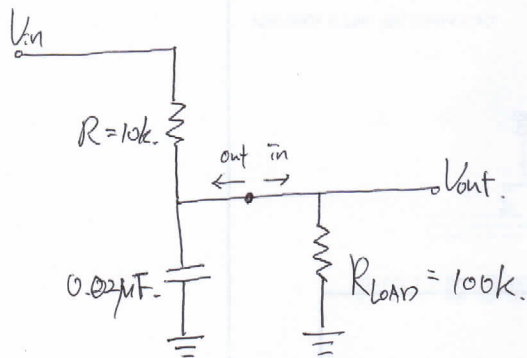


①.
17/09/18.

LPF.



but unclear.

$Z_C = \infty$ (Assumption) $\rightarrow$ really true?

Impedance = Generalized Resistance.

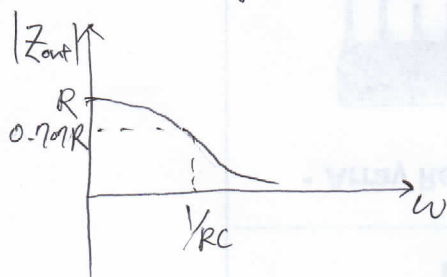
= Resistance + Reactance/Inductance.

$$Z_{out} = Z_R // Z_C = \frac{Z_R \cdot Z_C}{Z_R + Z_C}$$

$$Z_R = R, Z_C = \frac{1}{j\omega C}$$

$$Z_{out} = \frac{R \cdot \frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{R}{1 + j\omega RC}$$

$$|Z_{out}| = \frac{R}{\sqrt{1 + (\omega RC)^2}} \quad \angle = -\tan^{-1}(\omega RC)$$



$$Z_{in} = R_{Load} = 100k.$$

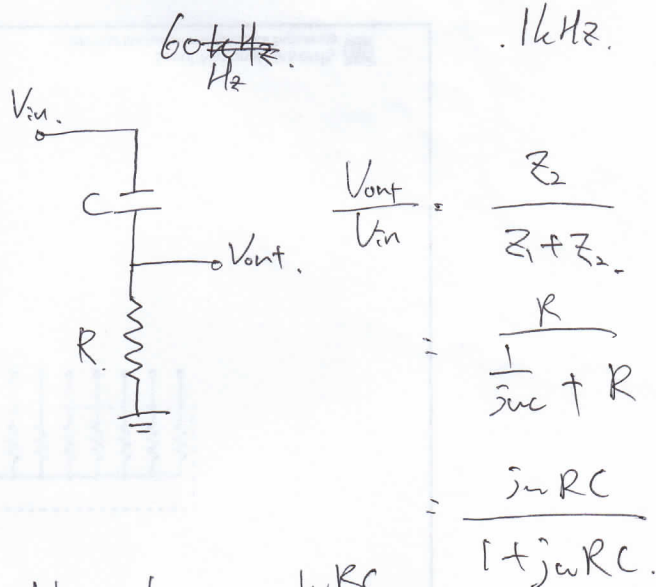
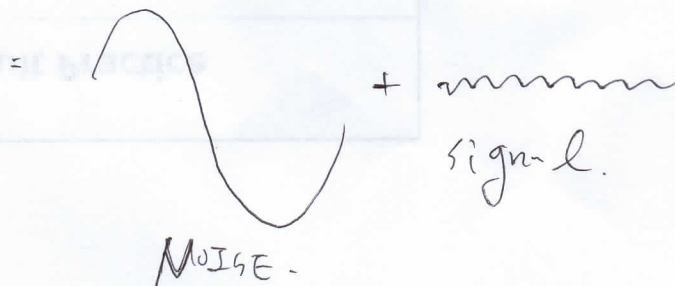
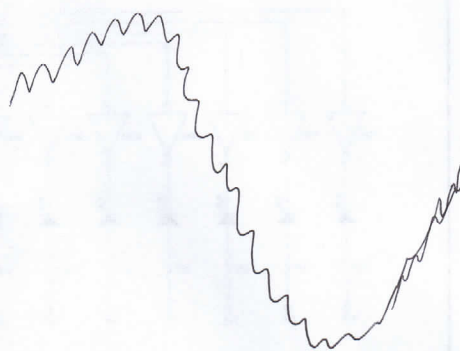
$$\therefore Z_{out} \leq \frac{1}{10} Z_{in} \quad \text{Satisfied.}$$

10k 10k.

$\Rightarrow$ Design rule of 10x.

" Z_{in} is 10 times or more stiff than Z_{out} "
(= bigger).

"HPF".



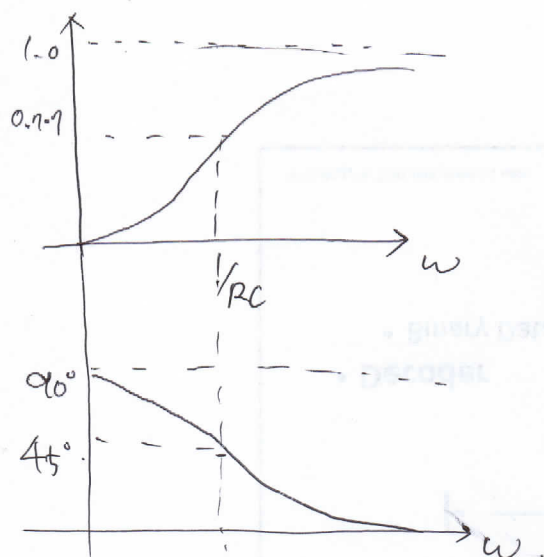
$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{\omega RC}{\sqrt{1 + (\omega RC)^2}}$$

$$\angle = 90^\circ - \tan^{-1}(\omega RC)$$

$$\omega \rightarrow 0, \left| \frac{V_{out}}{V_{in}} \right| \rightarrow 0. \quad \angle \rightarrow 90^\circ$$

$$\omega = \frac{1}{RC}, \left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{2}} = 0.707 \quad \angle = 45^\circ$$

② $\omega \rightarrow \infty, \left| \frac{V_{out}}{V_{in}} \right| \rightarrow 1, \angle = 0^\circ$



$\omega \geq \frac{1}{RC} = \omega_{3dB} \approx 0.707$

$\therefore$ High Pass Filter.

③ $\omega_{3dB} = \frac{1}{RC}$

Design a HPF, $f_{3dB} =$

Noise = 1kHz,

Signal = 16kHz...

① freq. Identification.

$f_{signal} = 16kHz,$

$f_{noise} = 1kHz.$

② Choose R.C s.t $\omega_{3dB} = 2\pi f_{signal}$ $Z_{out} = Z_C // Z_R = \frac{Z_C Z_R}{Z_C + Z_R}$

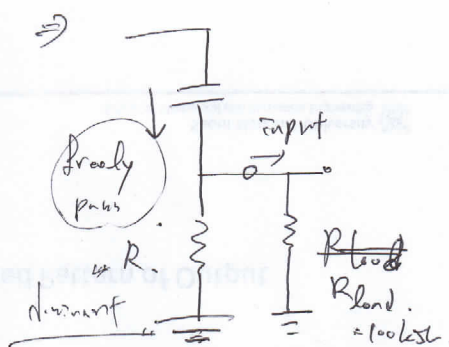
③ 10X rule.

④ performance verification

$\omega_{3dB} = 2\pi(16,000)$

$= \frac{1}{RC} \dots ①$

To drive AB converter. ^{= 6V p-p}
whose input impedance is 10k Ω



$R = \frac{1}{10} R_{load} = 10k\Omega \dots ②$

$\therefore C \approx 10^{-10} F = 0.0001 \mu F.$
→ commercially available
→ 100pF.

At. $f = 16,000Hz.$

$\left| \frac{V_{out}}{V_{in}} \right| = 0.707.$

$f_{noise} = 1kHz, \left| \frac{V_{out}}{V_{in}} \right| = 0.0628.$

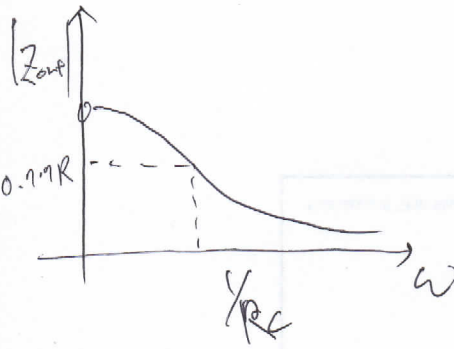
S/N Ratio = 11.25.

$Z_C \rightarrow 0$ at high freq
(Assumption)

$= \frac{\frac{1}{j\omega C} \cdot R}{\frac{1}{j\omega C} + R} = \frac{R}{1 + j\omega CR}$

$|Z_{out}| = \frac{R}{\sqrt{1 + (\omega CR)^2}}$

③



$$|Z_{out}| \leq R$$

$$Z_{in} = R_{load} = 100k\Omega$$

$$Z_{out} \leq \frac{1}{10} Z_{in}$$

"saturation"

$$\omega_1 = \frac{1}{R_1 C_1}, \quad \omega_2 = \frac{1}{R_2 C_2}$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{1 + j\omega R_1 C_1} \cdot \frac{j\omega R_2 C_2}{1 + j\omega R_2 C_2}$$

$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{\omega R_2 C_2}{\sqrt{1 + (\omega R_1 C_1)^2} \sqrt{1 + (\omega R_2 C_2)^2}}$$

$$\angle = 90^\circ - \tan^{-1}(\omega R_1 C_1) - \tan^{-1}(\omega R_2 C_2)$$

BPF
amplitude
cutoff 1.6kHz 8kHz

Band Pass Filter (BPF)

Design a BPF. to pass signals between 1.6kHz and 8kHz.
 $1.6kHz \leq f \leq 8kHz$

$$\omega_{3dB} = (8000)(2\pi) =$$

HPF

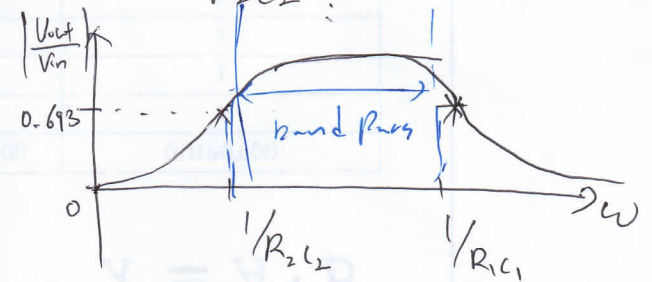
$$\omega_{3dB} = (1600)(2\pi)$$

"Band width can be passed"

$$BPF = \underline{LPF} + \underline{HPF}$$

$$LPF = \frac{1}{R_1 C_1} \quad \frac{1}{R_1 C_1} = 8000 \cdot 2\pi$$

$$HPF = \frac{1}{R_2 C_2}$$

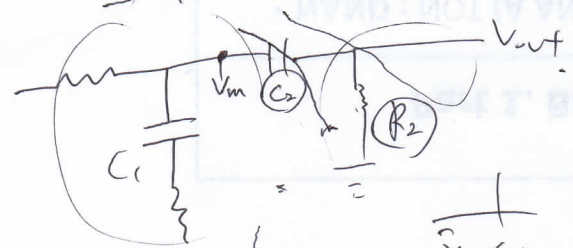
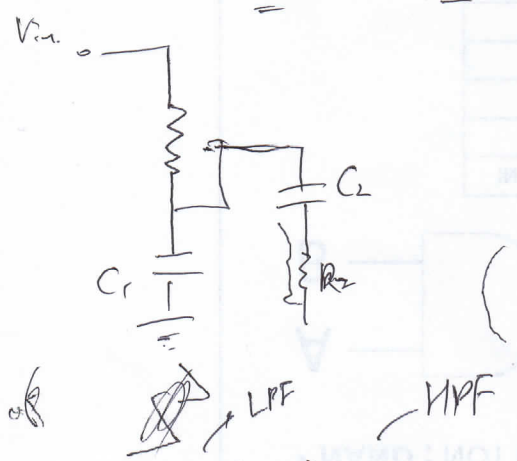


$$\text{At } \omega = \frac{1}{R_2 C_2} = (1600)(2\pi)$$

$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{1 + \left(\frac{R_1 C_1}{R_2 C_2} \right)^2}} \cdot \frac{1}{\sqrt{1 + \left(\frac{R_2 C_2}{R_1 C_1} \right)^2}}$$

$$= 0.693$$

$$\angle = 90^\circ - \tan^{-1}(1/5) - \tan^{-1}(1) = 33.7^\circ$$



$$\frac{V_{in}}{V_{out}} = \frac{Z_1}{Z_1 + Z_2} = \frac{\frac{1}{j\omega C_1}}{R_1 + \frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} + R_2}$$

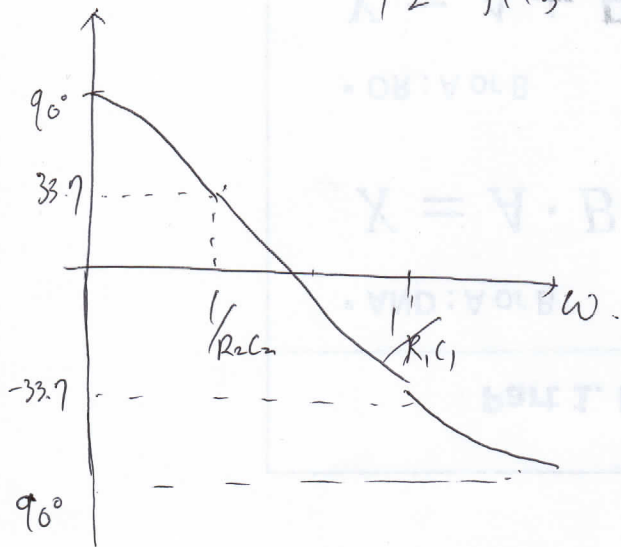
$$\frac{V_{in}}{V_{out}} = \frac{\frac{1}{j\omega C_1}}{\frac{1}{j\omega C_2} + R} = \frac{j\omega R_2 C_2}{1 + j\omega R_2 C_2}$$

④

At $\omega = \frac{1}{R_1 C_1} = (8000)(2\pi)$

$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{(R_2 C_2 / R_1 C_1)}{\sqrt{1 + \omega^2} \cdot \sqrt{1 + \left(\frac{R_2 C_2}{R_1 C_1} \right)^2}}$$

$$= \frac{5}{\sqrt{2} \cdot \sqrt{1 + 5^2}} = 0.693$$



For HPF

$\therefore R_2 = \frac{1}{10} R_{LOAD} = 100 k\Omega$

$\therefore C_2 = 9.95 \times 10^{-4} \mu F$

$10 \times 10^{-4} \mu F$

→ commercially available.

LPF.

$R_1 = 10 k\Omega$ by 10X Rule.

$C_1 = 1.99 \times 10^{-3} \mu F$

$\approx 0.002 \mu F$

HW 3

LPF - HPF $\Rightarrow$ HPF - LPF.

For LPF

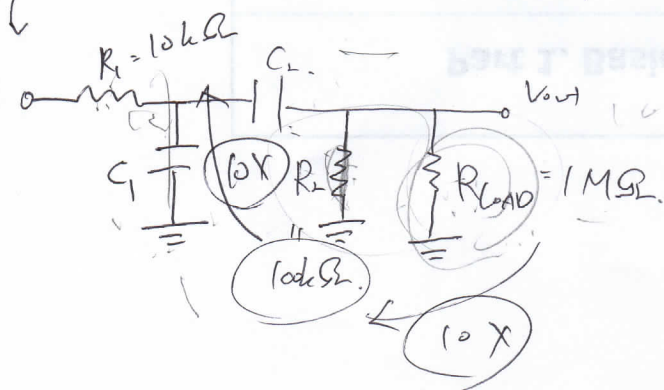
$\omega_{3dB} = \frac{1}{R_1 C_1} = (8000)(2\pi) \dots ①$

For HPF

$\omega_{3dB} = \frac{1}{R_2 C_2} = (1600)(2\pi) \dots ②$

To drive oscilloscope.

whose $Z_{in} = 1 M\Omega$.



→ not working.

→ why? $1.6 kHz \approx 8 kHz$

Design - BPF

① Design.

② plot

③ Verification

$R_{load} = 1 M\Omega$

if input $5 kHz$
 ~~$1.6 kHz \approx 8 kHz$~~

Mag? Phase? SN?

→ $5 kHz$ → signal

→ $20 kHz$ → noise

