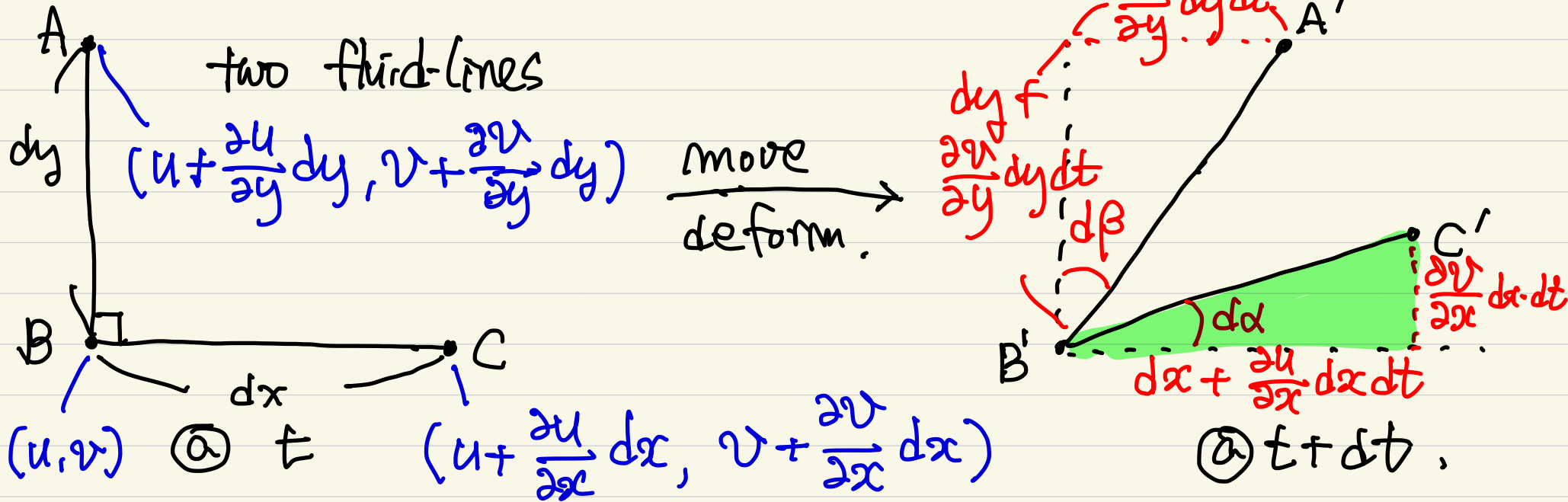


⊗, ⊙ Vorticity and Irrotationality.

(와동) (비회전성, zero vorticity).

⊙ vortex. (와류, eddy, swirl, ...)



angular velocity $\omega_z \equiv$ average rate of counter-clockwise turning of two lines.

$$\therefore \omega_z = \frac{1}{2} \left(\frac{d\alpha}{dt} - \frac{d\beta}{dt} \right) = \frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$$

$$d\alpha = \tan^{-1} \left(\frac{\frac{\partial v}{\partial x} dx dt}{dx + \frac{\partial u}{\partial x} dx dt} \right) \approx \frac{\partial v}{\partial x} dt$$

as $dt \rightarrow 0$

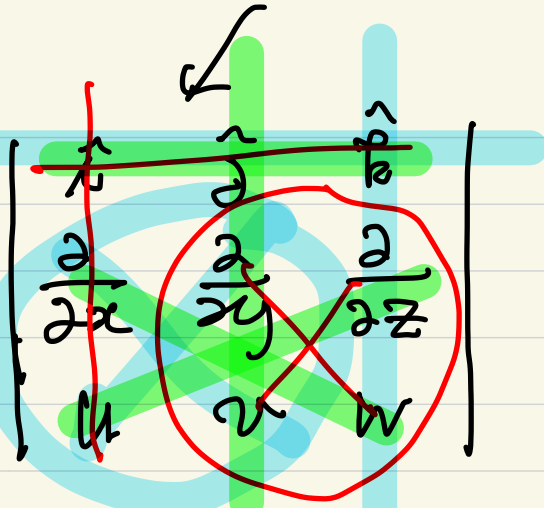
$$d\beta \approx \frac{\partial u}{\partial y} dt$$

also, $\omega_x = \frac{1}{2} \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right)$, $\omega_y = \frac{1}{2} \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right)$.

$$\Rightarrow \underline{\underline{\omega}} = \frac{1}{2} (\nabla \times \underline{v}) \quad : \text{angular velocity.}$$

$$\hookrightarrow \text{Vorticity: } \underline{\underline{\zeta}} = 2\underline{\underline{\omega}} = \nabla \times \underline{v}$$

↓
tendency of a local fluid to rotate.



$$= \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \hat{i} - \left(\frac{\partial w}{\partial x} - \frac{\partial u}{\partial z} \right) \hat{j} + \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \hat{k}.$$

• irrotational flow: $\nabla \times \underline{V} = 0$

$$\zeta_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = \frac{\partial}{\partial x} \left(-\frac{\partial \psi}{\partial x} \right) - \frac{\partial}{\partial y} \left(\frac{\partial \psi}{\partial y} \right) = 0$$

$$= - \left(\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) = -\nabla^2 \psi = 0$$

$$\nabla^2 \psi = 0$$

4.9 Frictionless rotational flows.

↓ (inviscid)

N-S eq. becomes $\rho \frac{\partial \underline{v}}{\partial t} + \rho (\underline{v} \cdot \nabla) \underline{v} = \rho \underline{g} - \nabla p$ (Euler eq.).

using a vector identity.

$$(\underline{v} \cdot \nabla) \underline{v} \equiv \nabla \left(\frac{1}{2} v^2 \right) + \underbrace{(\nabla \times \underline{v}) \times \underline{v}}_{= \underline{\zeta} \text{ (vorticity)}}$$

$$\therefore \left[\frac{\partial \underline{v}}{\partial t} + \nabla \left(\frac{1}{2} v^2 \right) + \underline{\zeta} \times \underline{v} + \frac{1}{\rho} \nabla p - \underline{g} \right] \cdot d\underline{r} = 0 \quad (*)$$

for arbitrary displacement vector

$$d\underline{r} = dx \hat{i} + dy \hat{j} + dz \hat{k}$$

↓ We want $(\underline{\xi} \times \underline{v}) \cdot d\underline{r} = 0$. When?

- ① $\underline{v} \equiv 0$ (no flow, trivial solution) ✓
- ② $\underline{\xi} = \nabla \times \underline{v} = 0$: irrotational flow. ☆ ✓
- ③ $d\underline{r} \perp (\underline{\xi} \times \underline{v})$: rare condition (Beltrami flow)
- ④ $d\underline{r} \parallel \underline{v}$: $d\underline{r}$ is a streamline ☆
- ⑤ $d\underline{r} \parallel \underline{\xi}$: $d\underline{r}$ is a vortex line ✓

$$(d\underline{r} = dx\hat{i} + dy\hat{j} + dz\hat{k})$$

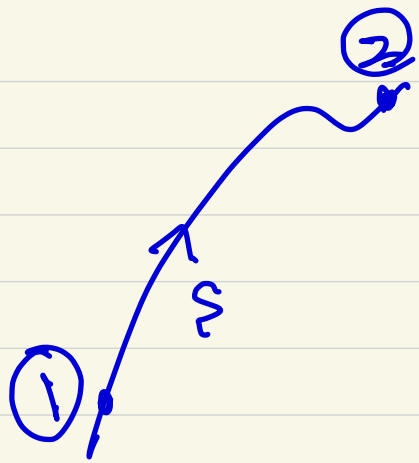
④ : $\underline{g} = -g\hat{k}$,

⑤ becomes

$$\frac{\partial \underline{v}}{\partial t} \cdot d\underline{r} + \nabla \left(\frac{1}{2} v^2 \right) \cdot d\underline{r} + \frac{1}{\rho} \nabla p \cdot d\underline{r} + g\hat{k} \cdot d\underline{r} = 0$$

$$\nabla \cdot d\underline{r} = dx \frac{\partial}{\partial x} + dy \frac{\partial}{\partial y} + dz \frac{\partial}{\partial z} = d.$$

$$\nabla = \frac{\partial}{\partial x} \hat{i} + \frac{\partial}{\partial y} \hat{j} + \frac{\partial}{\partial z} \hat{k}$$



$$\frac{\partial \underline{v}}{\partial t} ds + d\left(\frac{1}{2}v^2\right) + \frac{1}{\rho} dp + g dz = 0.$$

$$\int_1^2 \frac{\partial \underline{v}}{\partial t} ds + \frac{1}{2}(v_2^2 - v_1^2) + \int_1^2 \frac{1}{\rho} dp + g(z_2 - z_1) = 0.$$

along the streamline.

if steady, $\frac{p}{\rho} + \frac{1}{2}v^2 + gz = \text{constant}$

Bernoulli eq. (along the streamline)

$$\textcircled{2} \oint \underline{\omega} = \nabla \times \underline{v} = 0 \text{ (irrotational flow)}$$

$$\underline{v} = \nabla \phi$$

scalar function
(velocity potential)

$$\downarrow$$

$$u = \frac{\partial \phi}{\partial x}, \quad v = \frac{\partial \phi}{\partial y}, \quad w = \frac{\partial \phi}{\partial z}.$$

and lines of constant ϕ = potential lines.

$$(*) \quad \frac{\partial v}{\partial t} \cdot d\underline{r} = \frac{\partial}{\partial t} (\nabla \phi) \cdot d\underline{r} = \underline{\nabla \left(\frac{\partial \phi}{\partial t} \right)} \cdot \underline{d\underline{r}} = d \left(\frac{\partial \phi}{\partial t} \right)$$

$$\downarrow \quad \nabla \left(\frac{1}{2} v^2 \right) \cdot d\underline{r} = d \left(\frac{1}{2} v^2 \right), \quad \frac{1}{\rho} \nabla p \cdot d\underline{r} = \frac{1}{\rho} dp.$$

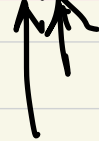
$$d \left(\frac{\partial \phi}{\partial t} + \int \frac{1}{\rho} dp + \frac{1}{2} |\nabla \phi|^2 + gz \right) = 0.$$

$$\Rightarrow \frac{\partial \phi}{\partial t} + \int \frac{1}{\rho} dp + \frac{1}{2} |\nabla \phi|^2 + gz = \text{constant}.$$

(unsteady irrotational Bernoulli eq.)
(inviscid)

\downarrow
valid all over the flow field!

* Orthogonality of ψ and ϕ (in 2D).



can be defined in 3D.

$$\nabla \times \underline{v} = 0 \text{ (irrotational flow)}$$

$$\underline{v} = \nabla \phi.$$

$$\begin{aligned} u &= \frac{\partial \psi}{\partial y} = \frac{\partial \phi}{\partial x} \\ v &= -\frac{\partial \psi}{\partial x} = \frac{\partial \phi}{\partial y}. \end{aligned}$$

continuity: $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \rightarrow \nabla^2 \phi = 0$

irrotational flow: $\zeta = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0 \rightarrow \nabla^2 \psi = 0$

"inviscid & irrotational flow"
 \rightarrow potential flow.

Solve for ϕ and ψ (Ch. 8)
 $\rightarrow u$ and $v \rightarrow P$ (Bernoulli eq.).

• lines of constant $\phi = \phi(x, y) = C$

$$d\phi = \frac{\partial \phi}{\partial x} dx + \frac{\partial \phi}{\partial y} dy = 0.$$

$= u$ $= v$

$$u dx + v dy = 0. \rightarrow$$

$$\left(\frac{dy}{dx} \right)_{\text{const } \phi} = - \frac{u}{v}$$

• lines of constant $\psi = \psi(x, y) = C$

$$d\psi = \frac{\partial \psi}{\partial x} dx + \frac{\partial \psi}{\partial y} dy = 0$$

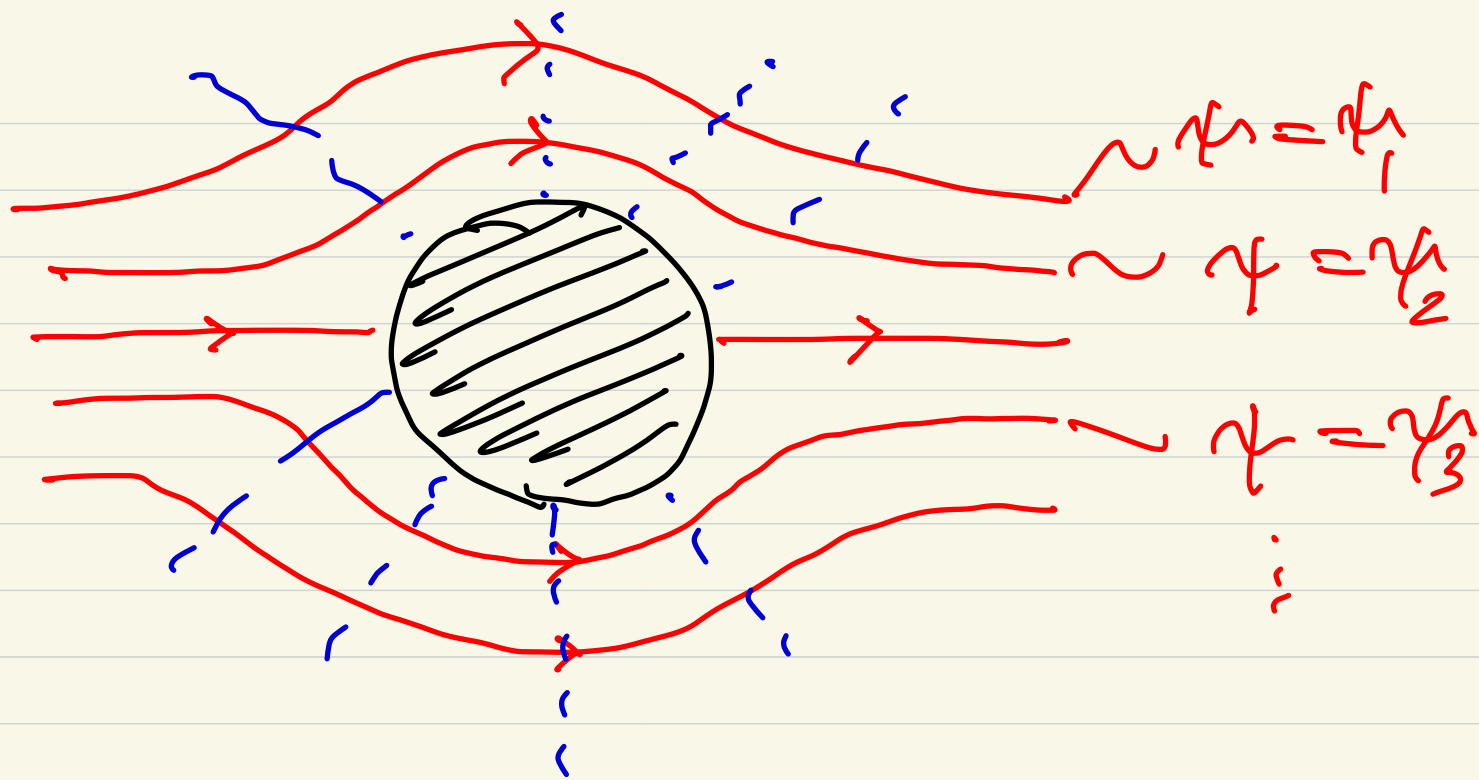
$= -v$ $= u$

$$\Rightarrow \left(\frac{dy}{dx} \right)_{\text{const } \psi} = \frac{v}{u}$$

$$\left(\frac{dy}{dx} \right)_{\psi = \text{const}} \times \left(\frac{dy}{dx} \right)_{\phi = \text{const}} = -1$$

Streamline potential line

“orthogonal”



* Generation of rotationality.

irrotational $\xrightarrow{\text{when?}}$ rotational

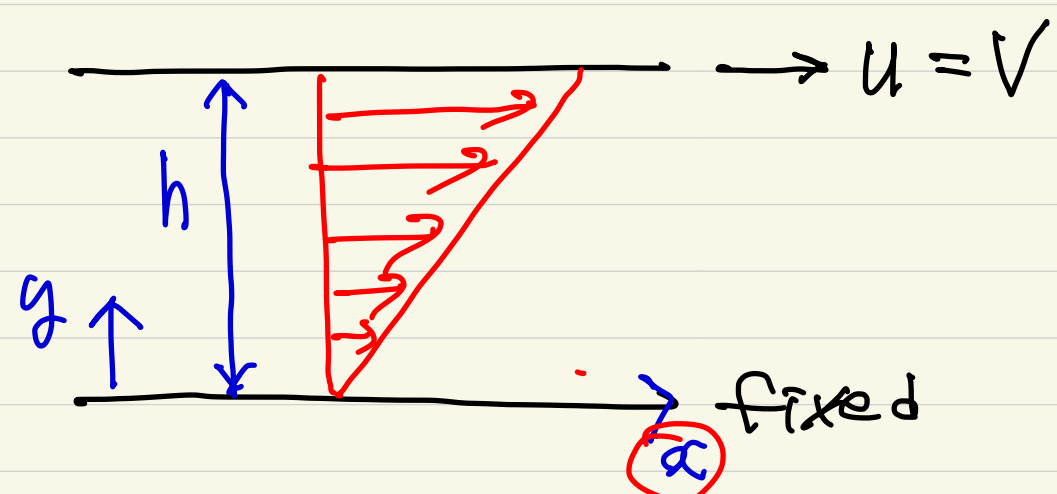
- ① viscous force dominant.
- ② entropy gradient (shock wave, ...)
- ③ density " (stratification)

④ non-inertial effect (Coriolis effect)

Bernoulli eq is still valid if the flow is irrotational.

4.10. Some illustrative incompressible viscous flow.

① Couette flow. → relative motion induces the flow.



steady, 2D.
 $\Delta p = 0$
 $\frac{\partial}{\partial x}(\cdot) = 0$ fully-developed.

continuity: $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \Rightarrow \frac{\partial v}{\partial y} = 0, v = \text{const.} = 0$

$$u = u(x, y) \Rightarrow u = u(y).$$

• N-S eq

$$x\text{-dir: } \cancel{\rho \frac{\partial u}{\partial t}} + \cancel{\rho u \frac{\partial u}{\partial x}} + \cancel{\rho v \frac{\partial u}{\partial y}} = -\cancel{\frac{\partial p}{\partial x}} + \mu \left(\cancel{\frac{\partial^2 u}{\partial x^2}} + \frac{\partial^2 u}{\partial y^2} \right).$$

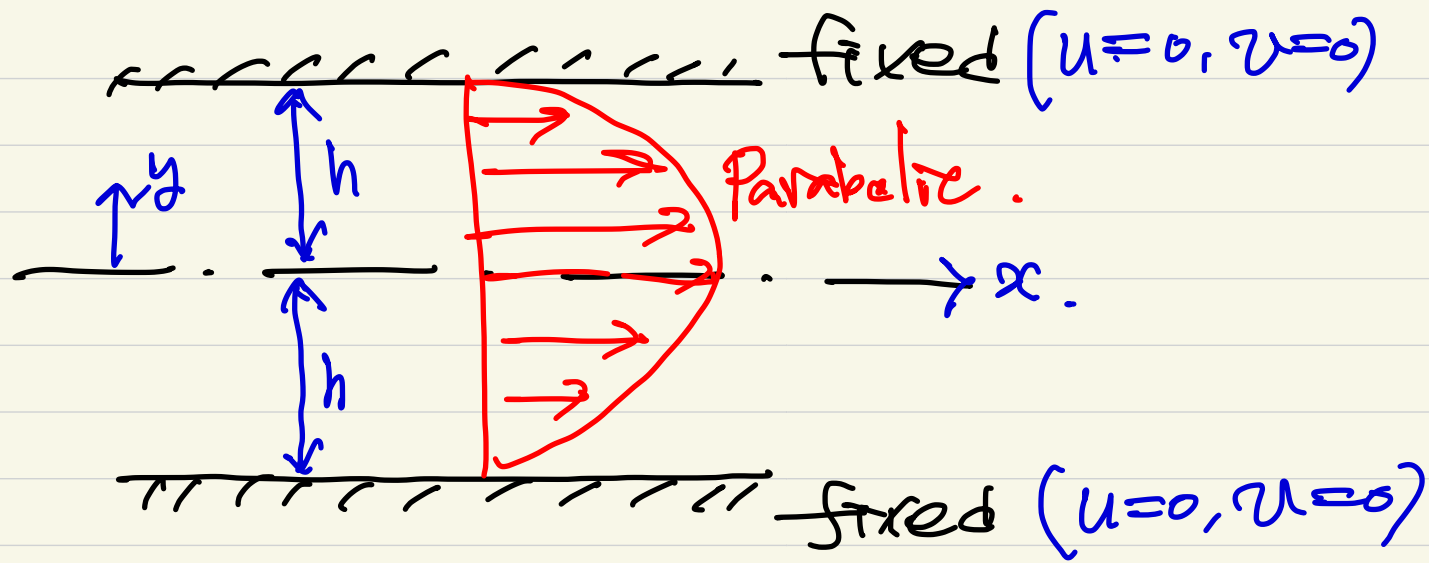
$$\therefore \frac{d^2 u}{dy^2} = 0 \rightarrow u(y) = C_1 y + C_2.$$

$$\text{BCs: } u = V \text{ @ } y = h$$

$$u = 0 \text{ @ } y = 0.$$

$$\therefore u(y) = \frac{y}{h} V.$$

② Flow due to pressure gradient between two fixed plates. (plane Poiseuille flow).
(2D)



- steady ($\partial/\partial t = 0$)
- fully-developed ($\partial/\partial x = 0$)
- $\partial p/\partial x \neq 0$ (< 0)

Continuity: $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \Rightarrow v = 0.$

N-S eq:

$$\cancel{\rho \frac{\partial u}{\partial t}} + \cancel{\rho (\mathbf{v} \cdot \nabla) u} = - \frac{dp}{dx} + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$$

$\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial y}$

$$\rightarrow \cancel{\rho \frac{\partial u}{\partial t}} + \cancel{\rho (\mathbf{v} \cdot \nabla) u} = - \frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$$

$$\Rightarrow \frac{\partial p}{\partial y} = 0 \Rightarrow p = p(x)$$

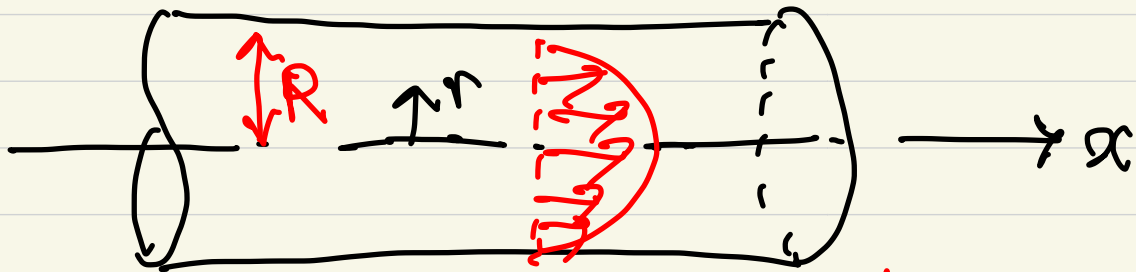
$$\therefore \mu \frac{\partial^2 u}{\partial y^2} = \frac{dp}{dx} = \text{constant.}$$

$$\therefore u(y) = \frac{1}{\mu} \frac{dp}{dx} \cdot \frac{1}{2} y^2 + C_1 y + C_2. \quad \left(u = 0 \text{ @ } y = \pm h \right)$$

$$\rightarrow u(y) = -\frac{dp}{dx} \cdot \frac{h^2}{2\mu} \left(1 - \frac{y^2}{h^2} \right). \quad \text{Parabole.}$$

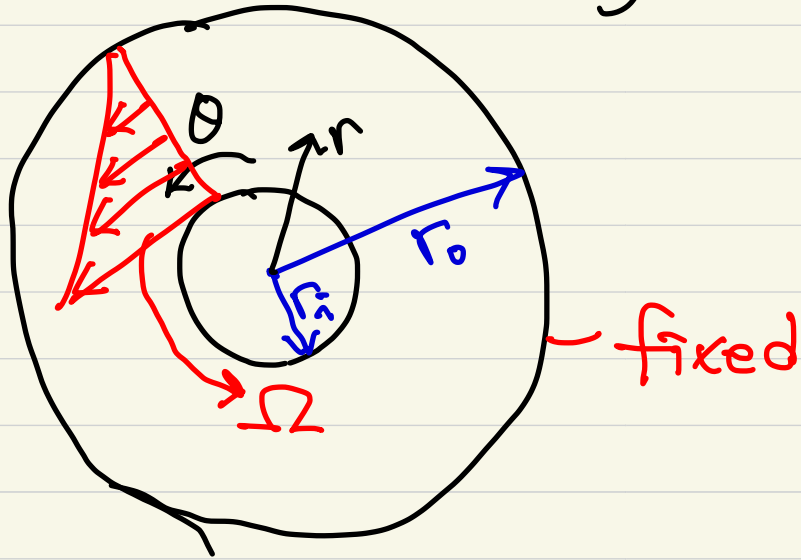
③ Fully-developed laminar pipe flow. (Hagen-Poiseuille flow)

$$\frac{\partial p}{\partial x} \neq 0.$$



$$u(r) = -\frac{dp}{dx} \cdot \frac{1}{4\mu} (R^2 - r^2) \Rightarrow \underline{\underline{\text{Ch. 6}}}$$

⊕ Flow between long concentric cylinders.



(r, θ, z) coordinate.

- no axial motion
 $\therefore v_z = 0, \frac{\partial}{\partial z}(\cdot) = 0.$

- no variation in θ $\therefore \frac{\partial}{\partial \theta}(\cdot) = 0.$

cont. $\therefore \frac{1}{r} \frac{\partial}{\partial r} (r v_r) + \frac{1}{r} \frac{\partial^2 v_\theta}{\partial \theta^2} = 0. \rightarrow r v_r = \text{constant}.$

at $r = r_i, v_r = 0. \Rightarrow v_r = 0.$

- N-S eq (θ -dir).

$$\rho (\underline{v} \cdot \nabla) v_\theta + \frac{\rho}{r} v_r v_\theta = - \frac{1}{r} \frac{\partial p}{\partial \theta} + \mu \left[\frac{1}{r} \frac{d}{dr} \left(r \frac{dv_\theta}{dr} \right) - \frac{v_\theta}{r^2} \right]$$

$$\therefore \frac{1}{r} \frac{d}{dr} \left(r \frac{dv_\theta}{dr} \right) = \frac{v_\theta}{r^2} \Rightarrow v_\theta(r) = C_1 r + \frac{C_2}{r}$$

$$\text{BC's: } v_\theta = 0 \text{ @ } r = r_0$$

$$v_\theta = r_i \Omega \text{ @ } r = r_i$$

$$\therefore v_\theta = \Omega r_i \frac{r_0/r - r/r_0}{r_0/r_i - r_i/r_0}$$