

**2017 Fall**

# **“Phase Transformation *in* Materials”**

**11.15.2017**

**Eun Soo Park**

**Office: 33-313**

**Telephone: 880-7221**

**Email: [espark@snu.ac.kr](mailto:espark@snu.ac.kr)**

**Office hours: by an appointment**

# Contents in Phase Transformation

Background  
to understand  
phase  
transformation

(Ch1) Thermodynamics and Phase Diagrams

(Ch2) Diffusion: Kinetics

(Ch3) Crystal Interface and Microstructure

Representative  
Phase  
transformation

(Ch4) Solidification: Liquid  $\rightarrow$  Solid

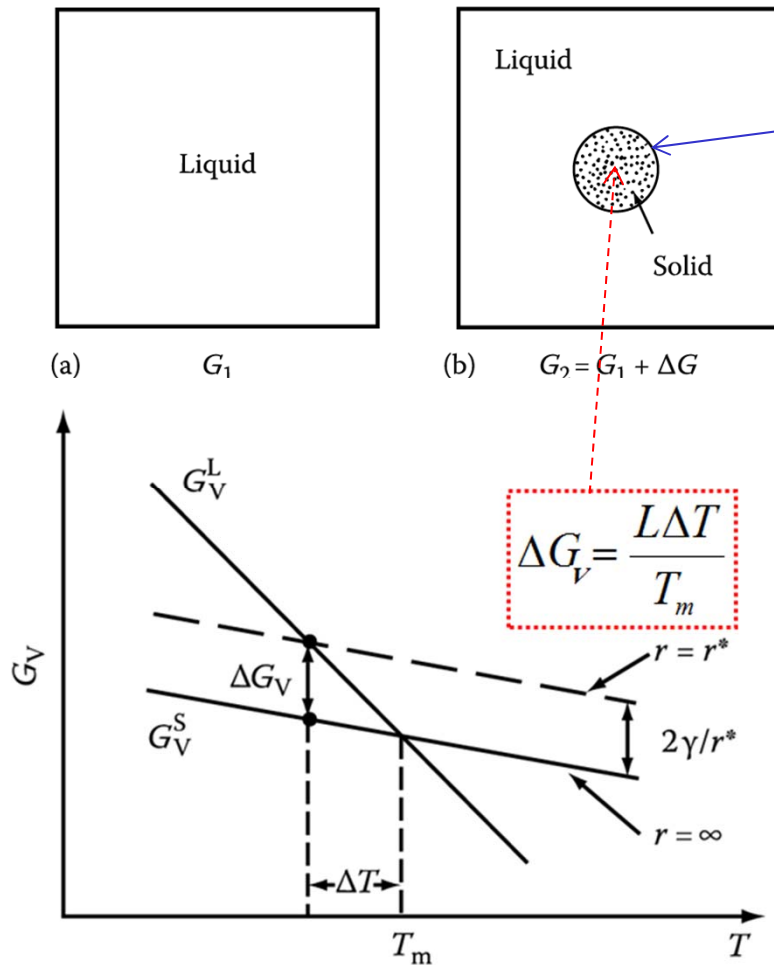
(Ch5) Diffusional Transformations in Solid: Solid  $\rightarrow$  Solid

(Ch6) Diffusionless Transformations: Solid  $\rightarrow$  Solid

# Contents for previous class

## Solidification: Liquid $\longrightarrow$ Solid

- Nucleation in Pure Metals
- Homogeneous Nucleation

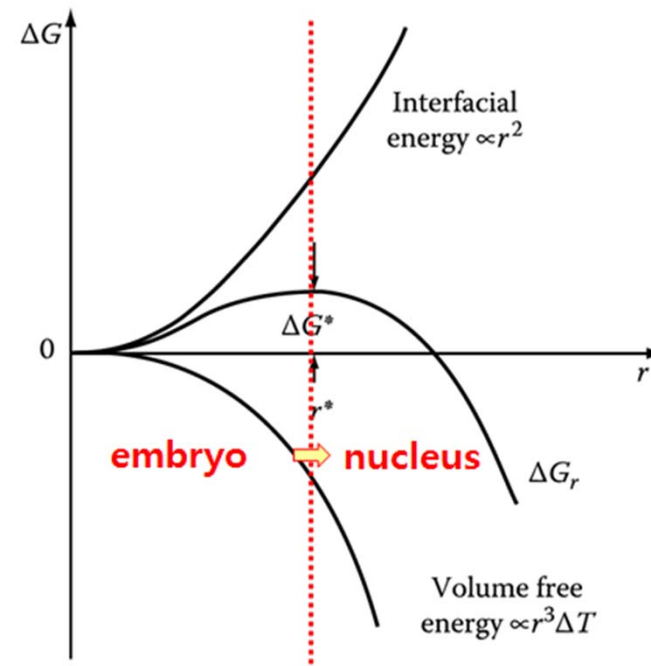


**"Undercooling  $\Delta T$ "**

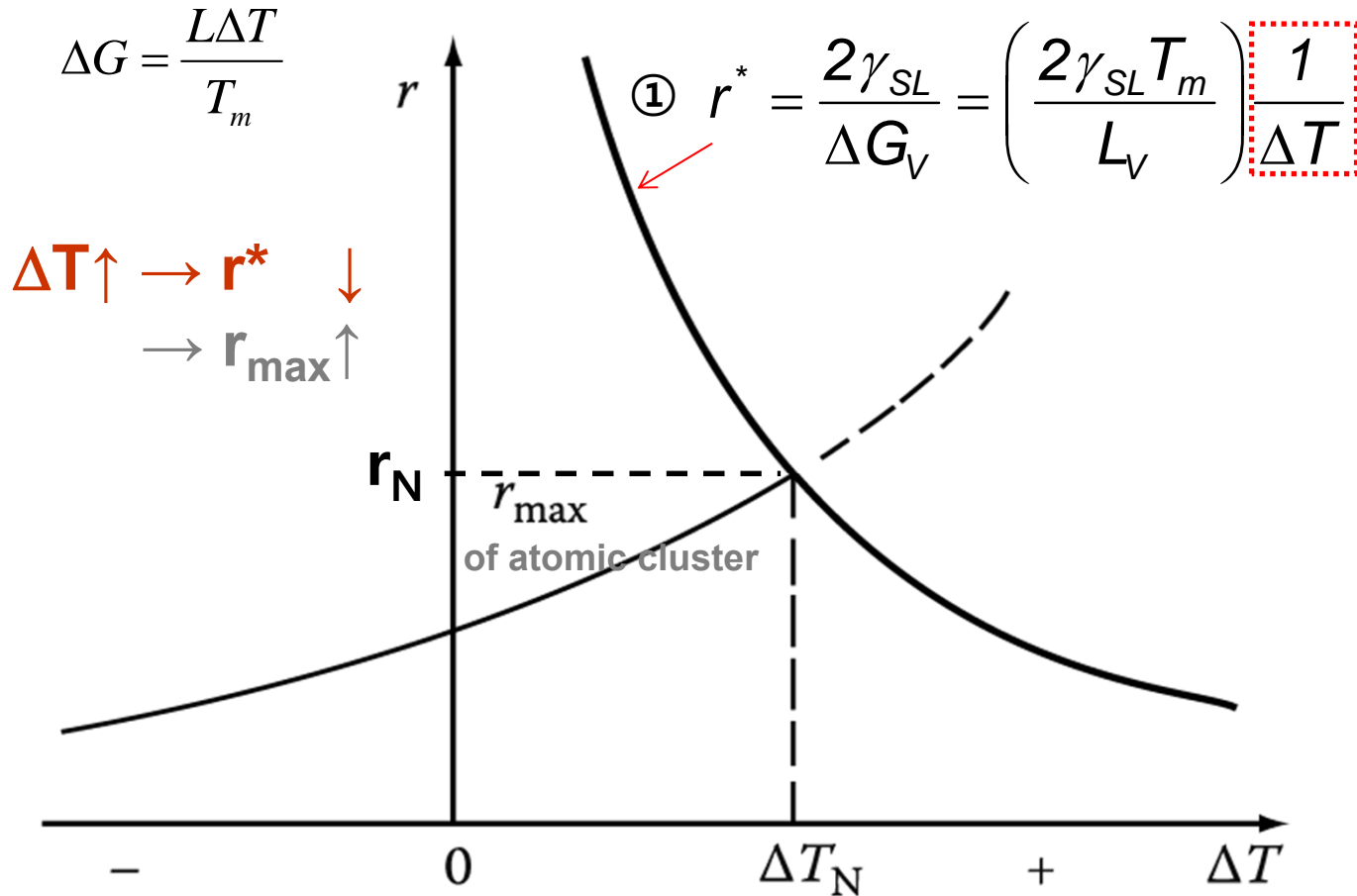
**$r^*$  &  $\Delta G^*$   $\downarrow$  as  $\Delta T$   $\uparrow$**

$$r^* = \frac{2\gamma_{SL}}{\Delta G_V}$$

$$\Delta G^* = \frac{16\pi\gamma_{SL}^3}{3(\Delta G_V)^2} = \left( \frac{16\pi\gamma_{SL}^3 T_m^2}{3L^2} \right) \frac{1}{(\Delta T)^2}$$



## The creation of a critical nucleus ~ thermally activated process



$\Delta T_N$  is **the critical undercooling** for homogeneous nucleation.

Fig. 4.5 The variation of  $r^*$  and  $r_{\max}$  with undercooling  $\Delta T$

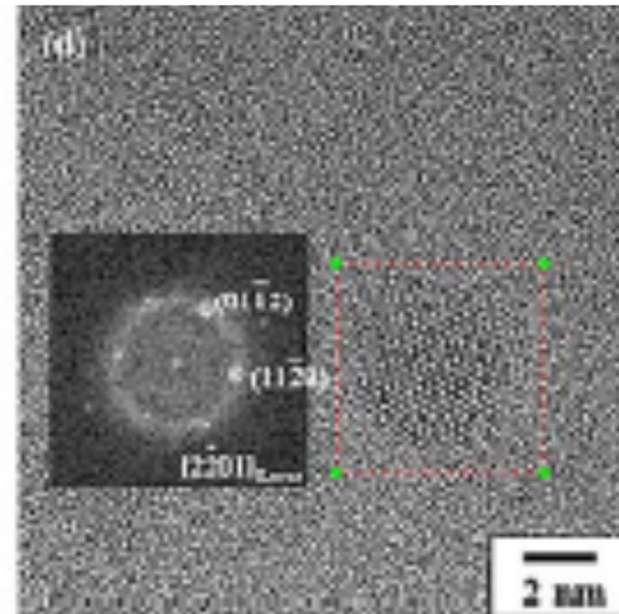
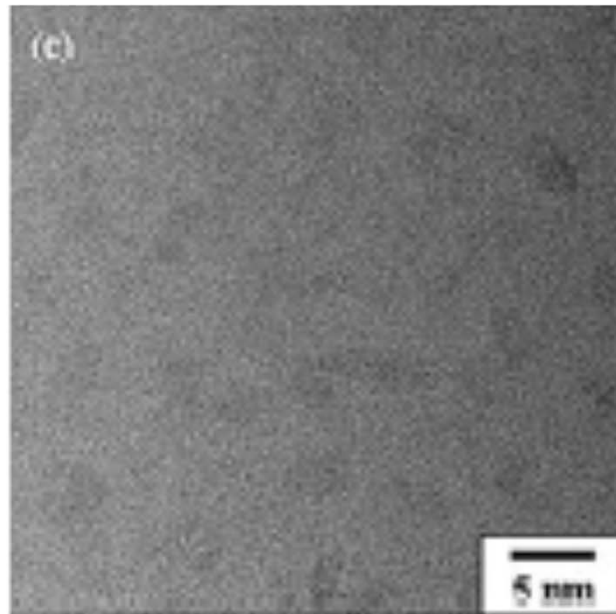
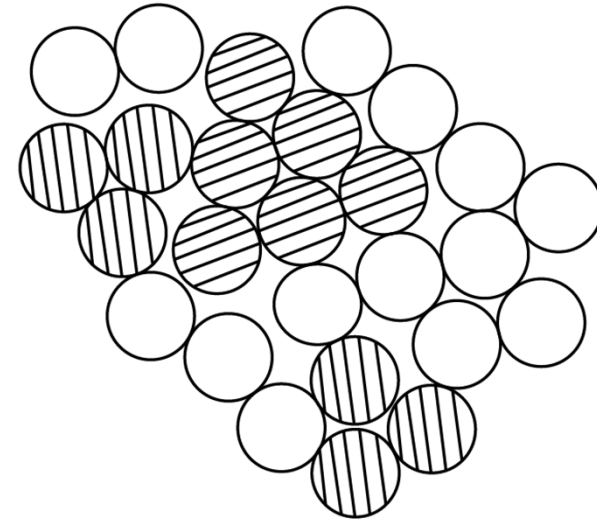
→ Condition for nucleation:

The number of clusters with  $r^*$  at  $T < \Delta T_N$  is negligible.

## ② Formation of Atomic Cluster

At the  $T_m$ , the liquid phase has a volume 2-4% greater than the solid.

**Fig. 4.4** A two-dimensional representation of an instantaneous picture of the liquid structure. Many close-packed crystal-like clusters (shaded) are instantaneously formed.

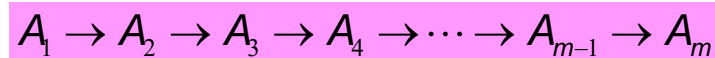


# Formation of Atomic Cluster

When the free energy of the atomic cluster with radius  $r$  is by

$$\Delta G_r = -\frac{4}{3}\pi r^3 \Delta G_V + 4\pi r^2 \gamma_{SL},$$

how many atomic clusters of **radius  $r$**  would exist in the presence of the total number of atoms,  $n_0$ ?



$$n_2 = n_1 \exp\left(-\frac{\Delta G^{1 \rightarrow 2}}{kT}\right) \text{ Excess free E associated with the cluster of } 1 \rightarrow 2 \text{ atoms}$$

$$n_3 = n_2 \exp\left(-\frac{\Delta G^{2 \rightarrow 3}}{kT}\right)$$

$$n_4 = n_3 \exp\left(-\frac{\Delta G^{3 \rightarrow 4}}{kT}\right)$$

$$\vdots$$

$$n_m = n_{m-1} \exp\left(-\frac{\Delta G^{m-1 \rightarrow m}}{kT}\right)$$

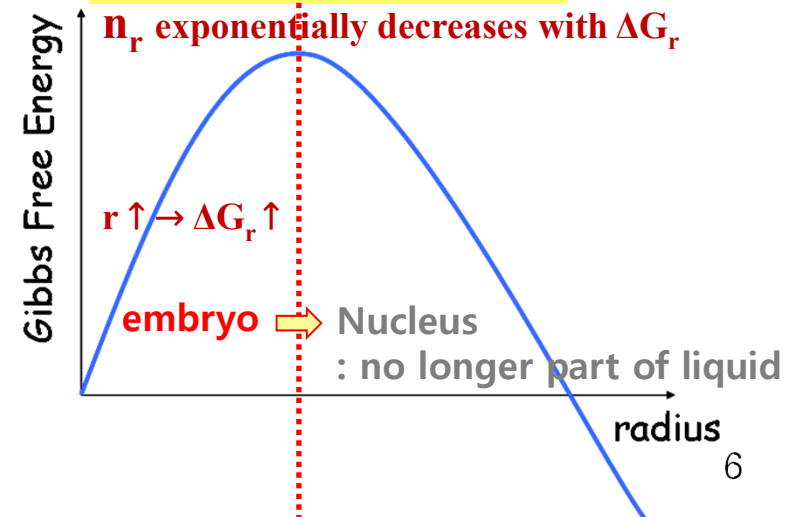
$$n_m = n_1 \exp\left(-\frac{\Delta G^{1 \rightarrow 2} + \Delta G^{2 \rightarrow 3} + \dots + \Delta G^{m-1 \rightarrow m}}{kT}\right)$$

$$n_m = n_1 \exp\left(-\frac{\Delta G^{1 \rightarrow m}}{kT}\right)$$

반지름  $r$ 인 구상의 균집체 수

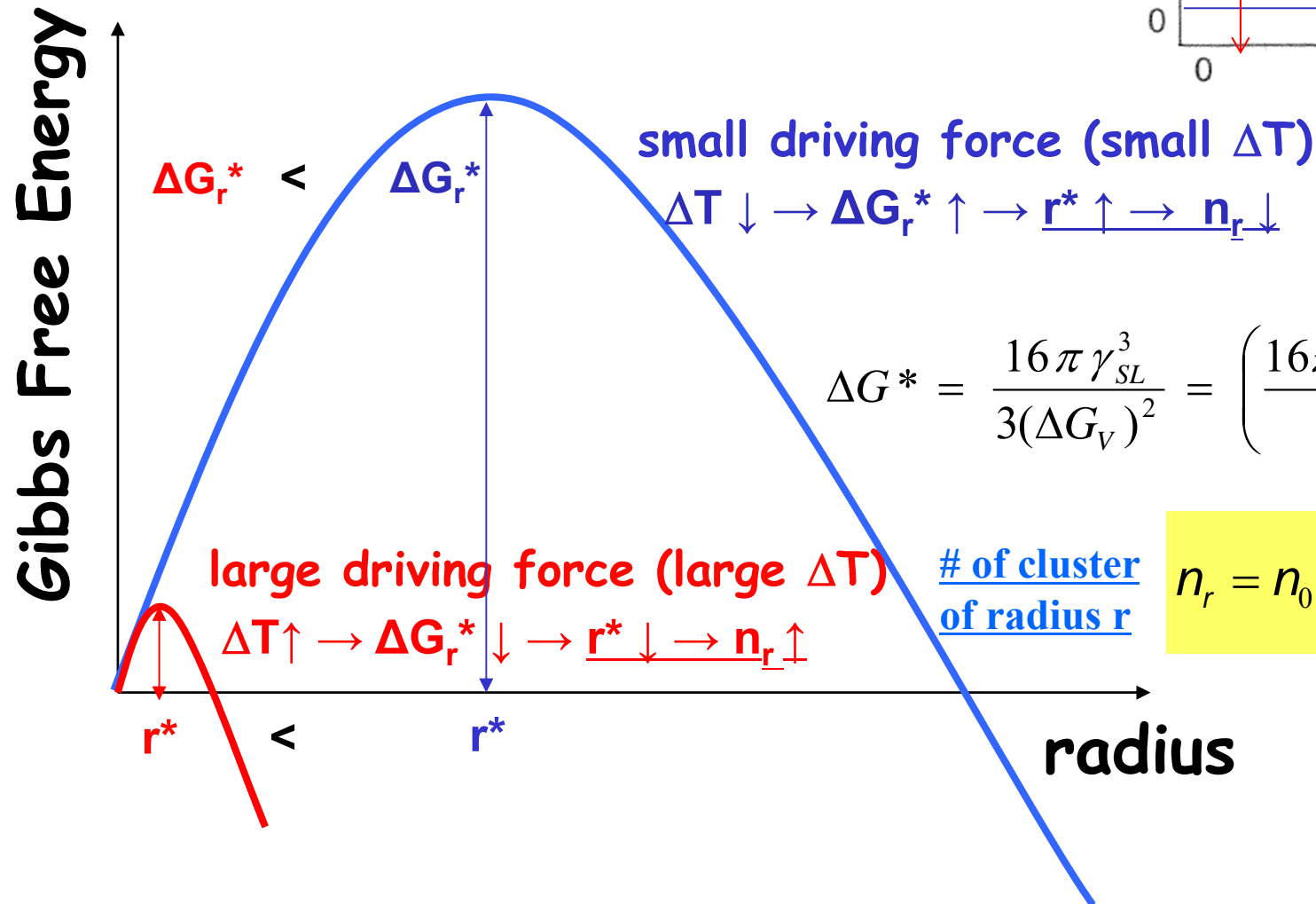
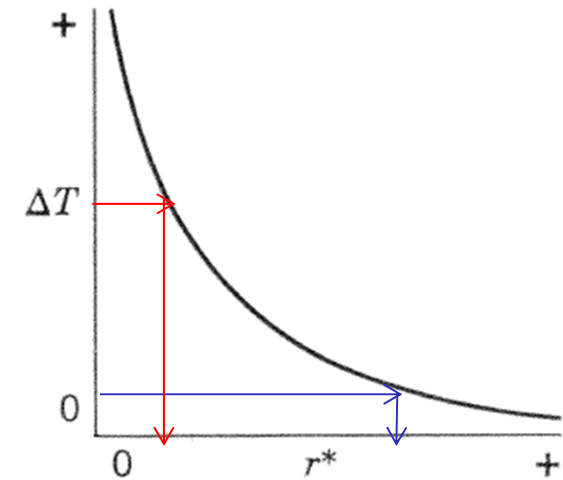
$$n_r = n_0 \exp\left(-\frac{\Delta G_r}{kT}\right)$$

# of cluster of radius  $r$



# Formation of Atomic Cluster

Compare the nucleation curves between small and large driving forces.



$$\Delta G^* = \frac{16\pi\gamma_{SL}^3}{3(\Delta G_V)^2} = \left( \frac{16\pi\gamma_{SL}^3 T_m^2}{3L_V^2} \right) \frac{1}{(\Delta T)^2}$$

$$n_r = n_0 \exp\left(-\frac{\Delta G_r}{kT}\right)$$

# Formation of Atomic Cluster

$n_0$  : total # of atoms.

$\Delta G_r$  : excess free energy associated with the cluster

$k$  : Boltzmann's constant

# of cluster of radius  $r$

$$n_r = n_0 \exp\left(-\frac{\Delta G_r}{kT}\right)$$

- holds for  $T > T_m$  /  $T < T_m$  and  $r \leq r^*$

Apply for all  $r$  /  $r \leq r^*$

( $\because r > r^*$ : no longer part of the liquid)

-  $n_r$  exponentially decreases with  $\Delta G_r$

**Ex. 1 mm<sup>3</sup> of copper at its melting point ( $n_0$ :  $10^{20}$  atoms)**

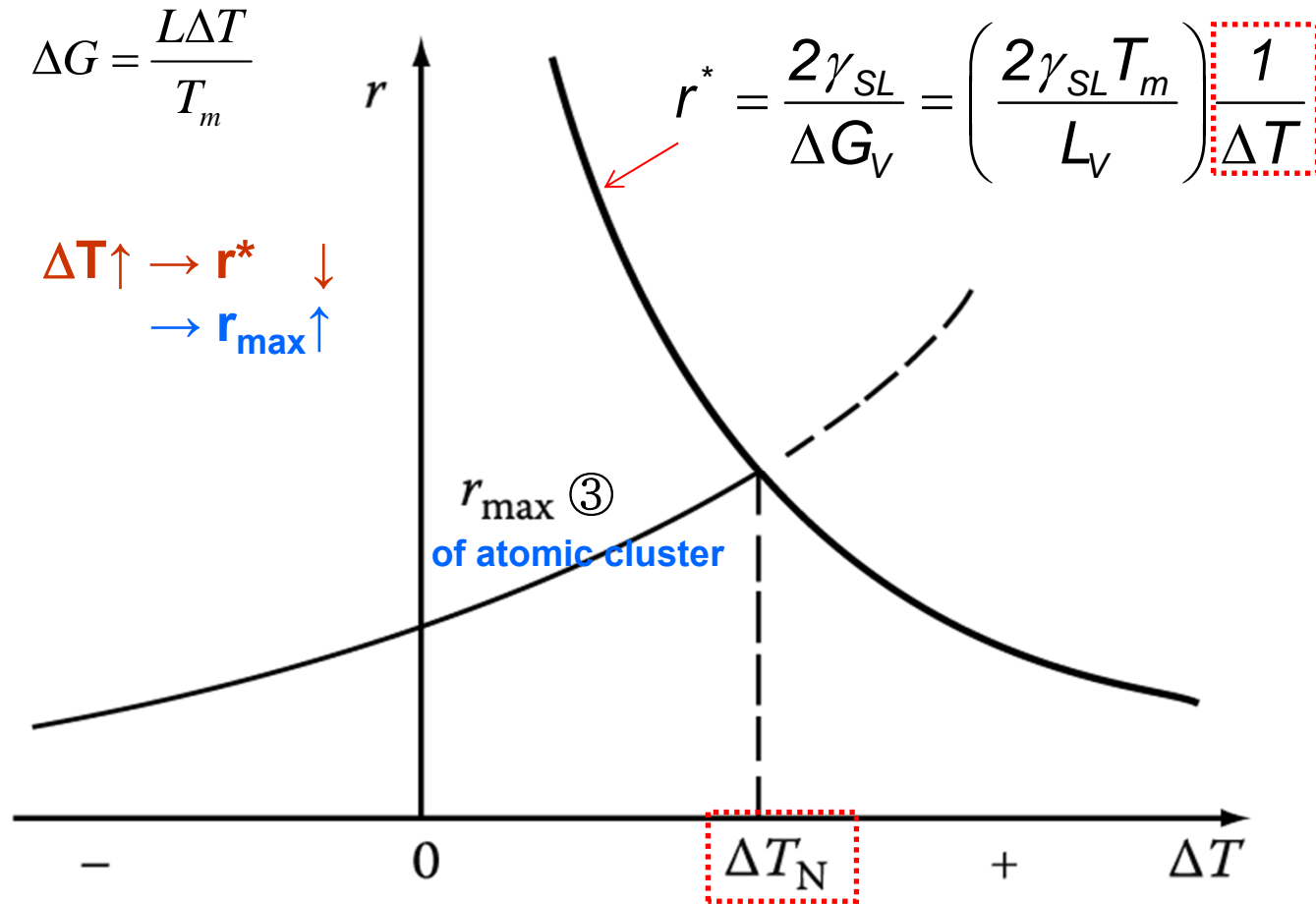
$r \downarrow \rightarrow n_r \uparrow \rightarrow \sim 10^{14}$  clusters of 0.3 nm radius (i.e.  $\sim 10$  atoms)

$r \uparrow \rightarrow n_r \downarrow \rightarrow \sim 10$  clusters of 0.6 nm radius (i.e.  $\sim 60$  atoms)

$\rightarrow$  **effectively a maximum cluster size,  $\sim 100$  atoms**  
 **$\sim 10^{-8}$  clusters mm<sup>-3</sup> or 1 cluster in  $\sim 10^7$  mm<sup>3</sup>**



## The creation of a critical nucleus ~ thermally activated process



$\Delta T_N$  is **the critical undercooling** for homogeneous nucleation.

Fig. 4.5 The variation of  $r^*$  and  $r_{\max}$  with undercooling  $\Delta T$

**The number of clusters with  $r^*$  at  $\Delta T < \Delta T_N$  is negligible.**

## 4.1.2. The homogeneous nucleation rate - kinetics

How fast solid nuclei will appear in the liquid at a given undercooling?

$C_0$  : atoms/unit volume

$C^*$  : # of clusters with size of  $C^*$  ( critical size ) 임계핵 크기의 cluster 수

$$C^* = C_0 \exp\left(-\frac{\Delta G_{\text{hom}}^*}{kT}\right) \text{ clusters / m}^3$$

The addition of one more atom to each of these clusters will convert them into stable nuclei. 한 개 원자 추가로 확산시 핵생성

Homogeneous  
Nucleation rate

$$N_{\text{hom}} = f_0 C_0 \exp\left(-\frac{\Delta G_{\text{hom}}^*}{kT}\right) \text{ nuclei / m}^3 \cdot \text{s}$$

$f_0 \sim 10^{11} \text{ s}^{-1}$ : frequency  $\propto$  vibration frequency energy of diffusion in liquid surface area (const.)

$$\Delta G^* = \left( \frac{16\pi\gamma_{SL}^3 T_m^2}{3L_v^2} \right) \frac{1}{(\Delta T)^2}$$

$C_0 \sim$  typically  $10^{29} \text{ atoms/m}^3$

$$N_{\text{hom}} \approx 1 \text{ cm}^{-3} \text{ s}^{-1} \text{ when } \Delta G^* \sim 78 kT$$

10

Reasonable nucleation rate

## 4.1.2. The homogeneous nucleation rate - kinetics

$$N_{\text{hom}} \approx f_0 C_o \exp\left\{-\frac{A}{(\Delta T)^2}\right\}$$

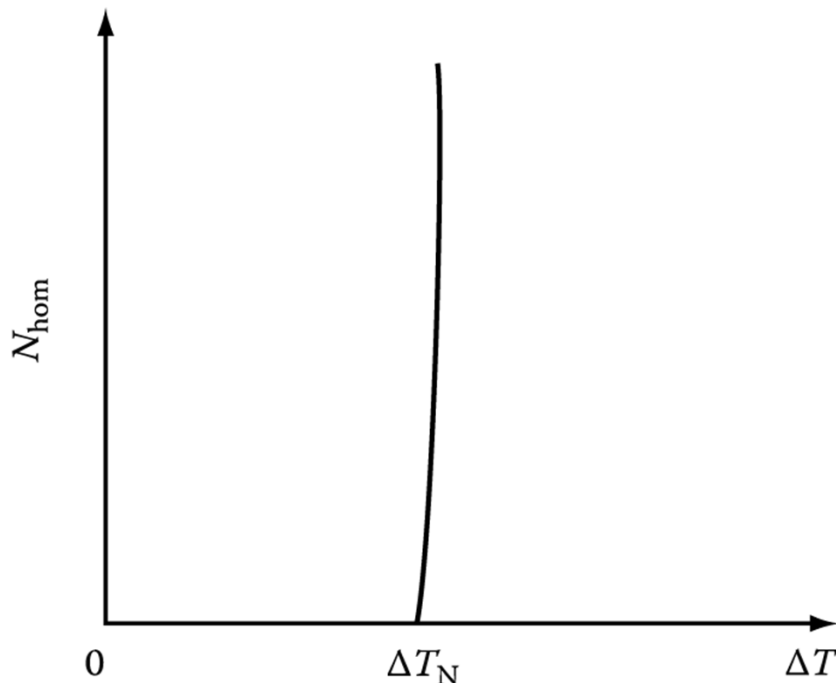
where  $A = \frac{16\pi\gamma_{SL}^3 T_m^2}{3L_v^2 kT}$

A = relatively insensitive to Temp.

How do we define  $\Delta T_N$ ?

$$N_{\text{hom}} \sim \frac{1}{\Delta T^2}$$

Changes by orders of magnitude from essentially zero to very high values over a very narrow temperature range



→ **critical value for detectable nucleation**

- critical supersaturation ratio
- critical driving force
- critical supercooling

→ **for most metals,  $\Delta T_N \sim 0.2 T_m$  (i.e.  $\sim 200\text{K}$ )**

Fig. 4.6 The homogeneous nucleation rate as a function of undercooling  $\Delta T$ .  $\Delta T_N$  is **the critical undercooling** for homogeneous nucleation.

### 4.1.3. Heterogeneous nucleation

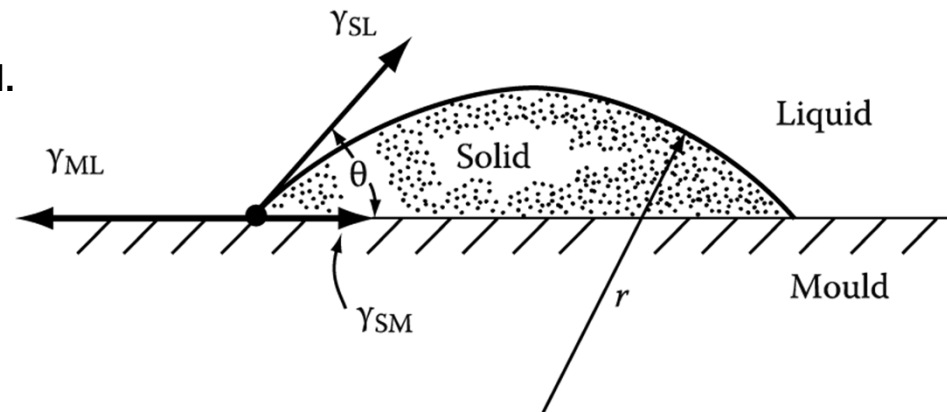
From 
$$\Delta G^* = \left( \frac{16\pi\gamma_{SL}^3 T_m^2}{3L_v^2} \right) \frac{1}{(\Delta T)^2}$$

Nucleation becomes easy if  $\gamma_{SL} \downarrow$  by forming nucleus from mould wall.

Fig. 4.7 Heterogeneous nucleation of spherical cap on a flat mould wall.

$$\gamma_{ML} = \gamma_{SL} \cos \theta + \gamma_{SM}$$

$$\cos \theta = (\gamma_{ML} - \gamma_{SM}) / \gamma_{SL}$$



$$\Delta G_{het} = -V_S \Delta G_V + A_{SL} \gamma_{SL} + A_{SM} \gamma_{SM} - A_{SM} \gamma_{ML}$$

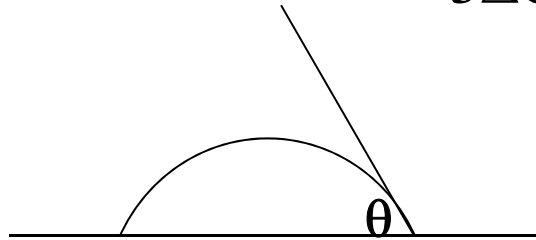
In terms of the wetting angle ( $\theta$ ) and the cap radius ( $r$ ) (Exercies 4.6)

$$\Delta G_{het} = \left\{ -\frac{4}{3} \pi r^3 \Delta G_V + 4\pi r^2 \gamma_{SL} \right\} S(\theta)$$

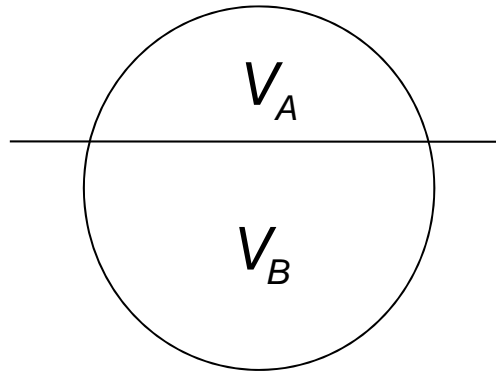
where  $S(\theta) = (2 + \cos \theta)(1 - \cos \theta)^2 / 4$

# Barrier of Heterogeneous Nucleation

$$\Delta G^* = \frac{16\pi\gamma_{SL}^3}{3\Delta G_V^2} \cdot S(\theta) = \frac{16\pi\gamma_{SL}^3}{3\Delta G_V^2} \cdot \frac{(2 - 3\cos\theta + \cos^3\theta)}{4}$$



$$\Delta G_{het}^* = S(\theta)\Delta G_{hom}^*$$



$$\Delta G_{sub}^* = \Delta G_{homo}^* \left( \frac{2 - 3\cos\theta + \cos^3\theta}{4} \right)$$

$$\frac{V_A}{V_A + V_B} = \frac{2 - 3\cos\theta + \cos^3\theta}{4} = S(\theta)$$

How about the nucleation at the crevice or at the edge?

## Contents for today's class

### Solidification: Liquid $\longrightarrow$ Solid

- Nucleation in Pure Metals
- Homogeneous Nucleation

$$r^* = \frac{2\gamma_{SL}}{\Delta G_V} \quad \Delta G^* = \frac{16\pi\gamma_{SL}^3}{3(\Delta G_V)^2} = \left( \frac{16\pi\gamma_{SL}^3 T_m^2}{3L_V^2} \right) \frac{1}{(\Delta T)^2}$$

$r^*$  &  $\Delta G^*$   $\downarrow$  as  $\Delta T$   $\uparrow$

$$N_{\text{hom}} \approx f_0 C_0 \exp\left\{-\frac{A}{(\Delta T)^2}\right\} \sim \frac{1}{\Delta T^2}$$

- Heterogeneous Nucleation

$$\Delta G_{\text{het}}^* = S(\theta)\Delta G_{\text{hom}}^*$$

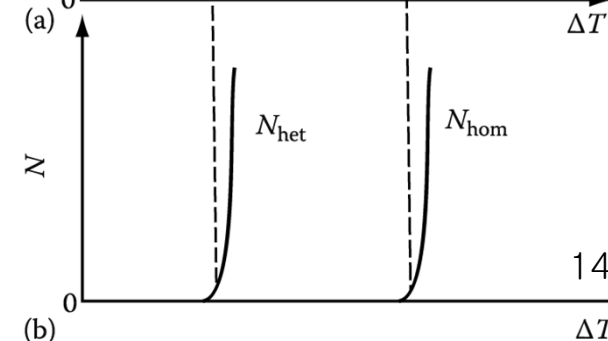
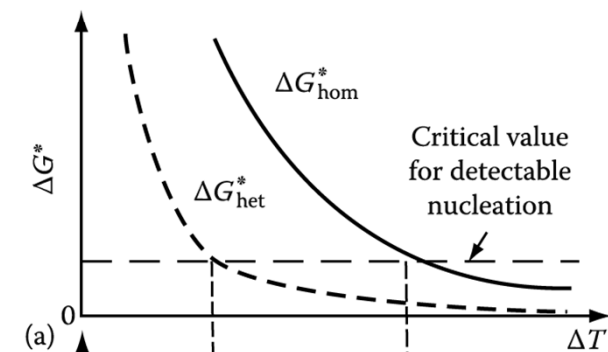
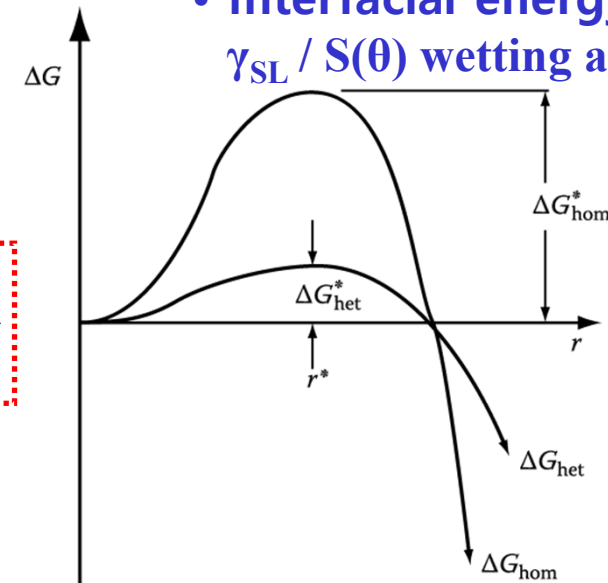
$$\frac{V_A}{V_A + V_B} = \frac{2 - 3\cos\theta + \cos^3\theta}{4} = S(\theta)$$

- Nucleation of melting

$$\gamma_{SL} + \gamma_{LV} < \gamma_{SV} \quad (\text{commonly})$$

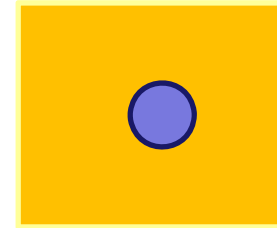
- Undercooling  $\Delta T$

- Interfacial energy  $\gamma_{SL}$  /  $S(\theta)$  wetting angle



# Melting and Crystallization are Thermodynamic Transitions

**Solidification:** Liquid  $\rightarrow$  Solid



<Thermodynamic>

• Interfacial energy  $\Rightarrow \Delta T_N$

Liquid

$T_m$

Undercooled Liquid

Solid

No superheating required!

• Interfacial energy  $\Rightarrow$  No  $\Delta T_N$

$$\gamma_{SL} + \gamma_{LV} < \gamma_{SV}$$

vapor



**Melting:** Liquid  $\leftarrow$  Solid

## Contents for today's class

# Solidification: Liquid $\longrightarrow$ Solid

< Nucleation >  
&

< Growth >

- Nucleation in Pure Metals

- Equilibrium Shape and Interface Structure on an Atomic Scale

- Growth of a pure solid

1) Continuous growth

: Atomically rough or diffuse interface

2) Lateral growth

: Atomically flat or sharply defined interface

- Heat Flow and Interface Stability

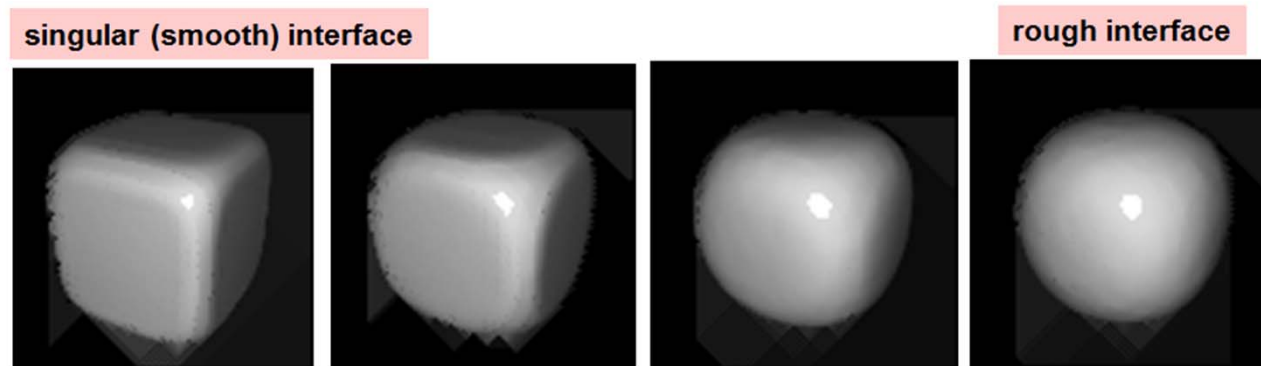
## 4.3 Alloy solidification

- Solidification of single-phase alloys
- Eutectic solidification
- Off-eutectic alloys
- Peritectic solidification



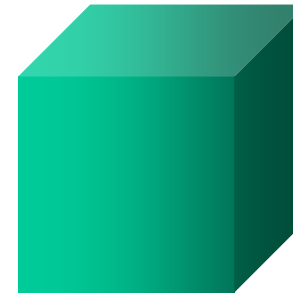
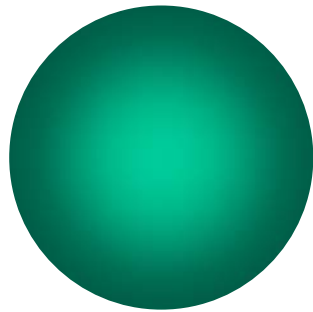
# Q: Rough interface vs Singular interface?

## Thermal Roughening



Heating up to the roughening transition.

# Equilibrium Shape and Interface Structure on an Atomic Scale



How do you like to call them?

**rough interface**

**singular (smooth) interface**

What about the dependence of surface energy on crystal directions?

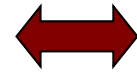
**isotropic  $\gamma$**

**anisotropic  $\gamma$**

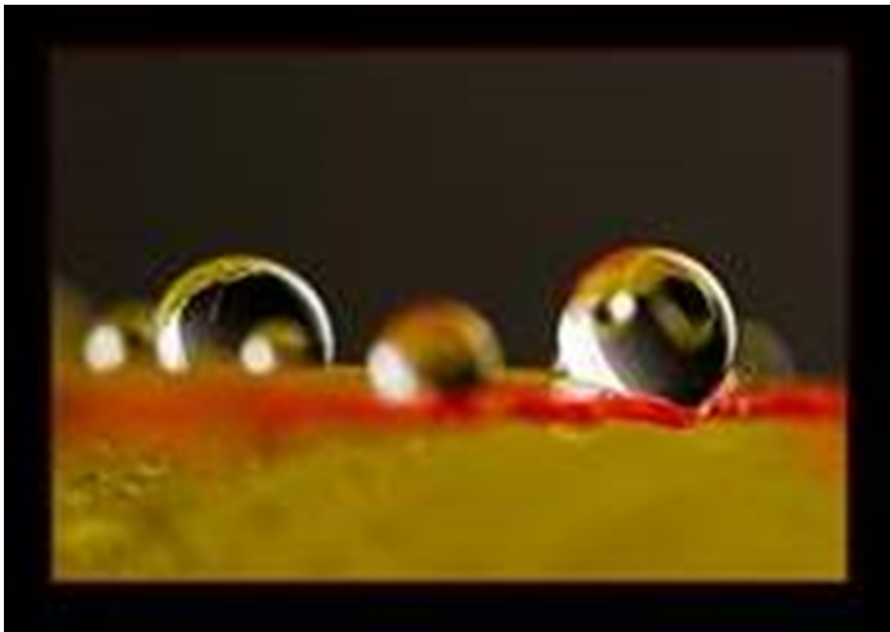
Do not vary with crystallographic orientation,  
i.e,  $\gamma$ -plots are spherical

Strong crystallographic effects,  
: solidify with low-index close-packed facets

**Water Drops**



**Natural Minerals**

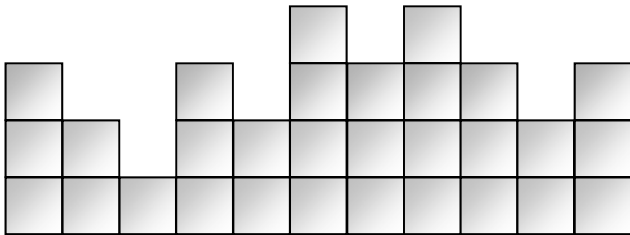
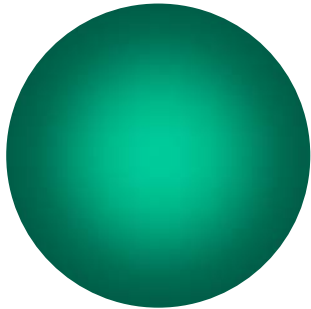


**Topaz (황옥)**

**Stibnite (휘안광)**

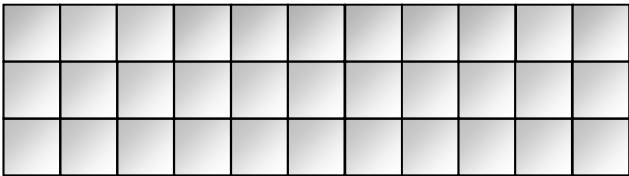
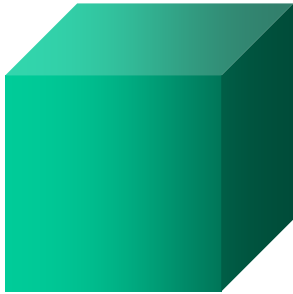
**How differ the structure of the surface on an atomic scale?**

# Equilibrium Shape and Interface Structure on an Atomic Scale



**atomically-disordered**

Ex) metallic systems



**atomically-flat**

nonmetals

Apply thermodynamics to this fact and derive more information.

**Entropy-dominant**

**weak bonding energy**

**stable at high T**

**Enthalpy-dominant**

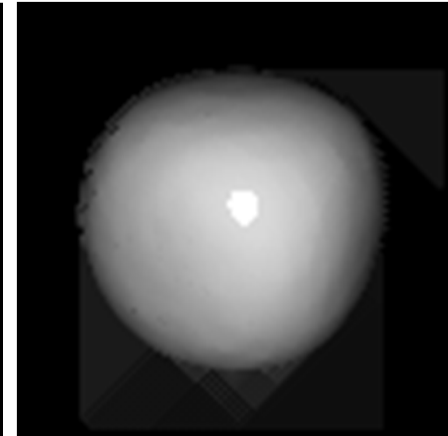
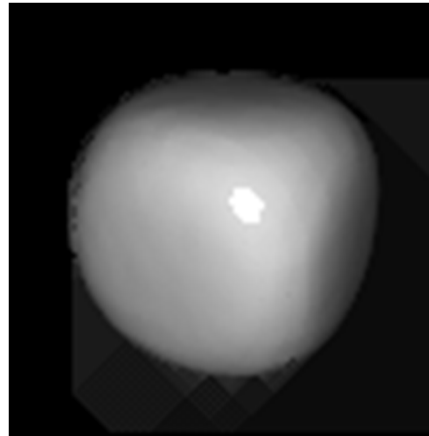
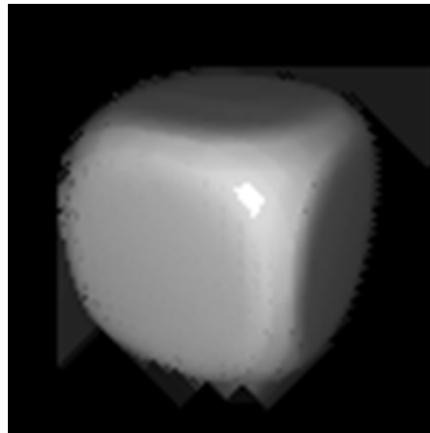
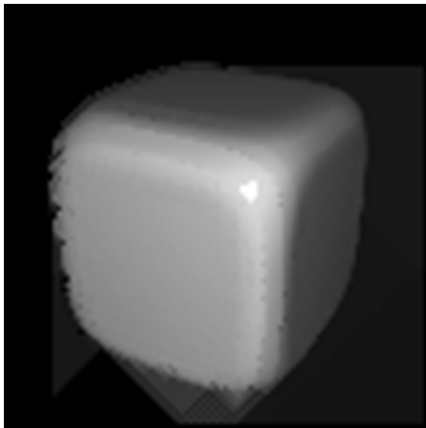
**strong bonding energy**

**stable at low T**



# Thermal Roughening

singular (smooth) interface



rough interface

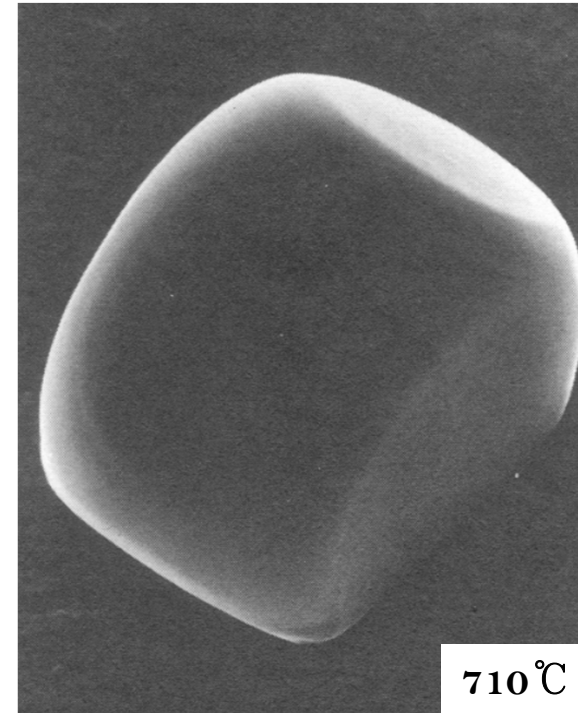
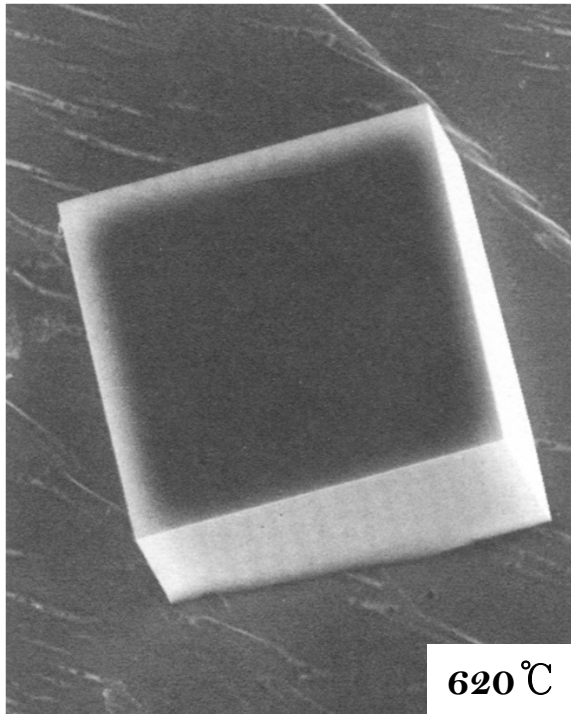
Enthalpy-dominant

Entropy-dominant

Heating up to the roughening transition.

## ✓ Equilibrium shape of NaCl crystal

### Thermal Roughening



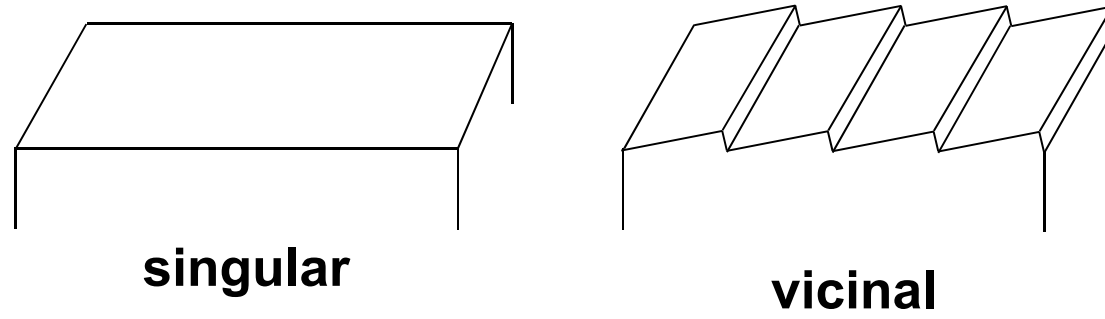
J.C. Heyraud, J.J. Metois, J. Crystal Growth , 84, 503 (1987)

**Compare the kinetic barrier for atomic attachment.**

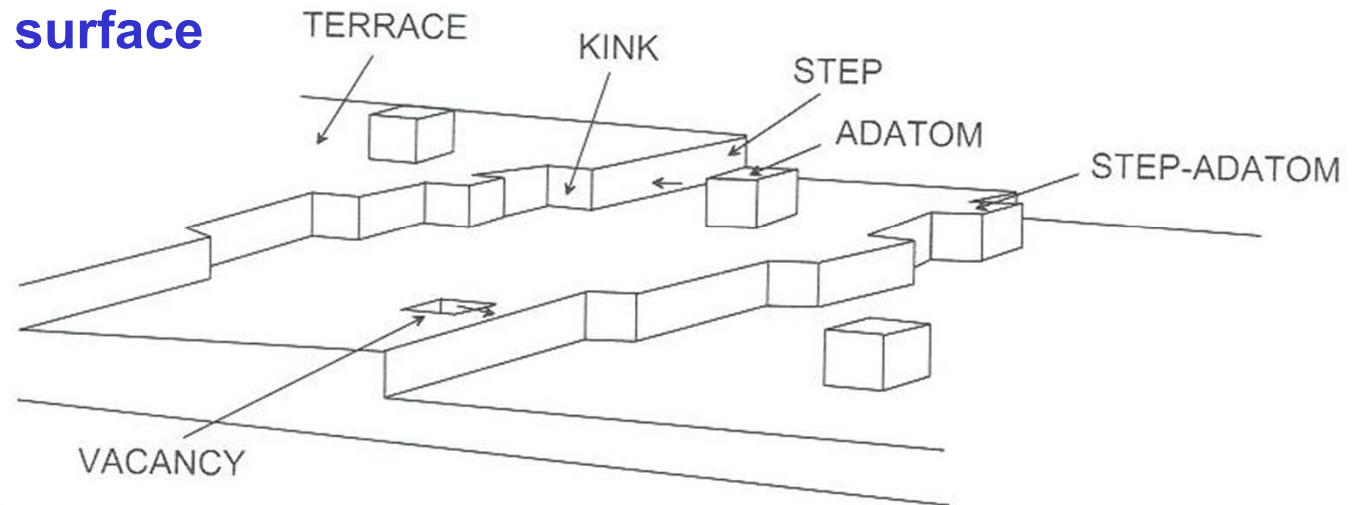
**Which has a low growth barrier?**

# Atomic View

## Ideal Surfaces



## More realistic surface



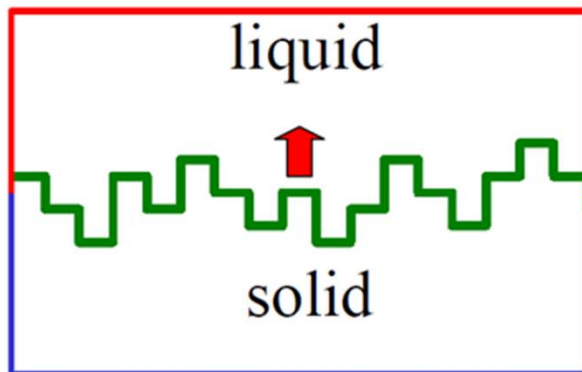
- Realistic surfaces of crystals typically look like this at low temperature
- At sufficiently high temperature, the structure becomes atomically rough (Thermal Roughening)

# Q: What kinds of Growth in a pure solid exist?

## Two types of solid-liquid interface

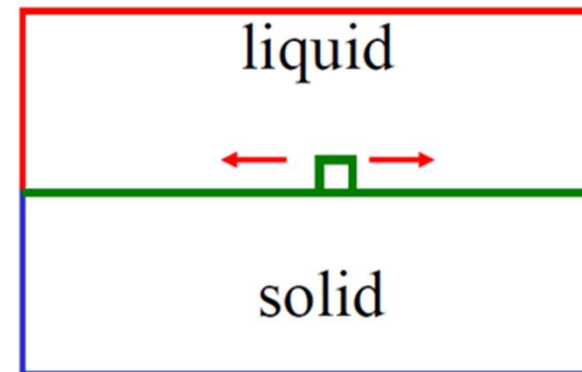
### a) Continuous growth

: Atomically rough or diffuse interface



### b) Lateral growth

: Atomically flat or sharply defined interface





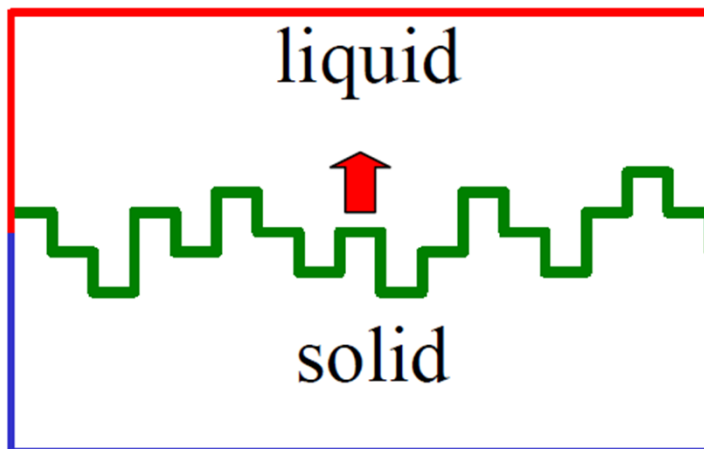
## 4.2. Growth of a pure solid

: The next step after the nucleation is growth.

### Two types of solid-liquid interface

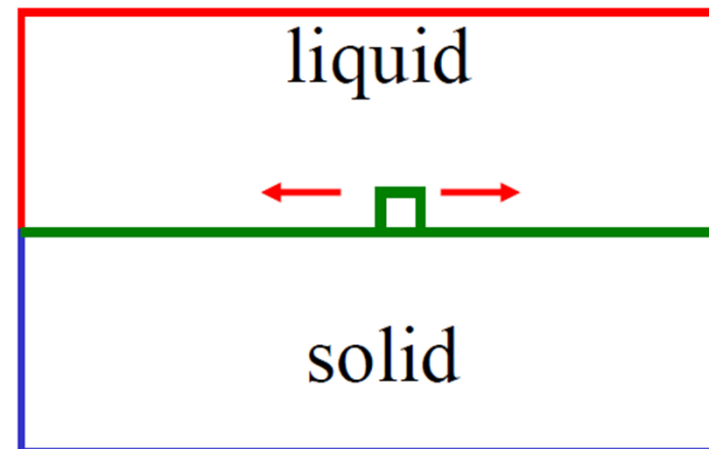
#### a) Continuous growth

: Atomically rough or diffuse interface



#### b) Lateral growth

: Atomically flat or sharply defined interface



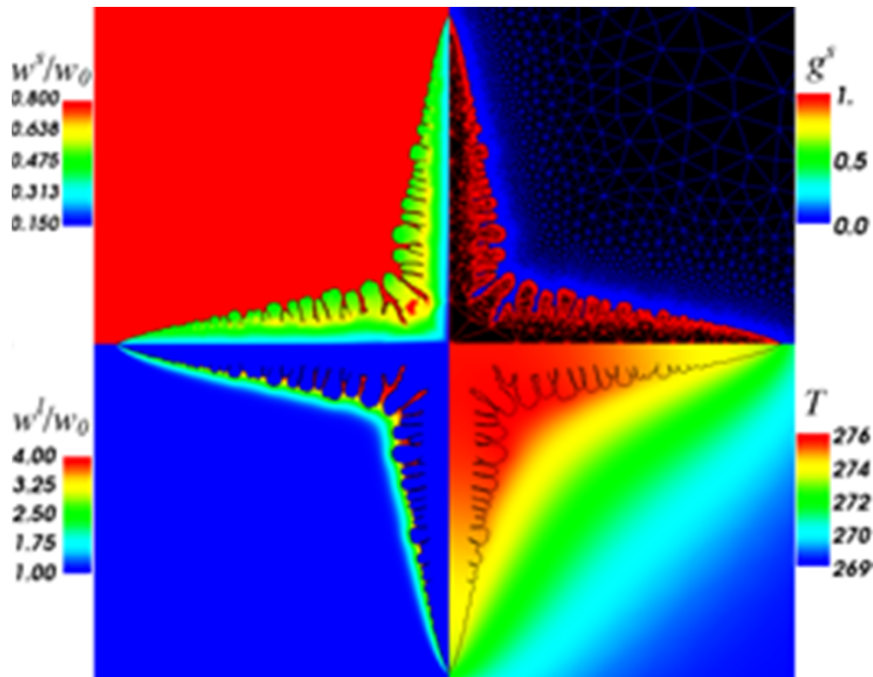
## 4.2. Growth of a pure solid

: The next step after the nucleation is growth.

### Two types of solid-liquid interface

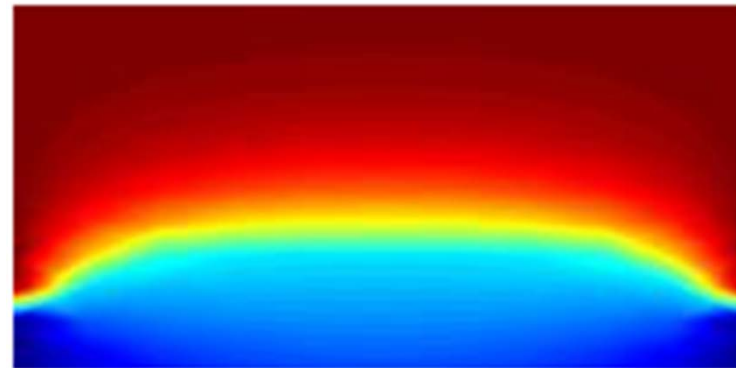
#### a) Continuous growth

: Atomically rough or diffuse interface



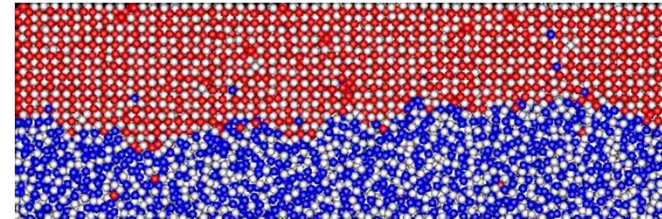
#### b) Lateral growth

: Atomically flat or sharply defined interface



## a) Continuous growth

The migration of a rough solid/liquid interface can be treated in a similar way to the migration of a random high angle grain boundary.

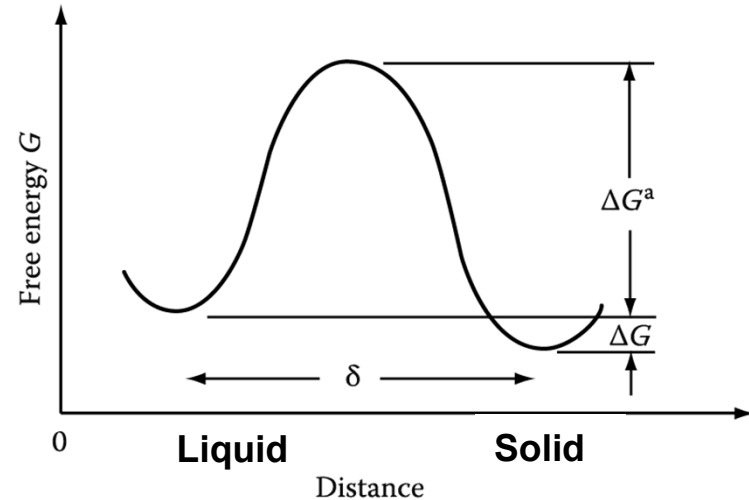


### - Driving force for solidification\_

$$\Delta G = \frac{L}{T_m} \Delta T_i$$

$L$ : latent heat of melting

$\Delta T_i$ : undercooling of the interface



### - Net rate of solidification\_

$$v = k_I \Delta T_i$$

$k_I$ : properties of boundary mobility

Reference (eq. 3.21)  $v = M \cdot \Delta G / V_m$

The rate of the continuous growth (typical for metals) is usually a “diffusion controlled process”.

- ┌ Pure metal grow at a rate controlled by heat transfer to the interfacial region.
- └ Alloy grow at a rate controlled by solute diffusion.

## b) Lateral growth

- Materials with a high entropy of melting ( $\sim$ high  $T_m$ ) prefer to form atomically smooth, closed-packed interfaces.
- For this type of interface the minimum free energy also corresponds to the minimum internal energy, i.e. a minimum number of broken 'solid' bonds.

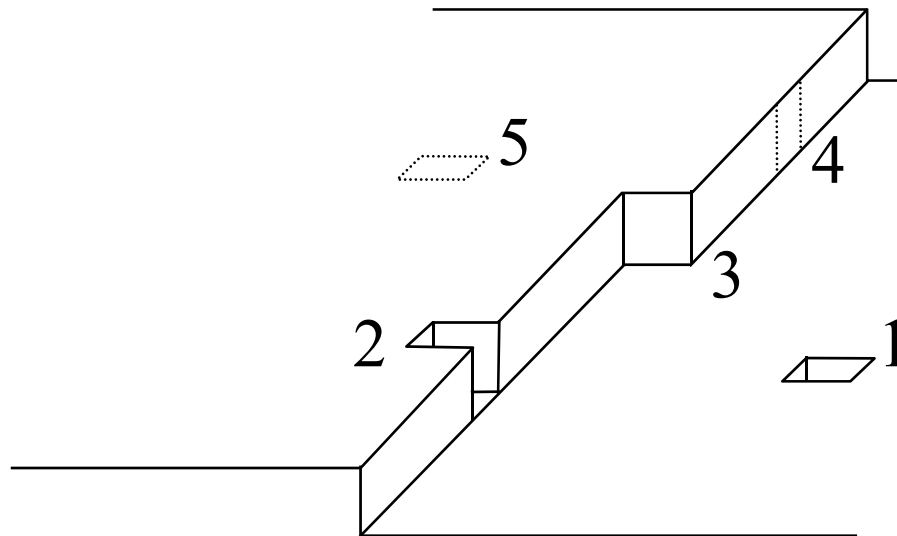
Two ways in which ledges and jogs (kinks) can be provided.

① Surface (2-D) nucleation

② Spiral growth


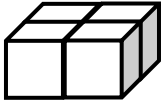
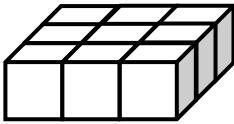
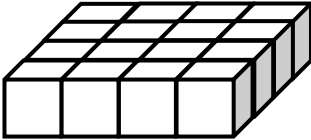
### Condition for Atomic Attachment

Suppose the building unit (atom) has 6 bonds to be saturated

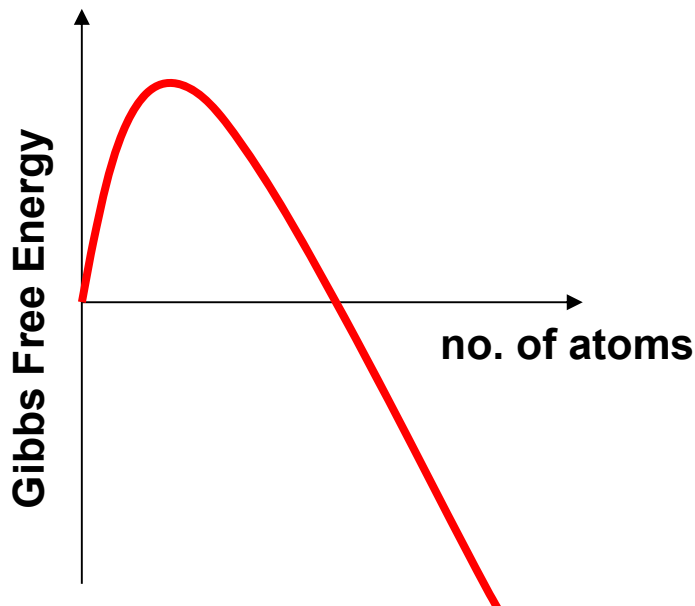


site	$\Delta E / atom$	
1	$-4\phi$	<i>stable</i>
2	$-2\phi$	<i>stable</i>
3	$0\phi$	<i>stable</i> : kink
4	$+2\phi$	<i>unstable</i>
5	$+4\phi$	<i>unstable</i>

How many unsaturated bonds are there if they are epitaxial to the underneath atomic layer?

				...
$+4\phi / atom$	$+8\phi / 4 atoms$	$+12\phi / 9 atoms$	$+16\phi / 16 atoms$	
$\Delta f = -kT \ln(P/P_e)$	$4\Delta f$	$9\Delta f$	$16\Delta f$	
$+4\phi / atom$	$+2\phi / atom$	$+\frac{4}{3}\phi / atom$	$+1\phi / atom$	
$\Delta E/atom$	$\Delta E/atom$	$\Delta E/atom$	$\Delta E/atom$	

Draw the plot showing how the free energy varies with the number of atoms in the presence of supersaturation (driving force) for growth.



→ 2-Dimensional Nucleation ①

- If large # of atoms form a disc-shaped layer,  
→ self-stabilized and continue to grow.

-  $\Delta T$  becomes large,  $r^* \downarrow$ .

-  $v \propto \exp(-k_2/\Delta T_i)$

## ② Spiral growth: Growth by Screw Dislocation

Crystals grown with a low supersaturation were always found to have a '**growth spirals**' on the growing surfaces.

- addition of atoms to the ledge cause it to rotate around the axis of screw dislocation
- If atoms add at an equal rate to all points along the step, the angular velocity of the step will be **initially greatest nearest to the dislocation core.**
- the spiral tightens until it reaches a minimum radius of  $r^*$

$$v = k_3(\Delta T_i)^2$$

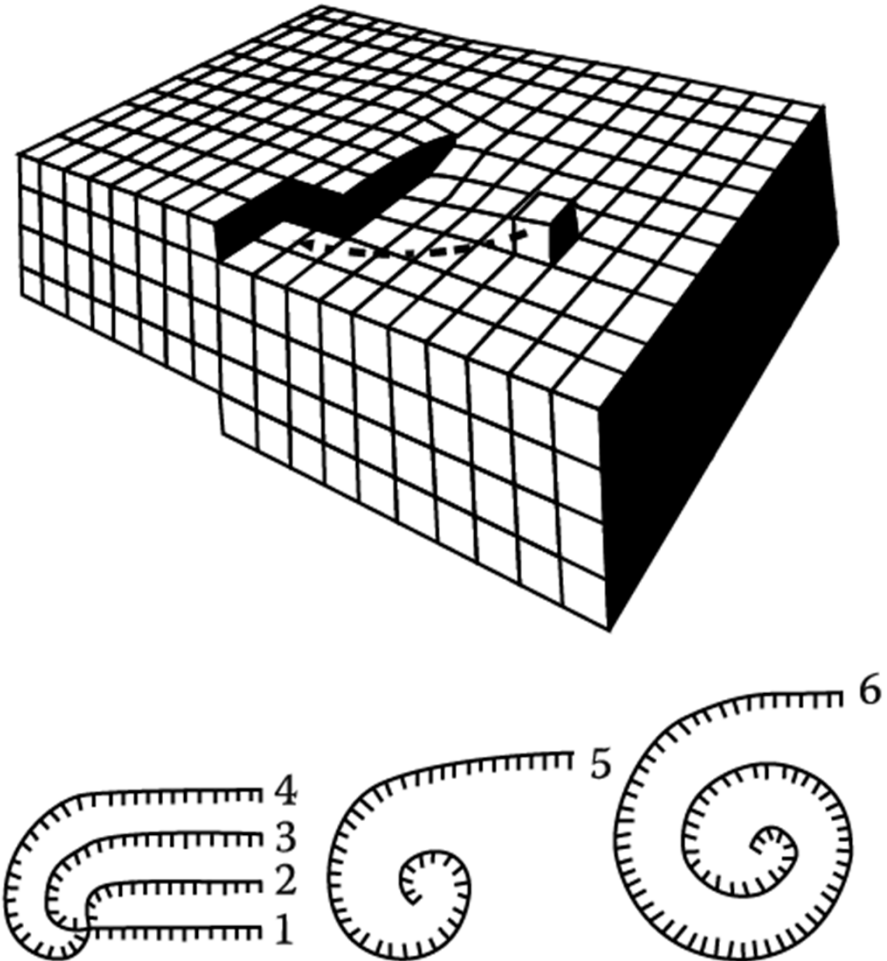
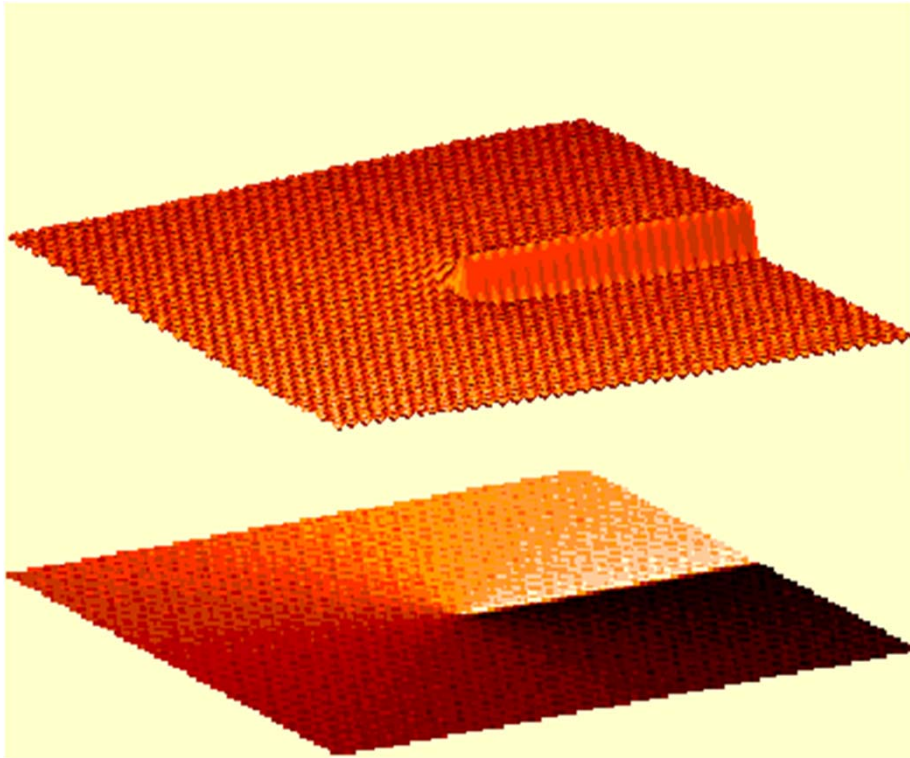


Fig. 4. 13 Spiral growth. (a) A screw dislocation terminating in the solid/liquid interface showing the associated ledge. Addition of atoms at the ledge causes it to rotate with an angular velocity decreasing away from the dislocation core so that a growth spiral develops as shown in (b).

## Growth by Screw Dislocation



Burton, Cabrera and Frank (BCF, 1948) elaborated the spiral growth mechanism, assuming **steps are atomically disordered...**

Their interpretation successfully explained the growth velocity of crystals as long as the assumption is valid...

- ③ **Growth from twin boundary** → “feather crystal” under small  $\Delta T$ 
  - another permanent source of steps like spiral growth
  - not monoatomic height ledge but macro ledge

# Kinetic Roughening

Rough interface - Ideal Growth → diffusion-controlled → dendritic growth

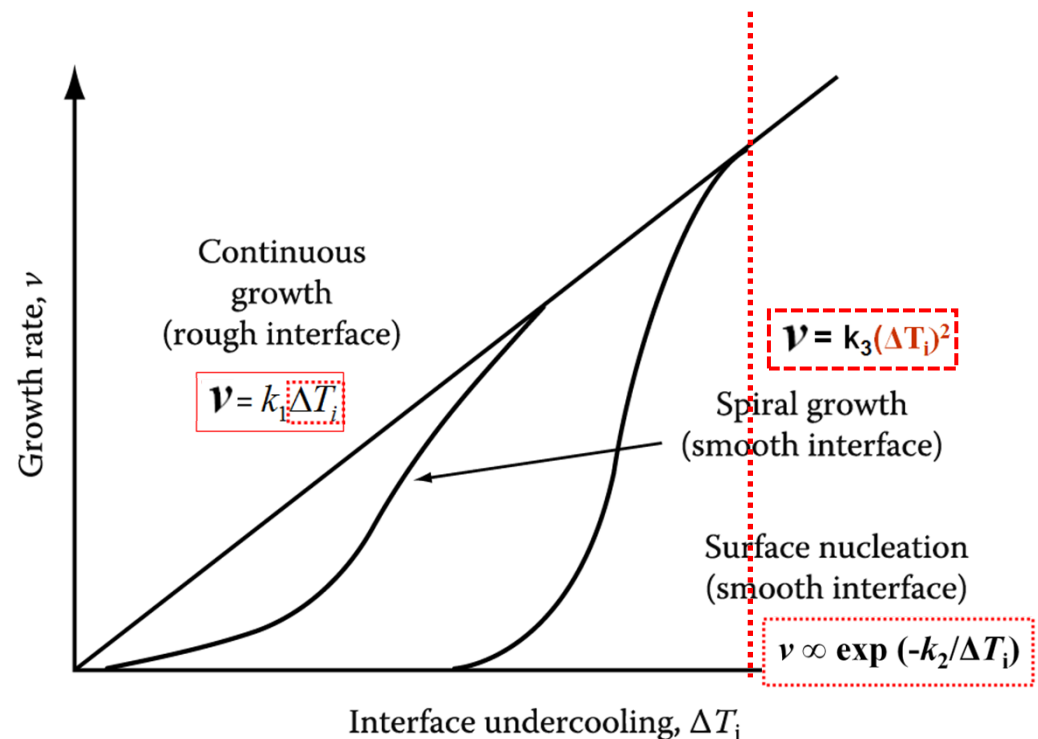
Smooth interface - **Growth by Screw Dislocation**  
**Growth by 2-D Nucleation**

Small  $\Delta T$  → “feather” type of growth ↔ Large  $\Delta T$  → cellular/dendritic growth

The growth rate of the singular interface cannot be higher than ideal growth rate.

When the growth rate of the singular interface is high enough, it follows the ideal growth rate like a rough interface.

→ kinetic roughening





# Q: Heat Flow and Interface Stability

## 1) Superheated liquid

: Extraction of latent heat by conduction in the crystal

## 2) Supercooled liquid

: conduction of latent heat into the liquid

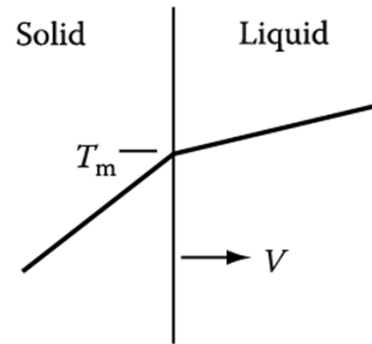
→ **Development of Thermal Dendrite**

## 4.2.3 Heat Flow and Interface Stability - Planar interface

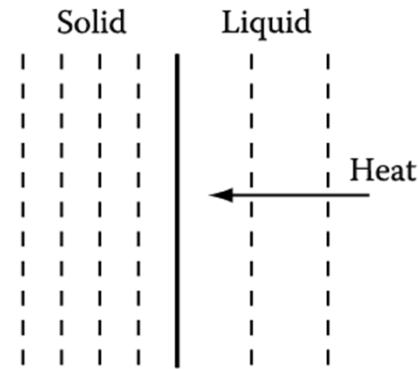
### 1) Superheated liquid

Consider the solidification front with heat flow from L to S.

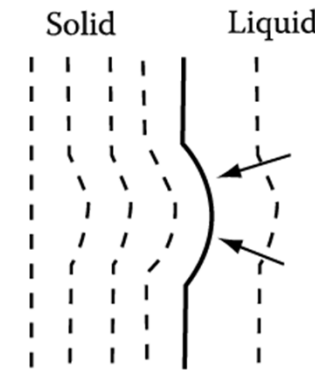
solid growing at  $v$   
(planar)



(a)



(b)



(c)

Heat flow away from the interface  
through the solid

$$K_S T'_S$$



$$K_L T'_L$$

- Heat flow from the liquid

$$vL_V$$

- Latent heat generated at the interface

Heat Balance Equation

$$K_S T'_S = K_L T'_L + vL_V$$

K: thermal conductivity

If  $r$  is so large  $\rightarrow$  Gibbs-Thompson effect can be ignored the solid/liquid interface remain at  $T_m$   
(  $r$  : radius of curvature of the protrusion )

$dT/dx$  in the liquid ahead of the protrusion will increase more positively.  $T'_L \uparrow$  &  $T'_S \downarrow$

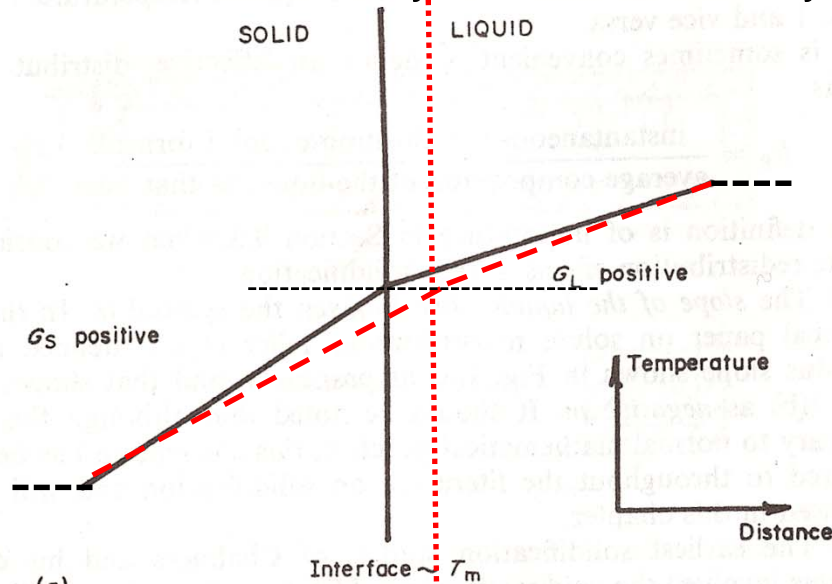
More heat to the protrusion  $\rightarrow$  melt away

$v$  of protrusion  $\downarrow$  to match other  $v$  in planar region

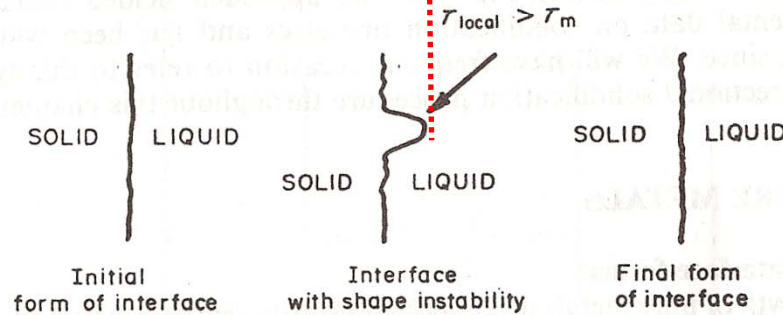
# “Removal of latent heat” → Heat Flow and Interface Stability

## 1) Superheated liquid

: Extraction of latent heat by conduction in the crystal

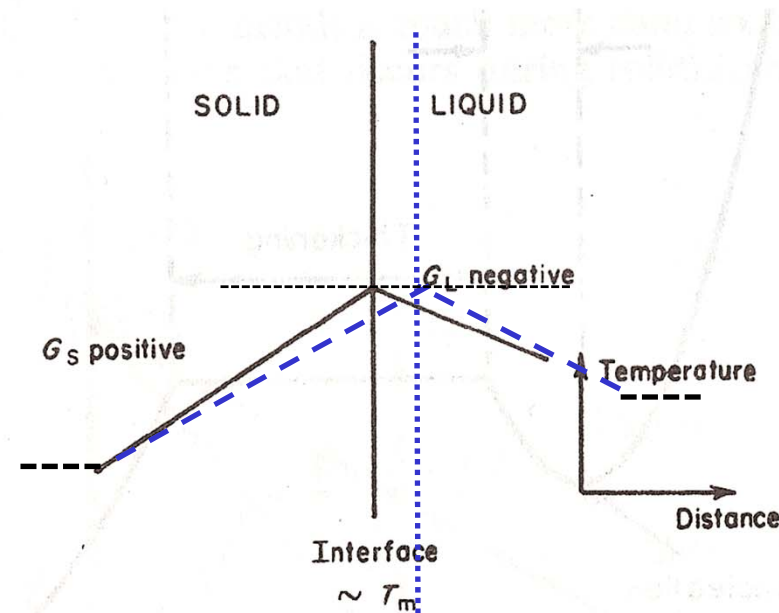


(a)

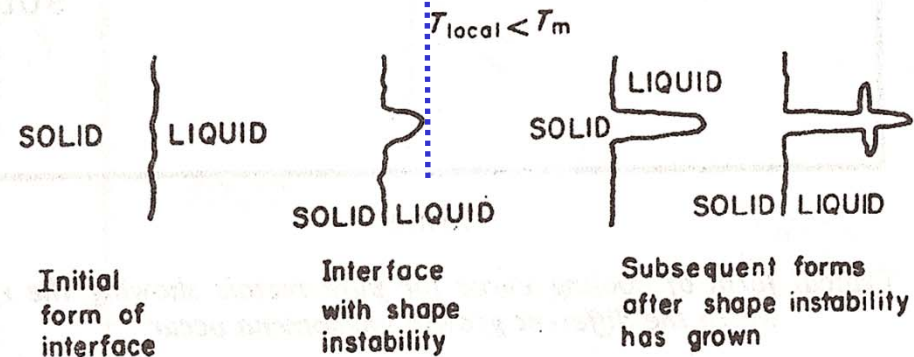


## 2) Supercooled liquid

: conduction of latent heat into the liquid

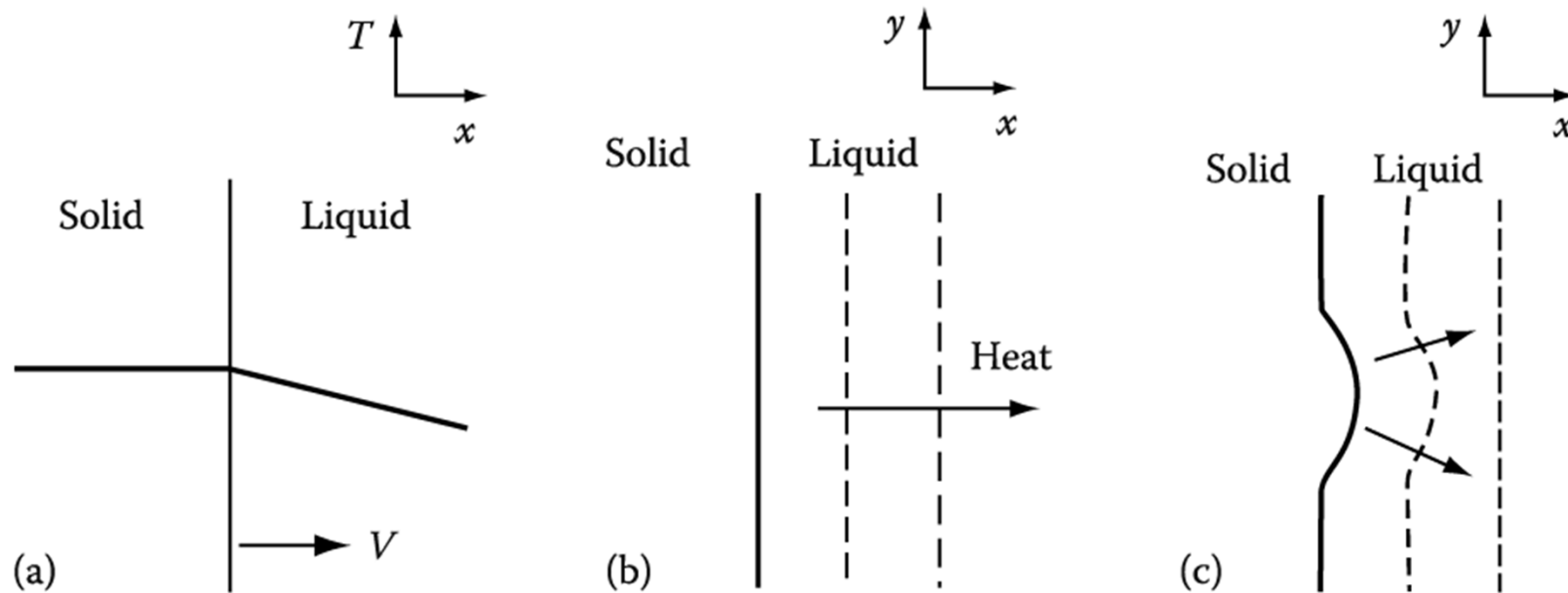


(a)



# Heat Flow and Interface Stability - Planar interface

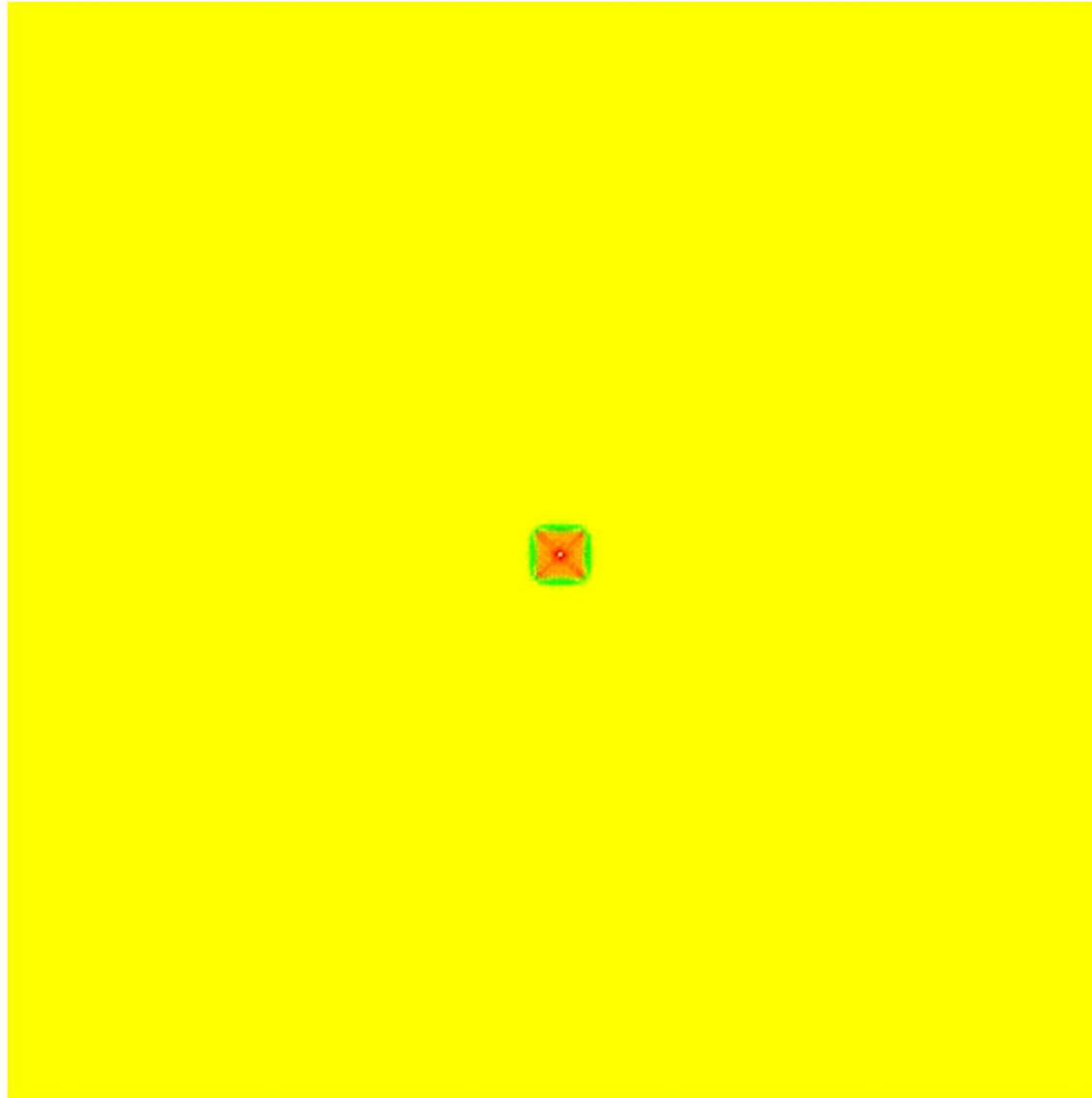
## 2) Solid growing into supercooled liquid



- protrusion  $\frac{dT'_L}{dX} < 0$  becomes more negative

- heat flow from solid = the protrusion grows preferentially.

**Solidification:** Liquid  $\longrightarrow$  Solid



**4 Fold Symmetric Dendrite Array**

## Development of Thermal Dendrite

### cf) constitutional supercooling

### When does heat flow into liquid?

- Liquid should be supercooled below  $T_m$ .
- Nucleation at impurity particles in the bulk of the liquid

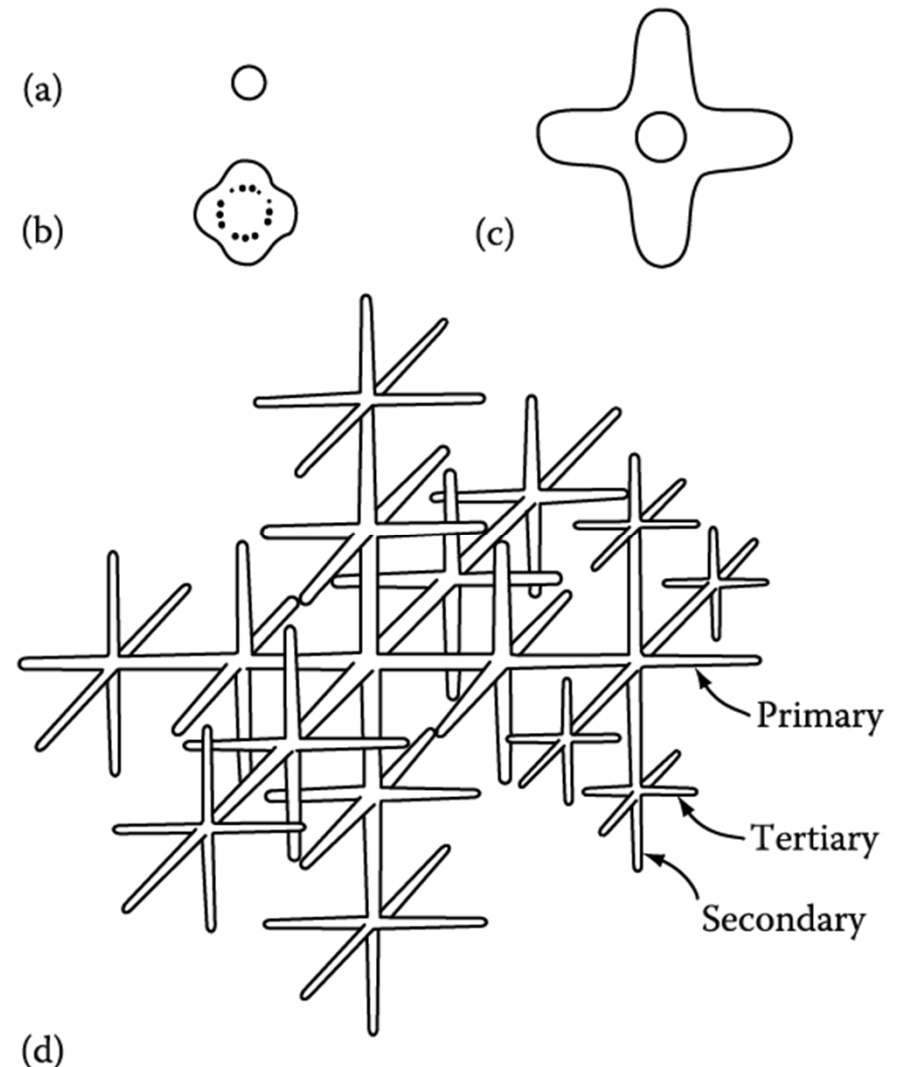


Fig. 4.17 The development of **thermal dendrites**: (a) a spherical nucleus; (b) the interface becomes unstable; (c) primary arms develop in crystallographic directions ( $\langle 100 \rangle$  in cubic crystals); (d) secondary and tertiary arms develop

**Q: How to calculate the growth rate ( $v$ )  
in the tip of a growing dendrite?**

# Closer look at the tip of a growing dendrite

different from a planar interface because heat can be conducted away from the tip in three dimensions.

Assume the solid is isothermal ( $T'_S = 0$ )

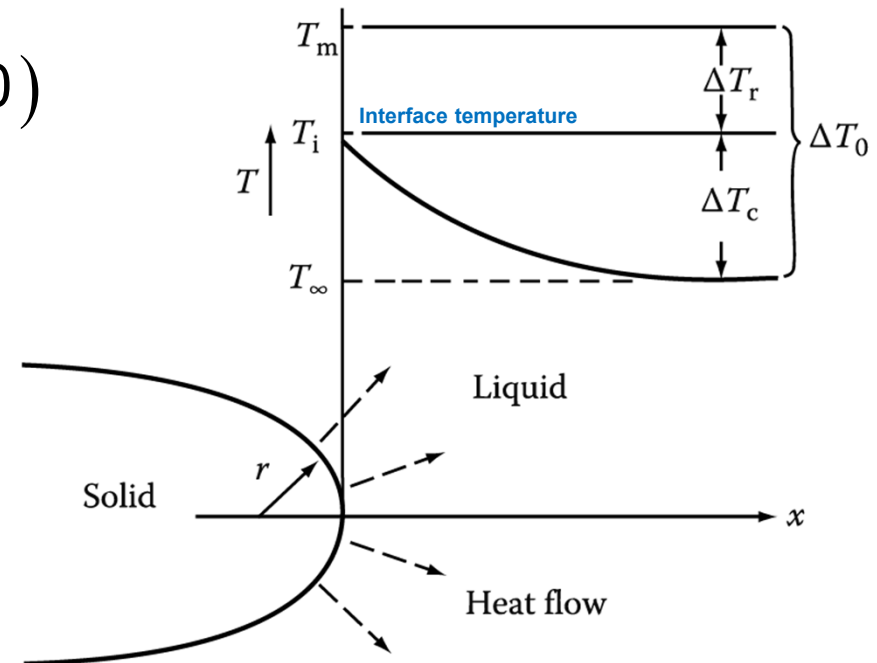
From  $K_S T'_S = K_L T'_L + v L_V$

If  $T'_S = 0$ ,  $v = \frac{-K_L T'_L}{L_V}$

A solution to the heat-flow equation for a hemispherical tip:

$T'_L (negative) \cong \frac{\Delta T_C}{r}$      $\Delta T_C = T_i - T_\infty$

$v = \frac{-K_L T'_L}{L_V} \cong \frac{K_L}{L_V} \cdot \frac{\Delta T_C}{r}$      $v \propto \frac{1}{r}$



However,  $\Delta T$  also depends on  $r$ .  
How?

## Thermodynamics at the tip?

Gibbs-Thomson effect:  
melting point depression

$$\Delta G = \frac{L_V}{T_m} \Delta T_r = \frac{2\gamma}{r} \quad \Delta T_r = \frac{2\gamma T_m}{L_V r}$$



## Minimum possible radius ( r )?

$$r_{min} : \Delta T_r \rightarrow \Delta T_0 = T_m - T_\infty \rightarrow r^*$$

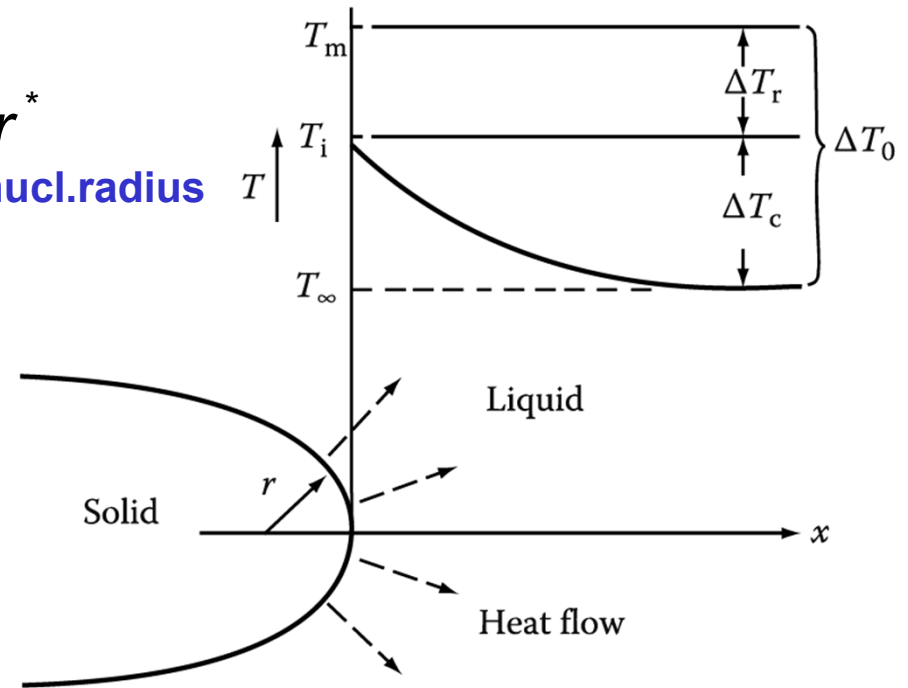
The crit.nucl.radius

$$r^* = \frac{2\gamma T_m}{L_v \Delta T_0}$$

$$\Delta T_r = \frac{2\gamma T_m}{L_v r}$$

Express  $\Delta T_r$  by  $r$ ,  $r^*$  and  $\Delta T_0$ .

$$\Delta T_r = \frac{r^*}{r} \Delta T_0$$



$$v \cong \frac{K_L}{L_v} \cdot \frac{\Delta T_c}{r} = \frac{K_L}{L_v} \cdot \frac{(\Delta T_0 - \Delta T_r)}{r} = \frac{K_L}{L_v} \cdot \frac{\Delta T_0}{r} \left( 1 - \frac{r^*}{r} \right)$$

$v \rightarrow 0$  as  $r \rightarrow r^*$  due to Gibbs-Thomson effect  
as  $r \rightarrow \infty$  due to slower heat conduction

Maximum velocity?

$$\rightarrow r = 2r^*$$