

# 458.401 Process & Product Design

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## Pinch Technology (2)

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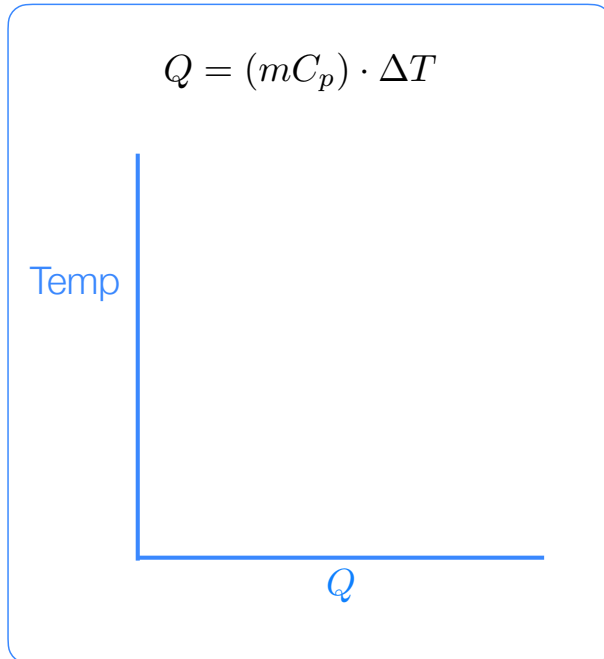
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Pinch Technology

## Graphical Method

- It is possible to generate the same Maximum Energy Recovery solution using a second method.
  - We can use this method for verification of the first method.
- The key results remain as
  - Where is the pinch?
  - What is the cold utility demand?
  - What is the hot utility demand?

# Graphical Method

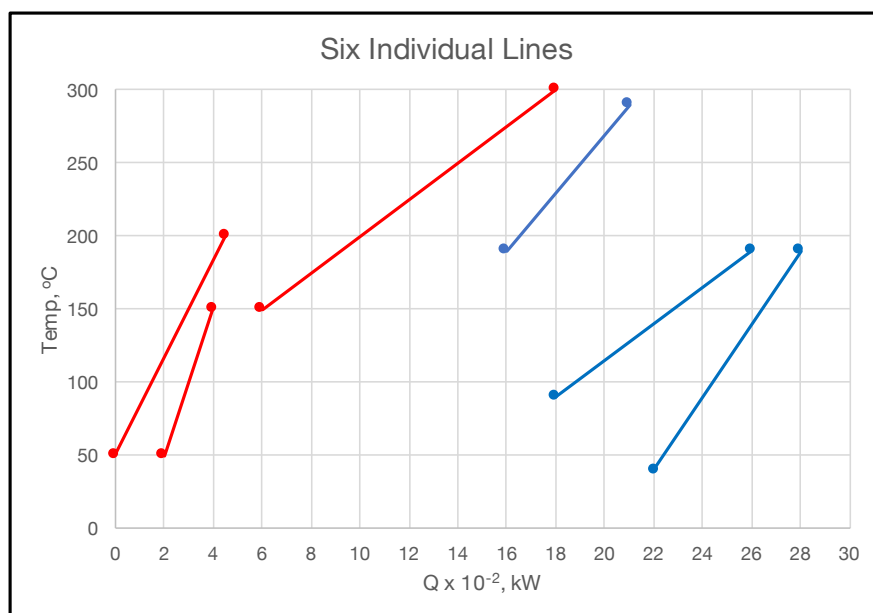


$$\square = \left( \frac{1}{mC_p} \right) \cdot \square$$

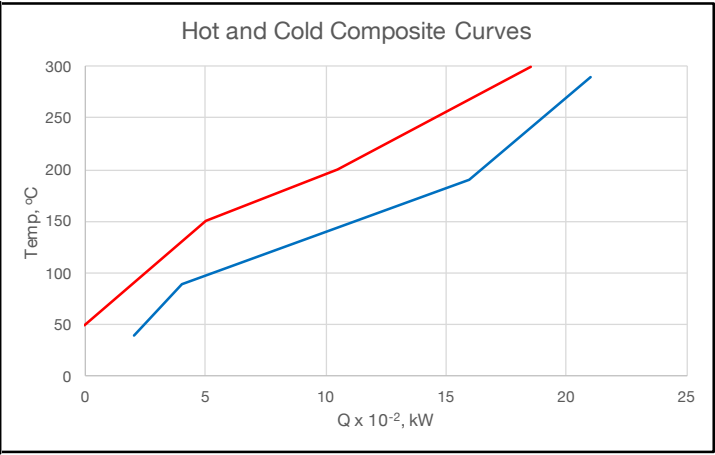
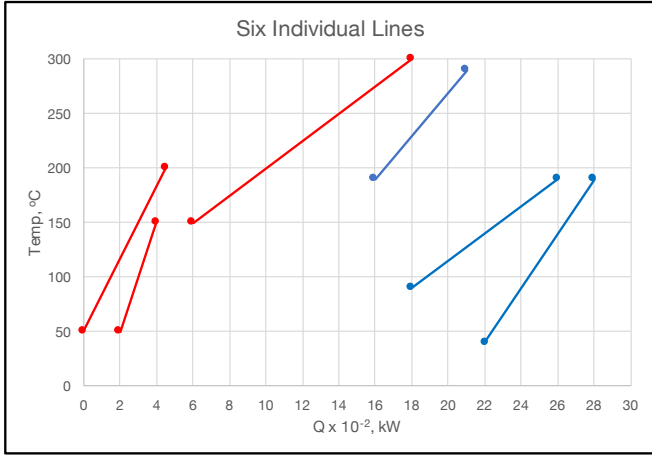
$$y = m \cdot x$$

$$\text{Slope} = \frac{\Delta y}{\Delta x}$$

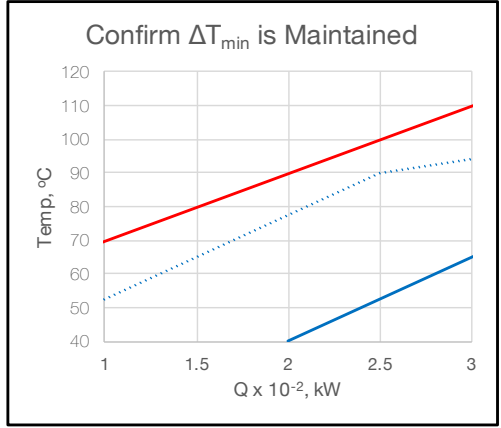
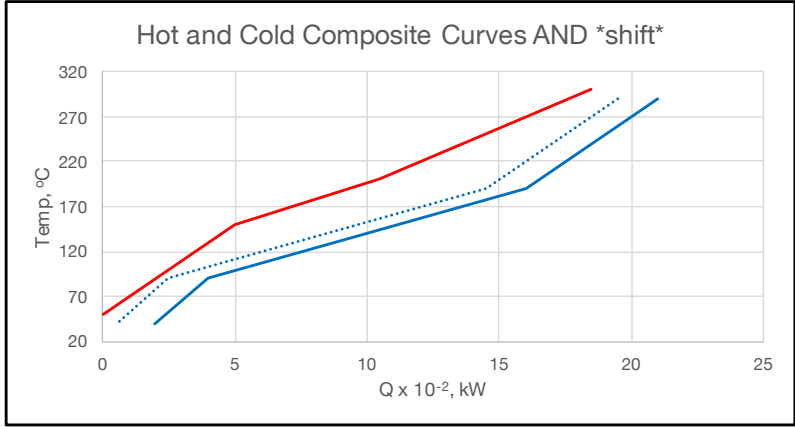
# Graphical Method



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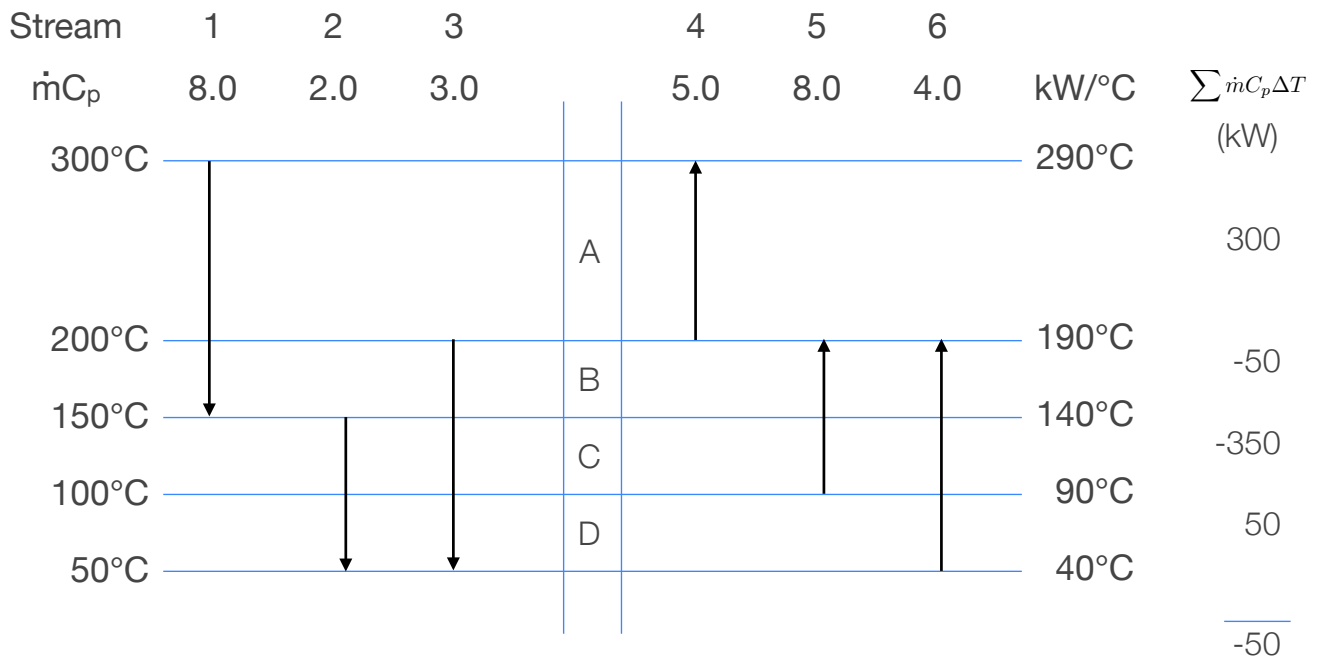


Pinch location = \_\_\_\_\_ °C (hot streams) and \_\_\_\_\_ °C (cold streams)

Total cooling water demand = \_\_\_\_\_ kW

Total steam demand = \_\_\_\_\_ kW

# Temperature Interval Diagram



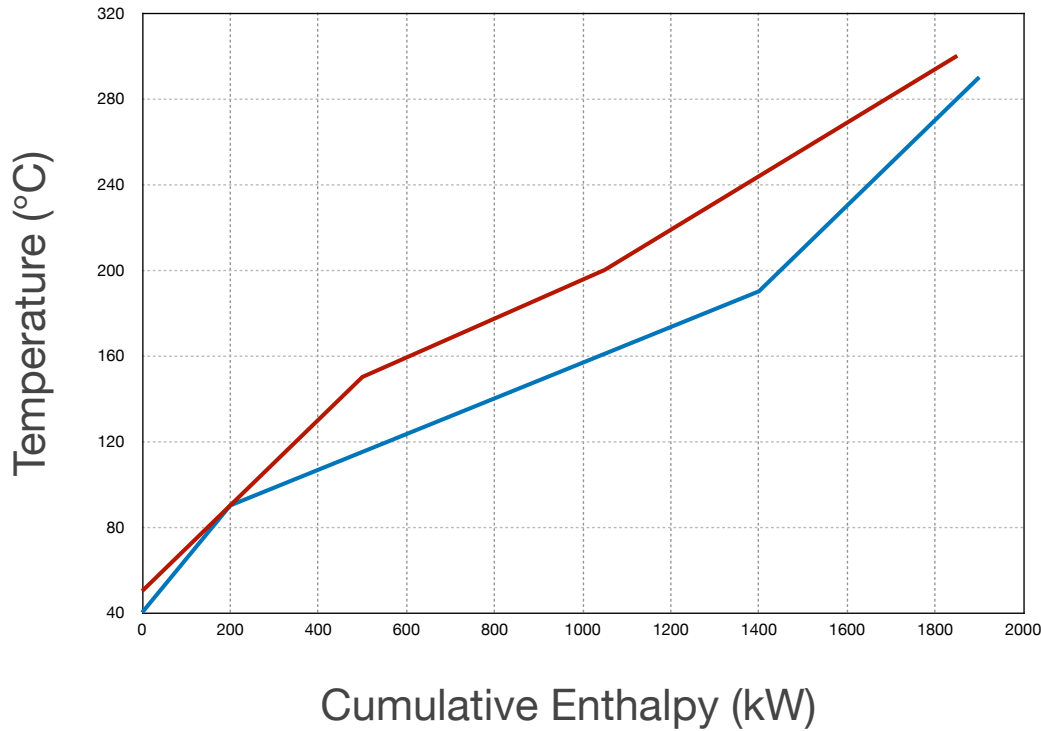
## Hot Streams

Temperature Interval	Temperature (°C)	Enthalpy of Hot Streams in Temperature Interval (kW)	Cumulative Enthalpy of Hot Streams (kW)
	50	0	0
D	100	$(2 + 3)(100 - 50) = 250$	250
C	150	$(2 + 3)(150 - 100) = 250$	500
B	200	$(8 + 3)(200 - 150) = 550$	1050
A	300	$(8)(300 - 200) = 800$	1850

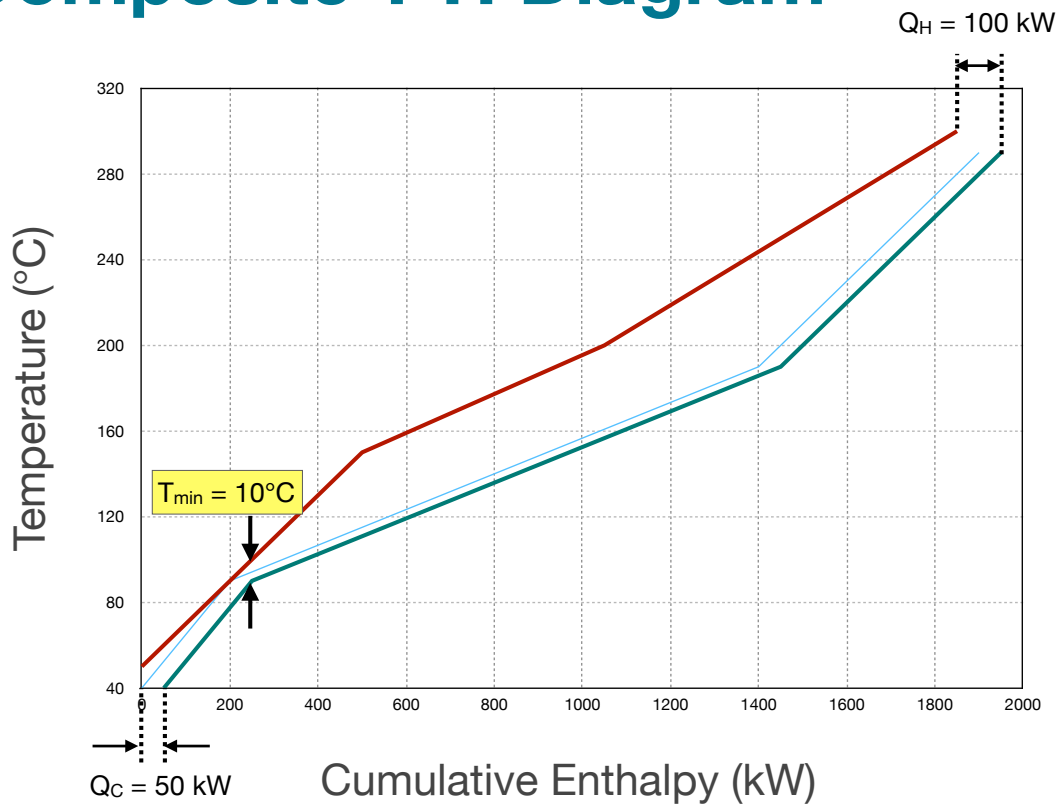
## Cold Streams

Temperature Interval	Temperature (°C)	Enthalpy of Cold Streams in Temperature Interval (kW)	Cumulative Enthalpy of Cold Streams (kW)
	40	0	0
D	90	$(4)(90 - 40) = 200$	200
C	140	$(8 + 4)(140 - 90) = 600$	800
B	190	$(8 + 4)(190 - 140) = 600$	1400
A	290	$(5)(290 - 190) = 500$	1900

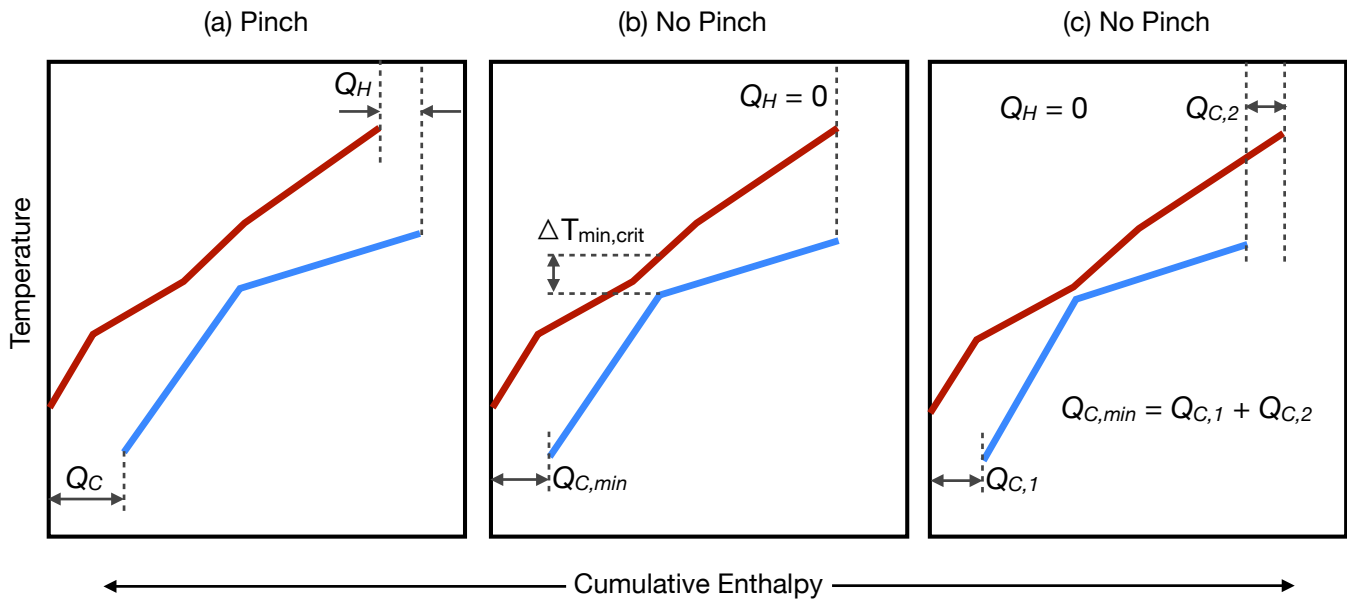
# Composite T-H Diagram



# Composite T-H Diagram



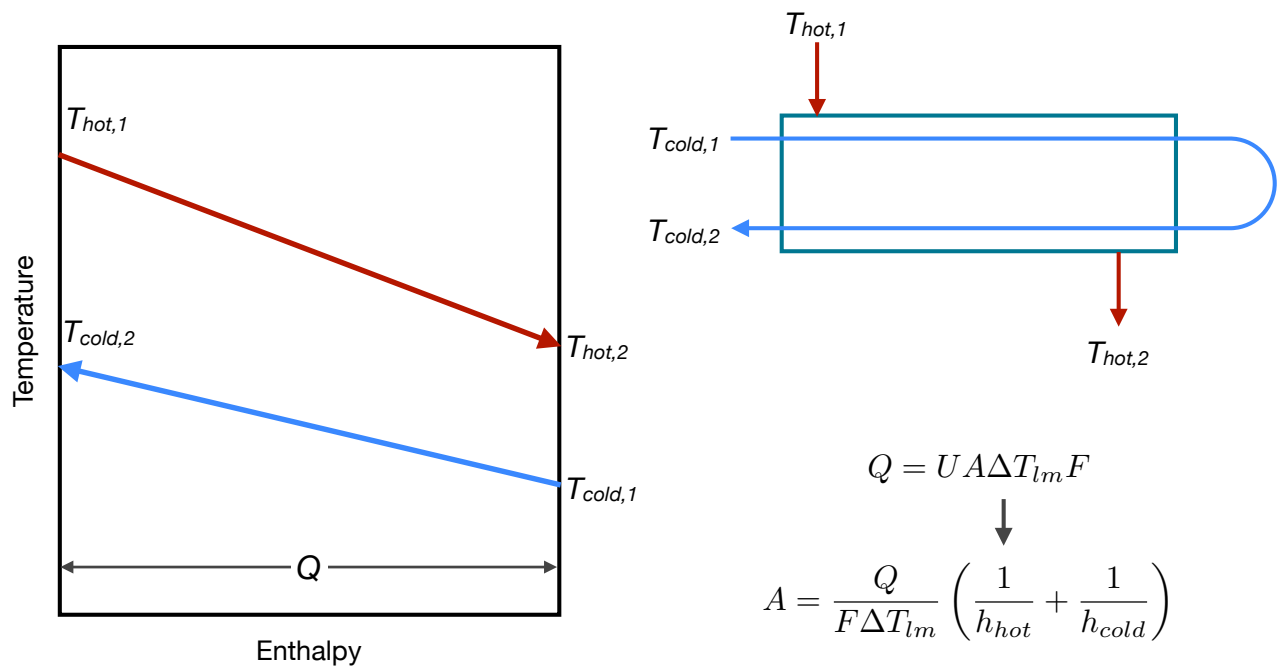
# Systems Without a Pinch



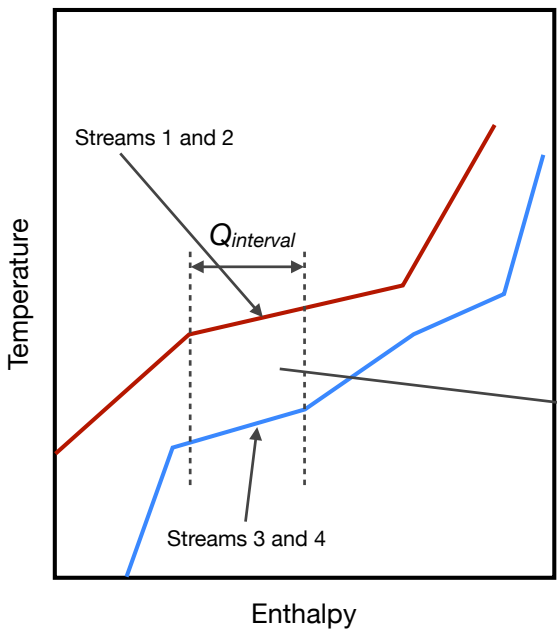
At  $\Delta T_{\min, \text{crit}}$ , the hot utility requirement ( $Q_H$ ) becomes zero and the cold utility requirement becomes a minimum

If  $\Delta T_{\min} < \Delta T_{\min, \text{crit}}$ , heat must be rejected to the cold utility at the high temperature end as well as the low temperature end. However,  $Q_{C, \text{min}}$  remains constant. Hence, below  $T_{\min, \text{crit}}$ , the cold utility duty is constant and the hot utility duty is zero.

# Estimation of Heat-Exchanger Area



# Estimation of Heat-Exchanger Area



$$Q_{interval} = Q_1 + Q_2 = Q_3 + Q_4$$

$$A_{interval} = \frac{1}{F \Delta T_{lm, interval}} \left( \sum_{i=1}^{hot\ streams} \frac{Q_i}{h_i} + \sum_{i=1}^{cold\ streams} \frac{Q_i}{h_i} \right)$$

## Example 15.5

