

2021 Spring

“Phase Equilibria *in* Materials”

04.20.2021

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Office: 33-313

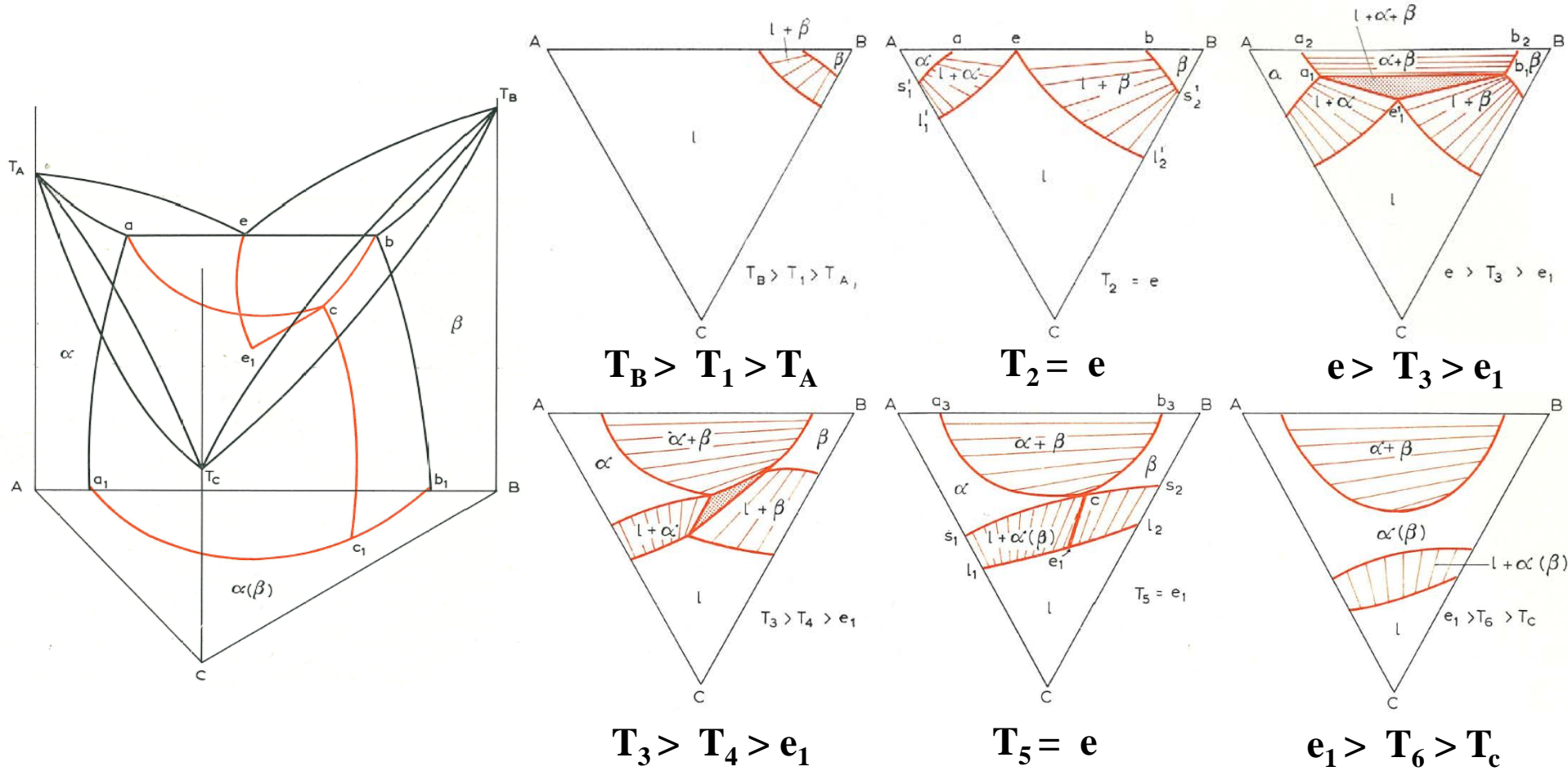
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9.3. THREE-PHASE EQUILIBRIUM INVOLVING EUTECTIC REACTIONS

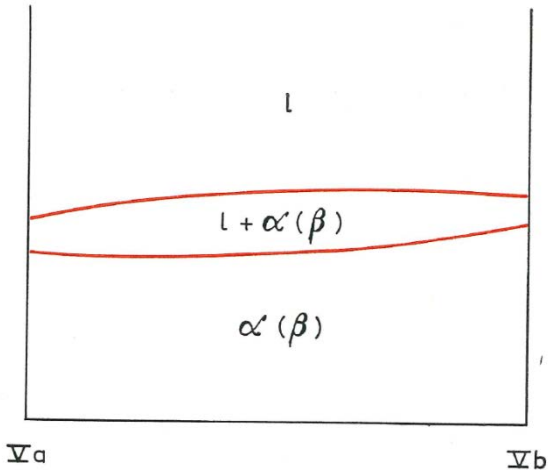
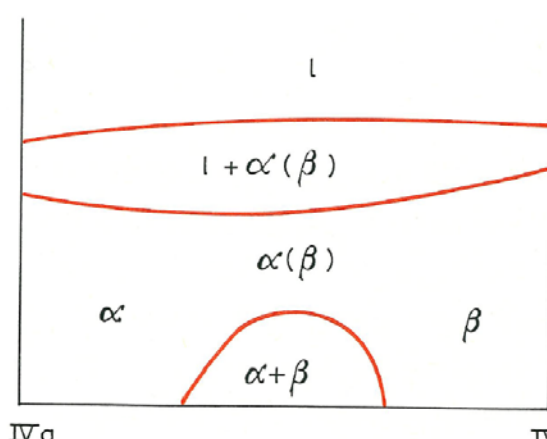
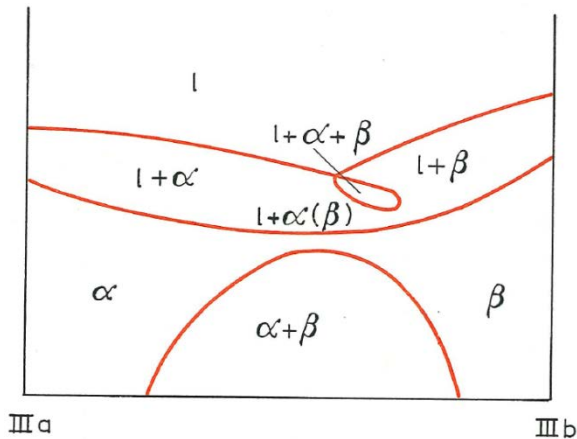
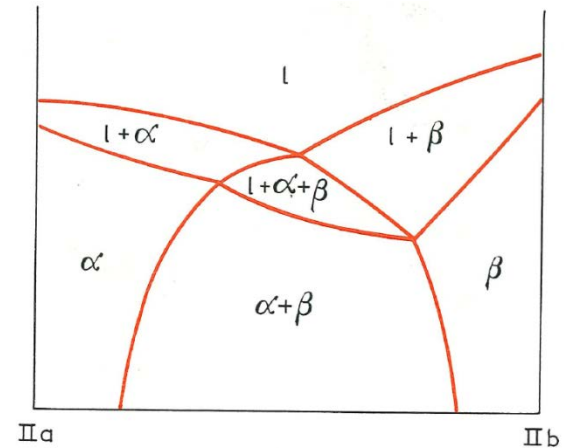
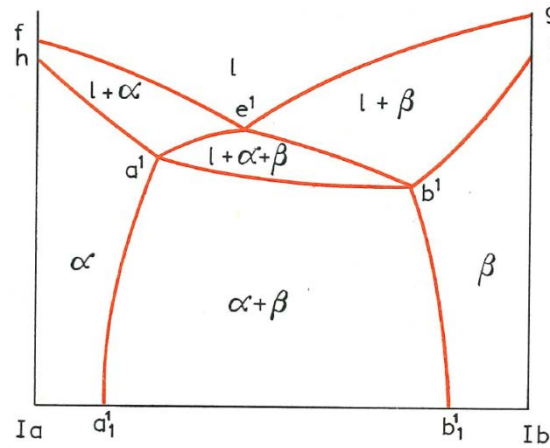
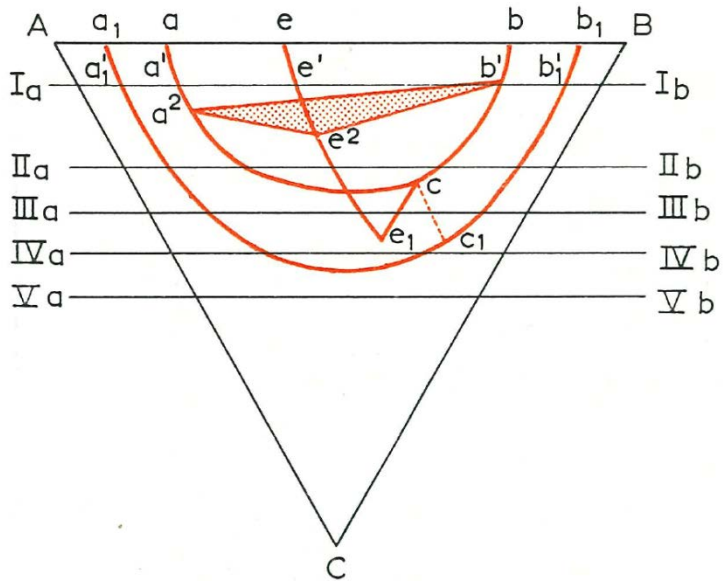
• Isothermal section



cf) Movie

9.3. THREE-PHASE EQUILIBRIUM INVOLVING EUTECTIC REACTIONS

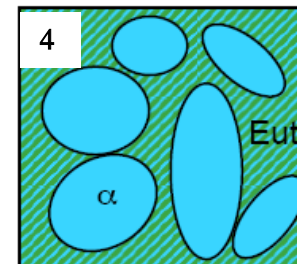
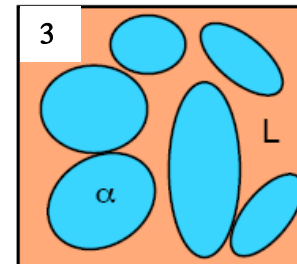
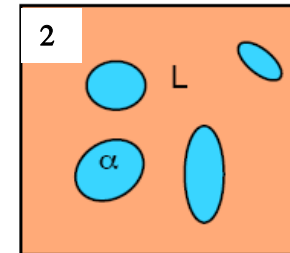
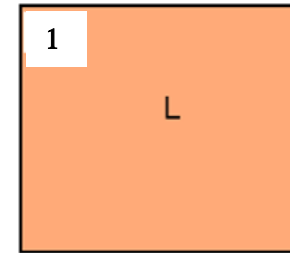
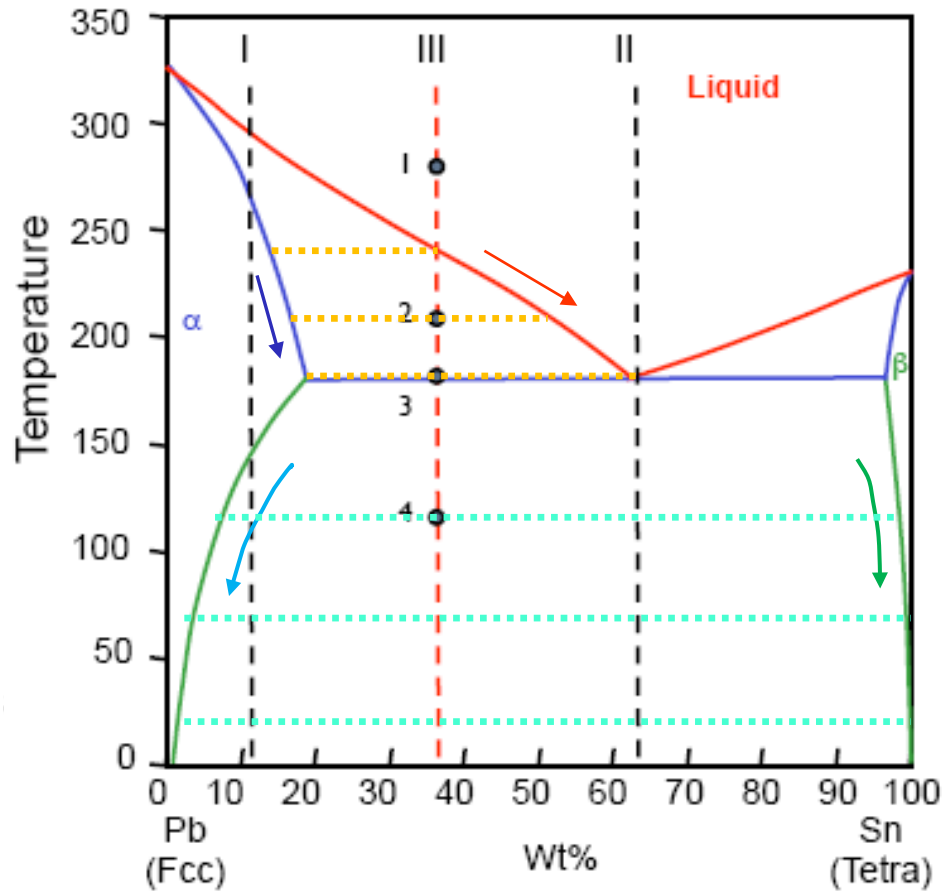
• Vertical section



1.5 Binary phase diagrams

Alloy III

Pb-Sn phase diagram



> Point 1: 4 on the α solidus surface

> Point 1- Point 2

* 4 \rightarrow 6 on the α solidus surface

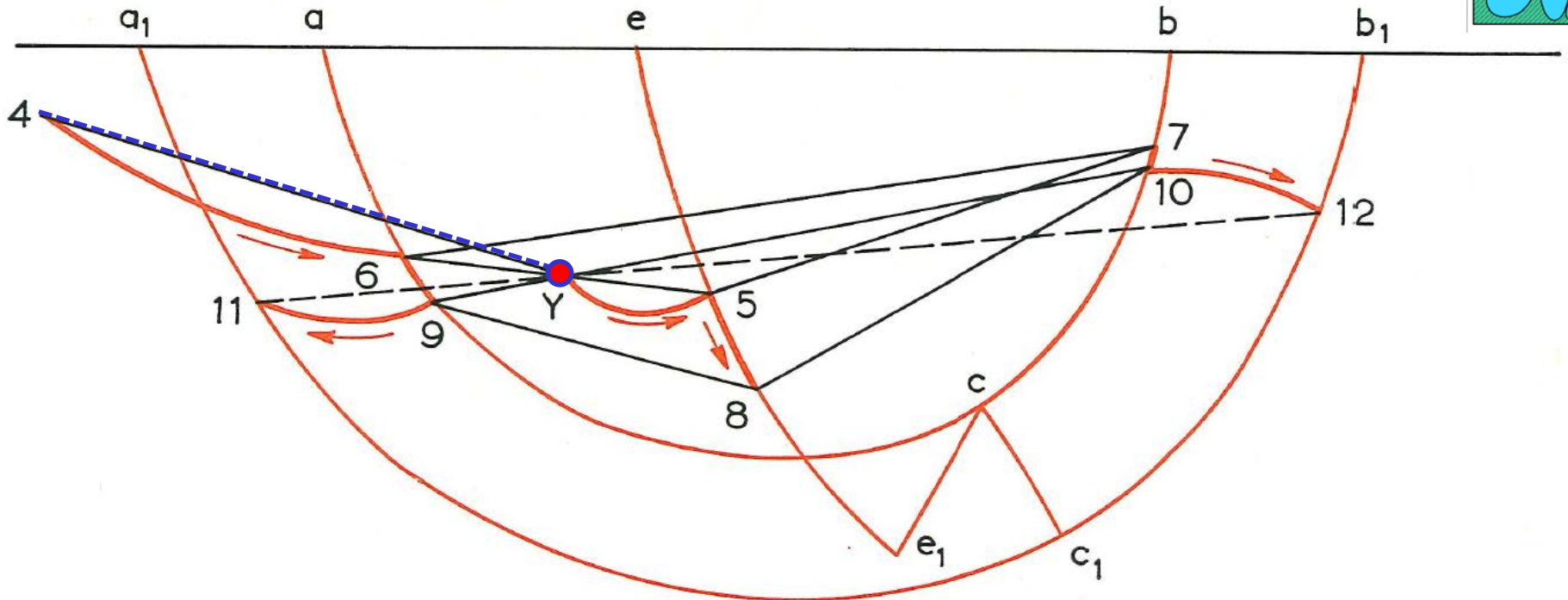
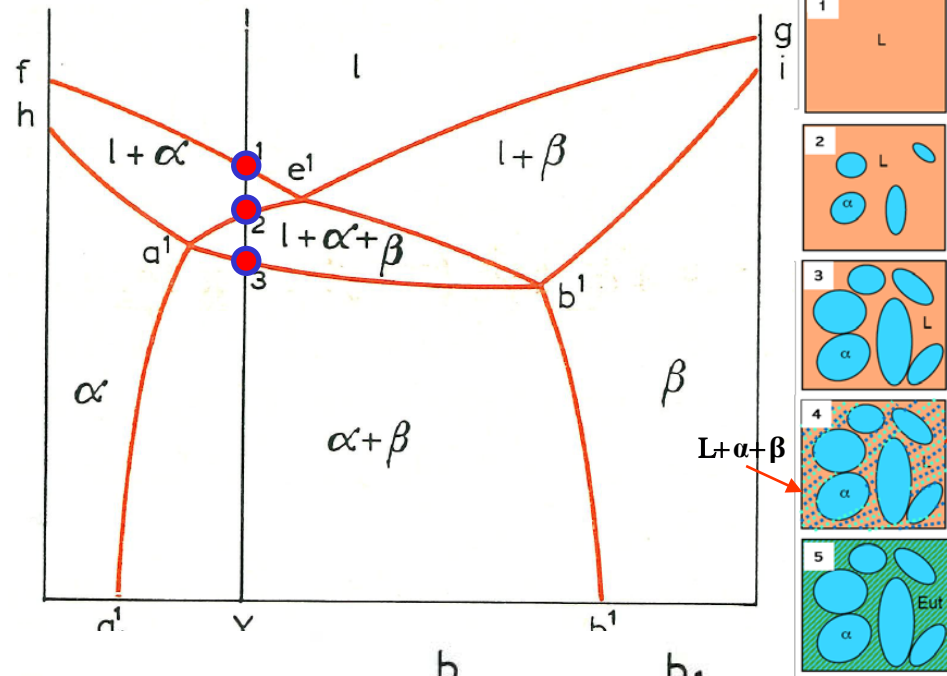
* 1 \rightarrow 5 on the α liquidus surface

Three phase equilibrium $l5, \alpha6, \beta7$

* α : 6 \rightarrow 9, β : 7 \rightarrow 10, l : 5 \rightarrow 8

> Point 3: on the tie line 9-10

> Point 3-Y: α : 9 \rightarrow 11, β : 10 \rightarrow 12

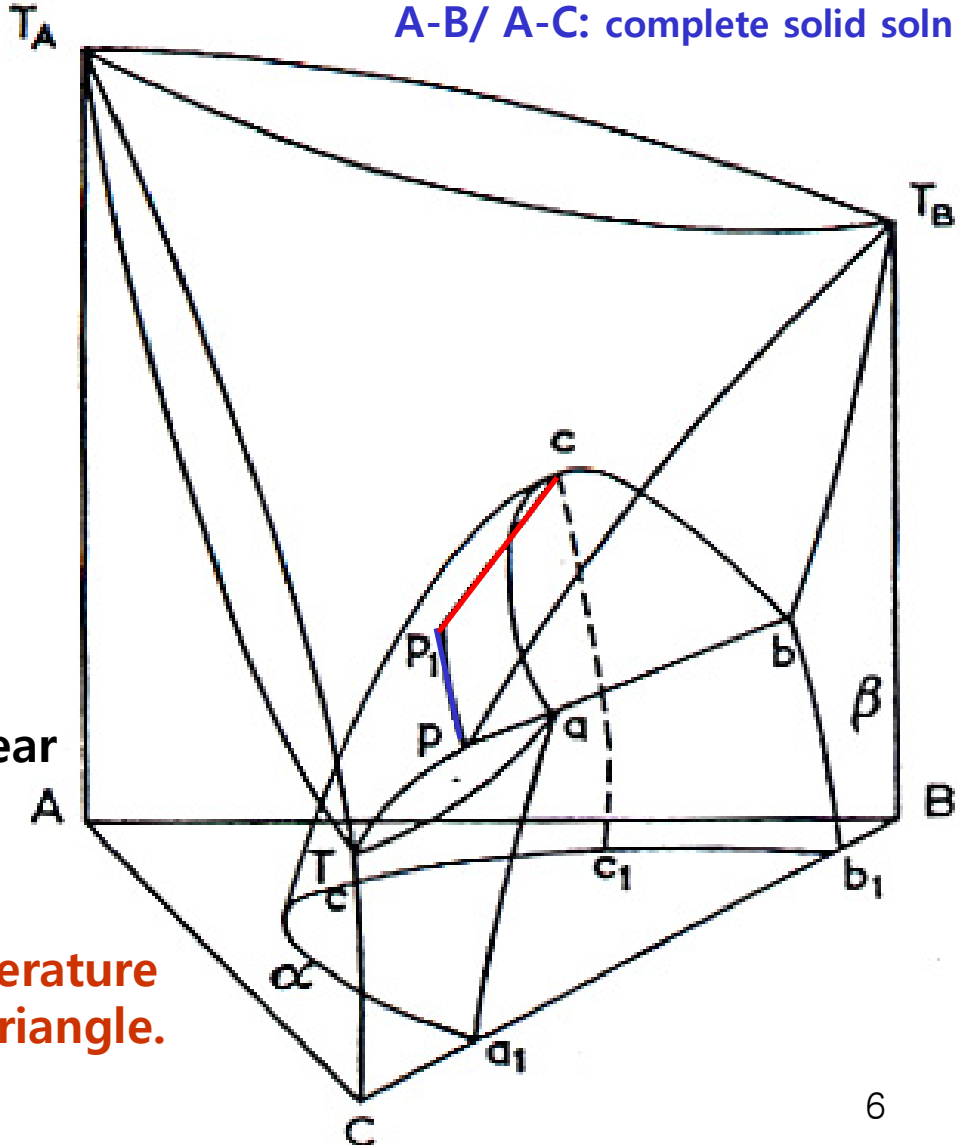
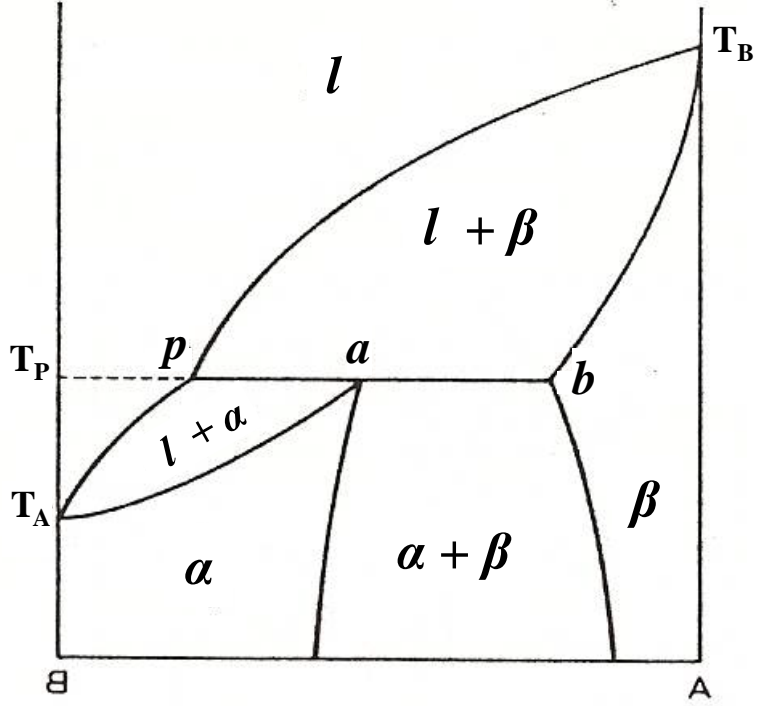


Projection of the solidification sequence for alloy Y on the concentration triangle

9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

- A peritectic solubility gap in one binary system

B-C: peritectic
 A-B/ A-C: complete solid soln



: A minimum or a maximum may appear in the monovariant liquid curve.

PP₁: monovariant curve for liquid

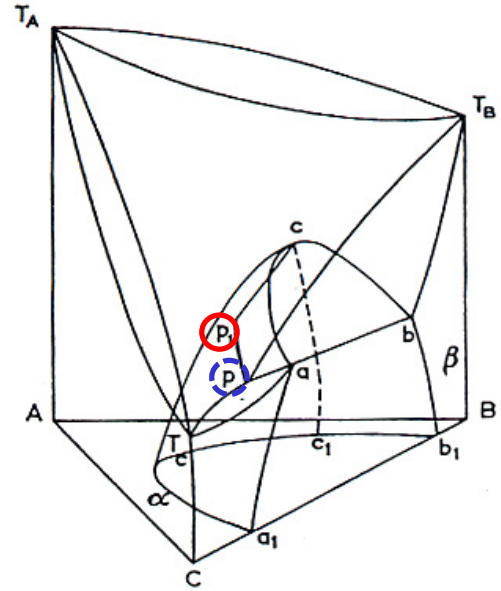
Points P₁ and c lie at the same temperature and the line P₁c is a degenerate tie triangle.

9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

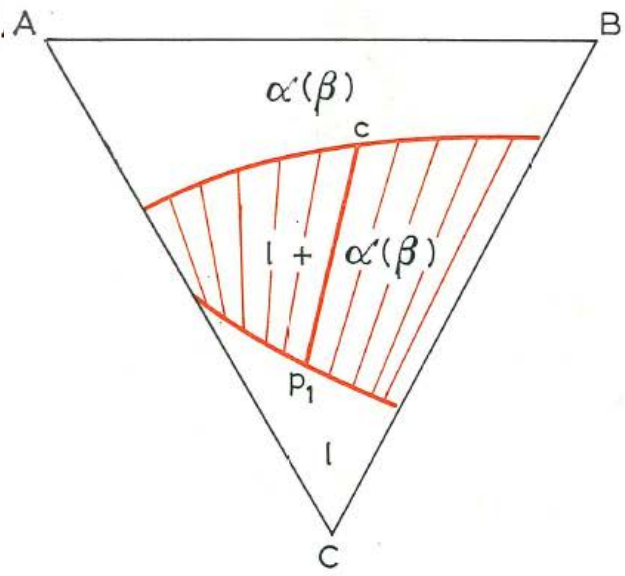
- A peritectic solubility gap in one binary system

PP_1 : monovariant curve for liquid

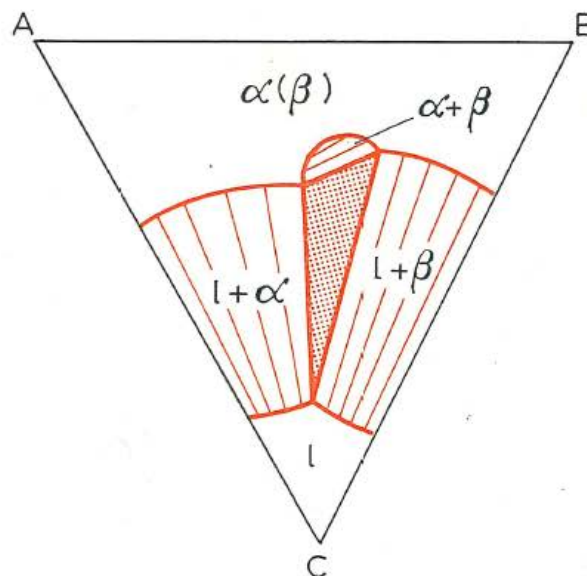
Points P_1 and c lie at the same temperature and the line P_1c is a degenerate tie triangle.



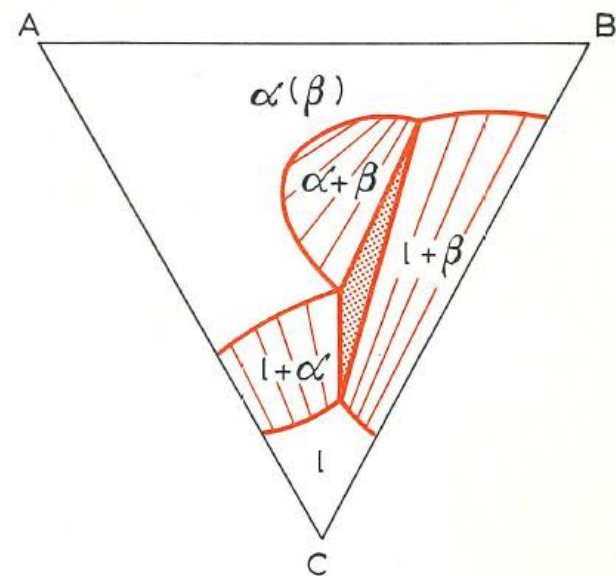
isothermal section



$T = P_1$



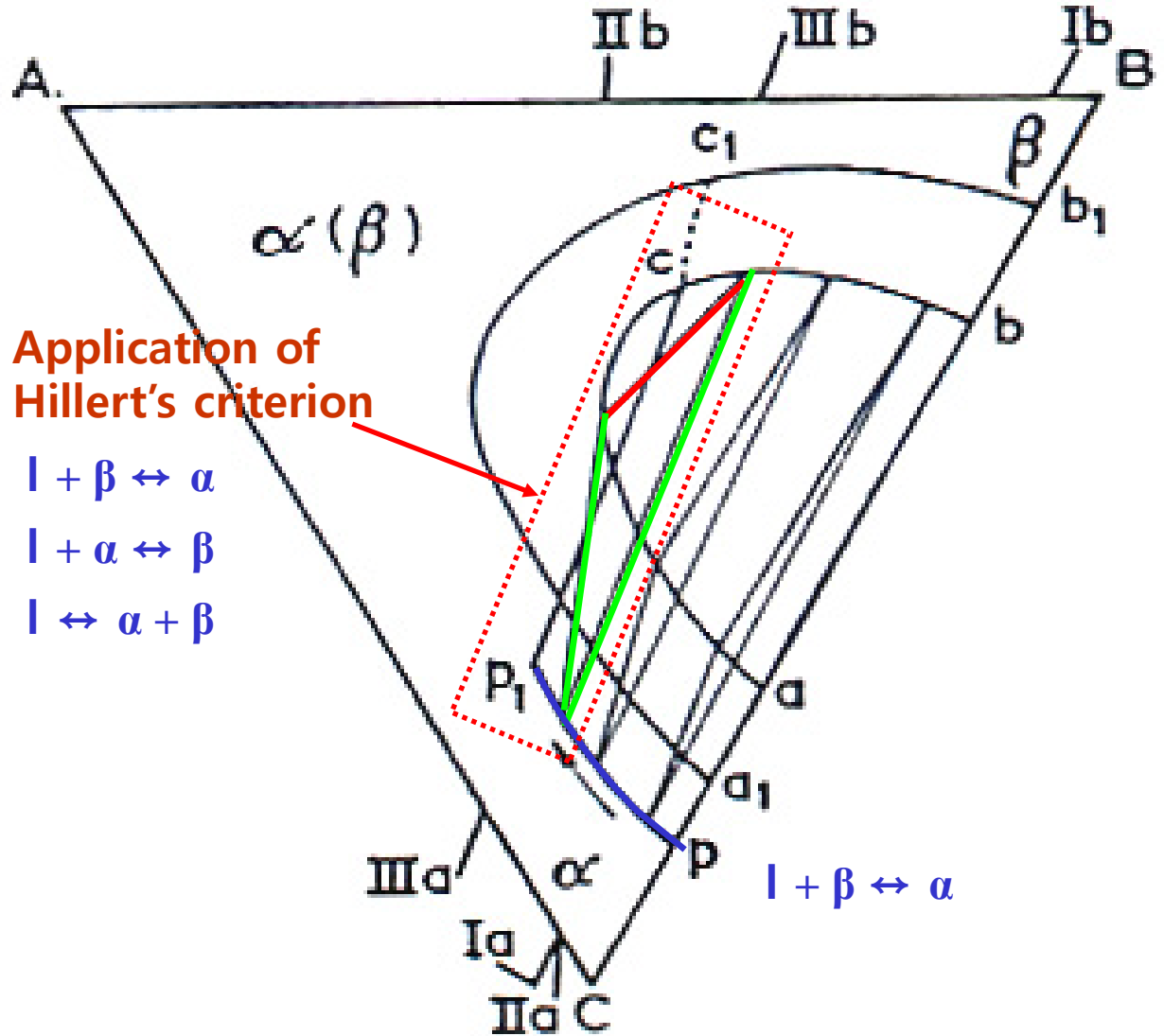
$P_1 > T_1 > P$



$T_1 > T_2 > P$

9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

- A peritectic solubility gap in one binary system



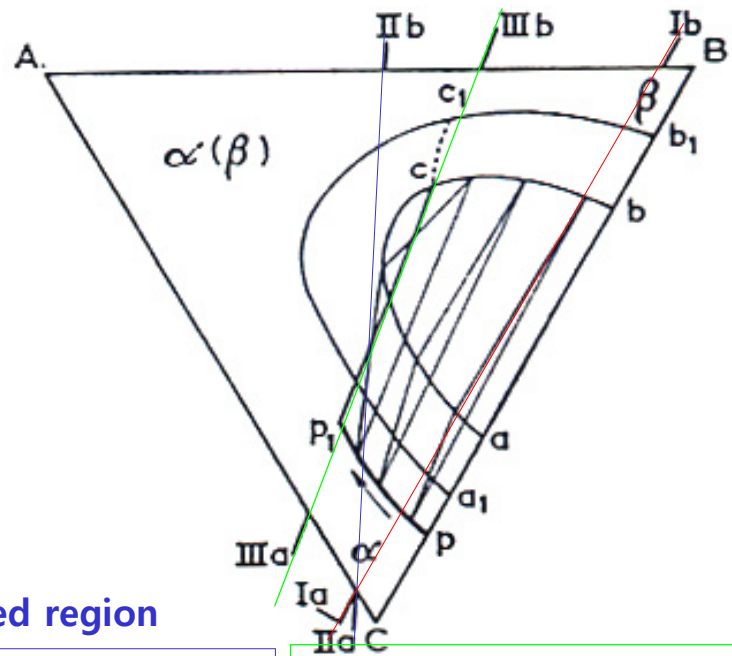
Application of Hillert's criterion

- $l + \beta \leftrightarrow \alpha$
- $l + \alpha \leftrightarrow \beta$
- $l \leftrightarrow \alpha + \beta$

$l + \beta \leftrightarrow \alpha$

9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

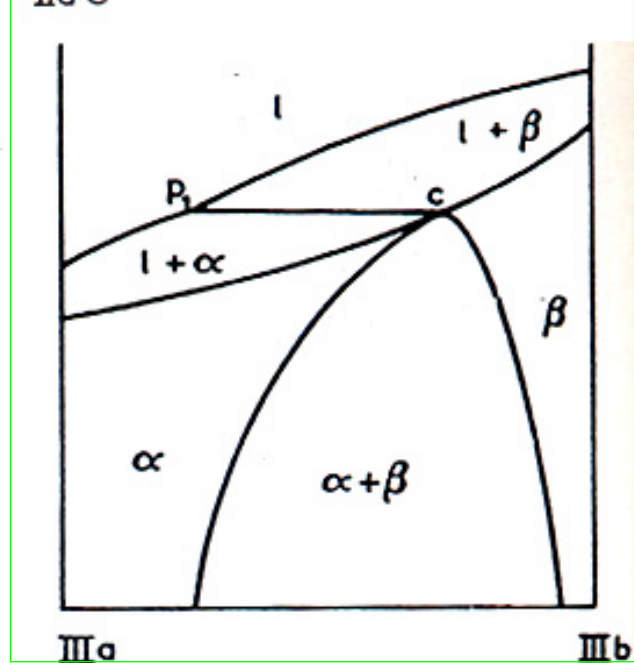
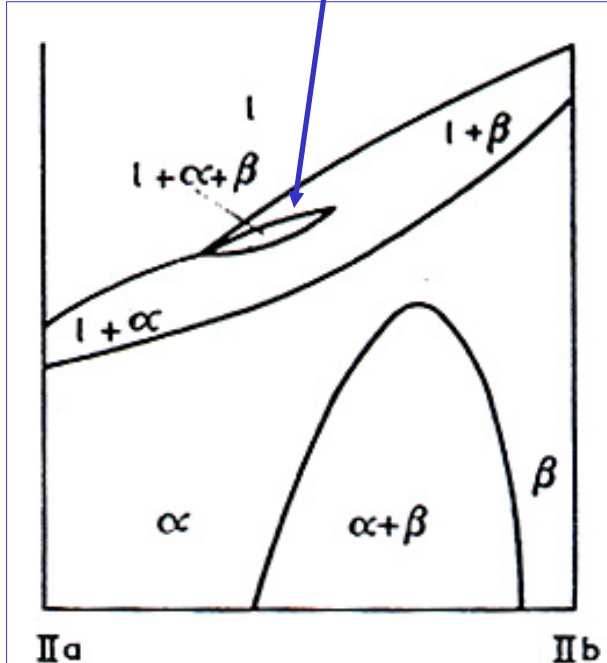
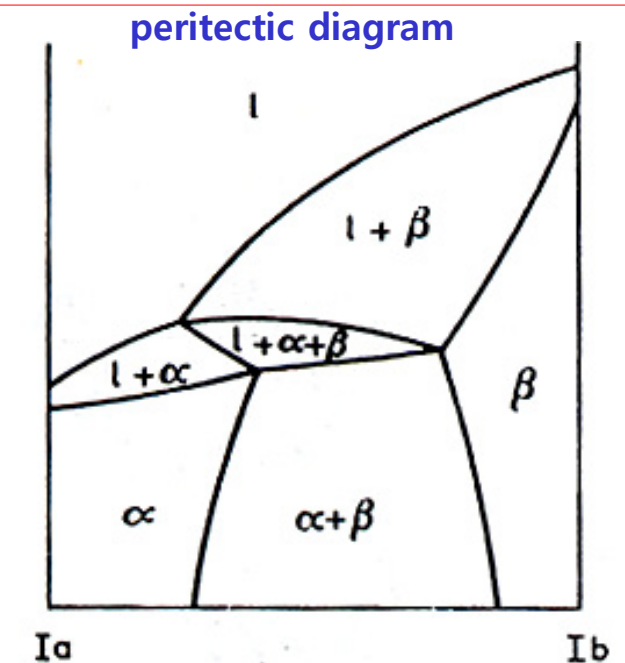
- A peritectic solubility gap in one binary system



<vertical section>

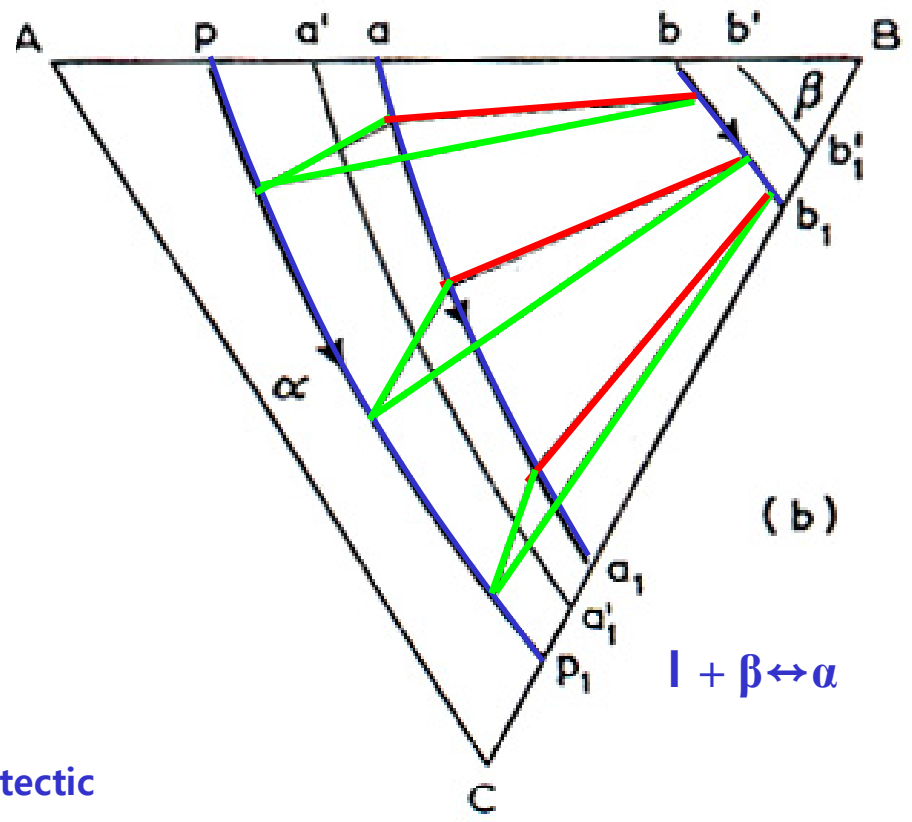
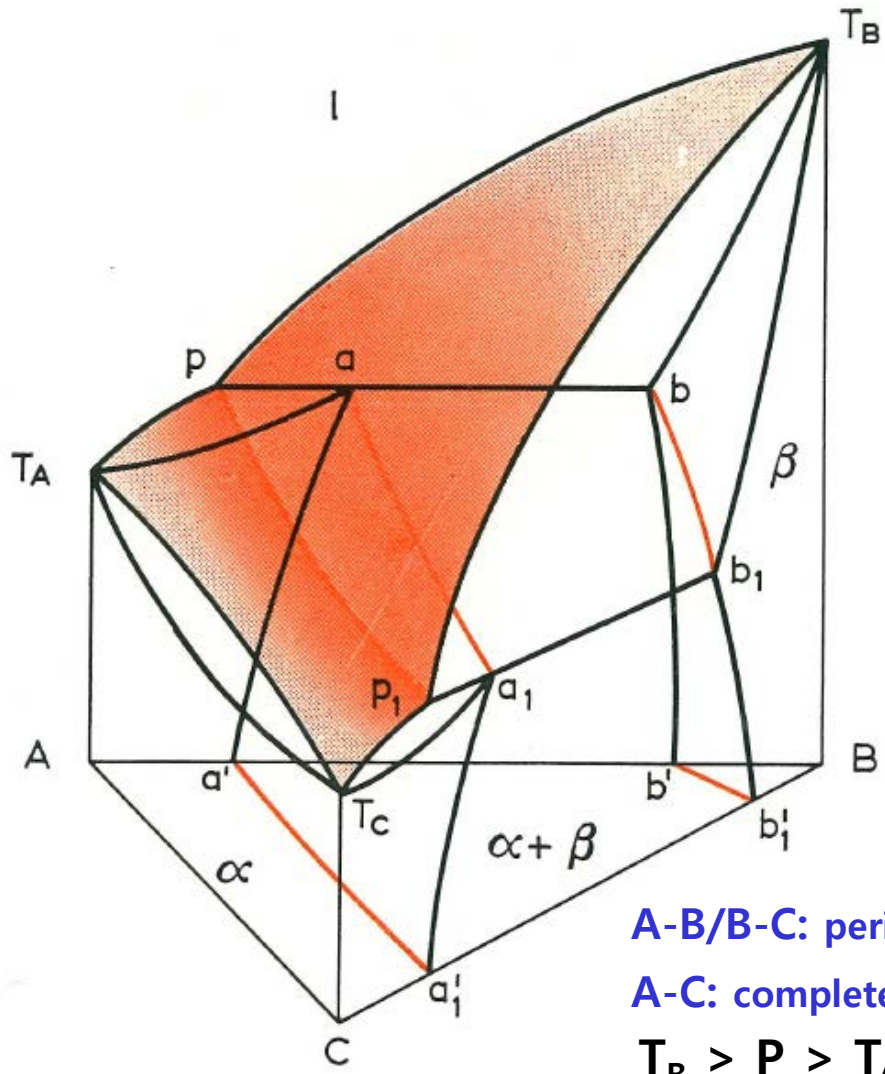
Similar to the binary peritectic diagram

loop shaped region

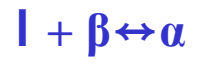


9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

- A peritectic solubility gap in two binary system



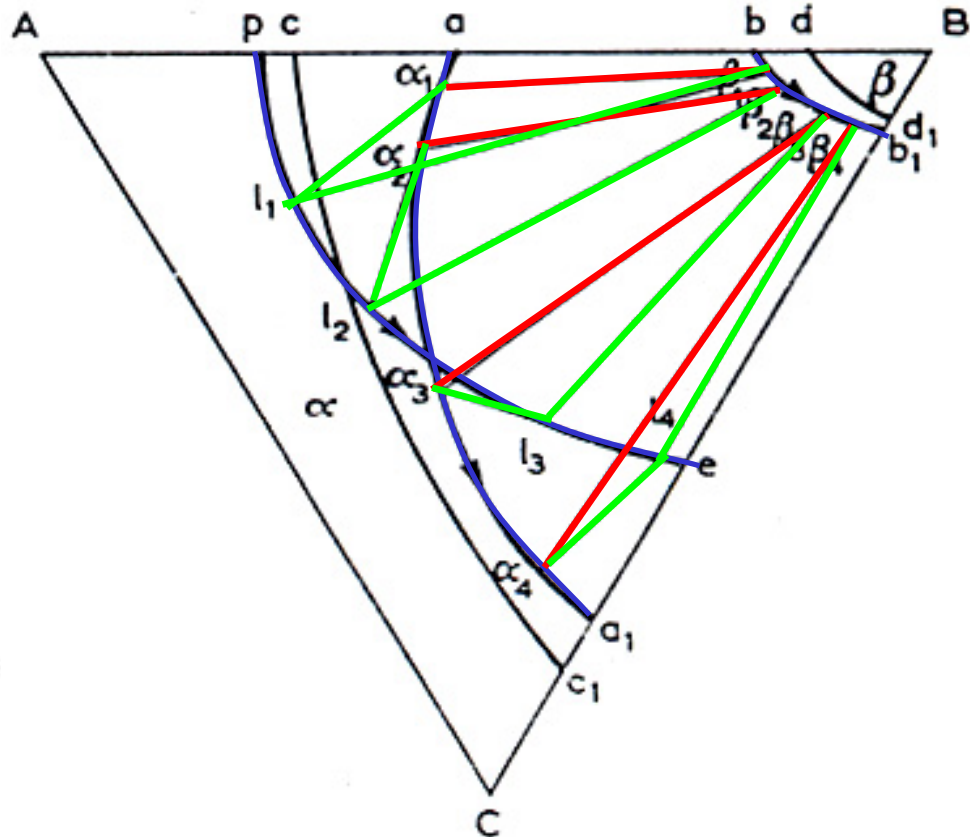
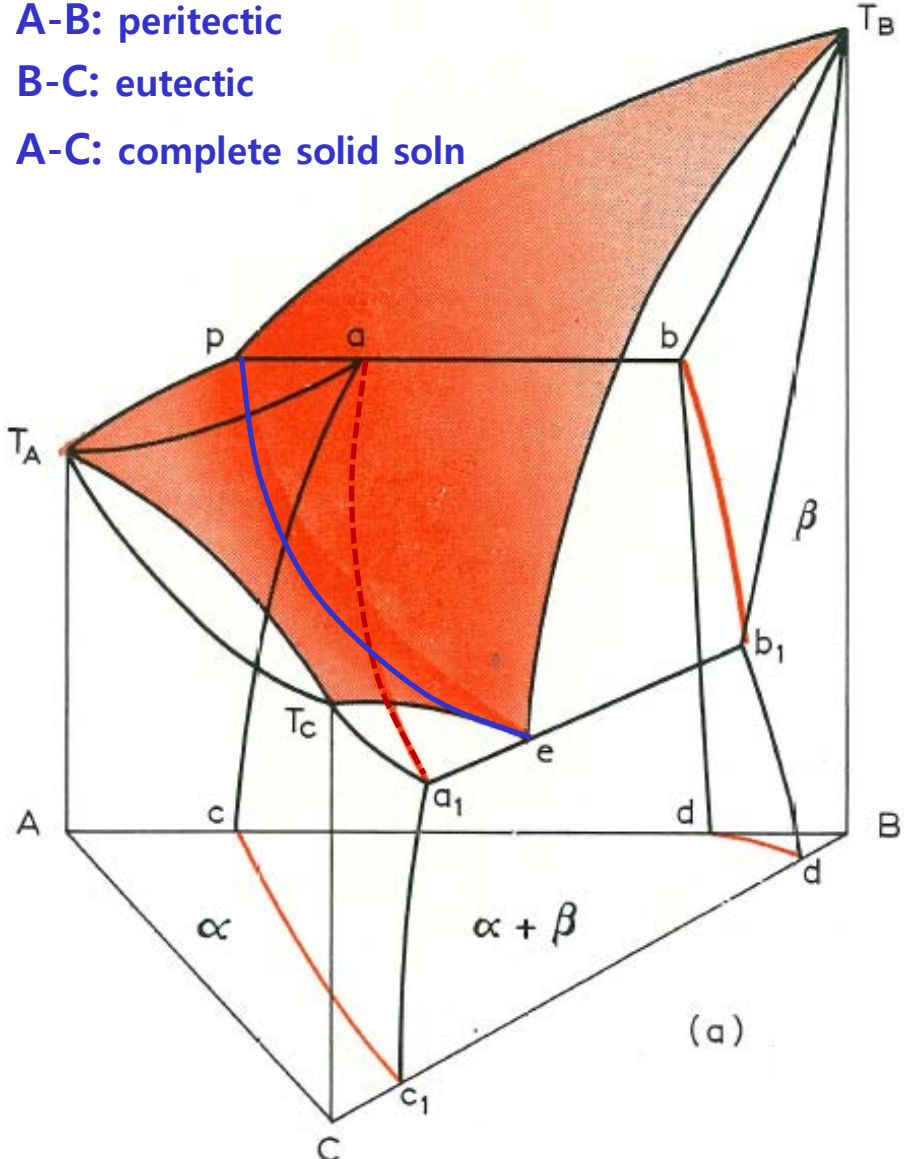
A-B/B-C: peritectic
A-C: complete solid soln
 $T_B > P > T_A > P_1 > T_C$



9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

- A transition from a binary eutectic to a binary peritectic reaction

A-B: peritectic
 B-C: eutectic
 A-C: complete solid soln

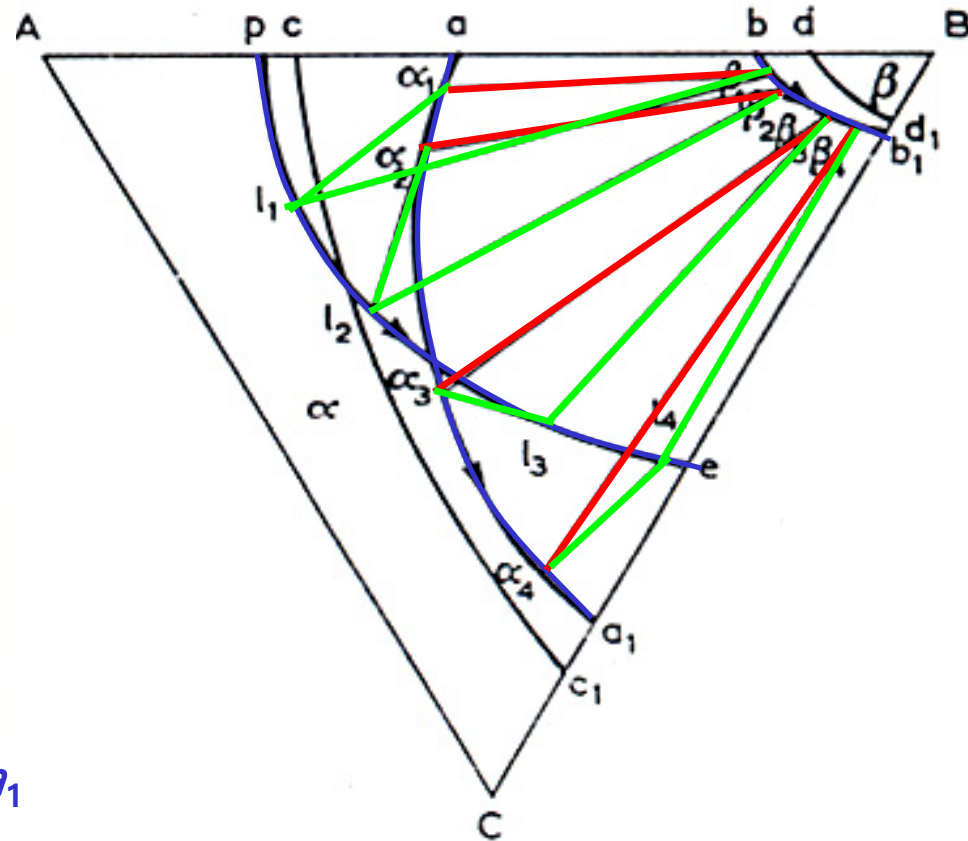
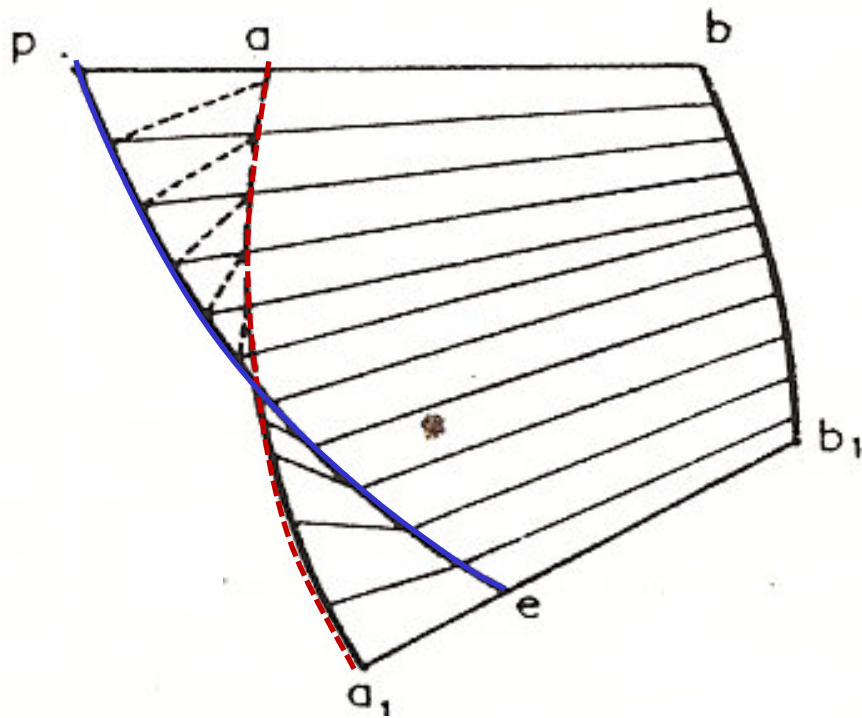


$$T_B > P > T_A > T_C > e$$

9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

- A transition from a binary eutectic to a binary peritectic reaction

$$T_B > P > T_A > T_C > e$$



- curve pe always lies above curve aa_1
- Tie lines are drawn on the $l\beta$ and $l\alpha$ surfaces only.
- By Hillert to show that the transition from a peritectic to a eutectic reaction does not occur at a unique temperature.

9.4. THREE-PHASE EQUILIBRIUM INVOLVING PERITECTIC REACTIONS

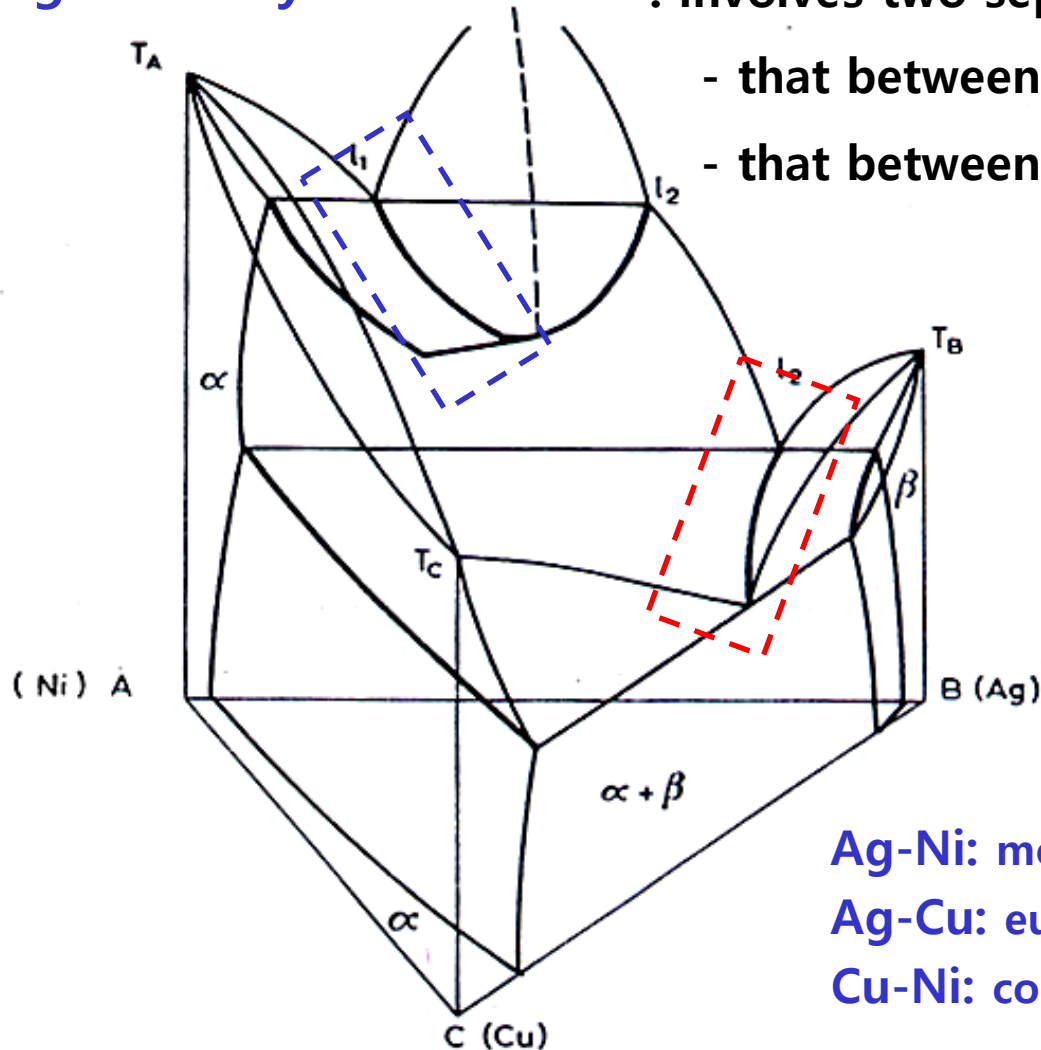
- Binary Monotectic, syntectic and metatectic reactions in combination with each other as well as with binary eutectic and peritectic reactions.

- **Ag-Cu-Ni system**

: involves two separate three phase equilibria

- that between α , l_1 and l_2 , and

- that between α , β and l_2



Ag-Ni: monotectic

Ag-Cu: eutectic

Cu-Ni: complete solid soln

Chapter 10. Ternary phase Diagrams

Four-Phase Equilibrium

- a. **THE TERNARY EUTECTIC EQUILIBRIUM** ($l = \alpha + \beta + \gamma$)

- b. **THE QUASI-PERITECTIC EQUILIBRIUM** ($l + \alpha = \beta + \gamma$)

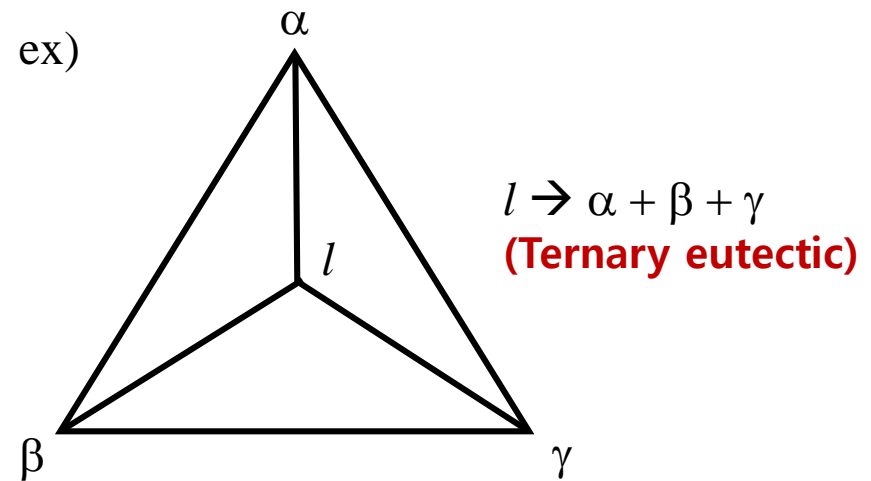
- c. **THE TERNARY PERIECTIC EQUILIBRIUM** ($l + \alpha + \beta = \gamma$)

10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

Three phase equil. ($f = 1$) - eutectic, peritectic

Now we consider of four-phase equilibrium

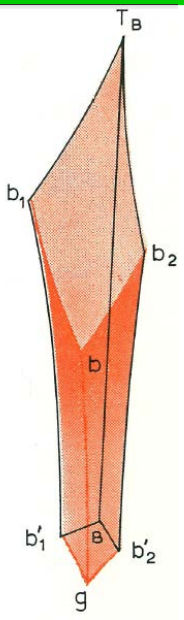
- max N of phase
- $f = 0$: composition of four phases at temp. \rightarrow fixed
- isothermal four phase regions



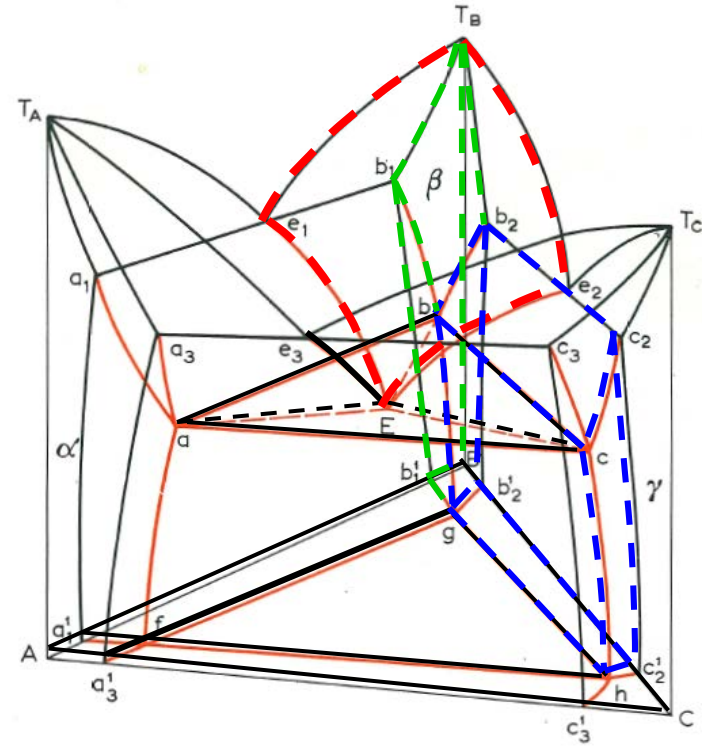
cf) $l + \alpha \rightarrow \beta + \gamma$: **ternary quasi-peritectic**
 $l + \alpha + \beta \rightarrow \gamma$: **ternary peritectic**

10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

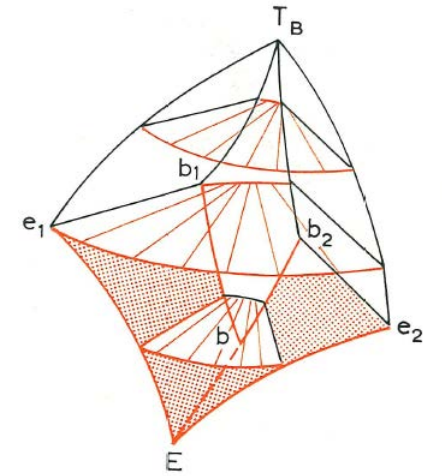
Ternary eutectic



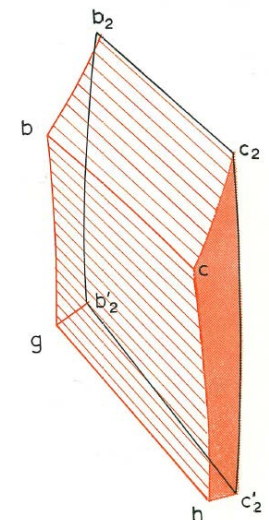
β phase region



(a)



$(l + \beta)$ phase region

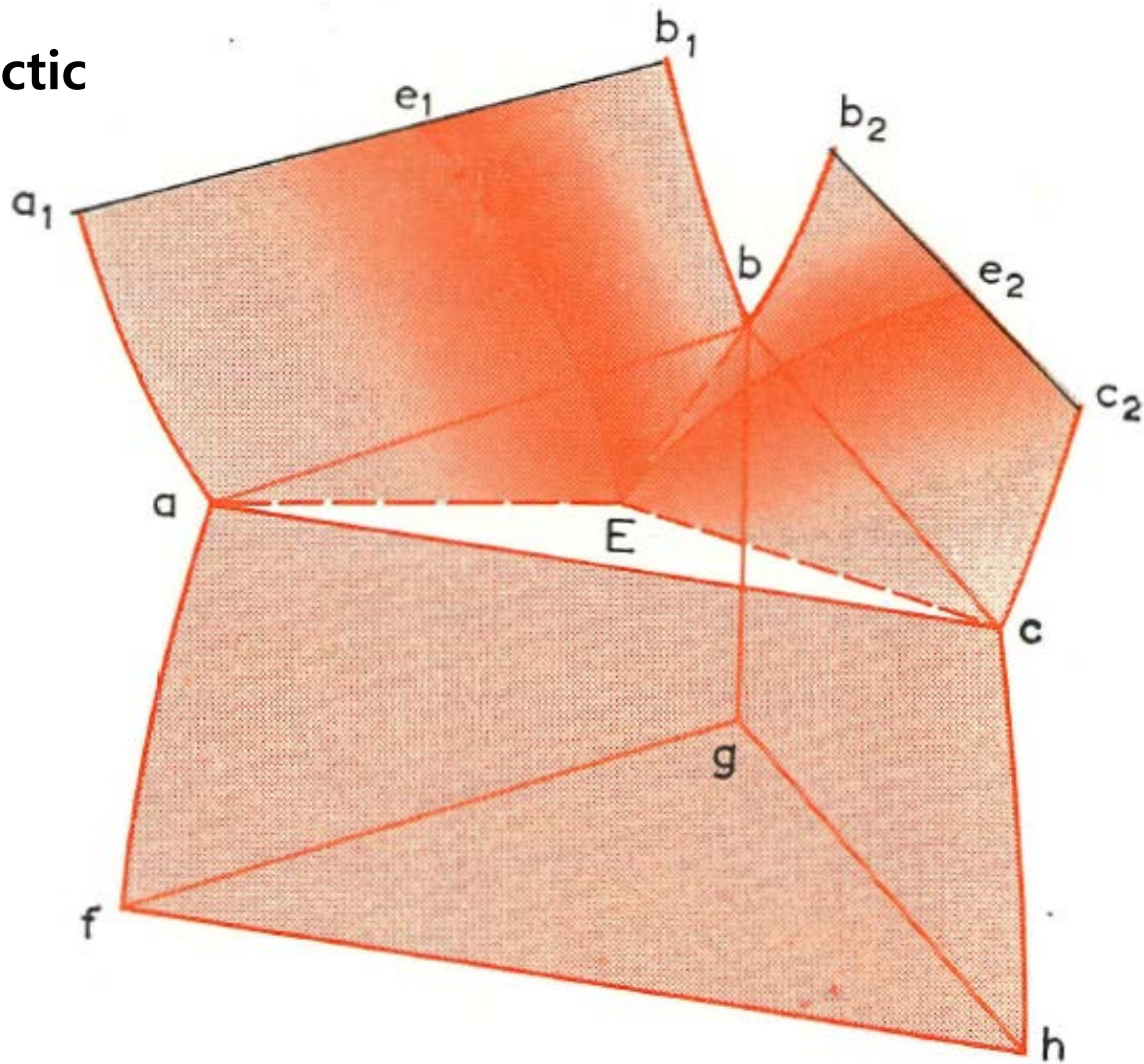


$(\beta + \gamma)$ phase region

$$T_A > T_B > T_C > e_1 > e_3 > e_2 > E$$

10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

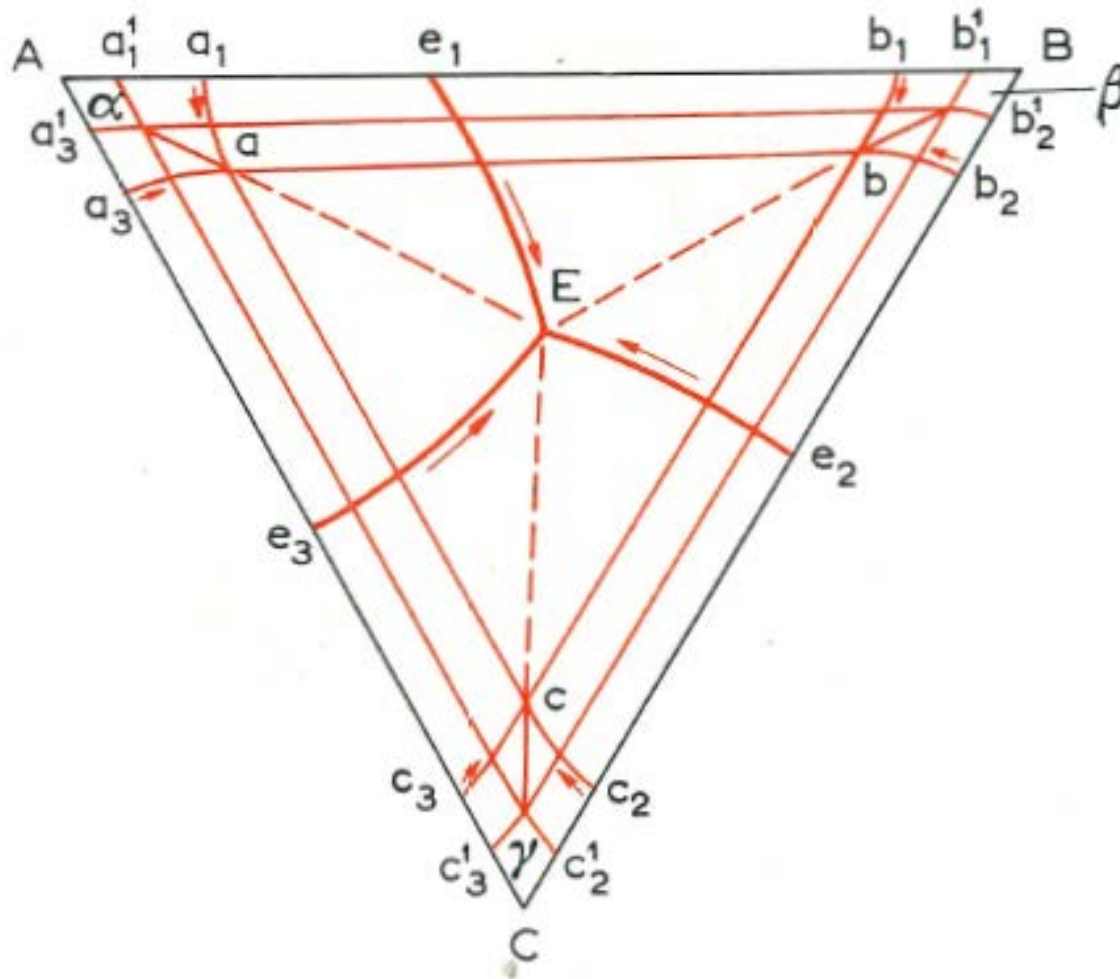
Ternary eutectic



The eutectic four-phase plane as the junction of four tie triangles

10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

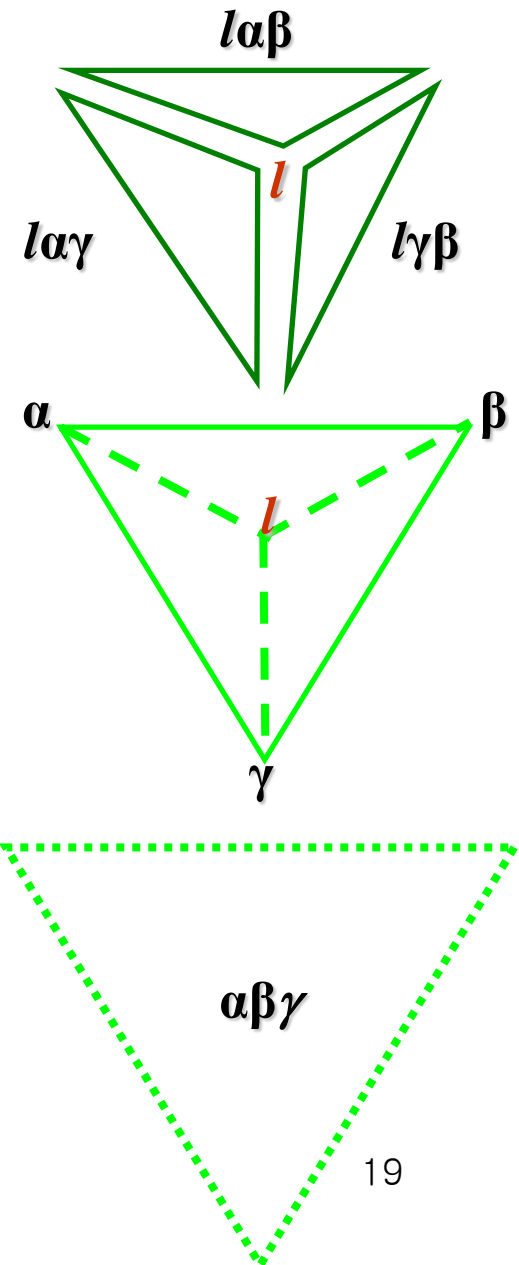
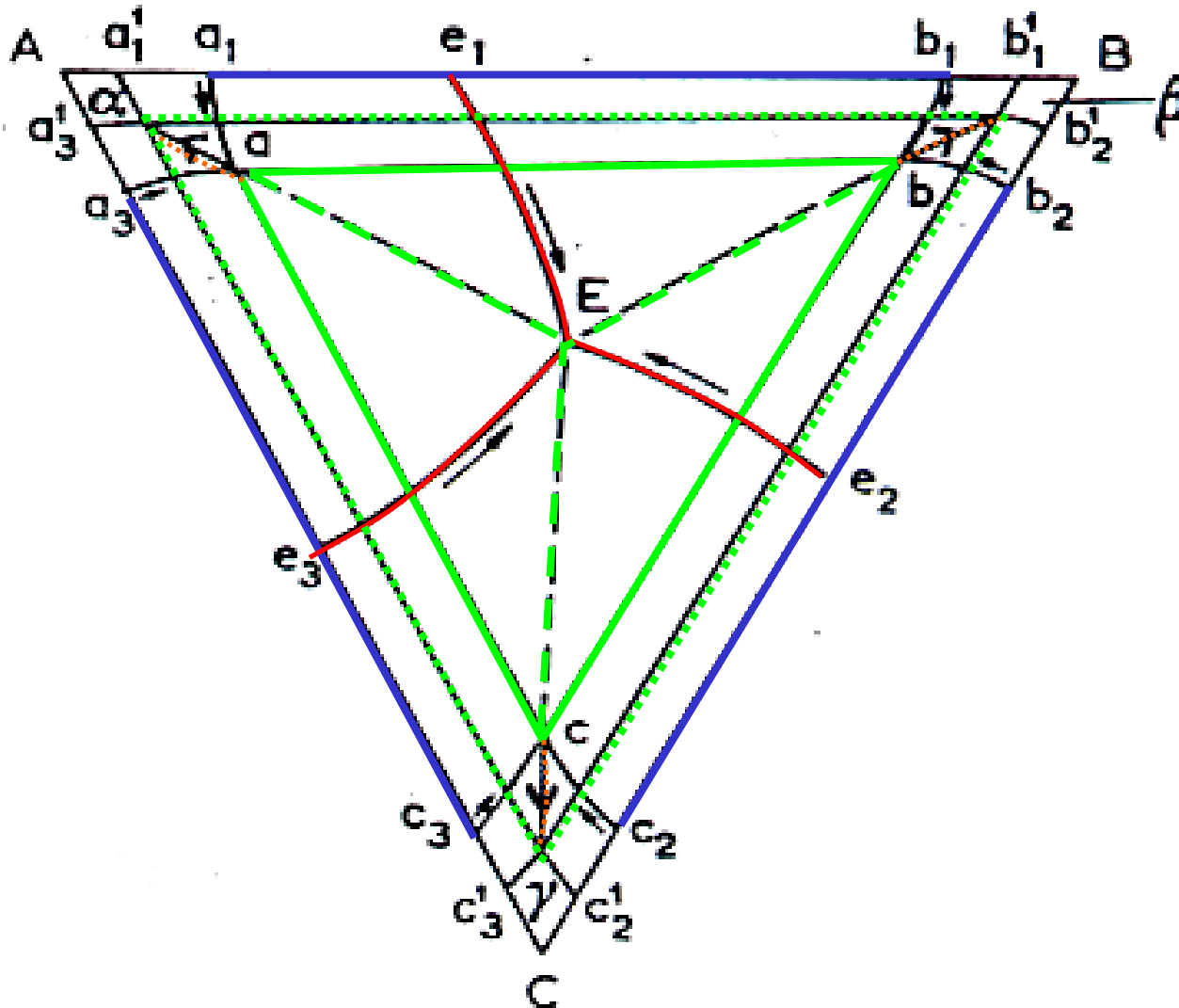
Ternary eutectic • Projection : solid solubility limit surface
: monovariant liquidus curve



$$T_A > T_B > T_C > e_1 > e_3 > e_2 > E$$

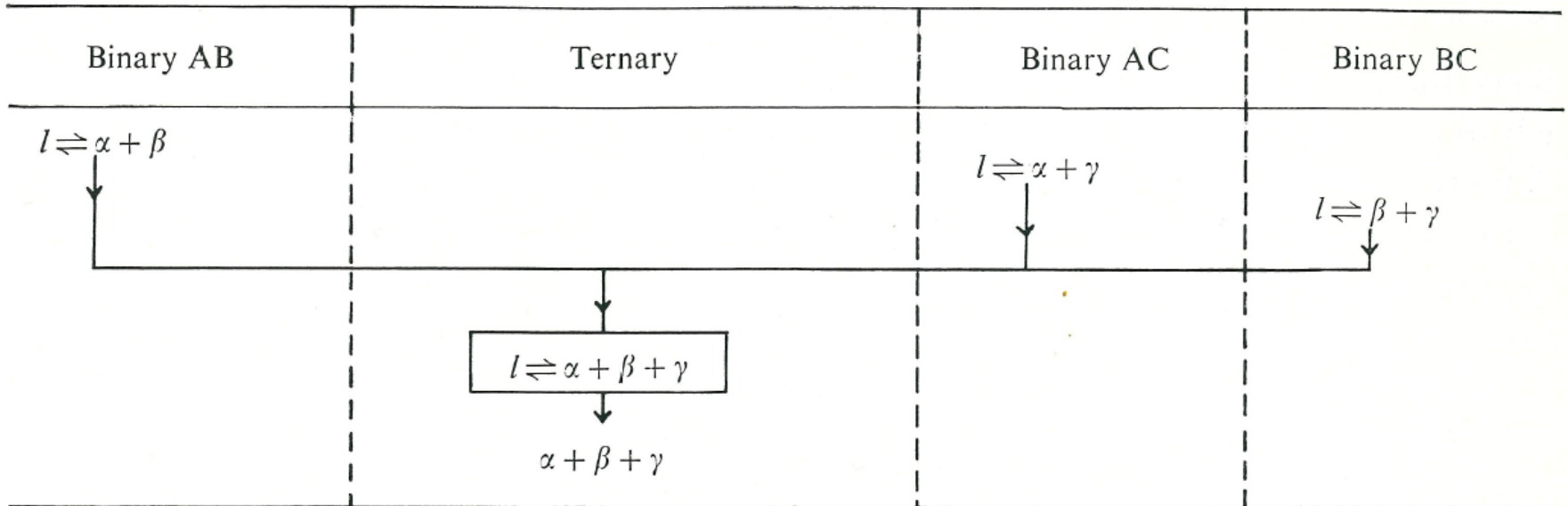
THE TERNARY EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

- **Projection** : solid solubility limit surface
: monovariant liquidus curve

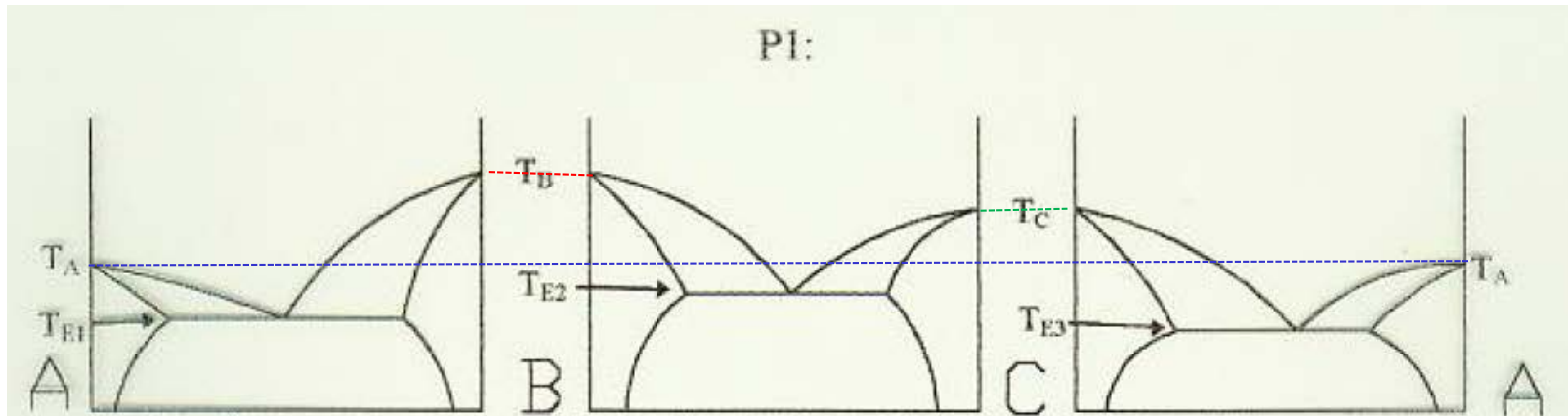


Tabular representation of ternary equilibria:
interlinks the binary and ternary reactions in tabular form

EUTECTIC EQUILIBRIUM $l \rightleftharpoons \alpha + \beta + \gamma$



Ternary Eutectic System (with Solid Solubility)



T_A : Melting Point Of Material A

T_B : Melting Point Of Material B

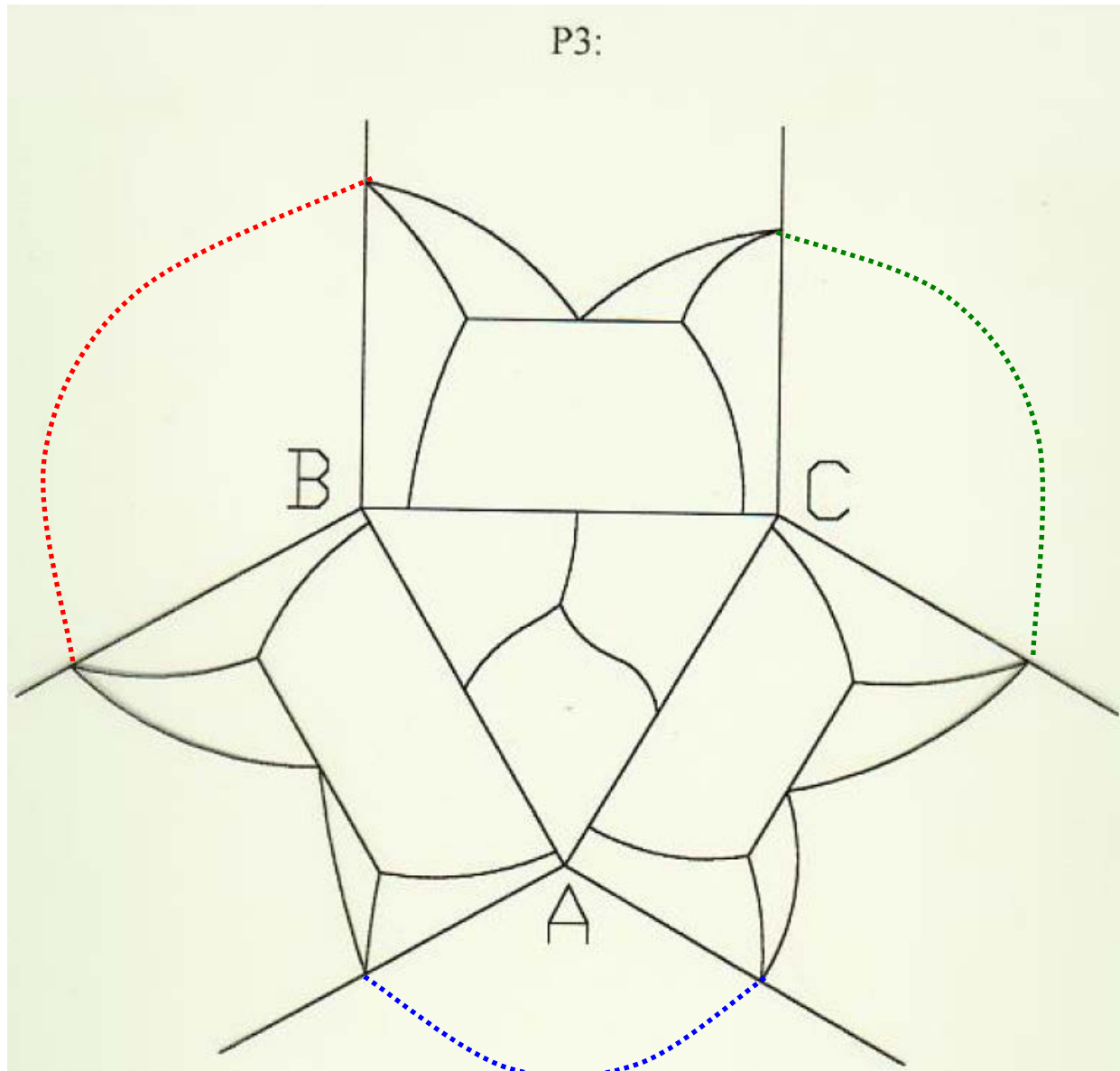
T_C : Melting Point Of Material C

T_{E1} : Eutectic Temperature Of A-B

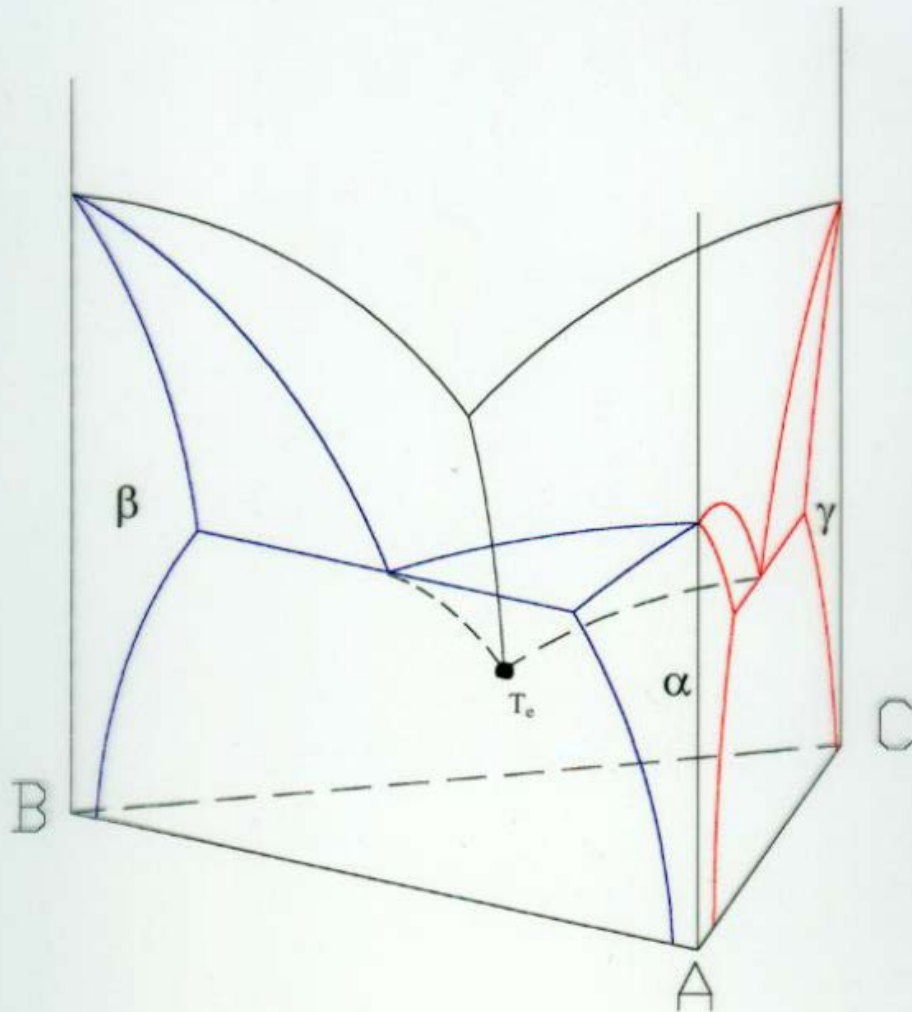
T_{E2} : Eutectic Temperature Of B-C

T_{E3} : Eutectic Temperature Of C-A

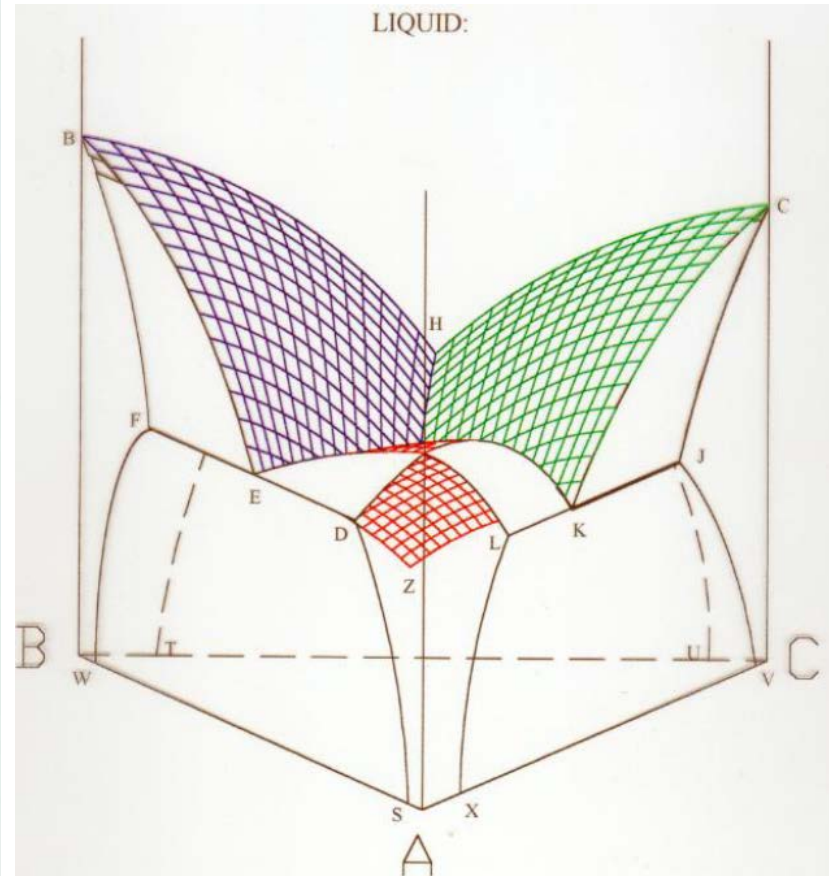
Ternary Eutectic System (with Solid Solubility)



Ternary Eutectic System (with Solid Solubility)

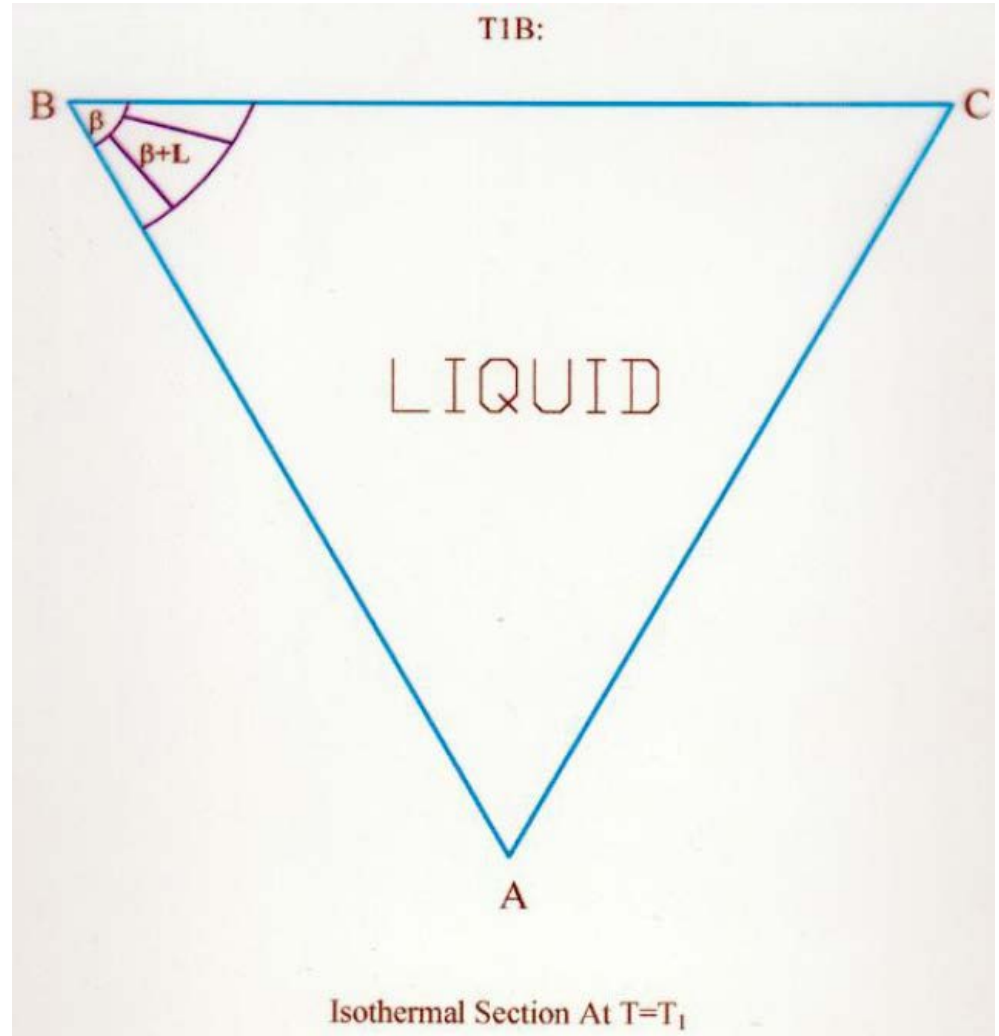
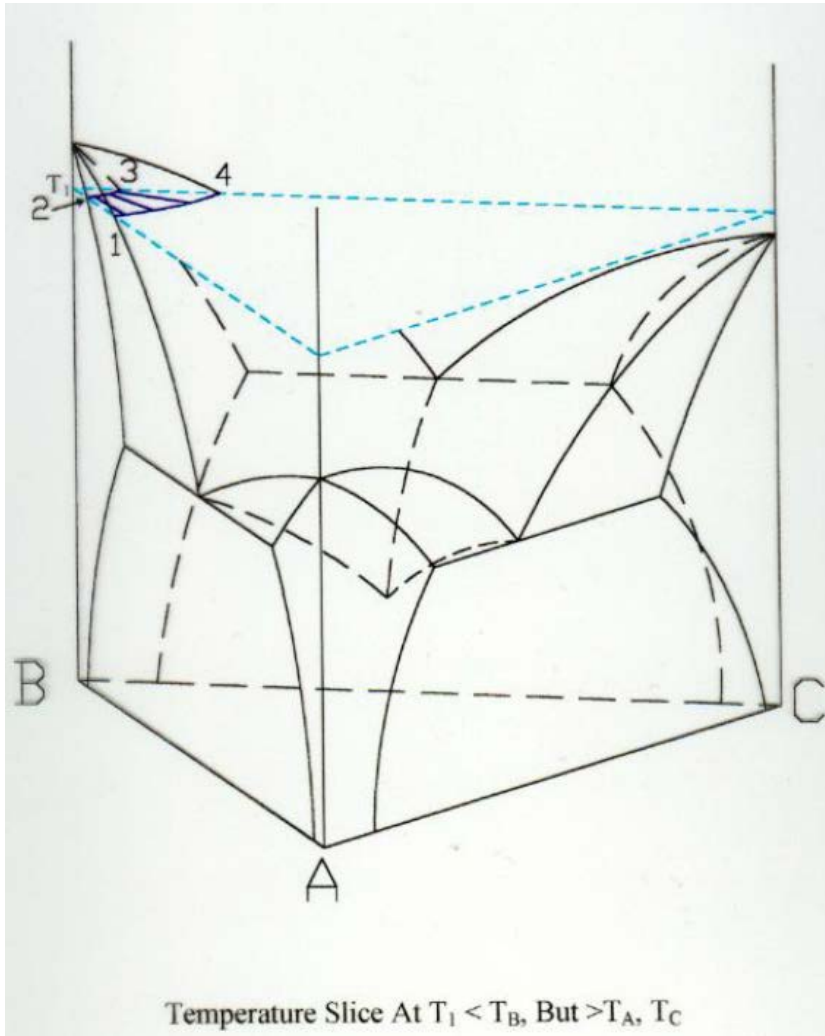


Main outline of Ternary Phase Diagram with Ternary Eutectic (T_e) and Solid Single Phase Regions Shown



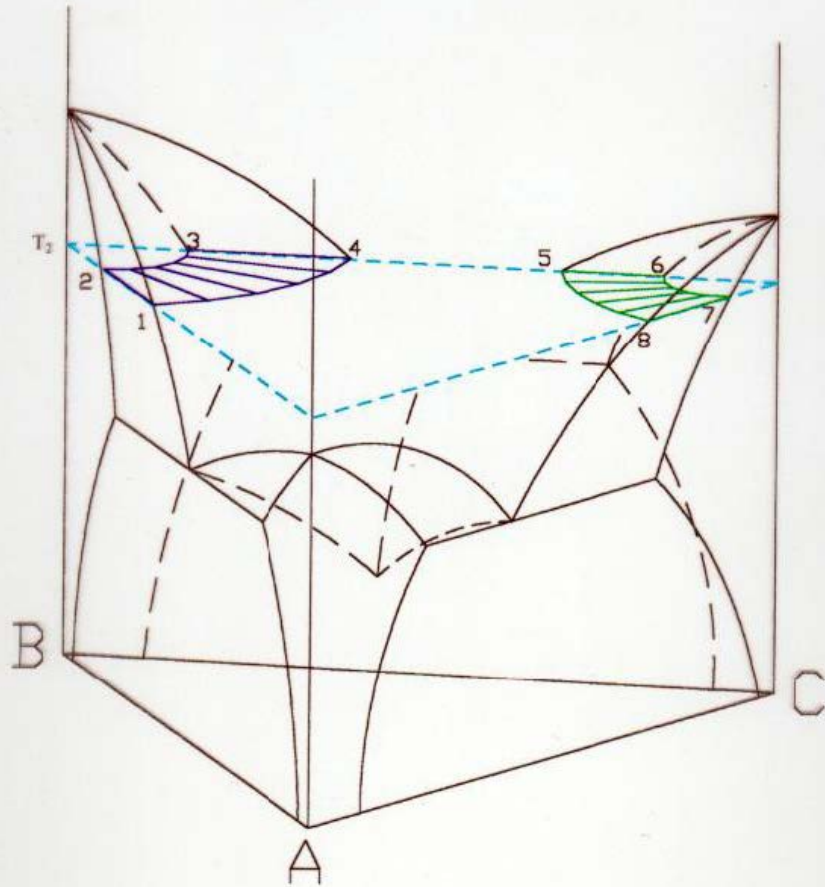
All Liquidus surfaces ($\alpha+L$ -Red, $\beta+L$ -Purple, $\gamma+L$ -Green)

Ternary Eutectic System (with Solid Solubility)



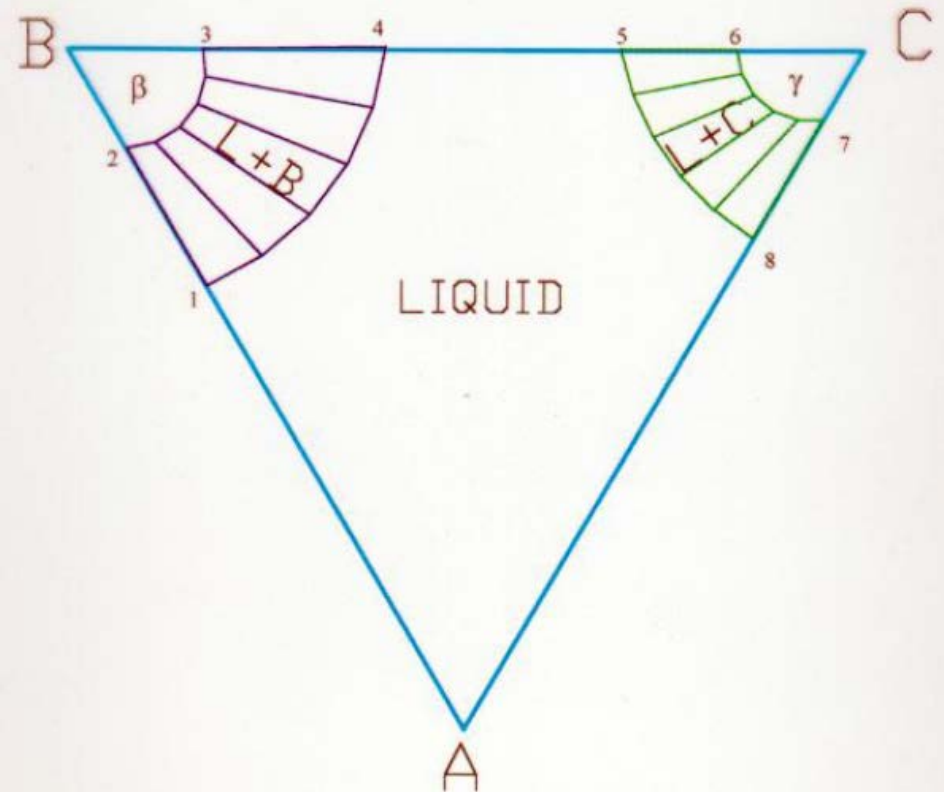
Ternary Eutectic System (with Solid Solubility)

T2A



Temperature Slice At $T_2 > T_A$ But, $T_2 < T_B, T_C$

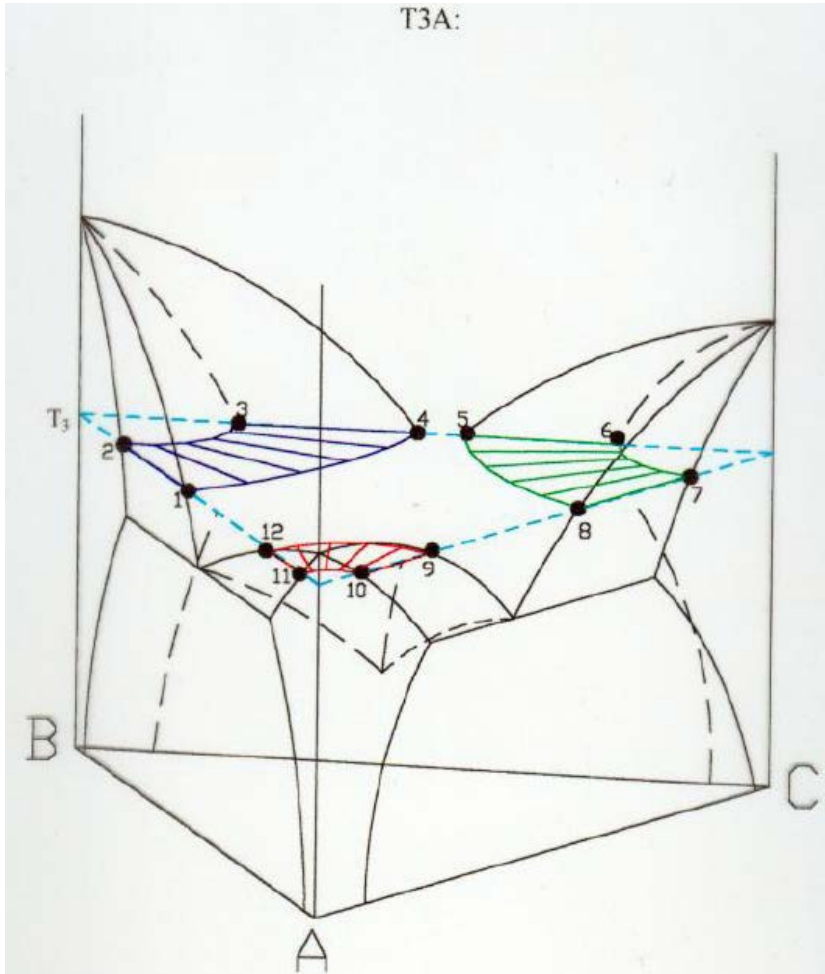
T2B



Isothermal Section At $T=T_2$

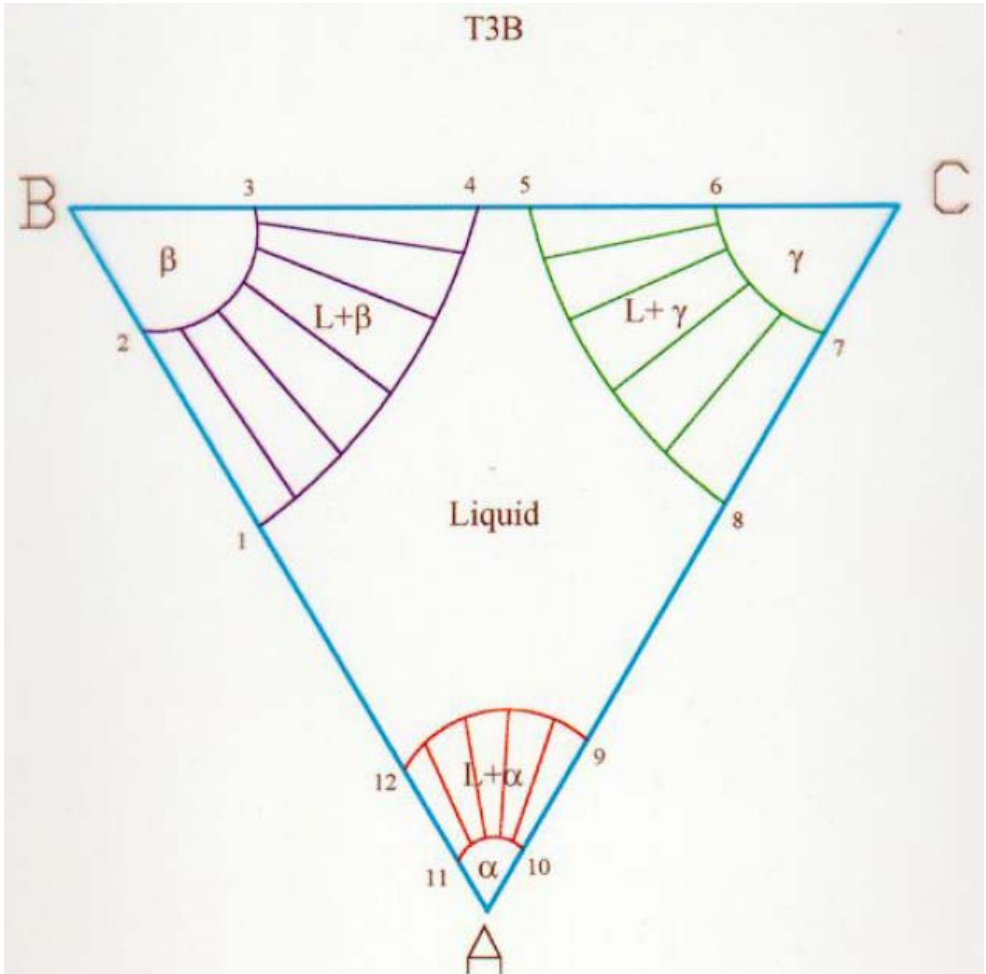
Ternary Eutectic System (with Solid Solubility)

T3A:



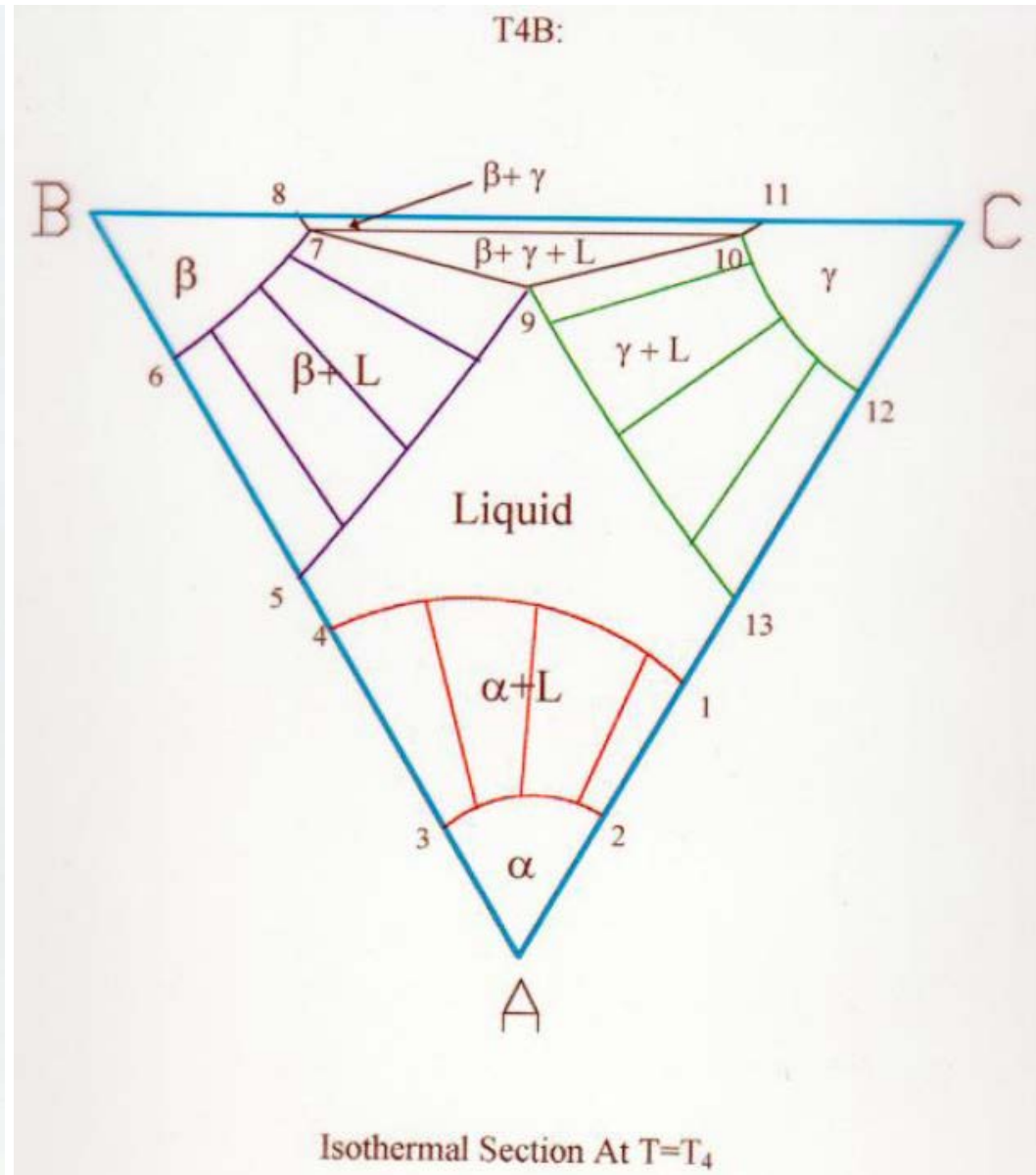
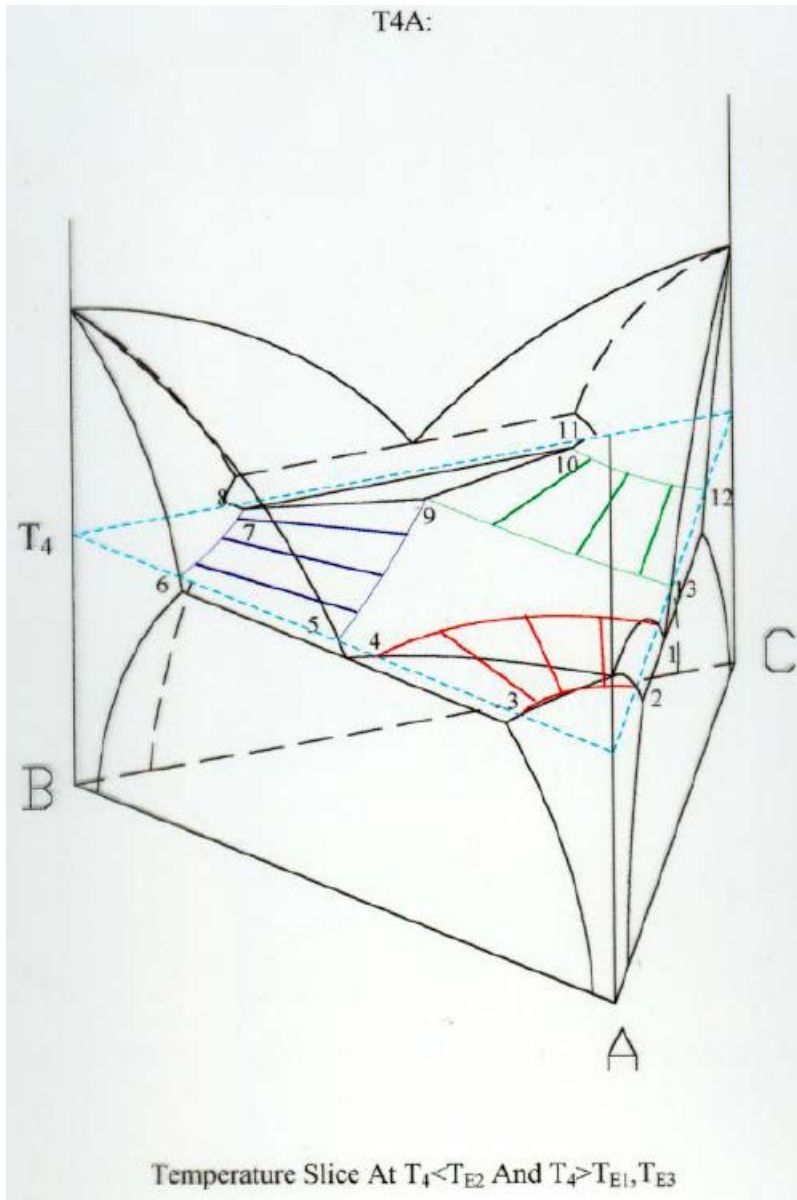
Temperature Slice At $T_3 < T_A, T_B, T_C$, But $T_3 > T_{E1}, T_{E2}, T_{E3}$

T3B



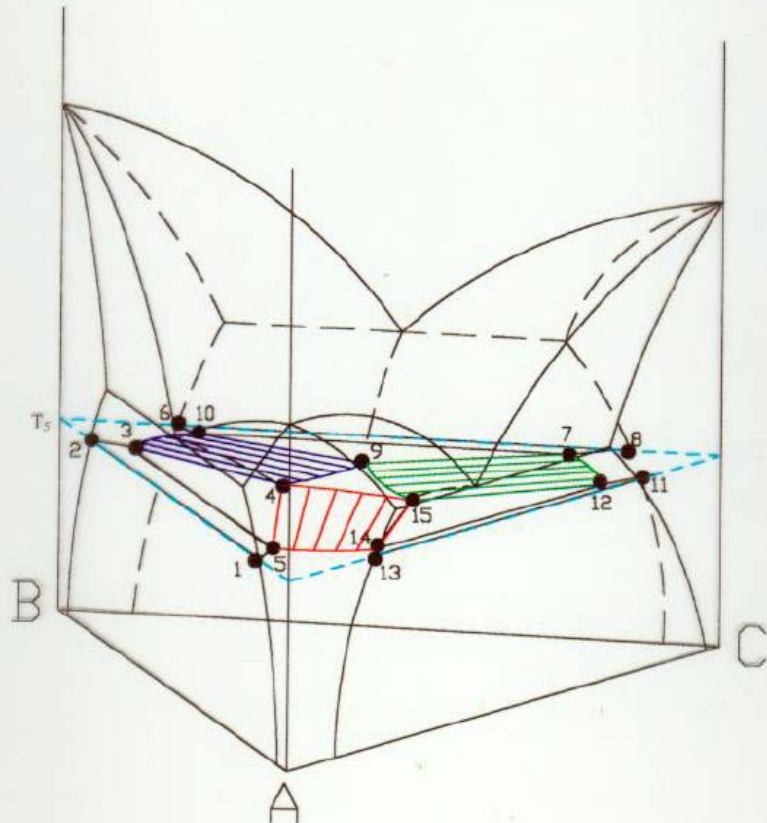
Isothermal Section At $T = T_3$

Ternary Eutectic System (with Solid Solubility)



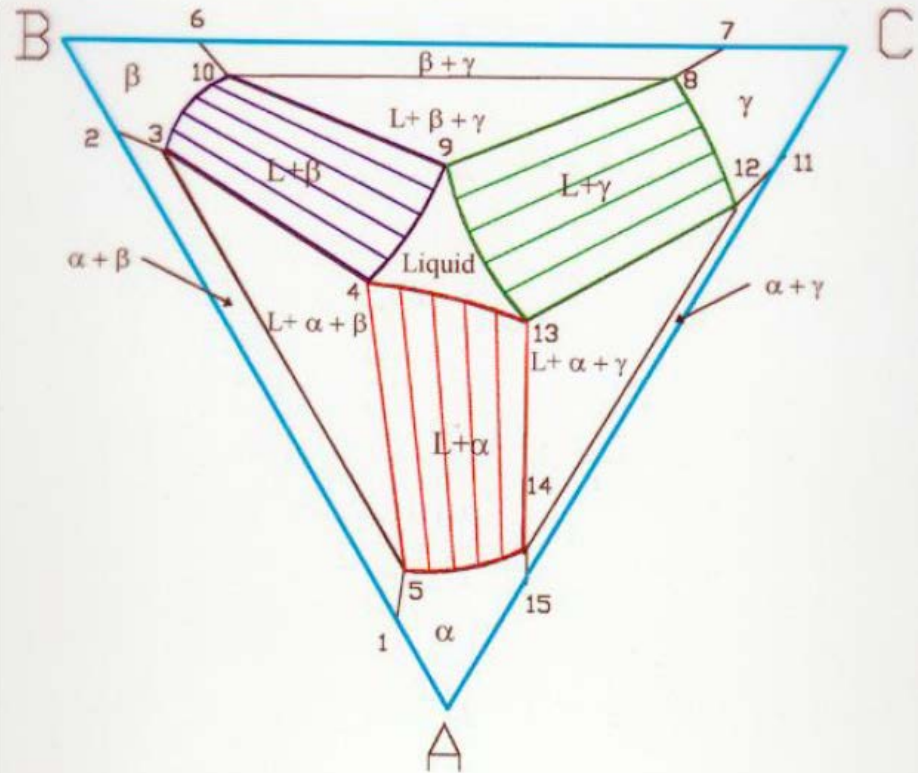
Ternary Eutectic System (with Solid Solubility)

T5A:



Temperature Slice Below All Binary Eutectics But, Above The Ternary Eutectic

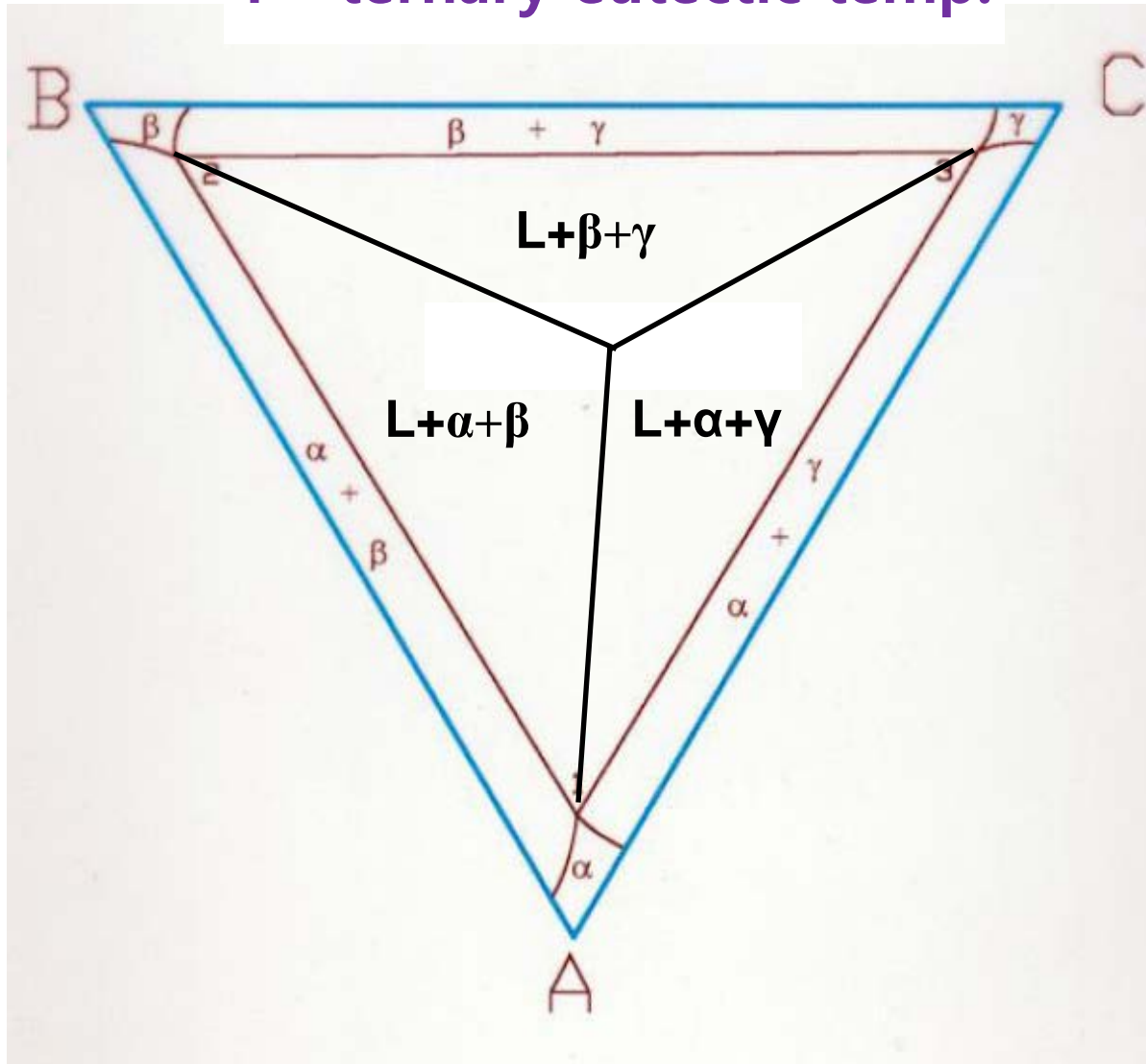
T5B:



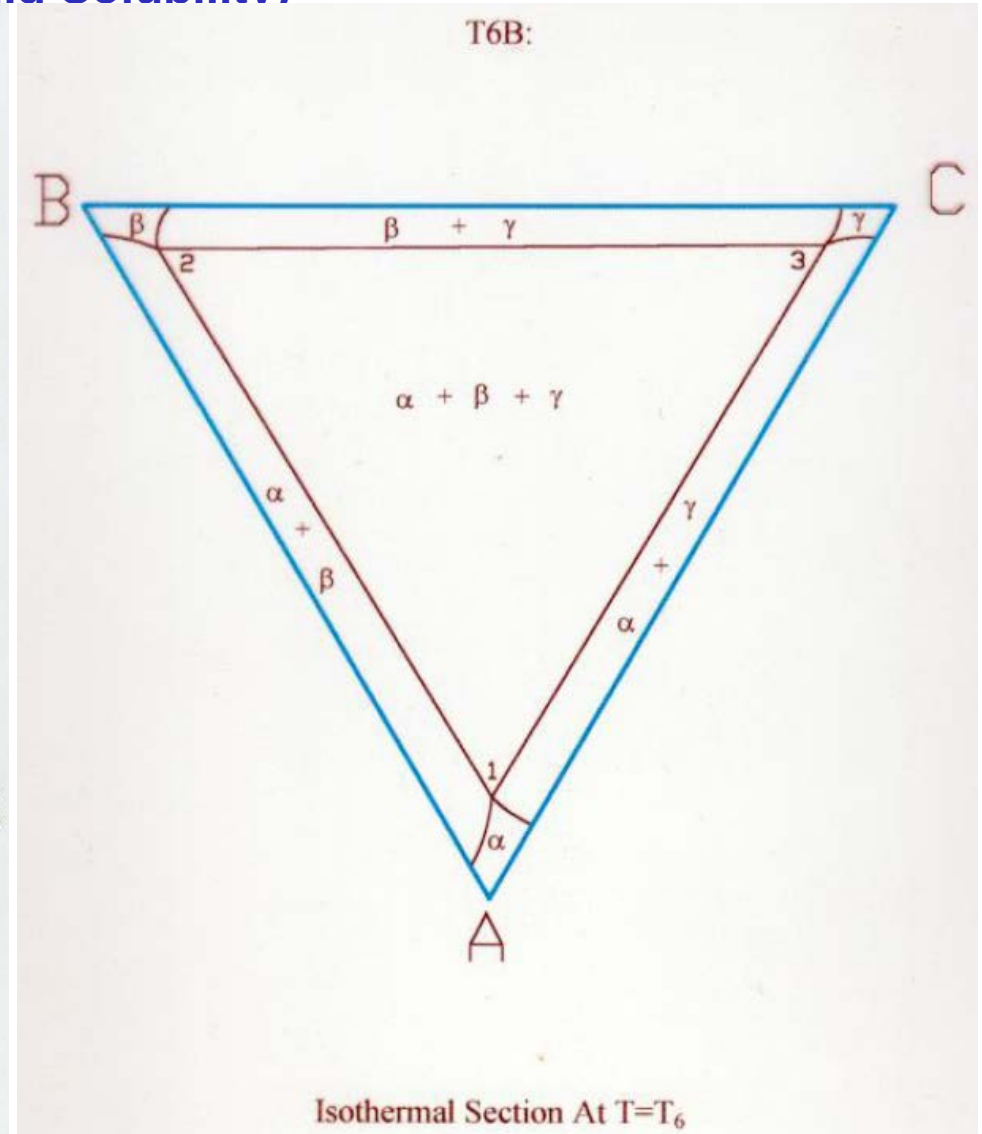
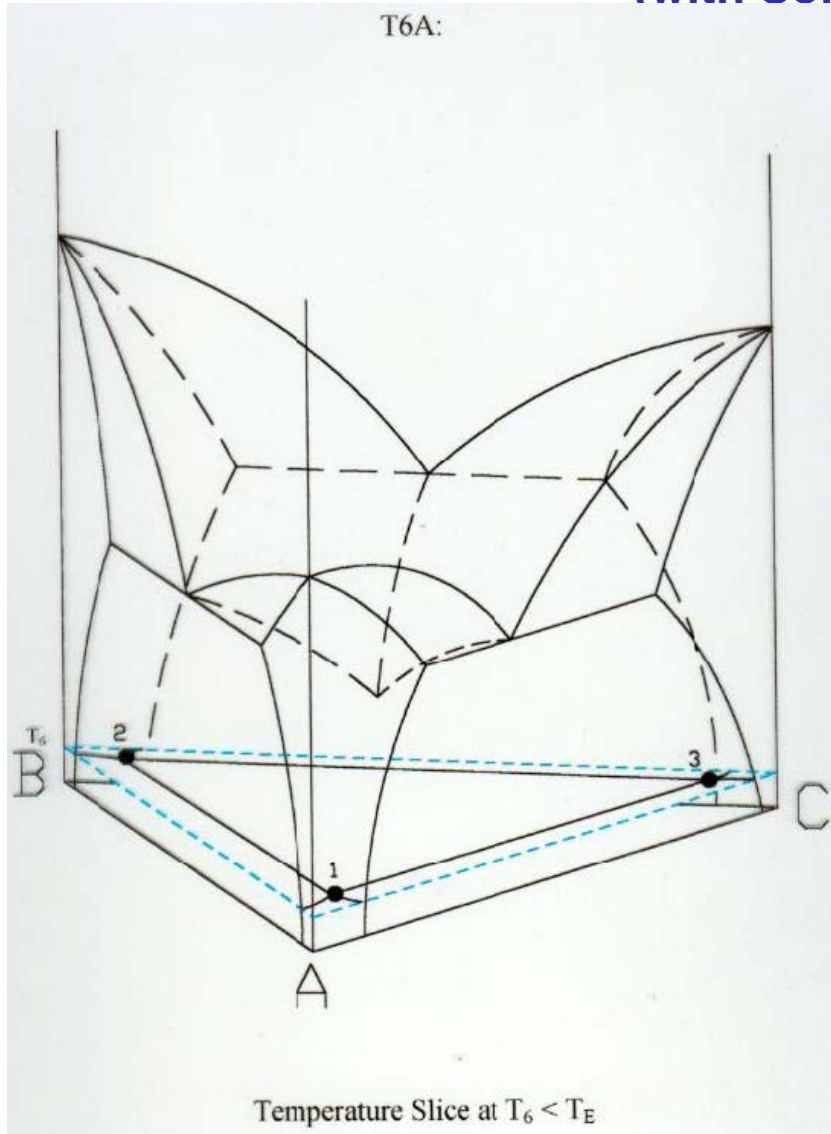
Isothermal Section At $T=T_5$

Ternary Eutectic System (with Solid Solubility)

$T =$ ternary eutectic temp.

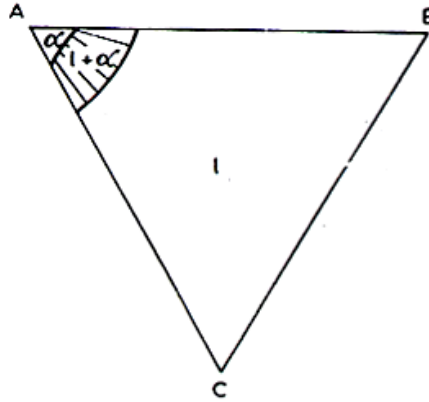


Ternary Eutectic System (with Solid Solubility)

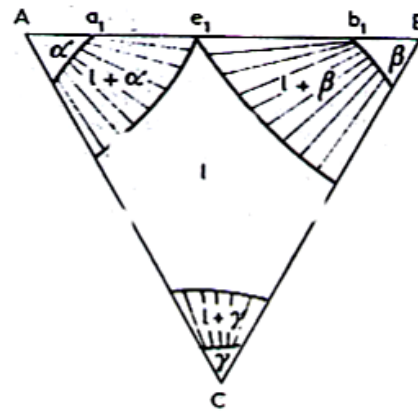


10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

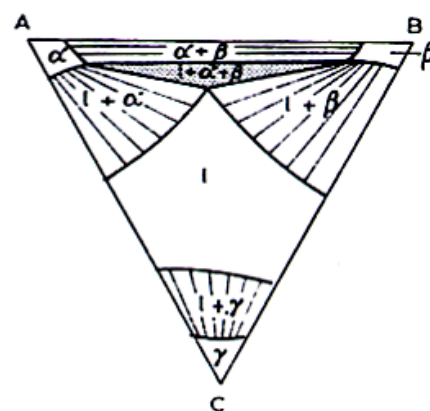
- Isothermal section ($T_A > T > T_B$)



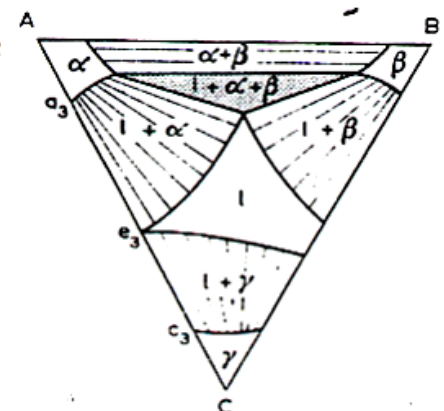
(a) $T_A > T > T_B$



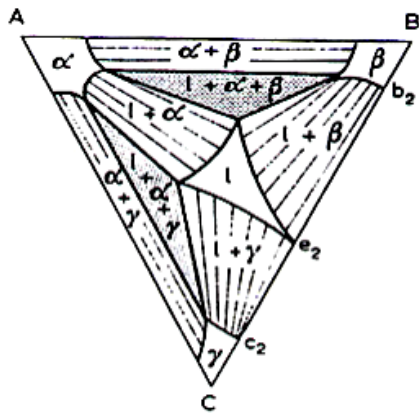
(b) $T = e_1$



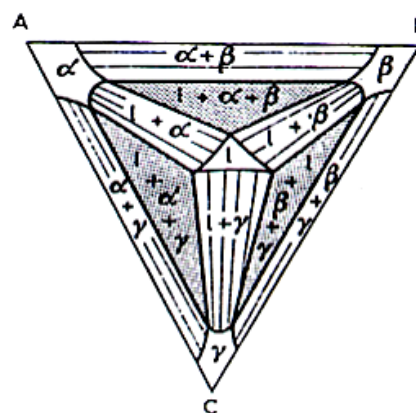
(c) $e_1 > T > e_3$



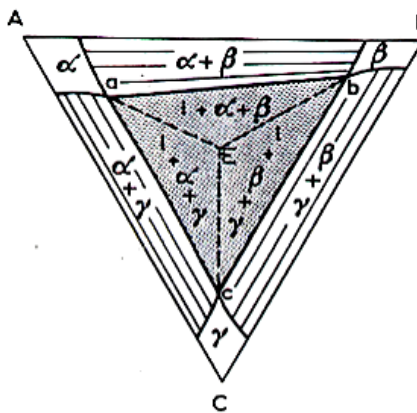
(d) $T = e_3$



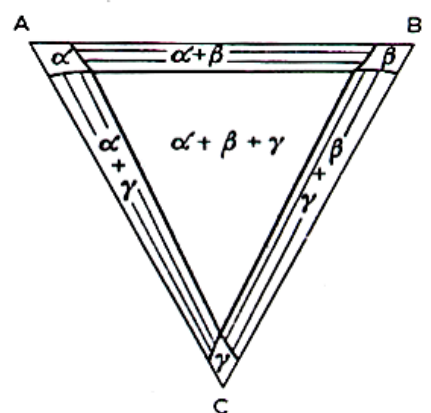
(e) $T = e_2$



(f) $e_2 > T > E$



(g) $T_A = E$



(h) $E = T$

10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

Vertical section

Location of vertical section

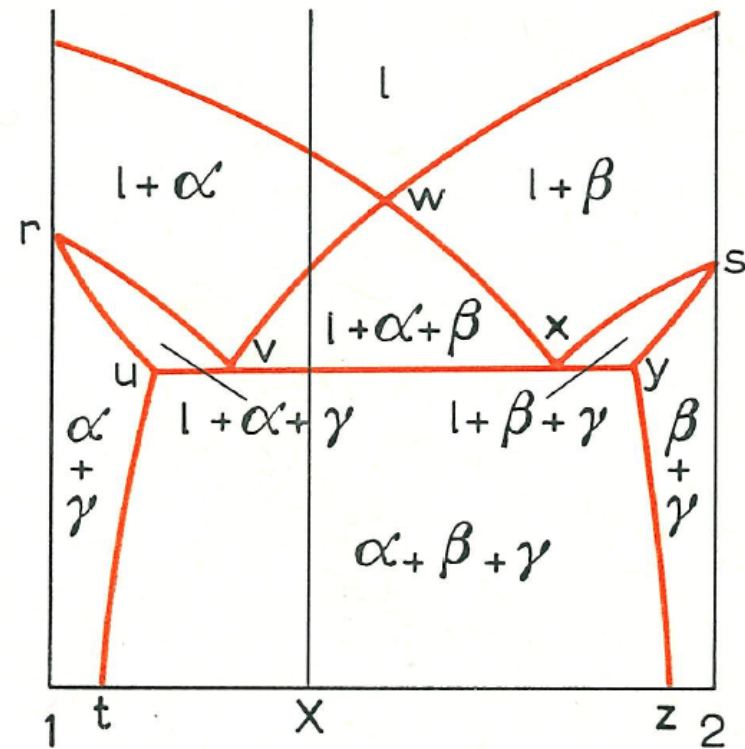
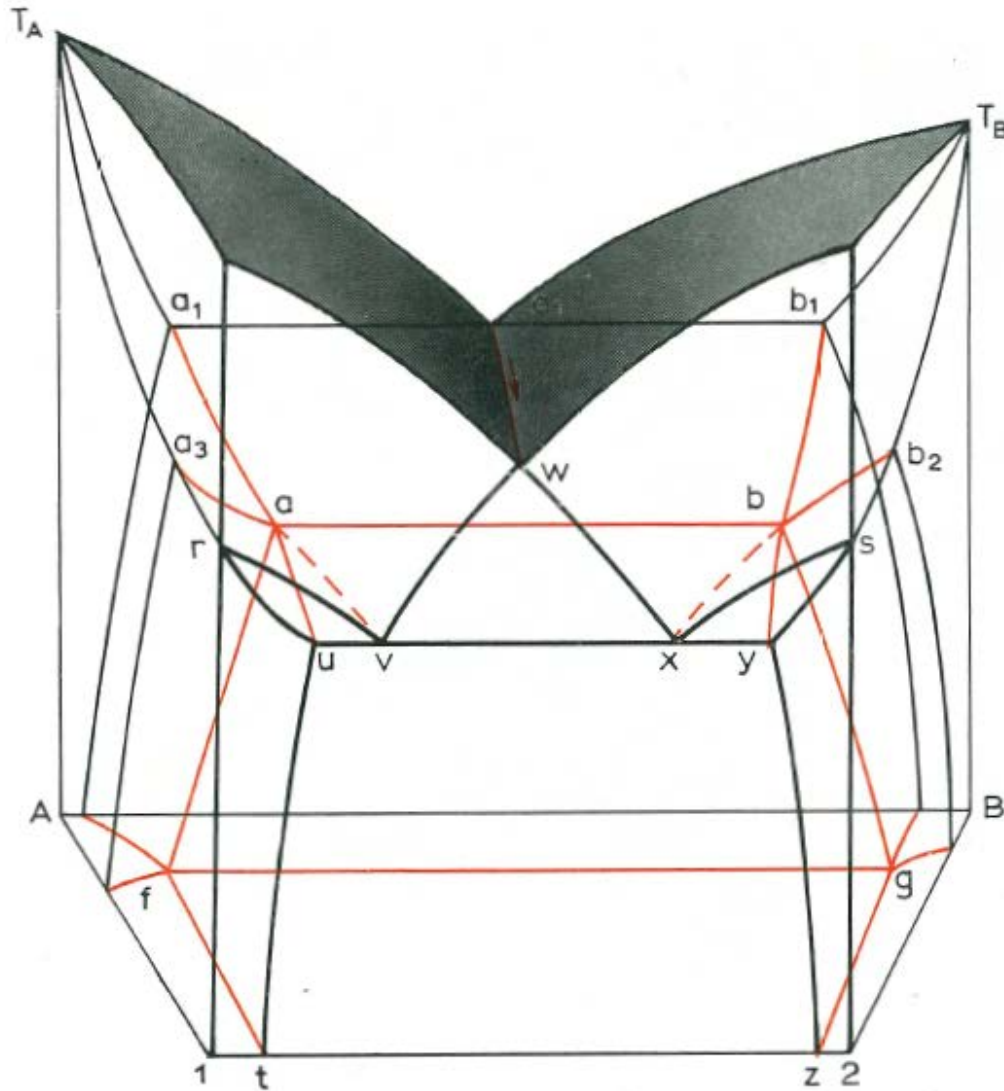


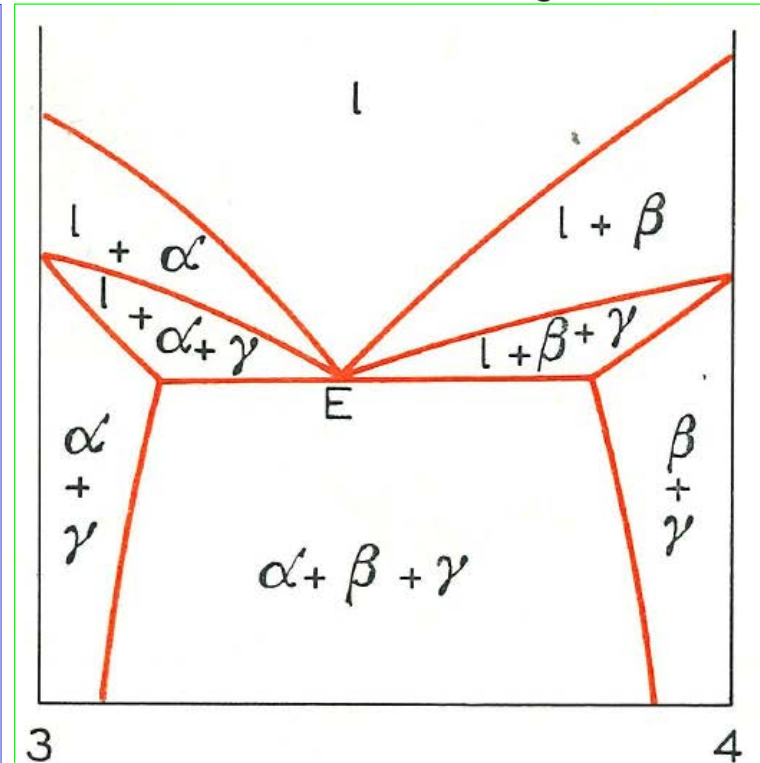
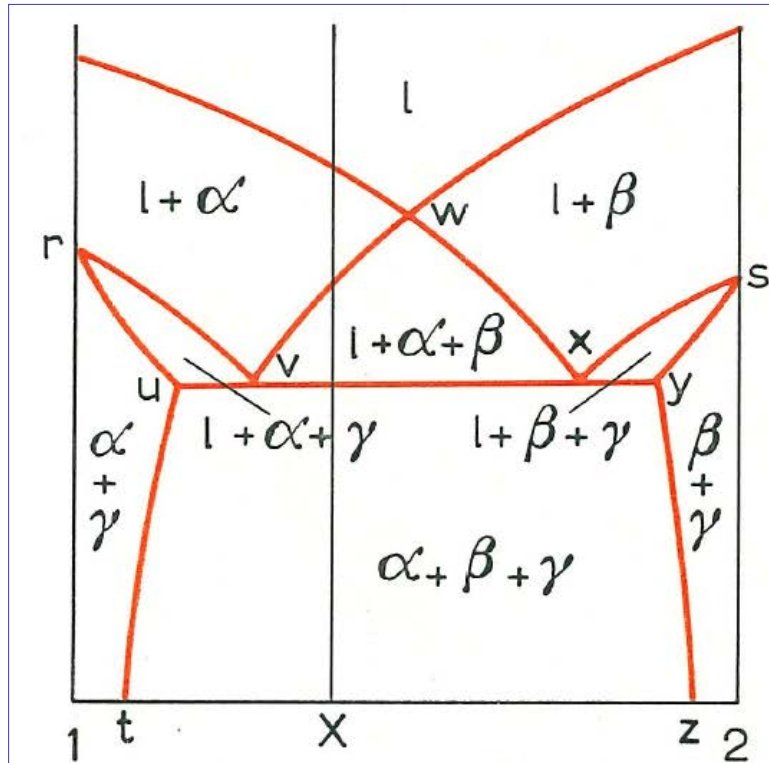
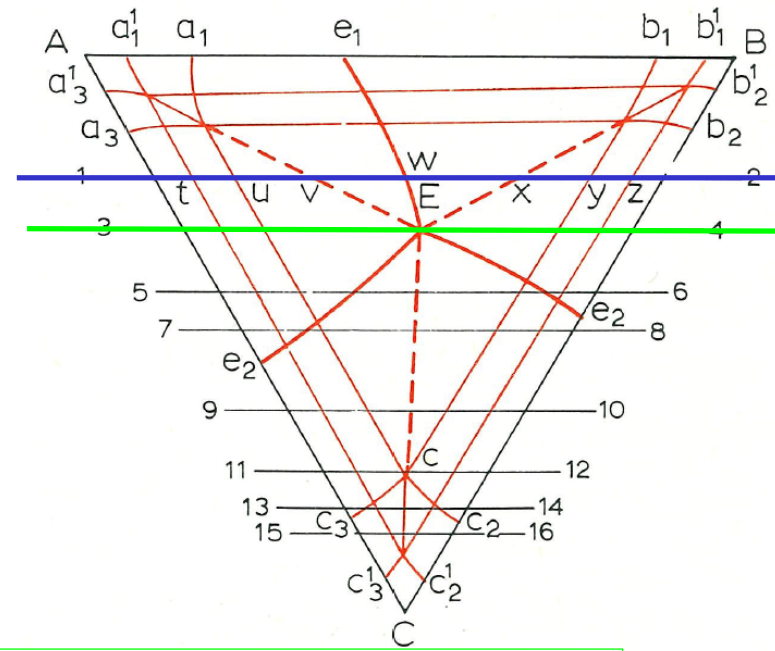
Fig. 179. Construction of vertical section 1-2.

10.1. THE EUTECTIC EQUILIBRIUM

$$(l = \alpha + \beta + \gamma)$$

Vertical section

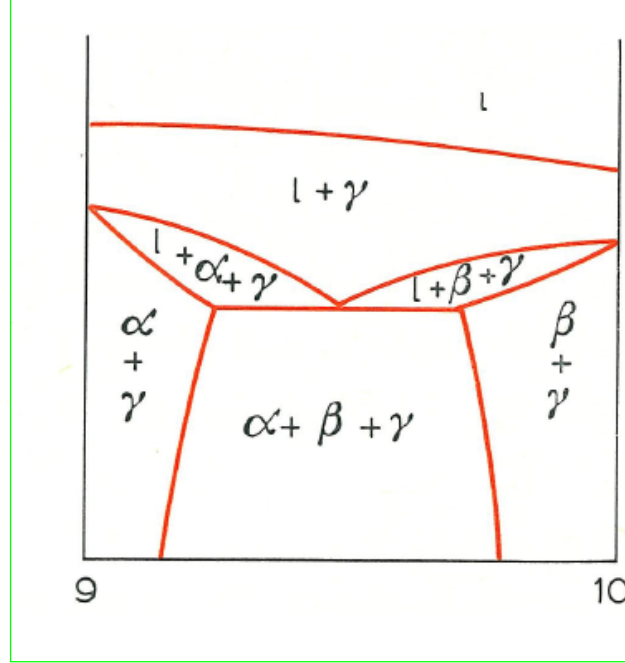
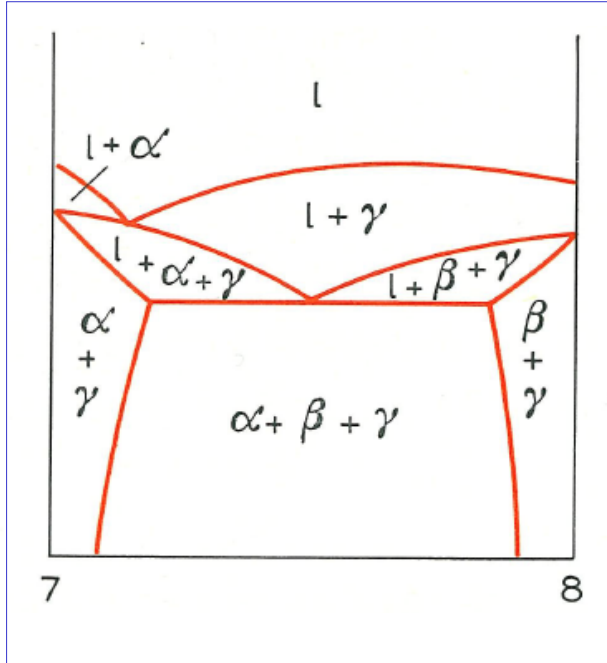
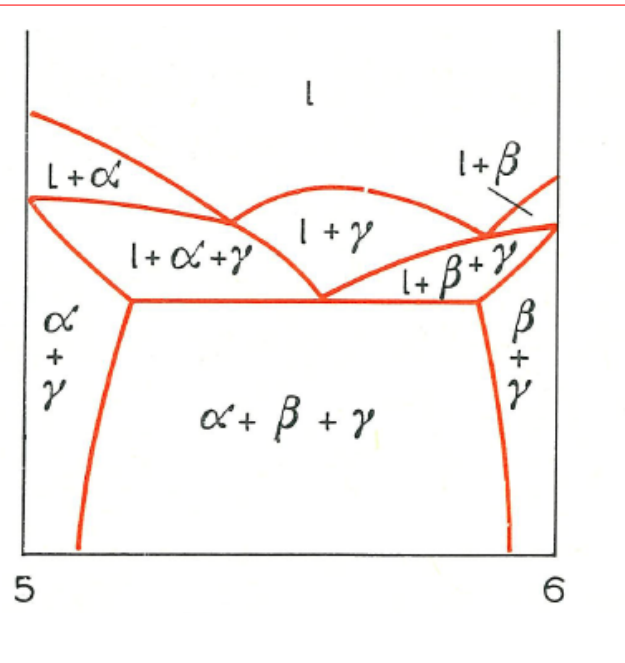
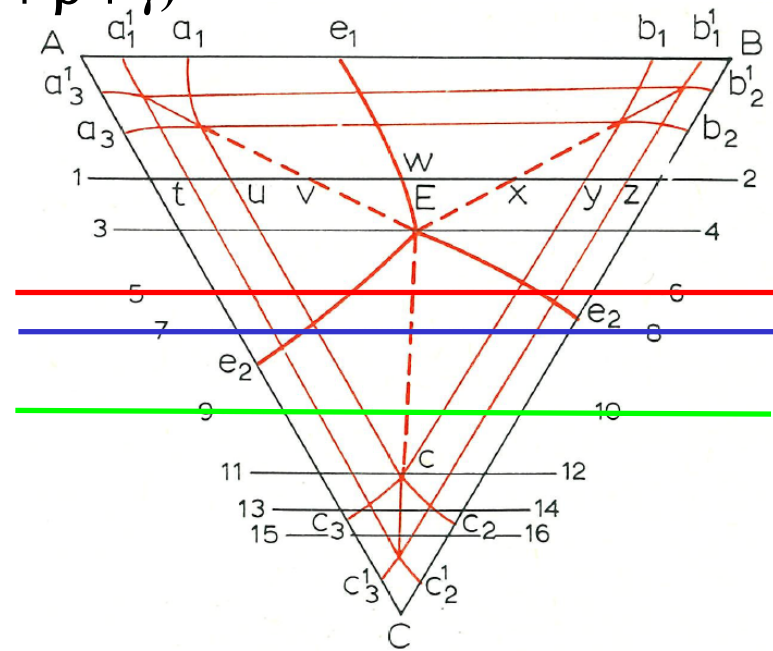
Location of vertical section



10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

Vertical section

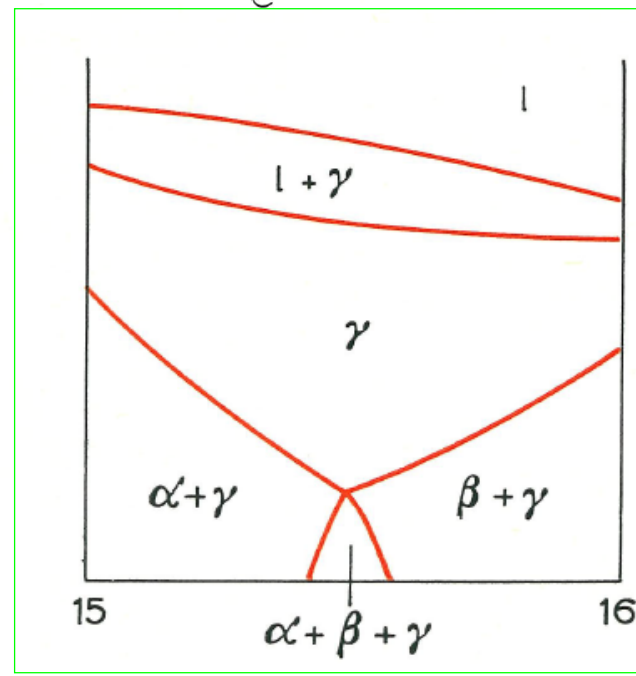
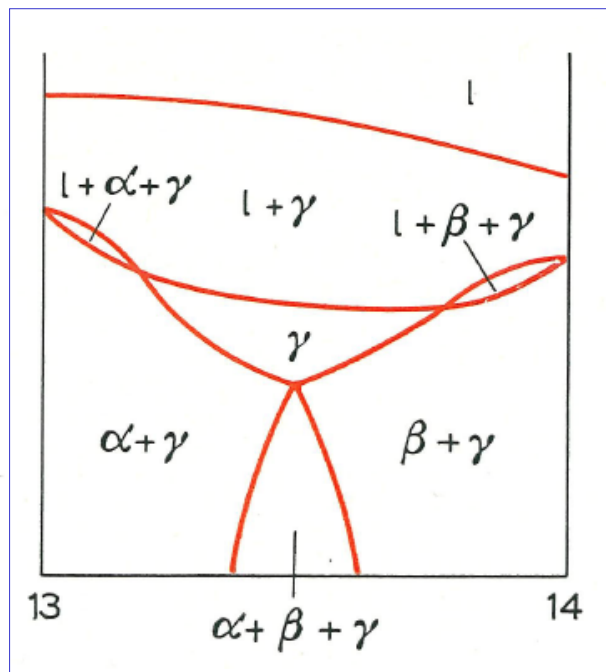
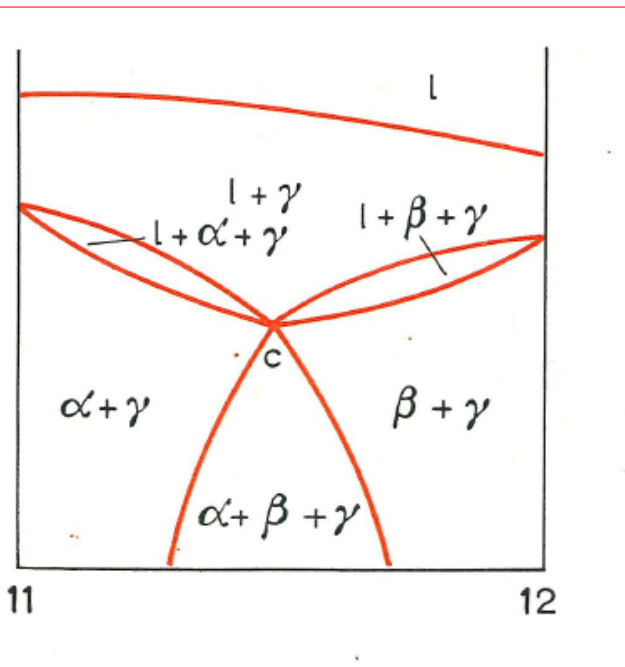
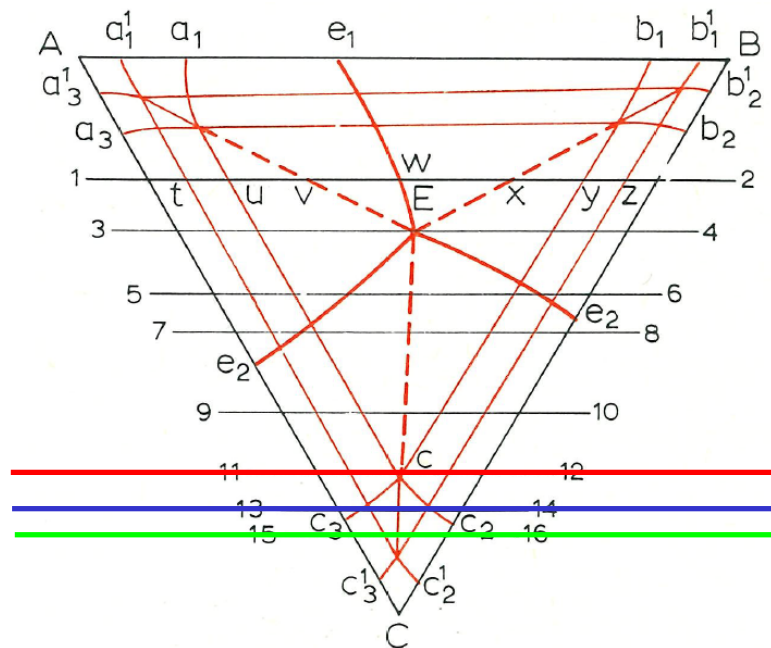
Location of vertical section



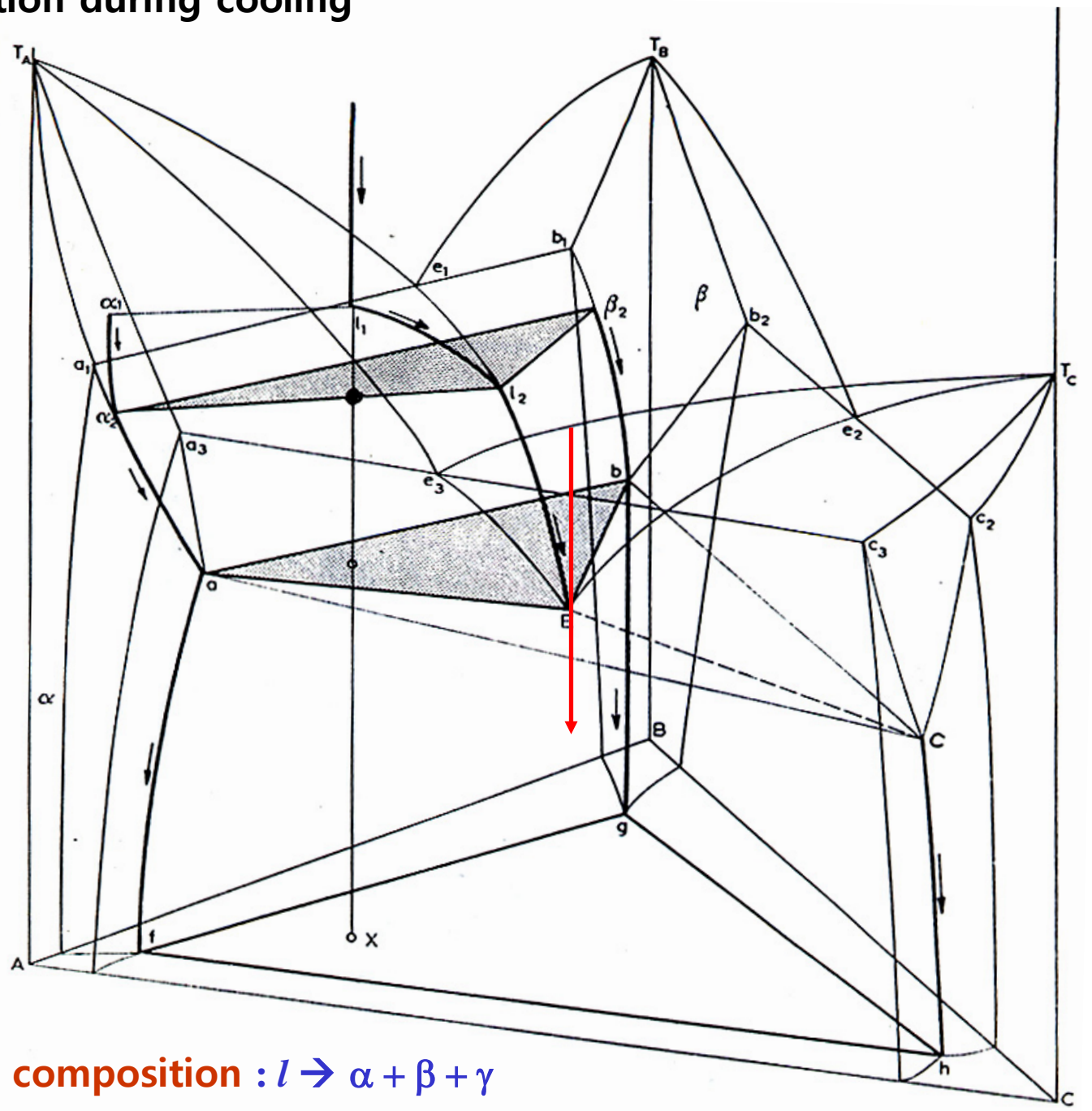
10.1. THE EUTECTIC EQUILIBRIUM ($l = \alpha + \beta + \gamma$)

Vertical section

Location of vertical section



Transformation during cooling



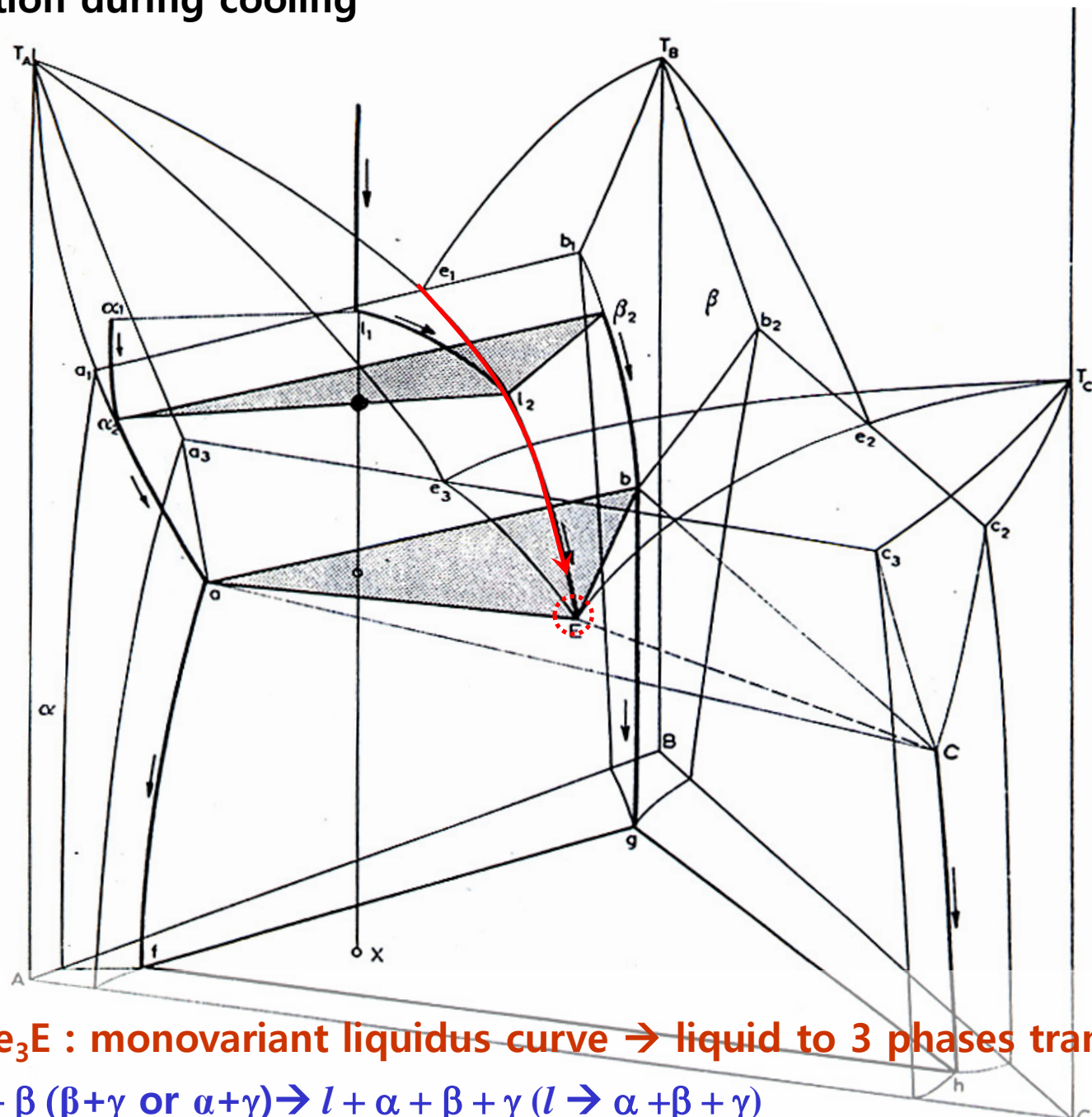
① Eutectic composition : $l \rightarrow \alpha + \beta + \gamma$

Ternary Eutectic microstructure



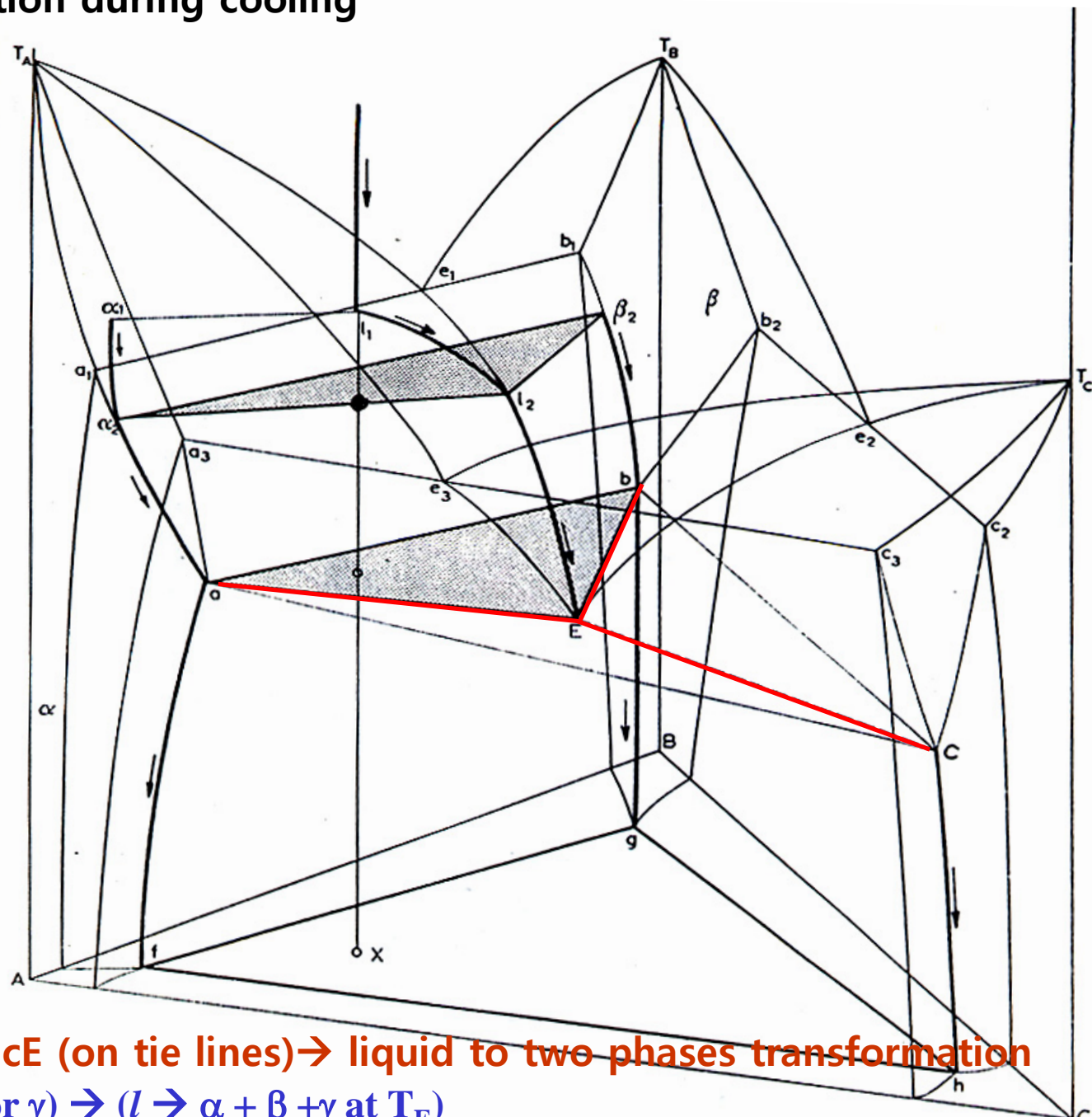
Microstructure of the ternary eutectic in the Al-Cu-Si system. α light, θ dark, Si grey, (x 900) 37

Transformation during cooling



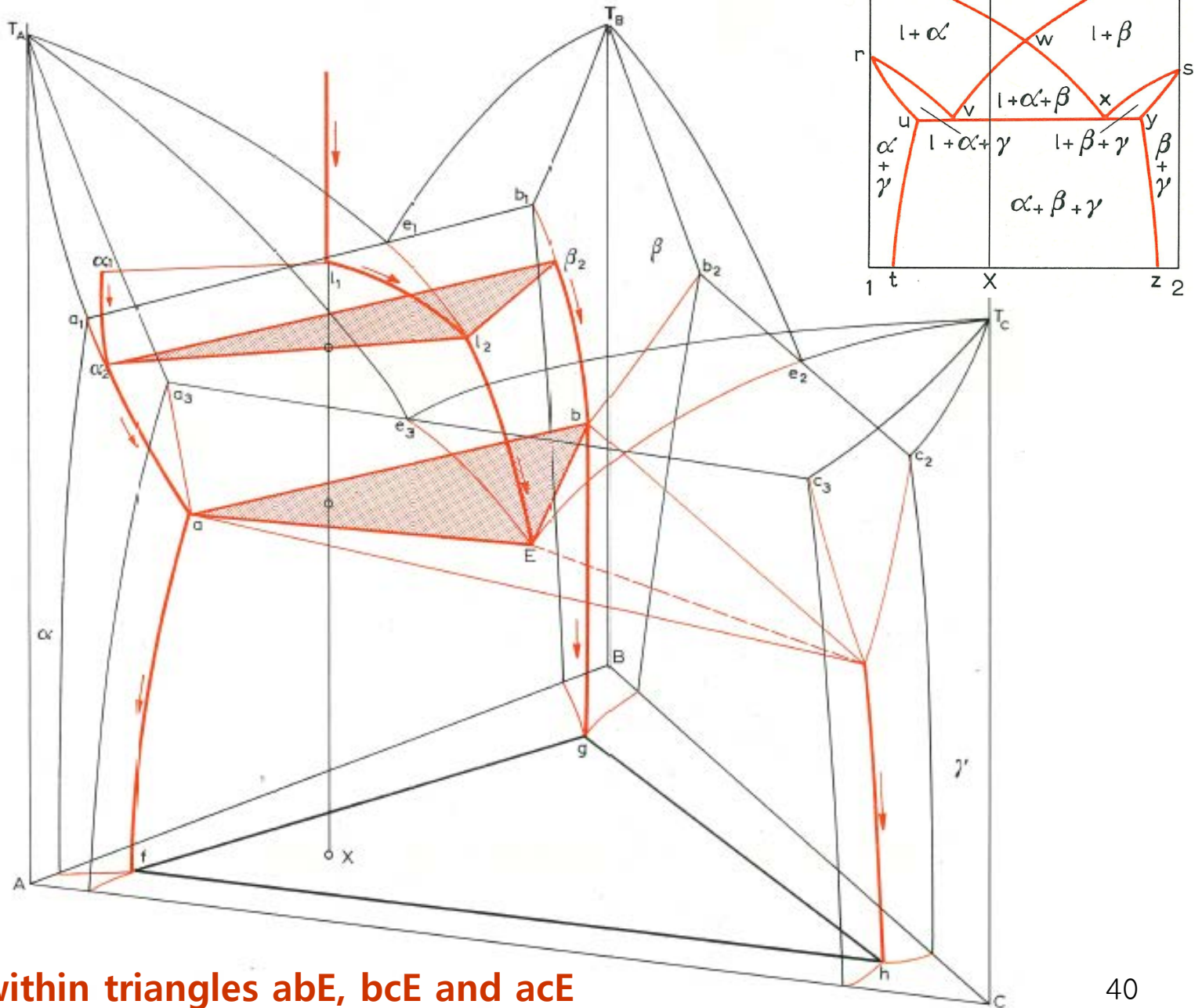
② e_1E, e_2E, e_3E : monovariant liquidus curve \rightarrow liquid to 3 phases transformation
 $: l \rightarrow l + \alpha + \beta (\beta + \gamma \text{ or } \alpha + \gamma) \rightarrow l + \alpha + \beta + \gamma (l \rightarrow \alpha + \beta + \gamma)$

Transformation during cooling



③ aE, bE, cE (on tie lines) \rightarrow liquid to two phases transformation
 $: l + \alpha (\beta \text{ or } \gamma) \rightarrow (l \rightarrow \alpha + \beta + \gamma \text{ at } T_E)$

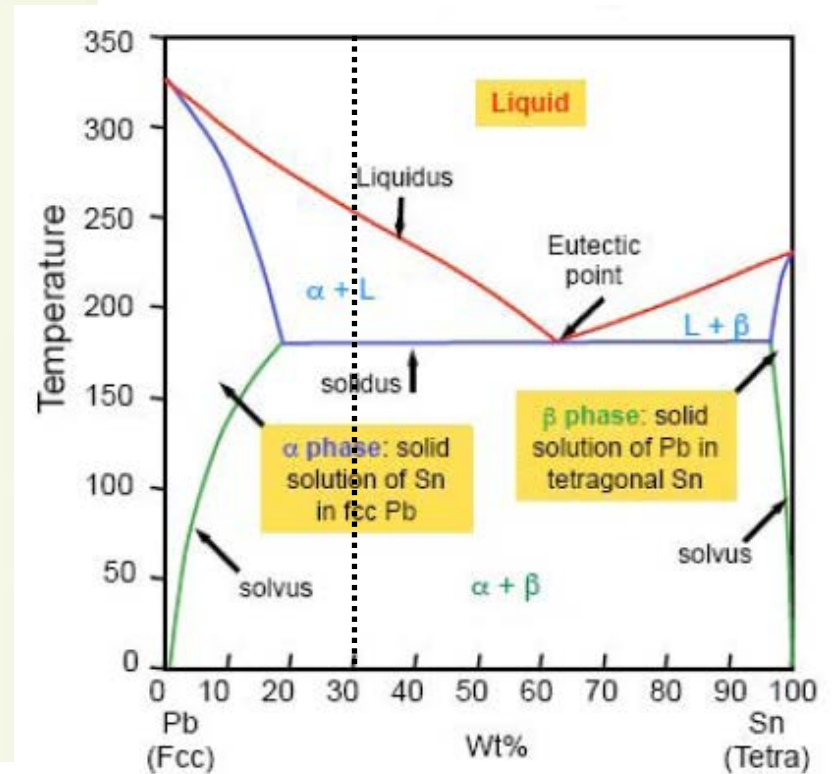
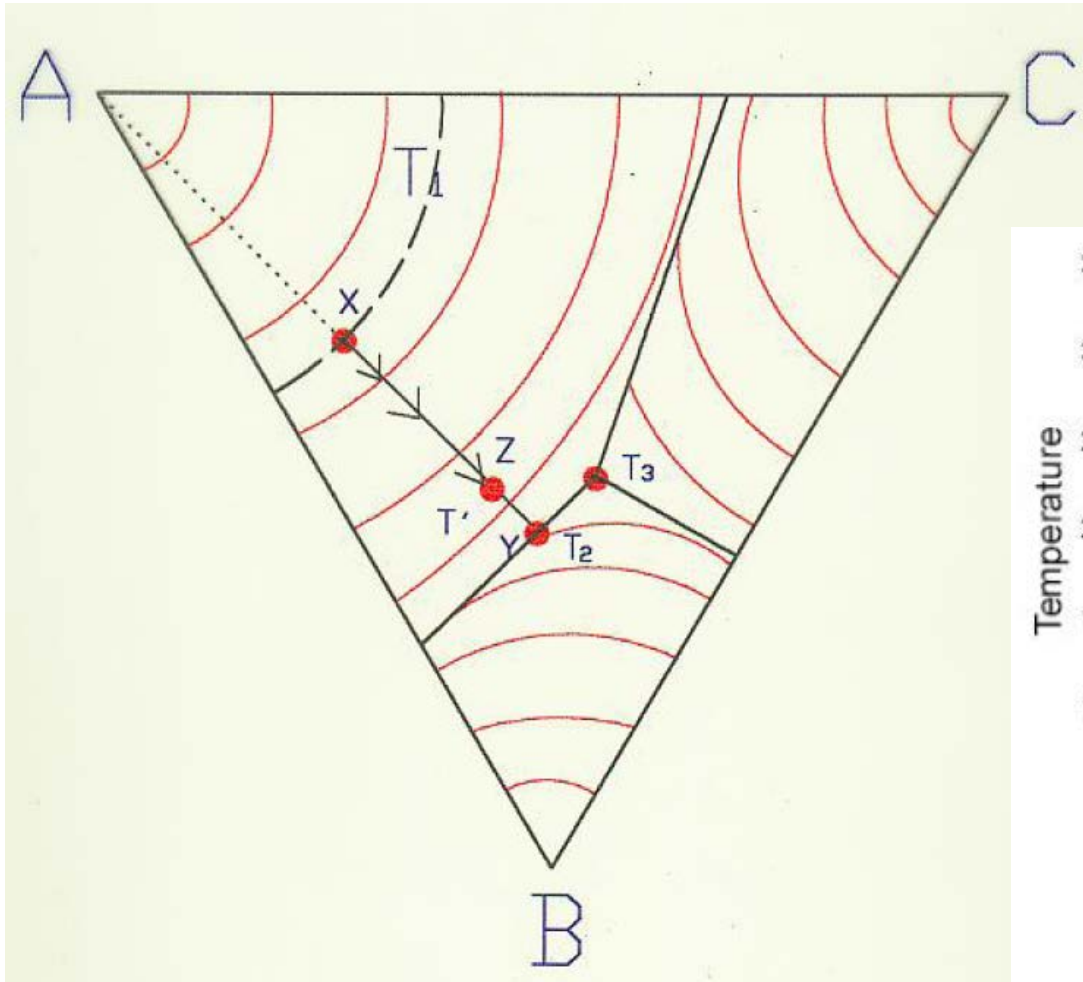
Transformation during cooling



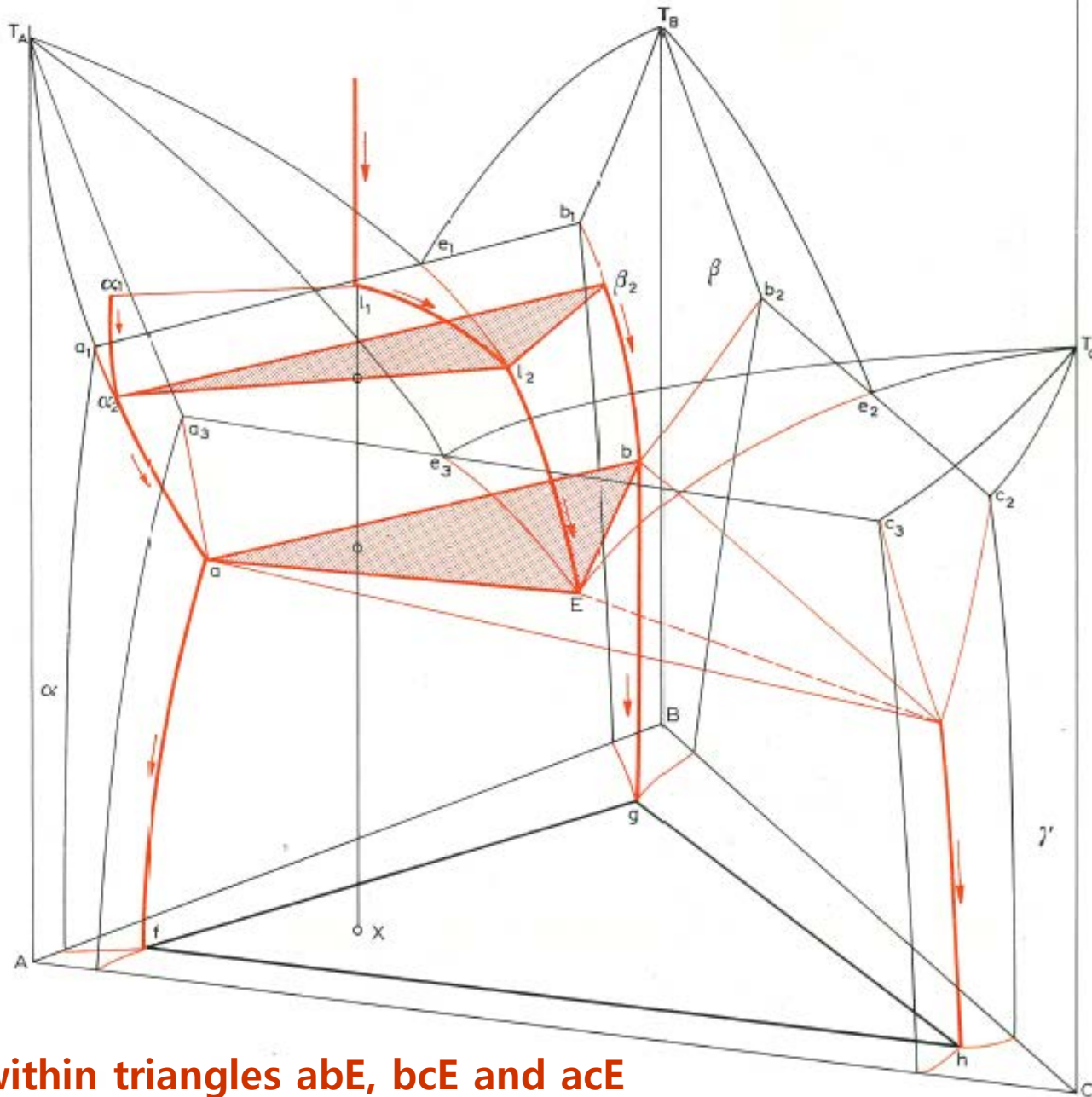
- ④ Alloys within triangles abE , bcE and acE
 ex) abE : $l + \alpha$ (or β) \rightarrow $l + \alpha + \beta$ \rightarrow ($l \rightarrow \alpha + \beta + \gamma$ at T_E)

Ternary Eutectic System

Solidification Sequence



Transformation during cooling



- ④ Alloys within triangles abE , bcE and acE
 ex) abE : $l + \alpha$ (or β) \rightarrow $l + \alpha + \beta$ \rightarrow ($l \rightarrow \alpha + \beta + \gamma$ at T_E)