmatrix} \quad \underline{K}' \underline{U} = \underline{P}'$$

⇓ Back - substitution

$$\begin{bmatrix} & & & \\ & & & \\ & & & \\ \underline{0} & & & \end{bmatrix} \begin{matrix} \uparrow \\ U_n \end{matrix} = \begin{bmatrix} \\ \\ P'_n \end{bmatrix} \quad U_n = P'_n / k'_{nn}$$

## LU - Factorization

$$\underline{K} \underline{V} = \underline{P}$$

$\underline{V}$  = unknown displacement

$$\underline{K} = \underline{L} \underline{U}$$

$\underline{L}$  = Lower triangular matrix

$\underline{U}$  = upper triangular matrix

$$\begin{bmatrix} k_{11} & k_{12} & k_{13} \\ k_{21} & k_{22} & k_{23} \\ k_{31} & k_{32} & k_{33} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ m_{21} & 1 & 0 \\ m_{31} & m_{32} & 1 \end{bmatrix} \cdot \begin{bmatrix} u_{11} & u_{12} & u_{13} \\ 0 & u_{22} & u_{23} \\ 0 & 0 & u_{33} \end{bmatrix}$$

$$k_{11} = u_{11}, \quad k_{12} = u_{12}, \quad k_{13} = u_{13}$$

$$k_{21} = m_{21} u_{11}, \quad k_{22} = m_{21} u_{12} + u_{22}, \quad \text{etc}$$

$$\underline{K} \underline{V} = \underline{P} \Rightarrow \underline{L} \underline{U} \underline{V} = \underline{P} \quad \text{set } \underline{U} \underline{V} = \underline{Y}$$

$$\underline{L} \underline{Y} = \underline{P} \quad \text{solve } \underline{Y}$$

$$\underline{U} \underline{V} = \underline{Y} \quad \text{solve } \underline{V}$$

## cholesky's method

If  $\underline{K}$  is symmetric and positive definite ( $\underline{X}^T \underline{K} \underline{X} > 0$ ),

$$\underline{U} = \underline{L}^T \quad \underline{K} = \underline{L} \underline{L}^T$$

$$\begin{bmatrix} k_{11} & k_{12} & k_{13} \\ k_{21} & k_{22} & k_{23} \\ k_{31} & k_{32} & k_{33} \end{bmatrix} = \begin{bmatrix} l_{11} & 0 & 0 \\ l_{21} & l_{22} & 0 \\ l_{31} & l_{32} & l_{33} \end{bmatrix} \begin{bmatrix} l_{11} & l_{21} & l_{31} \\ 0 & l_{22} & l_{32} \\ 0 & 0 & l_{33} \end{bmatrix}$$

$$\ominus \quad \underline{K} \underline{V} = \underline{P} \Rightarrow \underline{L} \underline{L}^T \underline{V} = \underline{P} \quad \text{set } \underline{L}^T \underline{V} = \underline{Y}$$

$$\underline{L} \underline{Y} = \underline{P} \quad \text{solve } \underline{Y}$$

$$\underline{L}^T \underline{V} = \underline{Y} \quad \text{solve } \underline{V}$$

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## Iterative Method

By using iterative method, rapid convergence can be achieved,

When 1) matrix has large main diagonal entries

2) matrix are sparse, that is, have very many zeros

$$\underline{K} \underline{U} = \underline{P} \Rightarrow \underline{K}' \underline{U} = \underline{P}'$$

$\underline{K}'$  = all diagonal terms are 1's.

$$\begin{array}{ccc} \begin{bmatrix} 1 & -0.25 & -0.25 & 0 \\ -0.25 & 1 & 0 & -0.25 \\ -0.25 & 0 & 1 & -0.25 \\ 0 & -0.25 & -0.25 & 1 \end{bmatrix} & \begin{bmatrix} U_1 \\ U_2 \\ U_3 \\ U_4 \end{bmatrix} & = & \begin{bmatrix} 50 \\ 50 \\ 25 \\ 25 \end{bmatrix} \\ \underline{K}' & \underline{U} & & \underline{P}' \end{array}$$

Gauss - Seidel Iteration Method (Successive correction)

Assuming  $\underline{U}^{(0)} = \begin{bmatrix} 100 \\ 100 \\ 100 \\ 100 \end{bmatrix}$

~~$$U_1^{(1)} = 0.25 U_2^{(0)} + 0.25 U_3^{(0)} + 50 = 100$$~~

~~$$U_2^{(1)} = 0.25 U_1^{(1)} + 0.25 U_4^{(0)} + 50 = 100$$~~

~~$$U_3^{(1)} = 0.25 U_1^{(1)} + 0.25 U_4^{(0)} + 25 = 75$$~~

~~$$U_4^{(1)} = 0.25 U_2^{(1)} + 0.25 U_3^{(1)} + 25 = 68.75$$~~

iterative calculation is required until  $\underline{U}^{(n)} \parallel \underline{U}^{(n-1)}$

$$\underline{U}^{(n)} \cdot \underline{U}^{(n-1)} = \|\underline{U}^{(n)}\| \|\underline{U}^{(n-1)}\| \cos \theta$$

if  $\underline{U}^{(n)} \parallel \underline{U}^{(n-1)}$ ,  $\cos \theta \rightarrow 1.0$

$$\underline{K} = \underline{I} + \underline{L} + \underline{U}$$

$$\underline{K}\underline{u} = (\underline{I} + \underline{L} + \underline{U})\underline{u} = \underline{P}$$

$$\underline{u}^{(m+1)} = \underline{P} - \underline{L}\underline{u}^{(m+1)} - \underline{U}\underline{u}^{(m)}$$

$$(\underline{I} + \underline{L})\underline{u}^{(m+1)} = \underline{P} - \underline{U}\underline{u}^{(m)}$$

$$\underline{u}^{(m+1)} = (\underline{I} + \underline{L})^{-1}\underline{P} - (\underline{I} + \underline{L})^{-1}\underline{U}\underline{u}^{(m)}$$

Jacobi Iteration method - (Simultaneous correction)

$$\underline{K}\underline{u} = \underline{I}\underline{u} + (\underline{K} - \underline{I})\underline{u} = \underline{P}$$

$$\underline{u}^{(m+1)} = \underline{P} + (\underline{I} - \underline{K})\underline{u}^{(m)}$$

An LU-factorization of a given square matrix  $A$  is of the form

$$(2) \quad \boxed{A = LU}$$

where  $L$  is lower triangular and  $U$  is upper triangular. For example,

$$A = \begin{bmatrix} 2 & 3 \\ 8 & 5 \end{bmatrix} = LU = \begin{bmatrix} 1 & 0 \\ 4 & 1 \end{bmatrix} \begin{bmatrix} 2 & 3 \\ 0 & -7 \end{bmatrix}$$

It can be proved that for any nonsingular matrix (see Sec. 6.7) the rows can be reordered so that the resulting matrix  $A$  has an LU-factorization (2) in which  $L$  turns out to be the matrix of the *multipliers*  $m_{jk}$  of the Gauss elimination, with main diagonal  $1, \dots, 1$ , and  $U$  is the matrix of the triangular system at the end of the Gauss elimination. (See Ref. [E3], pp. 155–156, listed in Appendix 1.)

The *crucial idea* now is that  $L$  and  $U$  in (2) can be computed directly, without solving simultaneous equations (thus, without using the Gauss elimination). As a count shows, this needs about  $n^3/3$  operations, about half as many as the Gauss elimination, which needs about  $2n^3/3$  (see Sec. 18.1). And once we have (2), we can use it for solving  $Ax = b$  in two steps, involving only about  $n^2$  operations, simply by noting that  $Ax = LUx = b$  may be written

$$(3) \quad \boxed{(a) \quad Ly = b \quad \text{where} \quad (b) \quad Ux = y}$$

and solving first (3a) for  $y$  and then (3b) for  $x$ . This is called **Doolittle's method**. Both systems (3a) and (3b) are triangular, so their solution is the same as back substitution in the Gauss elimination.

A similar method, **Crout's method**, is obtained from (2) if  $U$  (instead of  $L$ ) is required to have main diagonal  $1, \dots, 1$ . In either case the factorization (2) is unique.

#### Doolittle's method

Solve the system in Example 1 of Sec. 18.1 by Doolittle's method.

*Solution.* The decomposition (2) is obtained from

$$A = [a_{jk}] = \begin{bmatrix} 3 & 5 & 2 \\ 0 & 8 & 2 \\ 6 & 2 & 8 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ m_{21} & 1 & 0 \\ m_{31} & m_{32} & 1 \end{bmatrix} \begin{bmatrix} u_{11} & u_{12} & u_{13} \\ 0 & u_{22} & u_{23} \\ 0 & 0 & u_{33} \end{bmatrix}$$

by determining the  $m_{jk}$  and  $u_{jk}$ , using matrix multiplication. By going through  $A$  row by row we get successively

$a_{11} = 3 = u_{11}$	$a_{12} = 5 = u_{12}$	$a_{13} = 2 = u_{13}$
$a_{21} = 0 = m_{21}u_{11}$	$a_{22} = 8 = m_{21}u_{12} + u_{22}$	$a_{23} = 2 = m_{21}u_{13} + u_{23}$
$m_{21} = 0$	$u_{22} = 8$	$u_{23} = 2$
$a_{31} = 6 = m_{31}u_{11}$	$a_{32} = 2 = m_{31}u_{12} + m_{32}u_{22}$	$a_{33} = 8 = m_{31}u_{13} + m_{32}u_{23} + u_{33}$
$= m_{31} \cdot 3$	$= 2 \cdot 5 + m_{32} \cdot 8$	$= 2 \cdot 2 - 1 \cdot 2 + u_{33}$
$m_{31} = 2$	$m_{32} = -1$	$u_{33} = 6$

$$u_{1k} = a_{1k} \quad k = 1, \dots, n$$

$$m_{j1} = \frac{a_{j1}}{u_{11}} \quad j = 2, \dots, n$$

$$(4) \quad u_{jk} = a_{jk} - \sum_{s=1}^{j-1} m_{js}u_{sk} \quad k = j, \dots, n; \quad j \geq 2$$

$$m_{jk} = \frac{1}{u_{kk}} \left( a_{jk} - \sum_{s=1}^{k-1} m_{js}u_{sk} \right) \quad j = k+1, \dots, n; \quad k \geq 2.$$

## Cholesky's Method

For a *symmetric, positive definite* matrix  $A$  (thus  $A = A^T$ ,  $x^T A x > 0$  for all  $x \neq 0$ ) we can in (2) even choose  $U = L^T$ , thus  $u_{jk} = m_{kj}$  (but impose no conditions on the main

The popular method of solving  $Ax = b$  based on this factorization  $A = LL^T$  is called **Cholesky's method**. In terms of the entries of  $L = [l_{jk}]$  the formulas for the factorization are

$$\begin{aligned}
 (6) \quad & l_{11} = \sqrt{a_{11}} \\
 & l_{j1} = \frac{a_{j1}}{l_{11}} \quad j = 2, \dots, n \\
 & l_{jj} = \sqrt{a_{jj} - \sum_{s=1}^{j-1} l_{js}^2} \quad j = 2, \dots, n \\
 & l_{pj} = \frac{1}{l_{jj}} \left( a_{pj} - \sum_{s=1}^{j-1} l_{js} l_{ps} \right) \quad p = j+1, \dots, n; \quad j \geq 2.
 \end{aligned}$$

If  $A$  is symmetric but not positive definite, this method could still be applied, but then leads to a *complex* matrix  $L$ , so that it becomes impractical.

### Cholesky's method

Solve by Cholesky's method:

$$\begin{aligned}
 4x_1 + 2x_2 + 14x_3 &= 14 \\
 2x_1 + 17x_2 - 5x_3 &= -101 \\
 14x_1 - 5x_2 + 83x_3 &= 155.
 \end{aligned}$$

**Solution.** From (6) or from the form of the factorization

$$\begin{bmatrix} 4 & 2 & 14 \\ 2 & 17 & -5 \\ 14 & -5 & 83 \end{bmatrix} = \begin{bmatrix} l_{11} & 0 & 0 \\ l_{21} & l_{22} & 0 \\ l_{31} & l_{32} & l_{33} \end{bmatrix} \begin{bmatrix} l_{11} & l_{21} & l_{31} \\ 0 & l_{22} & l_{32} \\ 0 & 0 & l_{33} \end{bmatrix}$$

we compute, in the given order,

$$\begin{aligned}
 l_{11} &= \sqrt{a_{11}} = 2 & l_{21} &= \frac{a_{21}}{l_{11}} = \frac{2}{2} = 1 & l_{31} &= \frac{a_{31}}{l_{11}} = \frac{14}{2} = 7 \\
 l_{22} &= \sqrt{a_{22} - l_{21}^2} = \sqrt{17 - 1} = 4 \\
 l_{32} &= \frac{1}{l_{22}} (a_{32} - l_{31} l_{21}) = \frac{1}{4} (-5 - 7 \cdot 1) = -3 \\
 l_{33} &= \sqrt{a_{33} - l_{31}^2 - l_{32}^2} = \sqrt{83 - 7^2 - (-3)^2} = 5.
 \end{aligned}$$



## Gauss-Seidel Iteration Method

This is an iterative method of great practical importance, which we can simply explain in terms of an example.

### Gauss-Seidel iteration

We consider the linear system

$$\begin{aligned}
 (1) \quad & x_1 - 0.25x_2 - 0.25x_3 = 50 \\
 & -0.25x_1 + x_2 - 0.25x_4 = 50 \\
 & -0.25x_1 + x_3 - 0.25x_4 = 25 \\
 & -0.25x_2 - 0.25x_3 + x_4 = 25.
 \end{aligned}$$

(Equations of this form arise in the numerical solution of partial differential equations and in spline interpolation.)  
We write the system in the form

$$\begin{aligned}
 (2) \quad & x_1 = 0.25x_2 + 0.25x_3 + 50 \\
 & x_2 = 0.25x_1 + 0.25x_4 + 50 \\
 & x_3 = 0.25x_1 + 0.25x_4 + 25 \\
 & x_4 = 0.25x_2 + 0.25x_3 + 25.
 \end{aligned}$$

We use these equations for iteration, that is, we start from a (possibly poor) approximation to the solution, say,  $x_1^{(0)} = 100, x_2^{(0)} = 100, x_3^{(0)} = 100, x_4^{(0)} = 100$ , and compute from (2) a presumably better approximation

Use "old" values  
("New" values here not yet available)

$$\begin{aligned}
 (3) \quad & x_1^{(1)} = \quad \quad \quad 0.25x_2^{(0)} + 0.25x_3^{(0)} \quad \quad \quad + 50.00 = 100.00 \\
 & x_2^{(1)} = 0.25x_1^{(1)} \quad \quad \quad + 0.25x_4^{(0)} + 50.00 = 100.00 \\
 & x_3^{(1)} = 0.25x_1^{(1)} \quad \quad \quad + 0.25x_4^{(0)} + 25.00 = 75.00 \\
 & x_4^{(1)} = \quad \quad \quad 0.25x_2^{(1)} + 0.25x_3^{(1)} \quad \quad \quad + 25.00 = 68.75.
 \end{aligned}$$

Use "new" values

We see that these equations are obtained from (2) by substituting on the right the *most recent* approximations. In fact, corresponding elements replace previous ones as soon as they have been computed, so that in the second and third equations we use  $x_1^{(1)}$  (not  $x_1^{(0)}$ ), and in the last equation of (3) we use  $x_2^{(1)}$  and  $x_3^{(1)}$  (not  $x_2^{(0)}$  and  $x_3^{(0)}$ ). The next step yields

$$\begin{aligned}
 x_1^{(2)} &= 0.25x_2^{(1)} + 0.25x_3^{(1)} + 50.00 = 93.75 \\
 x_2^{(2)} &= 0.25x_1^{(2)} + 0.25x_4^{(1)} + 50.00 = 90.62 \\
 x_3^{(2)} &= 0.25x_1^{(2)} + 0.25x_4^{(1)} + 25.00 = 65.62 \\
 x_4^{(2)} &= 0.25x_2^{(2)} + 0.25x_3^{(2)} + 25.00 = 64.06.
 \end{aligned}$$

In practice, one would do further steps and obtain a more accurate approximate solution.

The reader may show that the exact solution is  $x_1 = x_2 = 87.5, x_3 = x_4 = 62.5$ .

To obtain an algorithm for the Gauss-Seidel iteration, let us derive the general formulas for this iteration.

We assume that  $a_{jj} = 1$  for  $j = 1, \dots, n$ . (Note that this can be achieved if we can rearrange the equations so that no diagonal coefficient is zero; then we may divide each equation by the corresponding diagonal coefficient.) We now write

$$(4) \quad A = I + L + U \quad (a_{jj} = 1)$$

where  $I$  is the  $n \times n$  unit matrix and  $L$  and  $U$  are respectively lower and upper triangular matrices with zero main diagonals. If we substitute (4) into  $Ax = b$ , we have

$$Ax = (I + L + U)x = b.$$

Taking  $Lx$  and  $Ux$  to the right, we obtain, since  $Ix = x$ ,

$$(5) \quad x = b - Lx - Ux.$$

Remembering from our computation in Example 1 that below the main diagonal we took "new" approximations and above the main diagonal "old" approximations, we obtain from (5) the desired iteration formulas

$$(6) \quad \boxed{x^{(m+1)} = b - Lx^{(m+1)} - Ux^{(m)}} \quad (a_{jj} = 1)$$

where  $x^{(m)} = [x_j^{(m)}]$  is the  $m$ th approximation and  $x^{(m+1)} = [x_j^{(m+1)}]$  is the  $(m + 1)$ st approximation. In components this gives the formula in line 1 in Table 18.2. The matrix

### Jacobi Iteration

The Gauss-Seidel iteration is a method of **successive corrections** because we replace approximations by corresponding new ones as soon as the latter have been computed. A method is called a method of **simultaneous corrections** if no component of an approximation  $x^{(m)}$  is used until *all* the components of  $x^{(m)}$  have been computed. A method of this type is the **Jacobi iteration**, which is similar to the Gauss-Seidel iteration but involves *not* using improved values until a step has been completed and then replacing  $x^{(m)}$  by  $x^{(m+1)}$  at once, directly before the beginning of the next cycle. Hence, if we write  $Ax = b$  (with  $a_{jj} = 1$  as before!) in the form  $x = b + (I - A)x$ , the Jacobi iteration in matrix notation is

$$(13) \quad \boxed{x^{(m+1)} = b + (I - A)x^{(m)}} \quad (a_{jj} = 1).$$

This method converges for every choice of  $x^{(0)}$  if and only if the spectral radius of  $I - A$  is less than 1. It has recently gained greater practical interest since on parallel processors all  $n$  equations can be solved simultaneously at each iteration step.

Modification of equations considering the support conditions

$$\underline{K} \underline{U} = \underline{P}$$

$$\begin{bmatrix} k_{11} & k_{12} & \dots & k_{1n} \\ k_{21} & k_{22} & \dots & k_{2n} \\ \vdots & & \ddots & \vdots \\ k_{n1} & k_{n2} & \dots & k_{nn} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_n \end{bmatrix} = \begin{bmatrix} P_1 \\ P_2 \\ \vdots \\ P_n \end{bmatrix}$$

$$\left[ \begin{array}{c|c} \underline{k}_{ff} & \underline{k}_{fs} \\ \hline \underline{k}_{sf} & \underline{k}_{ss} \end{array} \right] \begin{bmatrix} \underline{u}_f \\ \underline{u}_s \end{bmatrix} = \begin{bmatrix} \underline{P}_f \\ \underline{P}_s \end{bmatrix}$$

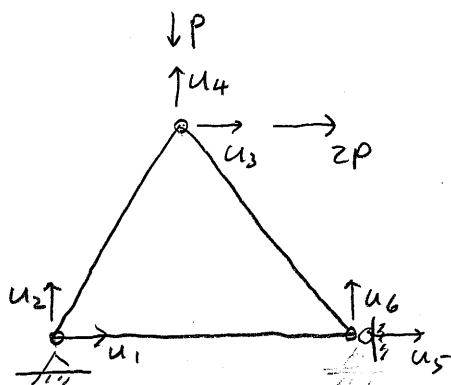
f : free  
s : support

$\underline{u}_f$  = unknown displacements

$\underline{P}_f$  = known (applied) forces

$\underline{u}_s$  = known (or given) displacements (boundary displacements)

$\underline{P}_s$  = unknown forces (reactions)



$$\underline{u} = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ u_3 \\ u_4 \\ 0 \\ u_6 \end{bmatrix} \Rightarrow \underline{u}_f$$

$$\underline{P} = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ P_4 \\ P_5 \\ P_6 \end{bmatrix} = \begin{bmatrix} P_1 \\ P_2 \\ 2P \\ -P \\ P_5 \\ 0 \end{bmatrix} \Rightarrow \underline{P}_f$$

$$\underline{k}_{ff} \underline{u}_f + \underline{k}_{fs} \underline{u}_s = \underline{P}_f$$

$$\underline{k}_{ff} \underline{u}_f = \underline{P}_f - \underline{k}_{fs} \underline{u}_s \Rightarrow \text{solve } \underline{u}_f$$

$$\underline{k}_{sf} \underline{u}_f + \underline{k}_{ss} \underline{u}_s = \underline{P}_s \Rightarrow \text{solve } \underline{P}_s$$

$k_{11}$	$k_{12}$	$k_{13}$	$k_{14}$	$k_{15}$	$k_{16}$	$u_1^0$	$P_1$
	$k_{22}$	$k_{23}$	$k_{24}$	$k_{25}$	$k_{26}$	$u_2^0$	$P_2$
		$k_{33}$	$k_{34}$	$k_{35}$	$k_{36}$	$u_3$	$2P$
sym.			$k_{44}$	$k_{45}$	$k_{46}$	$u_4$	$-P$
				$k_{55}$	$k_{56}$	$u_5^0$	$P_5$
					$k_{66}$	$u_6$	$0$

$$\begin{bmatrix} k_{33} & k_{34} & k_{36} \\ k_{43} & k_{44} & k_{46} \\ k_{63} & k_{64} & k_{66} \end{bmatrix} \begin{bmatrix} u_3 \\ u_4 \\ u_6 \end{bmatrix} = \begin{bmatrix} 2P \\ -P \\ 0 \end{bmatrix}$$

$$\underline{k}_{ff} \underline{u}_f = \underline{P}_f - \underline{k}_{fs} \underline{u}_s^0$$

solve  $\underline{u}_f$

$$\begin{bmatrix} k_{13} & k_{14} & k_{16} \\ k_{23} & k_{24} & k_{26} \\ k_{53} & k_{54} & k_{56} \end{bmatrix} \begin{bmatrix} u_3 \\ u_4 \\ u_6 \end{bmatrix} = \begin{bmatrix} P_1 \\ P_2 \\ P_5 \end{bmatrix}$$

$$\underline{k}_{sf} \underline{u}_f = \underline{P}_s - \underline{k}_{ss} \underline{u}_s^0$$

solve  $\underline{P}_s$

Technique not disturbing the size and order of the original stiffness matrix

$$\begin{bmatrix} \underline{k}_{ff} & | & \underline{0} \\ \hline \underline{0} & | & \underline{I} \end{bmatrix} \begin{bmatrix} \underline{u}_f \\ \underline{u}_s \end{bmatrix} = \begin{bmatrix} \underline{P}_f - \underline{k}_{fs} \underline{u}_s \\ \underline{u}_s \end{bmatrix}$$

1	0	0	0	0	0
0	1	0	0	0	0
0	0	$k_{33}$	$k_{34}$	0	$k_{36}$
0	0	$k_{43}$	$k_{44}$	0	$k_{46}$
0	0	0	0	1	0
0	0	$k_{63}$	$k_{64}$	0	$k_{66}$

$u_1^0$
$u_2^0$
$u_3$
$u_4$
$u_5^0$
$u_6$

 $=$ 

$u_1^0$
$u_2^0$
$2P$
$-P$
$u_5^0$
0

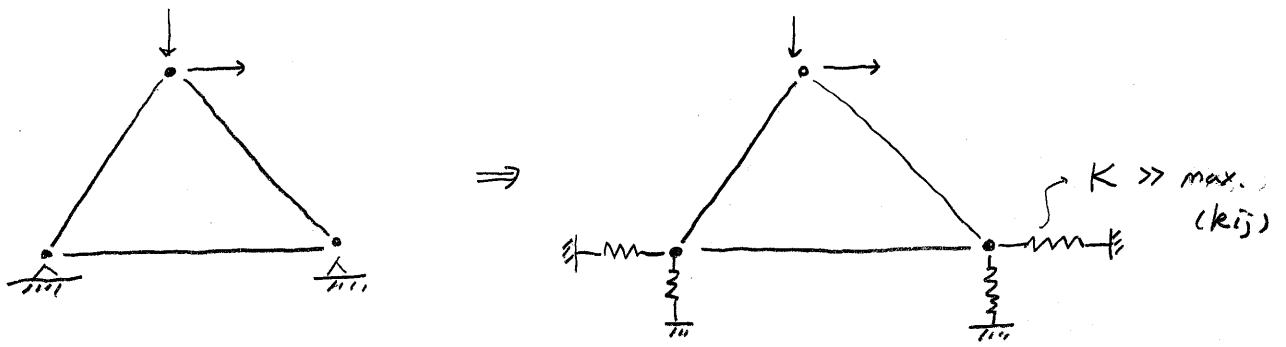
 $-$ 

$k_{31} u_1 + k_{32} u_2 + k_{35} u_5$
$k_{41} u_1 + k_{42} u_2 + k_{45} u_5$
0
$k_{61} u_1 + k_{62} u_2 + k_{65} u_5$

solve  $\underline{u}_f$

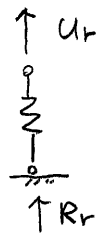
$$\underline{k}_{sf} \underline{u}_f + \underline{k}_{ss} \underline{u}_s = \underline{P}_s \Rightarrow \text{solve } \underline{P}_s$$

Modification of Stiffness matrix with big spring



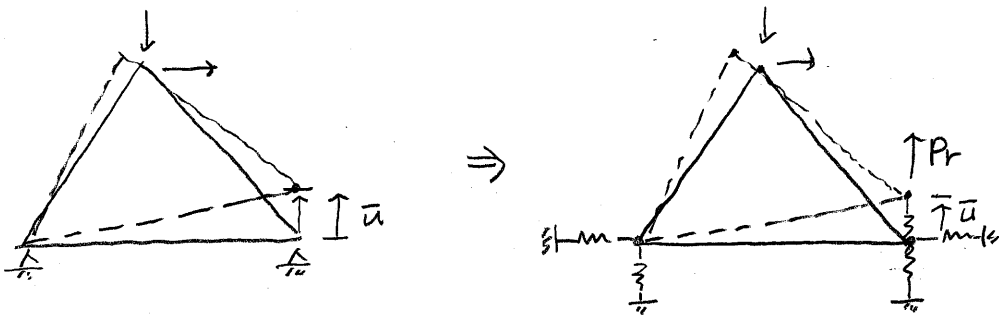
$$\begin{bmatrix} \vdots \\ \vdots \\ K + k_{rr} \\ \vdots \\ \vdots \end{bmatrix} \begin{bmatrix} \vdots \\ \vdots \\ u_r \\ \vdots \\ \vdots \end{bmatrix} = \begin{bmatrix} \vdots \\ \vdots \\ 0 \\ \vdots \\ \vdots \end{bmatrix}$$

$K = 10^7 \times \max(k_{ij})$   
Solve  $u_r$



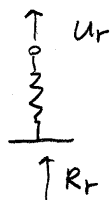
reaction  $R_r = -K u_r$  by equilibrium

Non-zero displacement boundary condition  $\bar{u}$



$$\begin{bmatrix} \vdots \\ \vdots \\ K + k_{rr} \\ \vdots \\ \vdots \end{bmatrix} \begin{bmatrix} \vdots \\ \vdots \\ u_r \\ \vdots \\ \vdots \end{bmatrix} = \begin{bmatrix} \vdots \\ \vdots \\ P_r \\ \vdots \\ \vdots \end{bmatrix}$$

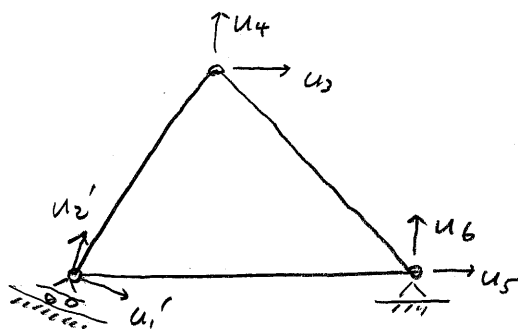
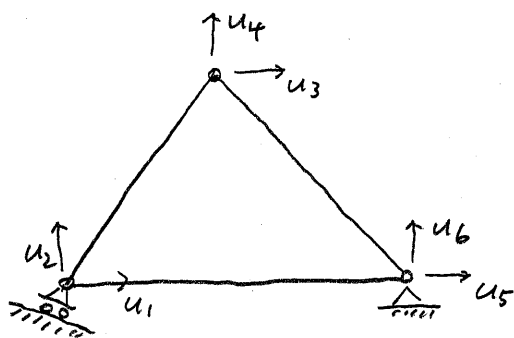
$P_r = K \cdot \bar{u}$



reaction  $R_r = -K u_r$

net reaction  $R_r' = -K (u_r - \bar{u})$

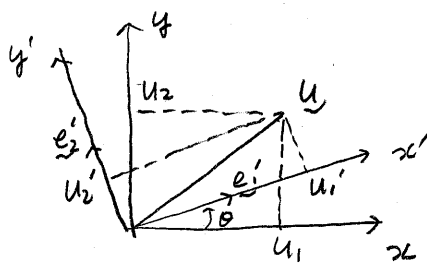
## Inclined supports



$$\underline{u} = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \end{bmatrix}$$

$$\underline{u}' = \begin{bmatrix} u_1' \\ u_2' \\ u_3 \\ u_4 \\ u_5 \\ u_6 \end{bmatrix}$$

$u_1', u_2'$   
 $\Rightarrow$  local  
 coordinate  
 system



$$\underline{e}_1' = \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix} \quad \text{directional vector of } x' \text{ axis}$$

$$\underline{e}_2' = \begin{bmatrix} -\sin \theta \\ \cos \theta \end{bmatrix} \quad \text{directional vector of } y' \text{ axis}$$

$$u_1' = \underline{e}_1' \cdot \underline{u} = \underline{e}_1'^T \underline{u}$$

$$u_2' = \underline{e}_2' \cdot \underline{u} = \underline{e}_2'^T \underline{u}$$

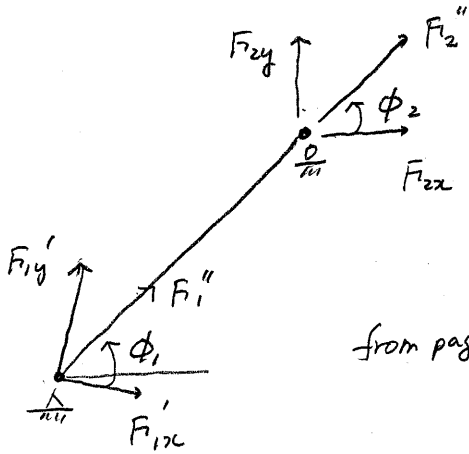
$$\begin{bmatrix} u_1' \\ u_2' \end{bmatrix} = \underbrace{\begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix}}_{\underline{R}} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$\underline{u}' = \underline{R} \underline{u}$$

$$\underline{u} = \underline{R}^T \underline{u}'$$

calculation of element stiffness in terms of local axis

11-16



when  $u_1' = v_1' = v_2' = 0$ ,

$$F_{2x} = F_2'' \cos \phi_2 = \frac{EA}{L} \cos^2 \phi_2 u_2$$

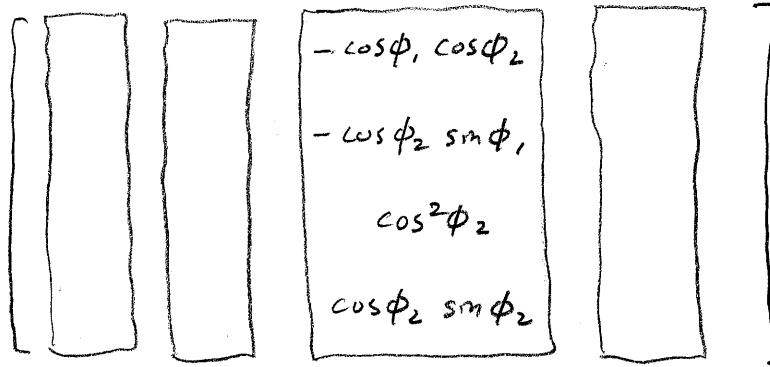
$$F_{2y} = F_2'' \sin \phi_2 = \frac{EA}{L} \cos \phi_2 \sin \phi_2 u_2$$

from page 17.

$$F_{1x}' = F_1'' \cos \phi_1 = -\frac{EA}{L} \cos \phi_1 \cos \phi_2 u_2$$

$$F_{1y}' = F_1'' \sin \phi_1 = -\frac{EA}{L} \cos \phi_2 \sin \phi_1 u_2$$

$$k \sim = \frac{EA}{L}$$



Element stiffness matrix should be constructed considering the local coordinate system.

The bottom horizontal element's stiffness can also be calculated considering the local axis.

