

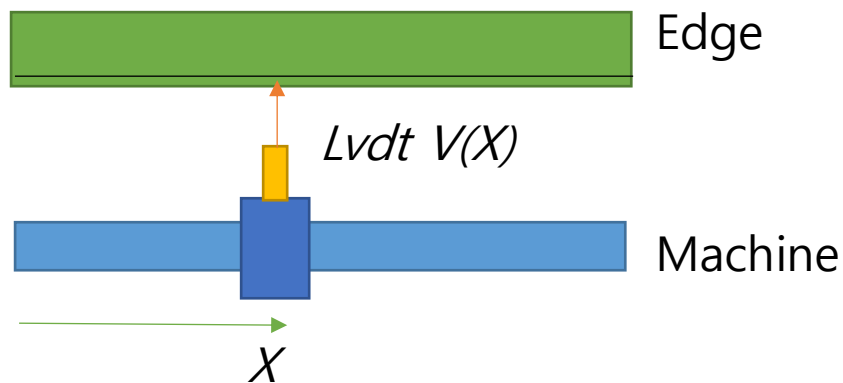
## Precision Metrology 13- Straightness Measurement

### Straightness measurement using the Straight Edge

Straight edge: Artefact of precision straight line feature, made of steel (by grinding/lapping), cast iron (by scraping), granite (by lapping). Typical sizes are 300mm, 600mm, 1m, etc. Few  $\mu\text{m}$  tolerance per 1 metre, typically.



Source: wonkee-donkee tools(UK)



Sign convention: + for away; – for near

When  $M(X)$  is the machine's straightness profile, and  $V(X)$  is the measured profile at  $X$  location by the LVDT or Capacitance gauge along the machine axis.

The measured profile,  $V(X)$ , is

$$V(X) = -M(X) + aX + b$$

where  $a$ ,  $b$  are the slope and offset; and the slope and offset can be physically interpreted as the non-parallelism and stand-offs encountered during the set-up procedure

Because the straightness error is the deviation from the reference straight line, thus the 3 methods of reference fitting techniques such as the end-points fit, least squares fit, and the minimum zone fit can be applied

to calculate the slope and offset. Calculation of a, b can be used to obtain pure straightness error after removing the slope and offset effects,

$$\underline{V} = V(X) - aX - b (= -M(X))$$

∴ The straightness error =  $\max \underline{V} - \min \underline{V}$

*( Q: Straight edge is really straight? )*

### Reversal Technique for Straightness Measurement

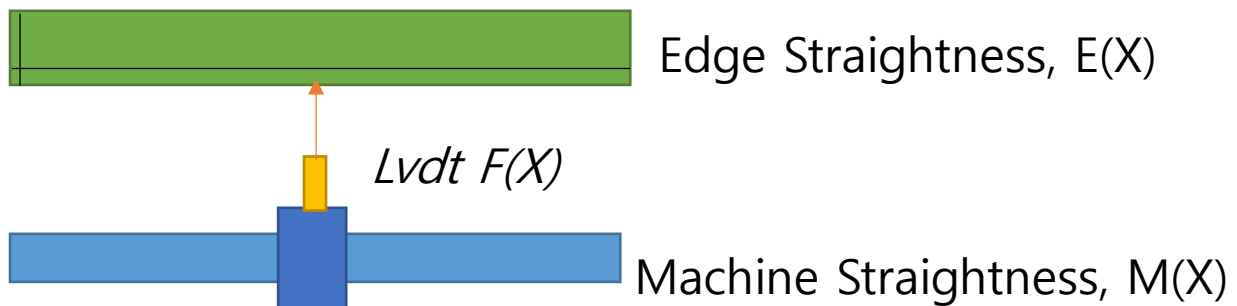
:To eliminate the straightness error, or self-error, of the straight edge. F type and M type measurement methods

#### 1.F type measurement method

:Fixed edge type measurement method

Sign convention: + for away; – for near

## Forward measurement

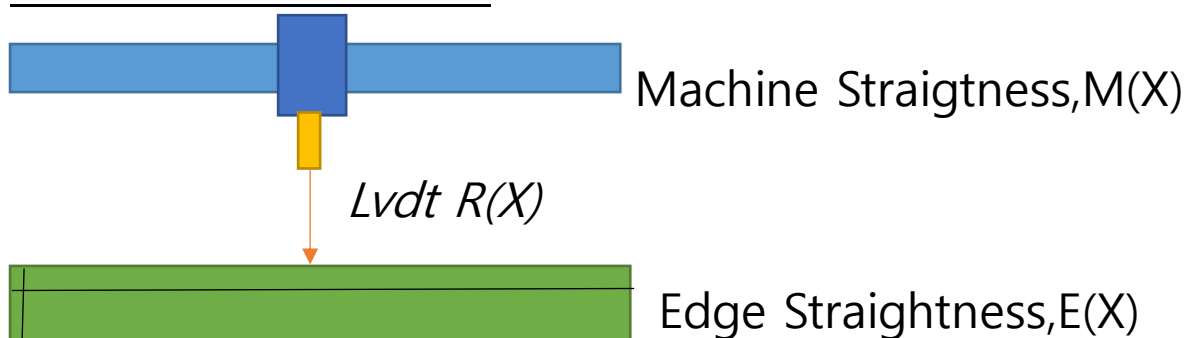


Forward measurement,  $F(X) = -E(X) - M(X) + a_F X + b_F$

where  $a_F, b_F$  are slope and offset of the best fit line, and from the non-parallelism and stand-offs.

$$\text{Thus, } \underline{E} = F(X) - (a_F X + b_F) = -E(X) - M(X) \quad (1)$$

## Reverse Measurement



Reverse measurement,  $R(X) = -E(X) + M(X) + a_R X + b_R$

where  $a_R, b_R$  are slope and offset of the best fit line, and from the non-parallelism and stand-offs.

$$\text{Similarly, } \underline{R} = R(X) - (a_R X + b_R) = -E(X) + M(X) \quad (2)$$

From (1)+(2) and (1)-(2)

$$E(X) = \text{Edge straightness} = -(\underline{F} + \underline{R})/2$$

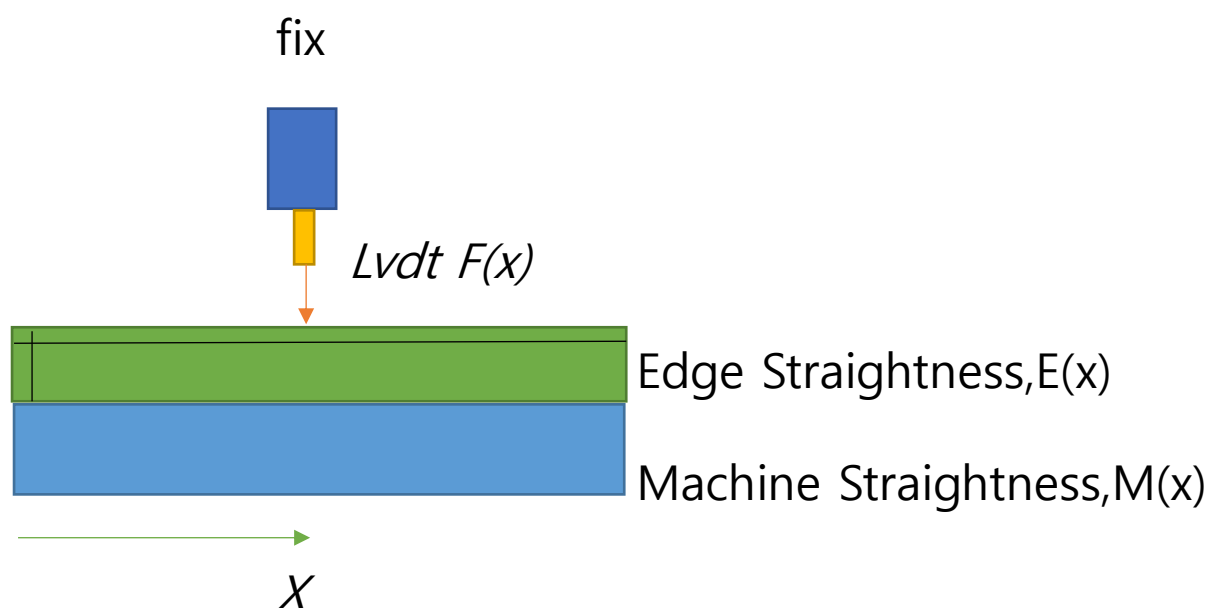
$$M(X) = \text{Machine straightness} = (\underline{R} - \underline{F})/2$$

Therefore Edge straightness and Machine straightness can be measured.

## 2. M type measurement method

:Moving edge type measurement method

### Forward measurement



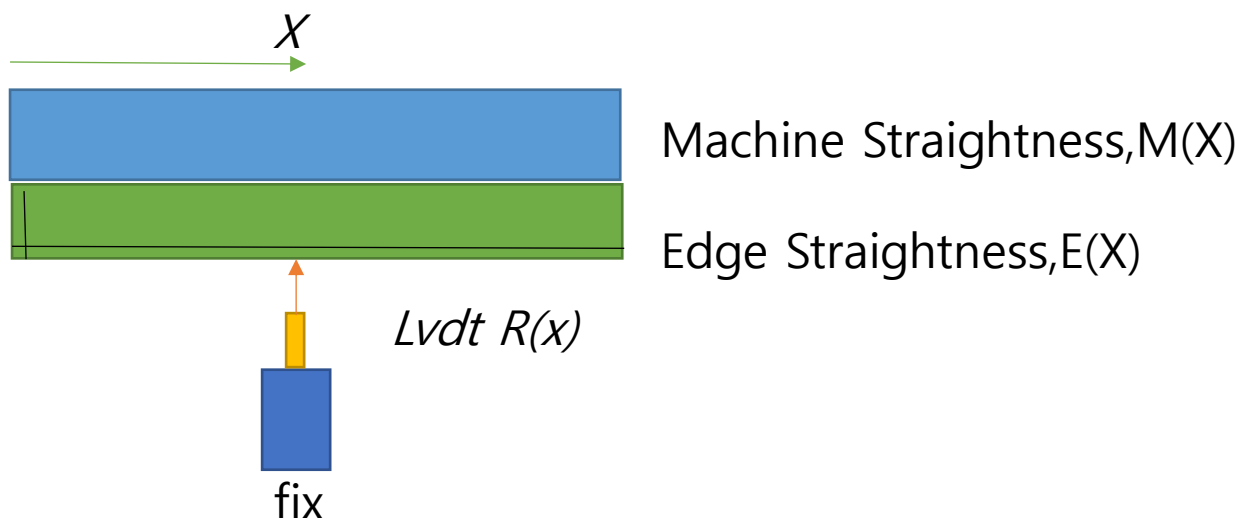
Forward measurement  $F(x) = -E(x) - M(x) + a_F x + b_F$

where  $a_F, b_F$  are slope and offset of the best fit lines, and physically due to the non-parallelism and stand-offs.

The end points fit, least squares fit, or the minimum zone fit can be used for the best fit reference line.

$$\text{Thus, } \underline{F} = F(X) - (a_F X + b_F) = -E(X) - M(X) \quad (3)$$

### Reverse measurement



Reverse measurement  $R(X) = -E(X) + M(X) + a_R X + b_R$

where  $a_R, b_R$  are slope and offset of the best fit line, and from the non-parallelism and stand-offs.

$$\text{Similarly, } \underline{R} = R(X) - (a_R X + b_R) = -E(X) + M(X) \quad (4)$$

From (3)+(4) and (3)-(4)

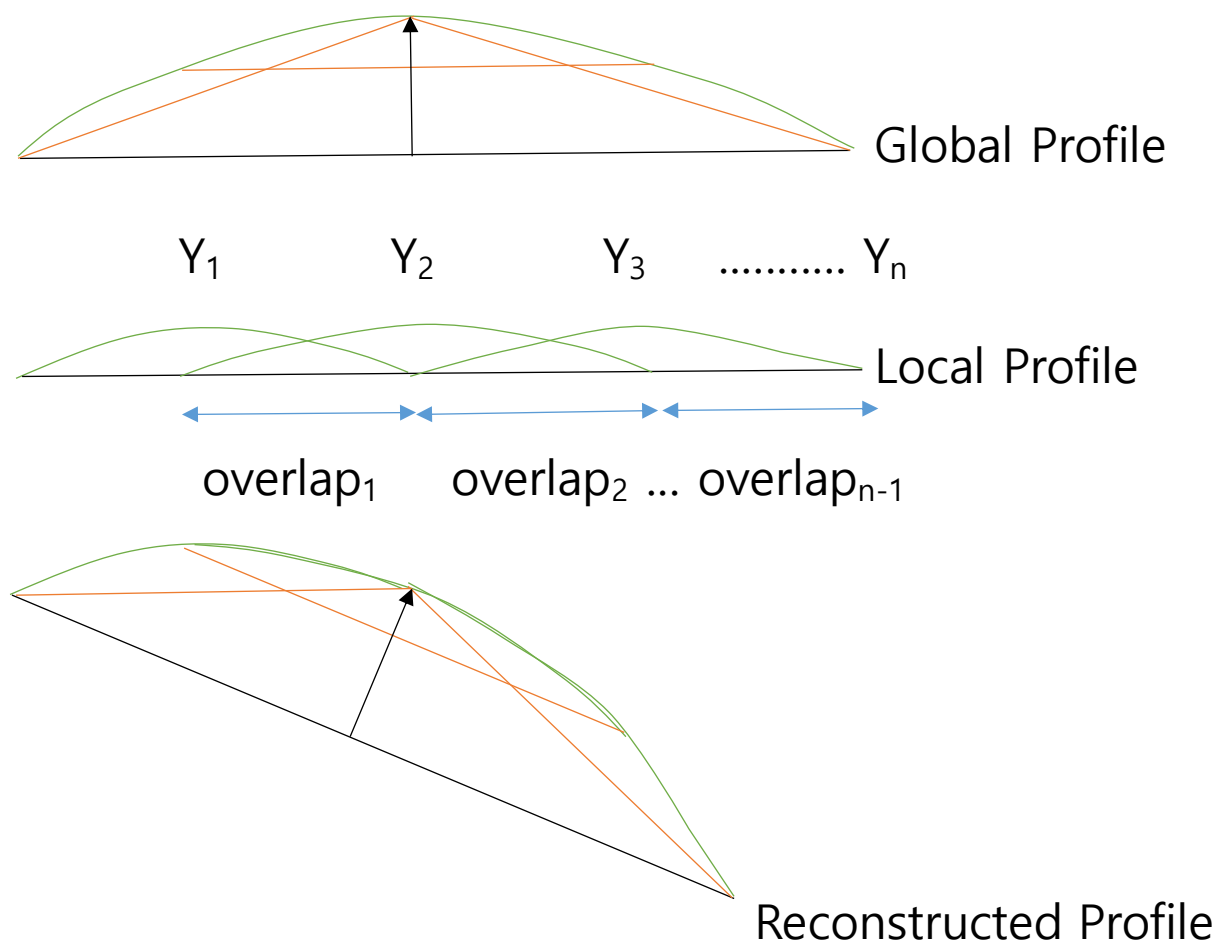
$$E(X) = \text{Edge straightness} = -(\underline{F} + \underline{R})/2$$

$$M(X) = \text{Machine straightness} = (\underline{R} - \underline{F})/2$$

Therefore Edge straightness and Machine straightness can be measured.

## Profile matching method or stitching method

:To use a short straight edge to measure the straightness of the long travel, by matching the profile over the region overlapped.



When  $Y_1, Y_2, \dots, Y_n$  are the straightness measurement data, or local profile, from the short straight edge, the total straightness error, or global profile, can be obtained by



the sum of the local straightness error, or local profile.

For overlap<sub>1</sub> region,  $Y_1$  must be the same as  $Y_2$ , that is,  $Y_1 \equiv Y_2$ ; and any difference is due to the slope and offset of the local straight lines of each local profile.

For the overlap<sub>1</sub> region,  $Y_1 - Y_2 = A_1X + B_1$ , and  $A_1, B_1$  are the slope and offset to be determined from the best fit line along the distance  $X$  over the overlap<sub>1</sub> region.

Similarly, for the overlap<sub>2</sub> region,  $Y_2 - Y_3 = A_2X + B_2$ , and  $A_2, B_2$  are the slope and offset to be determined from the best fit line along the distance  $X$  over the overlap<sub>2</sub> region.

Thus, it can be extended to the  $n$ th local profile,  $Y_n$

$$Y_1 - Y_2 = A_1X + B_1$$

$$Y_2 - Y_3 = A_2X + B_2$$

.....

$$\underline{Y_{n-1} - Y_n = A_{n-1}X + B_{n-1}} \quad +$$

$$Y_1 - Y_n = \sum(A_kX + B_k)$$

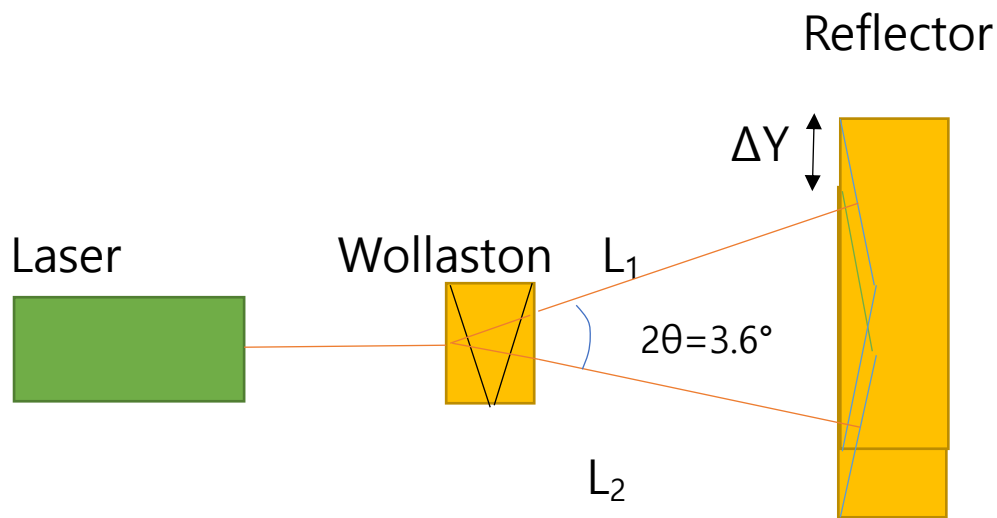
$$\therefore Y_1 = Y_n + \sum(A_kX + B_k), \quad k=1,2,\dots,n-1$$

and  $n$ =number of Local profiles. Thus for the local profile,  $Y_n$ , can be transformed to the global profile reconstructed,  $Y_1$ . Then the best fit reference line can be applied to the reconstructed profile, thus the global straightness error can be evaluated.

In this way, the global straightness profile can be obtained by the sum of the local straightness profiles transformed, using the profile matching method. This profile matching method firstly proposed by SNU\*, and is sometimes called as the stitching method, and expanded to 2D surface, such as stitching method for semiconductor wafer, giving wide applications or surface metrology.

\*Development of Straightness Measurement using Profile Matching Method, H.J.Pahk, J.S.Park, I.J.Yeo, Int.J.Machine Tools and manufacture, Vol.37(2), 135-147, 1997

## Straightness Interferometer



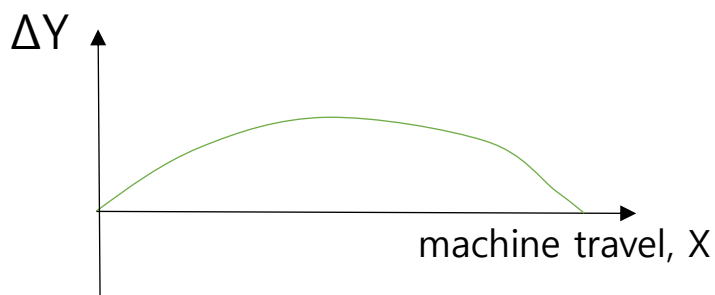
Let  $L_1^*$ ,  $L_2^*$  be the changed length of  $L_1$ ,  $L_2$  after  $\Delta Y$  movement ;

$$L_1^* = L_1 + \Delta Y \cdot \sin\theta, \quad L_2^* = L_2 - \Delta Y \cdot \sin\theta$$

$$L_1^* - L_2^* = L_1 - L_2 + 2\Delta Y \cdot \sin\theta$$

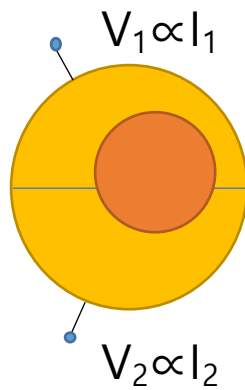
$$\therefore \Delta Y = [(L_1^* - L_2^*) - (L_1 - L_2)] / 2\sin\theta$$

3-5 times repeat straightness measurements,  $\Delta Y$ ,  
over the machine travel



## Tooling laser with Photosensor, Photodiode, CCD

### For Bisector Photo Sensor

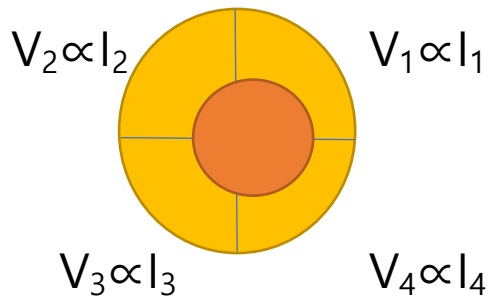


$$\text{Centroid} = (I_1 - I_2) / (I_1 + I_2) = (V_1 - V_2) / (V_1 + V_2),$$

or Pixel count

∴ The straightness error can be measured.

## For Quadrant Photo Sensor



$$X \text{ Centroid} = [(I_1 + I_4) - (I_2 + I_3)] / [I_1 + I_2 + I_3 + I_4]$$

$$= [(V_1 + V_4) - (V_2 + V_3)] / [V_1 + V_2 + V_3 + V_4]$$

Or, Pixel count

$$Y \text{ Centroid} = [(I_1 + I_2) - (I_3 + I_4)] / [I_1 + I_2 + I_3 + I_4]$$

$$= [(V_1 + V_2) - (V_3 + V_4)] / [V_1 + V_2 + V_3 + V_4]$$

Or, Pixel count

∴ Two straightness error components can be measured

This is a simple and convenient measurement, but sensitive to beam fluctuation due to temperature, airflow, especially in the long distance.