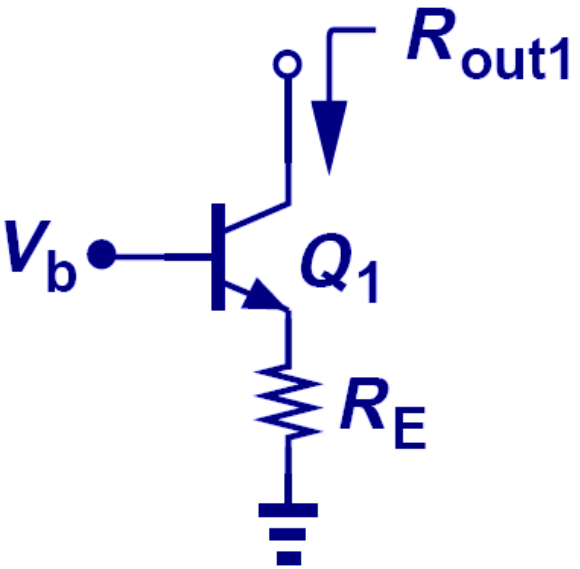
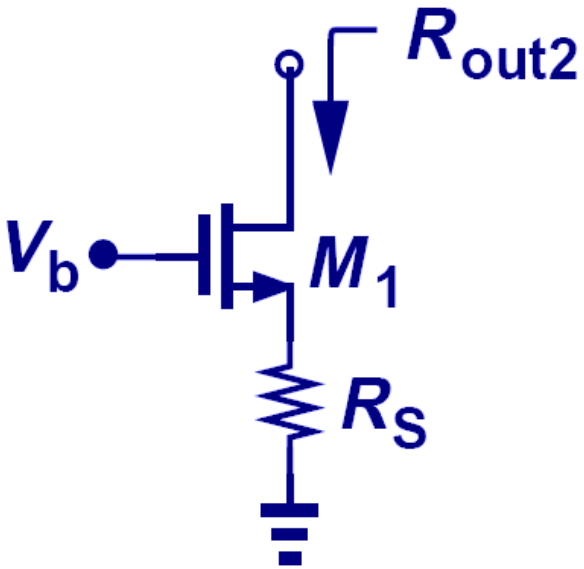
Chapter 9 Cascode Stages and Current Mirrors

- 9.1 Cascode Stage
- 9.2 Current Mirrors

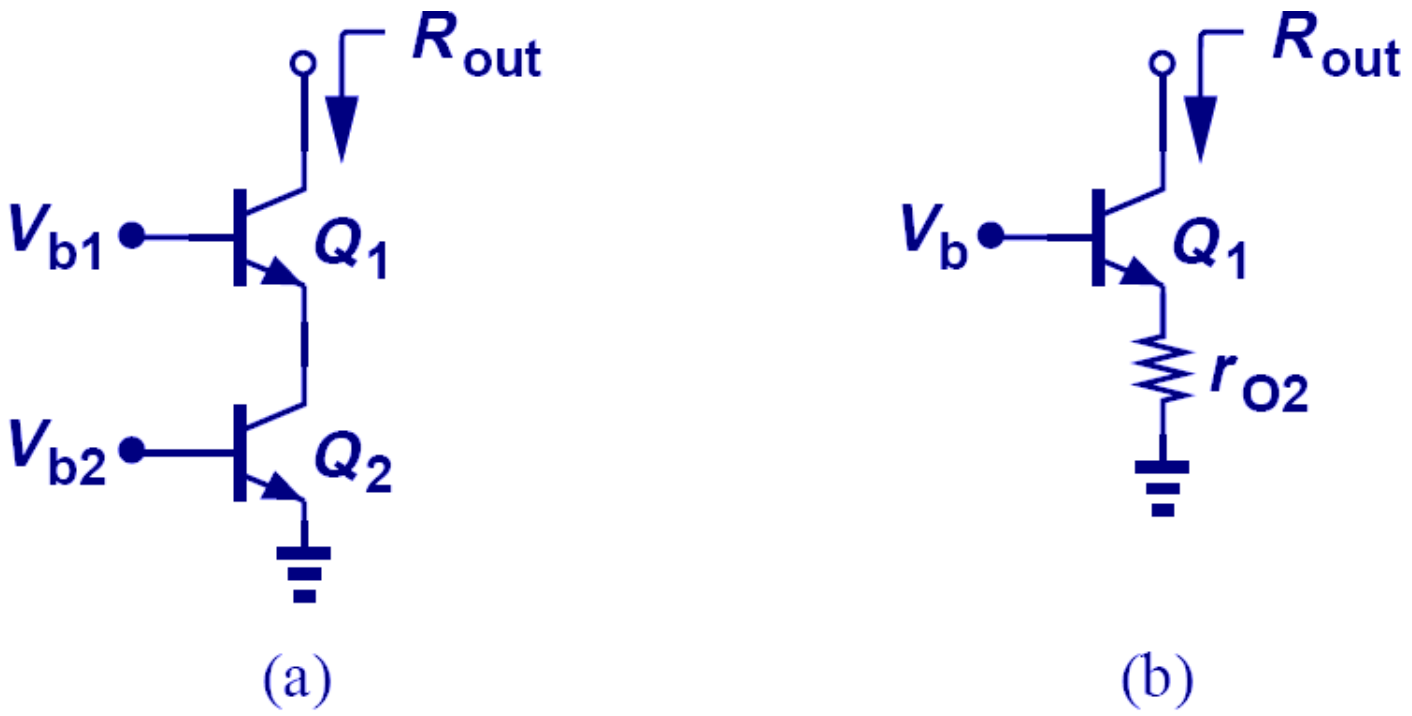
Boosted Output Impedances





$$R_{out1} = [1 + g_m(R_E \parallel r_\pi)]r_O + R_E \parallel r_\pi$$
$$R_{out2} = (1 + g_m R_S)r_O + R_S$$

Bipolar Cascode Stage

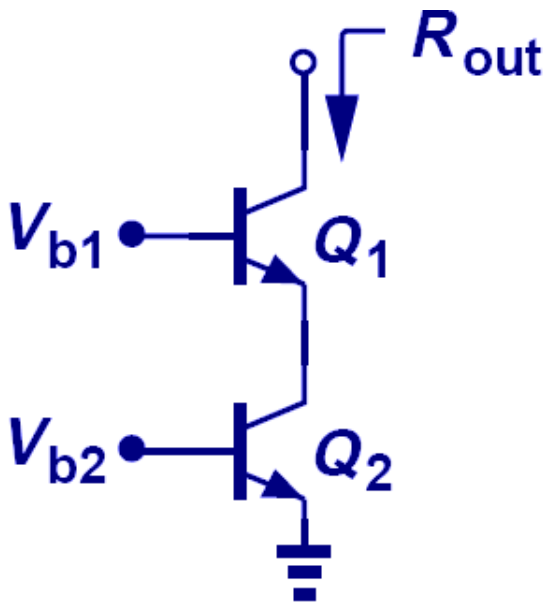


$$R_{out} = [1 + g_{m1}(r_{O2} \| r_{\pi 1})]r_{O1} + r_{O2} \| r_{\pi 1}$$

$$R_{out} \approx g_{m1} r_{O1} (r_{O2} \| r_{\pi 1})$$

Example 9.1

- If Q_1 and Q_2 in Fig.9.2(a) are biased at a collector current of 1mA, determine the output resistance. Assume β =100 and V_A=5V for both transistors.



(a)

$$g_m = I_C/V_T, r_O = V_A/I_C,$$

$$r_\pi = \beta V_T/I_C$$

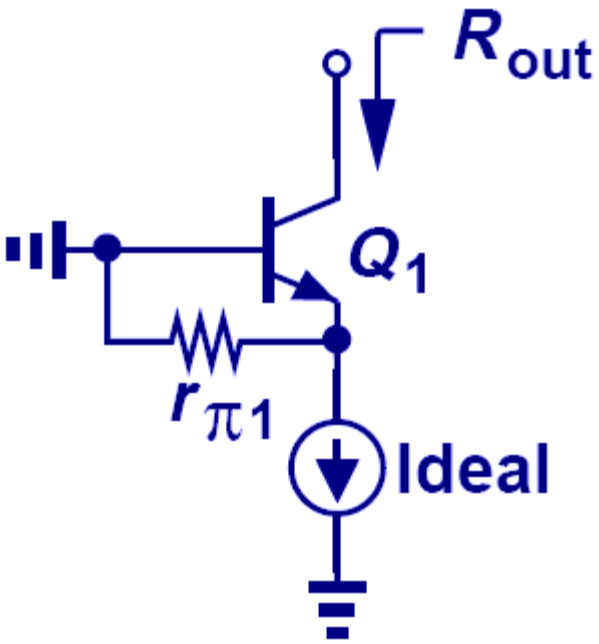
$$R_{out} \approx \frac{I_{C1}}{V_T} \cdot \frac{V_{A1}}{I_{C1}} \cdot \frac{\frac{V_{A2}}{I_{C2}} \cdot \frac{\beta V_T}{I_{C1}}}{\frac{V_{A2}}{I_{C2}} + \frac{\beta V_T}{I_{C1}}}$$

$$\approx \frac{1}{I_{C1}} \cdot \frac{V_A}{V_T} \cdot \frac{\beta V_A V_T}{V_A + \beta V_T},$$

$$I_C = I_{C1} = I_{C2} \text{ and } V_A = V_{A1} = V_{A2}$$

$$R_{out} \approx 328.9\ \text{k}\Omega.$$

Maximum Bipolar Cascode Output Impedance



$$R_{out,\max} \approx g_{m1} r_{O1} r_{\pi 1}$$

$$R_{out,\max} \approx \beta_1 r_{O1}$$

- **The maximum output impedance of a bipolar cascode is bounded by the ever-present r_π between emitter and ground of Q_1.**

Example 9.2

- **Suppose in Example 9.1, the Early voltage of Q_2 is equal to 50V. Compare the resulting output impedence of the cascade with the upper bound given by Eq.(9.12).**

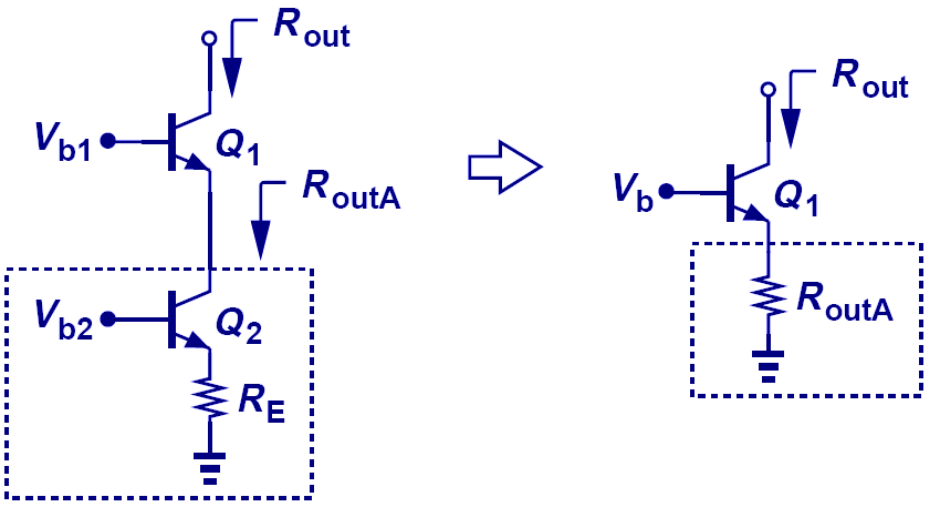
Since $g_{m1} = (26\ \Omega)^{-1}$, $r_{\pi 1} = 2.6\ \text{k}\Omega$, $r_{O1} = 5\ \text{k}\Omega$, and $r_{O2} = 50\ \text{k}\Omega$, we have

$$\begin{aligned} R_{out} &\approx g_{m1} r_{O1} (r_{O1} || r_{\pi 1}) \\ &\approx 475\ \text{k}\Omega. \end{aligned}$$

The upper bound is equal to $500\ \text{k}\Omega$, about 5% higher.

Example 9.3

- We wish to increase the output resistance of the bipolar cascade of Fig. 9.2(a) by a factor of two through the use of resistive degeneration in the emitter of Q_2. Determine the required value of the degeneration resistor if Q_1 and Q_2 are identical.



$$R_{outA} = [1 + g_{m2}(R_E||r_{\pi 2})]r_{O2} + R_E||r_{\pi 2}.$$

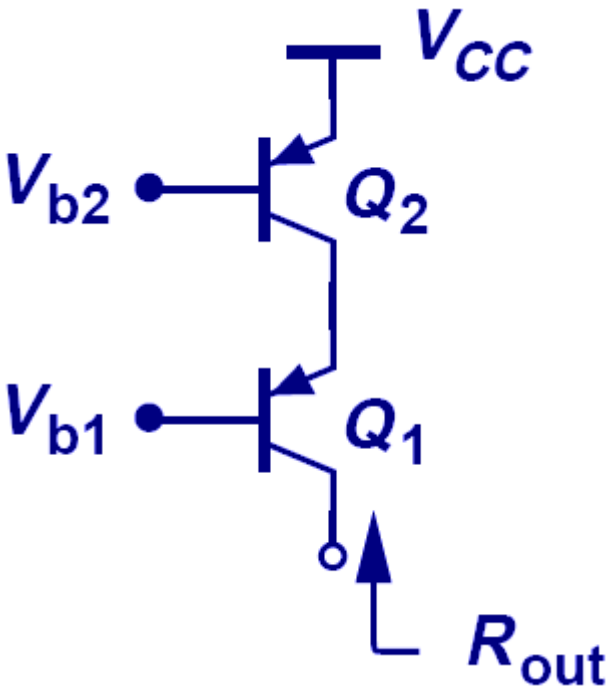
$$R_{out} \approx g_{m1} r_{O1} (R_{outA}||r_{\pi 1}).$$

$$R_{outA}||r_{\pi 1} = 2(r_{O2}||r_{\pi 1}).$$

$$R_{outA} = \frac{2r_{O2}r_{\pi 1}}{r_{\pi 1} - r_{O2}}$$

- Typically r_π is smaller than r_O, so in general it is **impossible** to double the output impedance by degenerating Q_2 with a resistor.

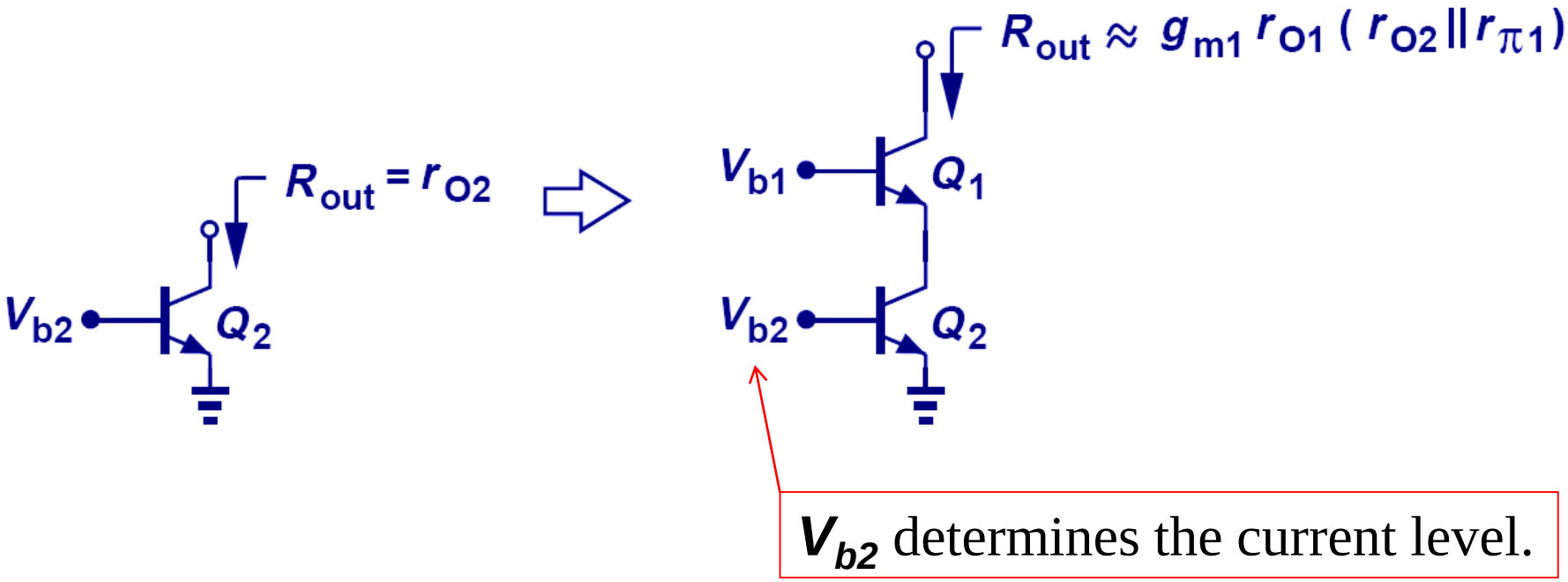
PNP Cascode Stage



$$R_{out} = [1 + g_{m1}(r_{O2} \| r_{\pi 1})]r_{O1} + r_{O2} \| r_{\pi 1}$$

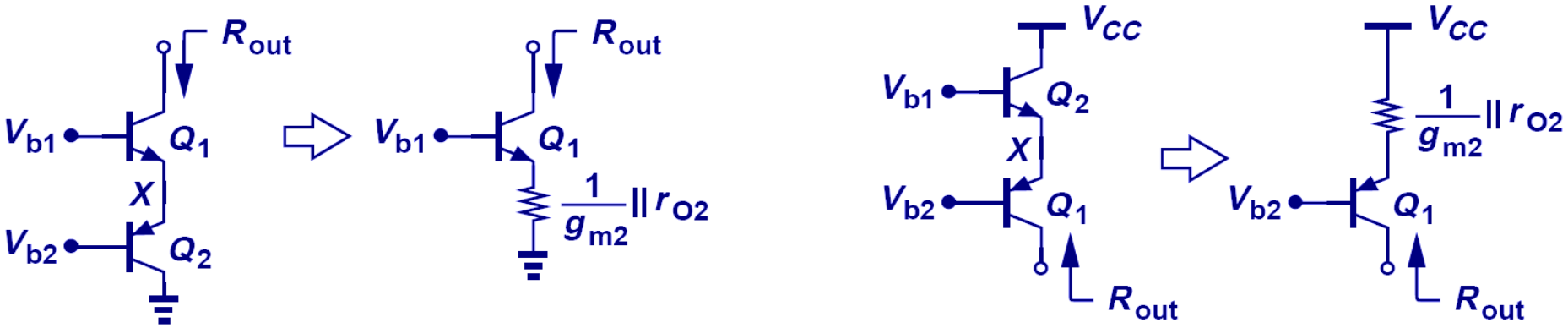
$$R_{out} \approx g_{m1} r_{O1} (r_{O2} \| r_{\pi 1})$$

Another Interpretation of Bipolar Cascode



- **Instead of treating cascode as Q_2 degenerating Q_1, we can also think of it as Q_1 stacking on top of Q_2 (current source) to boost Q_2's output impedance.**

False Cascodes



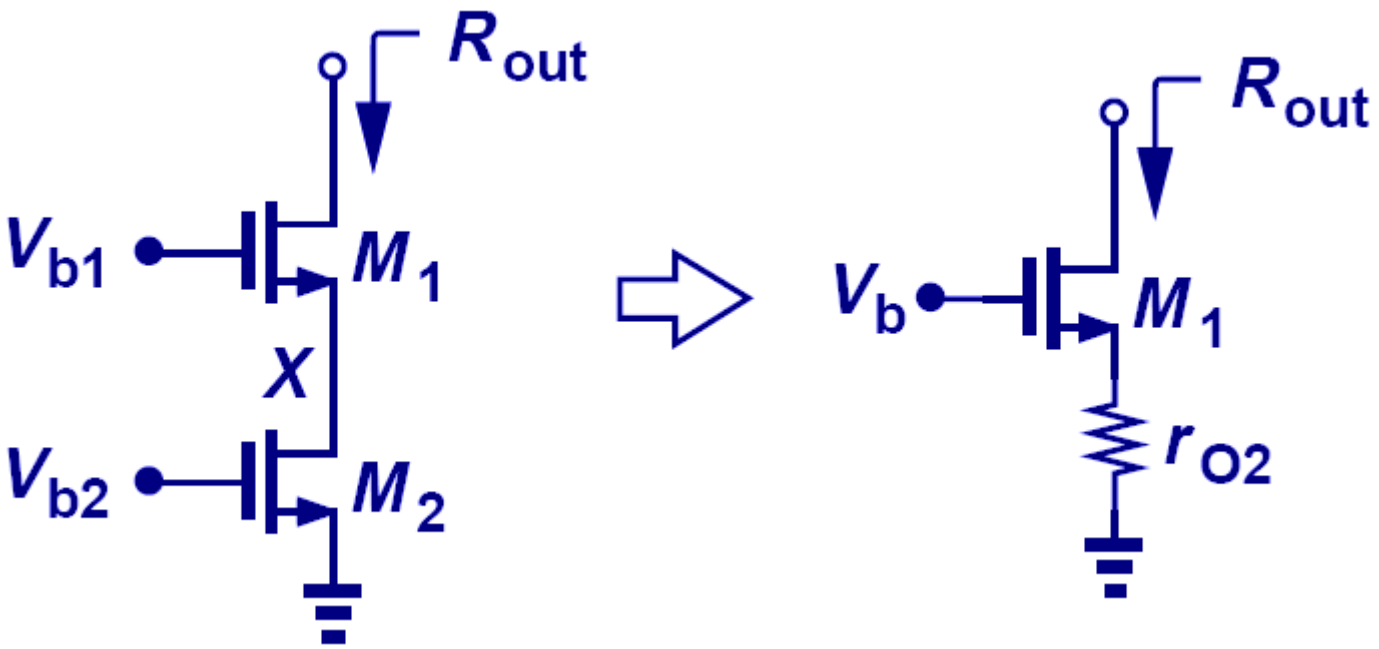
(a) (b)

$$R_{out} = \left[1 + g_{m1}\left(\frac{1}{g_{m2}} \| r_{O2} \| r_{\pi 1}\right)\right] r_{O1} + \frac{1}{g_{m2}} \| r_{O2} \| r_{\pi 1}$$

$$R_{out} \approx \left(1 + \frac{g_{m1}}{g_{m2}}\right) r_{O1} + \frac{1}{g_{m2}} \approx 2 r_{O1}$$

- **When the emitter of Q_1 is connected to the emitter of Q_2, it's no longer a cascode since Q_2 becomes a diode-connected device instead of a current source.**

MOS Cascode Stage



$$R_{out} = (1 + g_{m1} r_{O2}) r_{O1} + r_{O2}$$

$$R_{out} \approx g_{m1} r_{O1} r_{O2}$$

Example 9.5

- **Design an NMOS cascade for an output impedance of 500kΩ and a current of 0.5mA. For simplicity, assume M_1 and M_2 in Fig 9.8 are identical (they need not be). Assume $\mu_n C_{ox} = 100\mu A/V^2$ and $\lambda = 0.1V^{-1}$.**

We must determine W/L for both transistors such that

$$g_{m1} r_{O1} r_{O2} = 500 \text{ k}\Omega.$$

Since $r_{O1} = r_{O2} = (\lambda I_D)^{-1} = 20 \text{ k}\Omega$, we require that $g_{m1} = (800 \ \Omega)^{-1}$ and hence

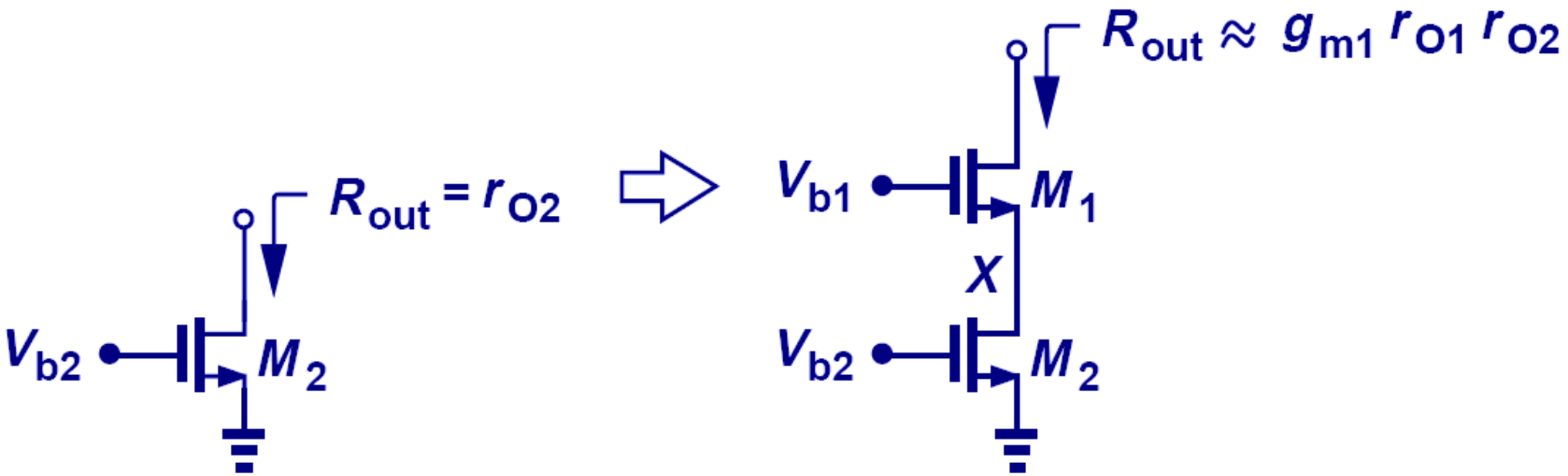
$$\sqrt{2\mu_n C_{ox} \frac{W}{L} I_D} = \frac{1}{800 \ \Omega}.$$

It follows that

$$\frac{W}{L} = 15.6.$$

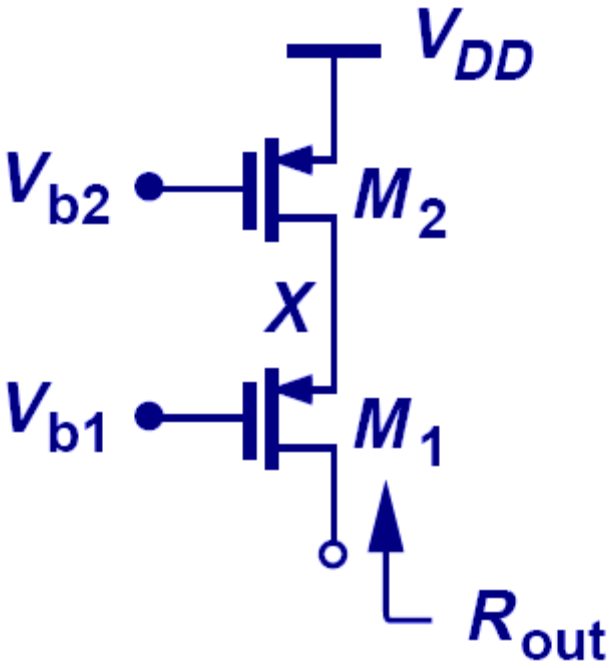
We should also note that $g_{m1} r_{O1} = 25 \gg 1$.

Another Interpretation of MOS Cascode



- **Similar to its bipolar counterpart, MOS cascode can be thought of as stacking a transistor on top of a current source.**
- **Unlike bipolar cascode, the output impedance is not limited by β.**

PMOS Cascode Stage

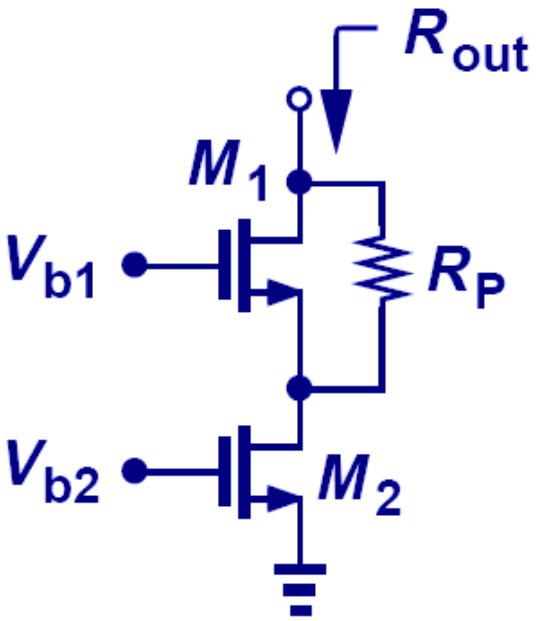


$$R_{out} = (1 + g_{m1} r_{O2}) r_{O1} + r_{O2}$$

$$R_{out} \approx g_{m1} r_{O1} r_{O2}$$

Example 9.6

- **During manufacturing, a large parasitic resistor, R_P ,has appeared in a cascode as shown in Fig. 9. 11. Determine the output resistance.**



R_p is in parallel with r_{O1}.

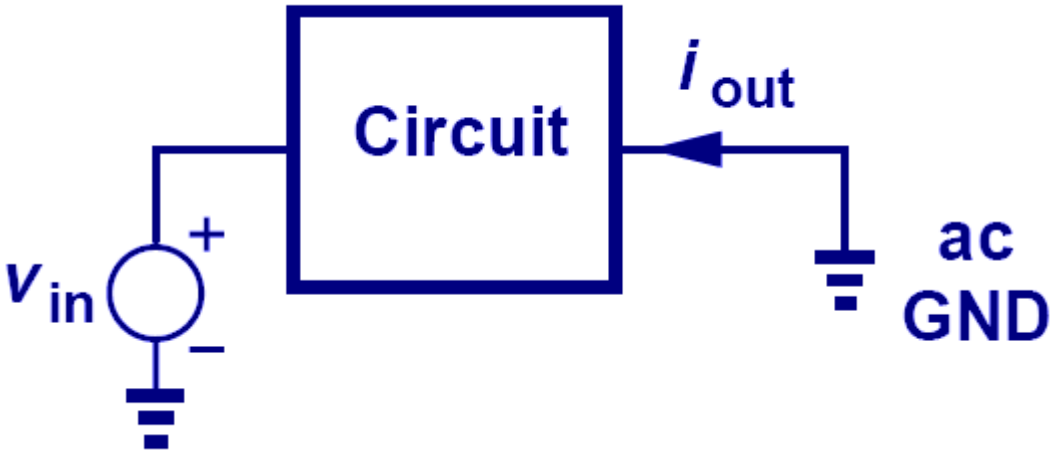
$$R_{out} = g_{m1}(r_{O1}||R_p)r_{O2}.$$

If $g_{m1}(r_{O1}||R_p)$ is not much greater than unity, we return to the original equation, (9.22),

$$R_{out} = (1+g_{m1}r_{O2})(r_{O1} \parallel R_P) + r_{O2}$$

- **R_P will lower the output impedance, since its parallel combination with r_{O1} will always be lower than r_{O1}.**

Short-Circuit Transconductance

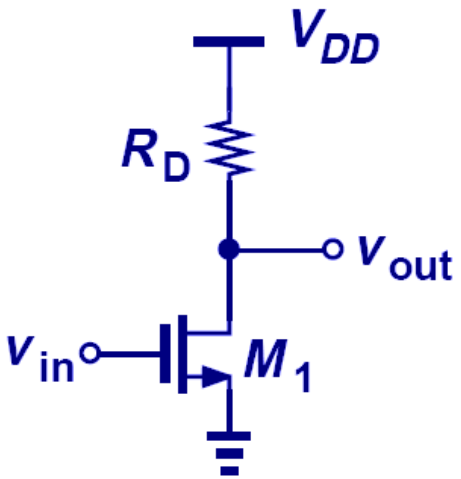


$$G_m = \left.\frac{i_{out}}{v_{in}}\right|_{v_{out}=0}$$

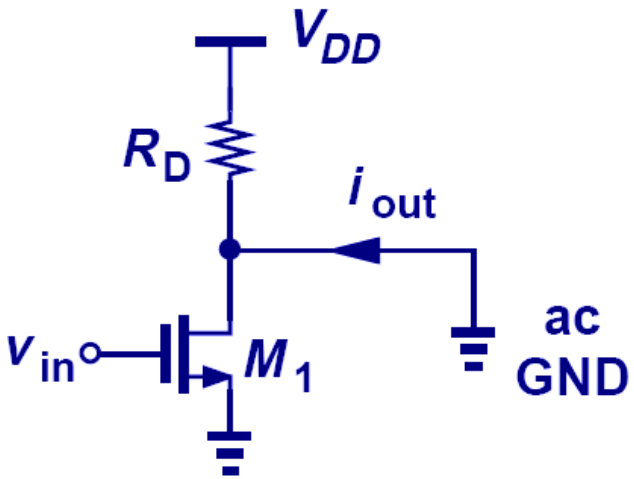
- **The short-circuit transconductance of a circuit measures its strength in converting input voltage to output current.**

Example 9.7

- **Calculate the transconductance of the CS stage shown in Fig. 9.13(a).**



(a)

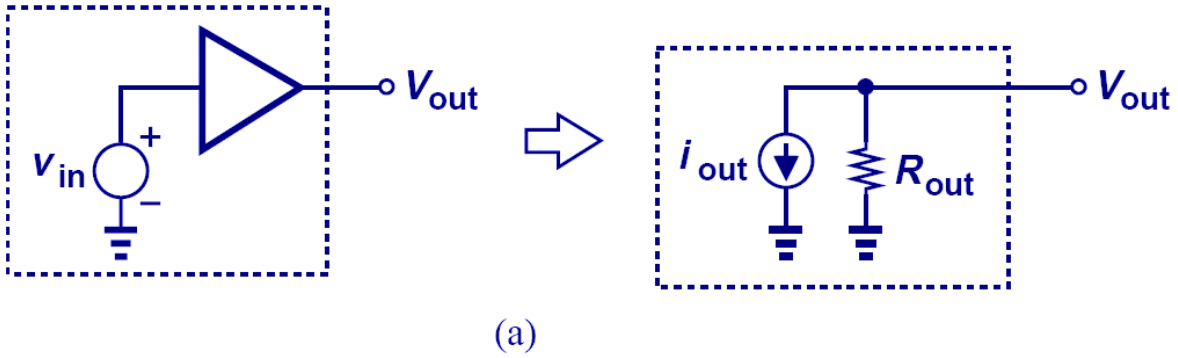


(b)

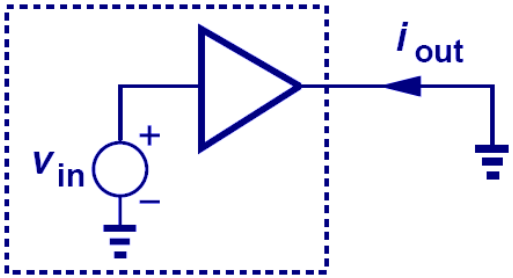
$$G_m = \frac{i_{out}}{v_{in}} = \frac{i_{D1}}{v_{GS1}} = g_{m1}.$$

$$G_m = g_{m1}$$

Derivation of Voltage Gain



(a)



(b)

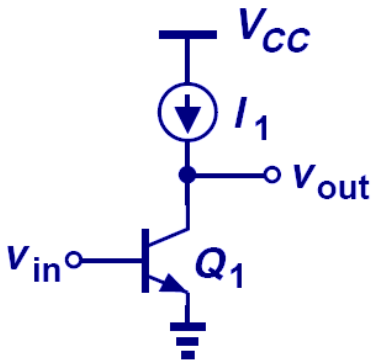
$$v_{out} = -i_{out}R_{out} = -G_m v_{in} R_{out}$$

$$v_{out} / v_{in} = -G_m R_{out}$$

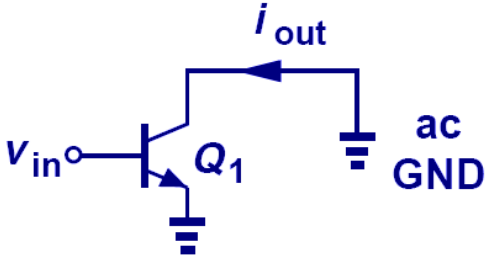
- **By representing a linear circuit with its Norton equivalent, the relationship between V_{out} and V_{in} can be expressed by the product of G_m and R_{out}.**

Example 9.8

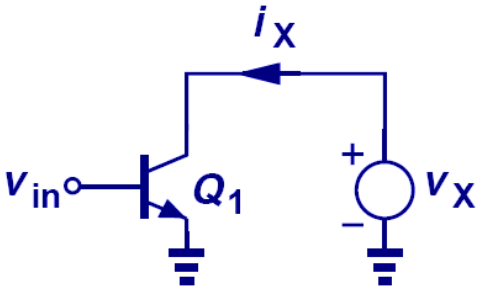
- **Determine the voltage gain of the common-emitter stage shown in Fig. 9.15(a).**



(a)



(b)



(c)

i_{out} is simply equal to the $g_{m1}v_{in}$, i.e., r_O does not carry a current

$$G_m = \frac{i_{out}}{v_{in}} = g_{m1}.$$

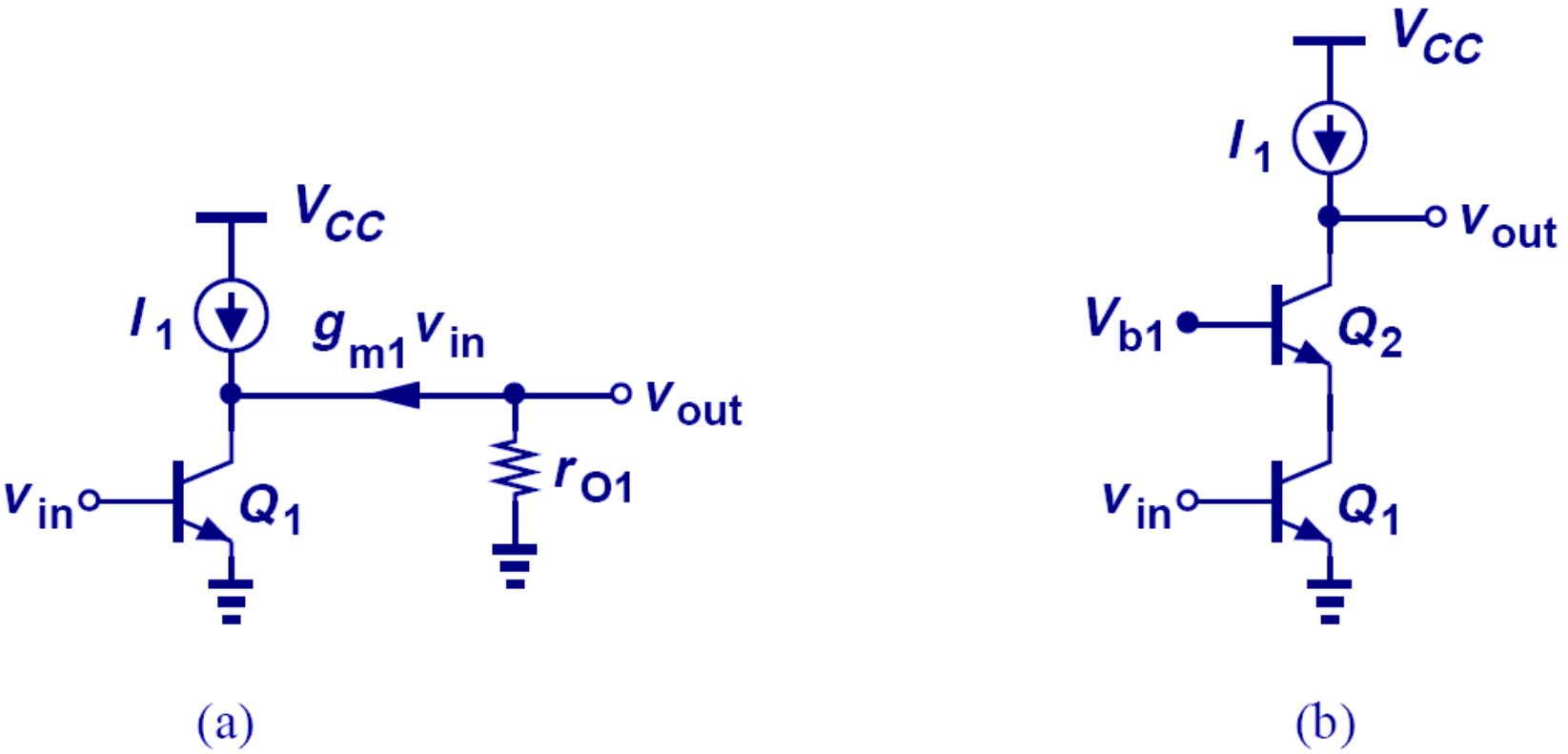
$$R_{out} = \frac{v_X}{i_X} = r_{O1}.$$

It follows that

$$A_v = -G_m R_{out} = -g_{m1} r_{O1}.$$

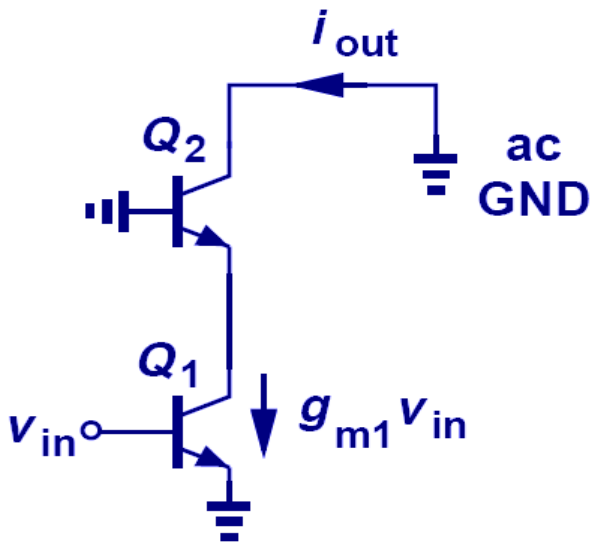
$$\boxed{A_v = -g_{m1} r_{O1}}$$

Comparison between Bipolar Cascode and CE Stage

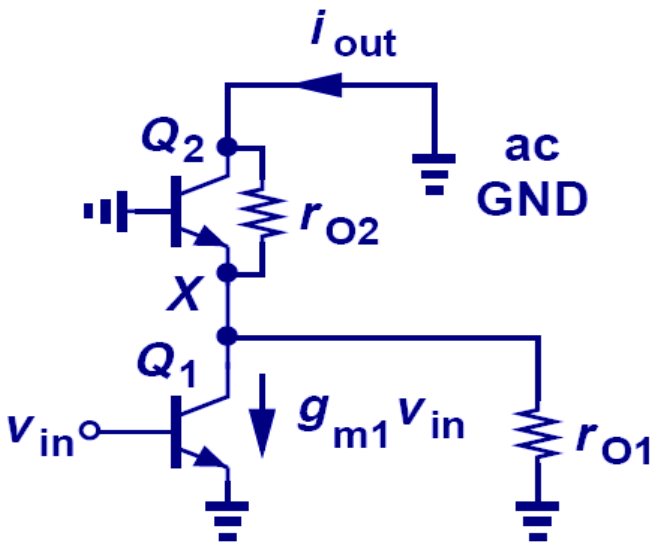


- **Since the output impedance of bipolar cascode is higher than that of the CE stage, we would expect its voltage gain to be higher as well.**

Voltage Gain of Bipolar Cascode Amplifier



(a)



(b)

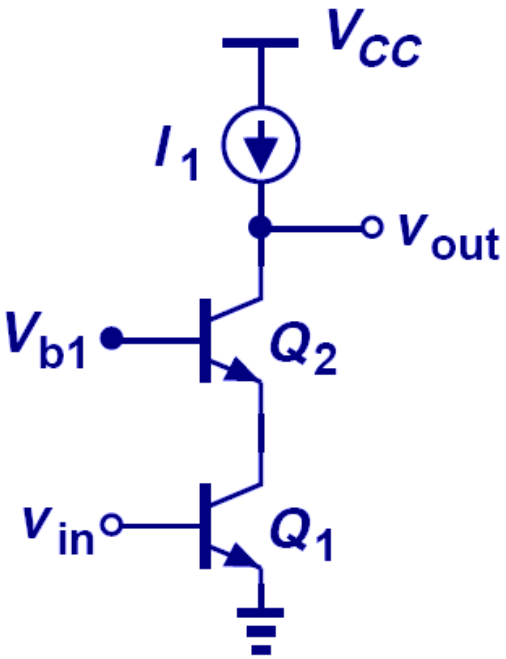
$$G_m \approx g_{m1}$$

$$A_v \approx -g_{m1} r_{O2} g_{m2} (r_{O1} \| r_{\pi 2})$$

- **Since r_O is much larger than $1/g_m$, most of $I_{C,Q1}$ flows into the diode-connected Q_2. Using R_{out} as before, A_V is easily calculated.**

Example 9.9

- **The bipolar cascade of Fig.9.16(b) is biased at a current of 1mA. If V_A=5V and β=100 for both transistors, determine the voltage gain. Assume the load is an ideal current source.**



(b)

$g_{m1} = (26\ \Omega)^{-1}, r_{\pi 1} \approx r_{\pi 2} \approx 2600\ \Omega,$
$r_{O1} \approx r_{O2} = 5\ \text{k}\Omega$. Thus,

$$g_{m1}(r_{O1} || r_{\pi 2}) = 65.8$$

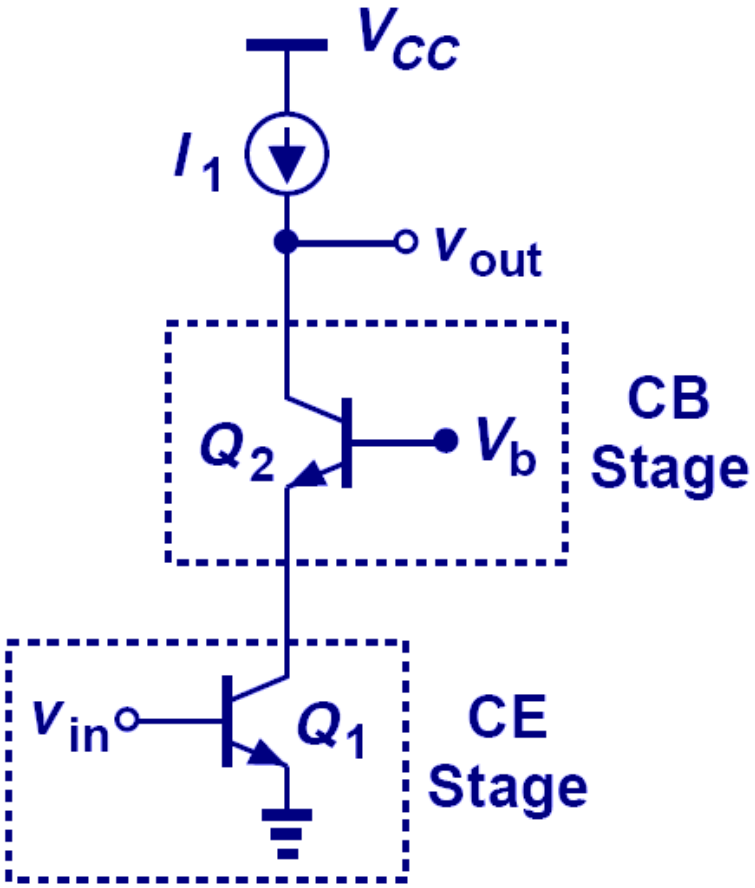
$$G_m \approx g_{m1}$$

$$A_v \approx -g_{m1} r_{O2} g_{m2} (r_{O1} \,||\, r_{\pi 2})$$

$$|A_v| = 12,654.$$

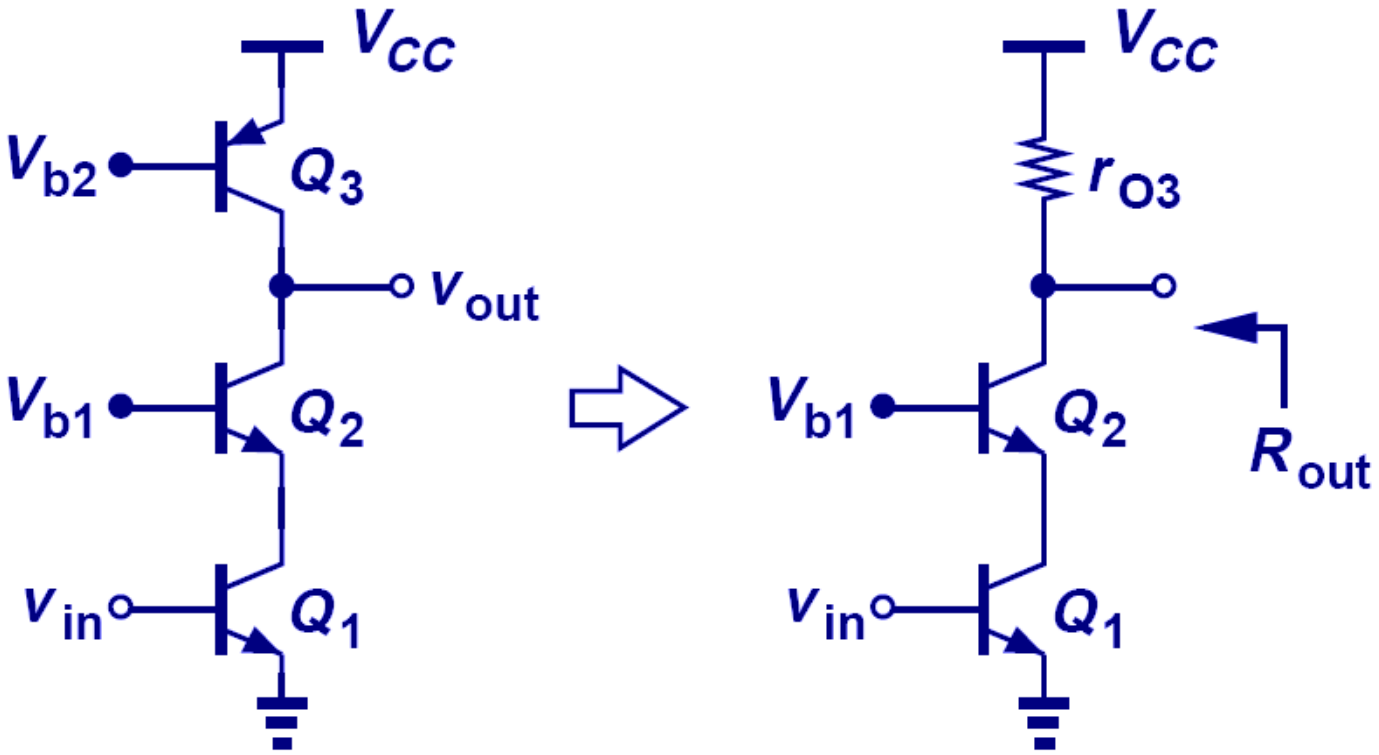
- **Cascoding thus raises the voltage gain by a factor of 65.8.**

Alternate View of Cascode Amplifier



- **A bipolar cascode amplifier is also a CE stage in series with a CB stage.**

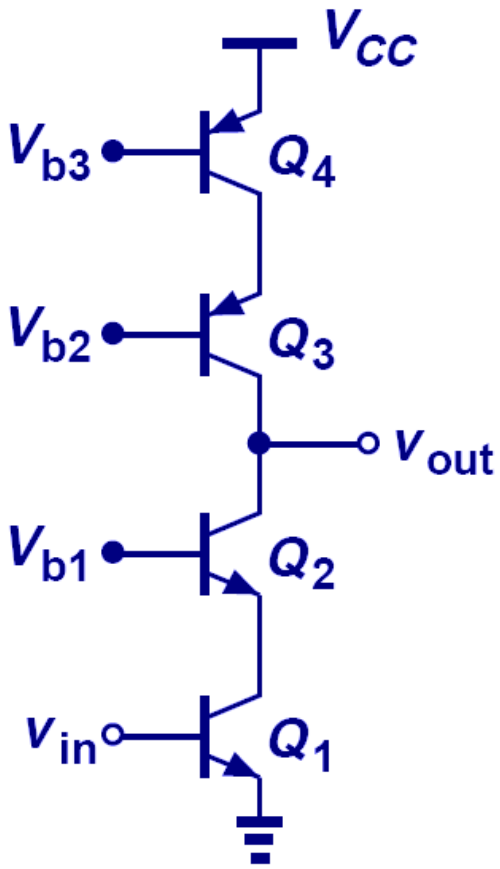
Practical Cascode Stage



$$R_{out} \approx r_{O3} \parallel g_{m2} r_{O2} (r_{O1} \parallel r_{\pi 2})$$

- **Since no current source can be ideal, the output impedance drops.**

Improved Cascode Stage

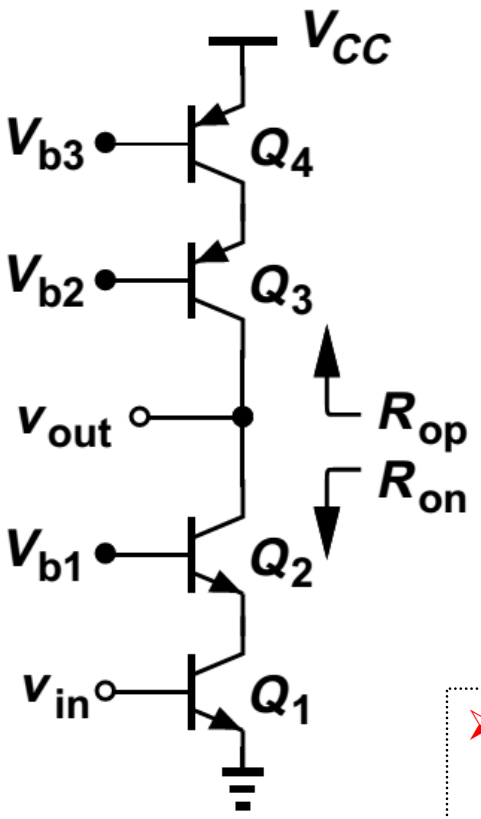


$$R_{out} \approx g_{m3} r_{O3} (r_{O4} \parallel r_{\pi 3}) \parallel g_{m2} r_{O2} (r_{O1} \parallel r_{\pi 2})$$

- **In order to preserve the high output impedance, a cascode PNP current source is used.**

Example 9.10

- **Suppose the circuit of Example 9.9 incorporates a cascode load using *pnp* transistors with V_A = 4V and β = 50. What is the voltage gain?**



$$R_{on} \approx g_{m2} r_{O2} (r_{O1} || r_{\pi 2})$$

$$R_{op} \approx g_{m3} r_{O3} (r_{O4} || r_{\pi 3}).$$

The load transistors carry a collector current of approximately 1 mA. Thus,

$$R_{op} = g_{m3} r_{O3} (r_{O4} || r_{\pi 3})$$

$$= 151 \text{ k}\Omega$$

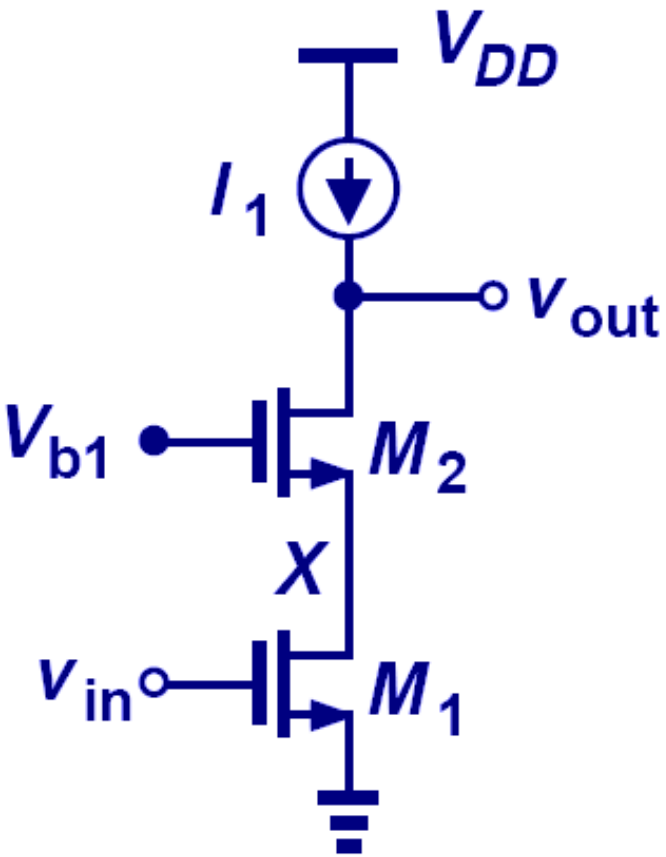
$$R_{on} = 329 \text{ k}\Omega.$$

$$|A_v| = g_{m1} (R_{on} || R_{op})$$

$$= 3,981.$$

- **Compared to the ideal current source case, the gain has fallen by approximately a factor of 3 because the *pnp* devices suffer from a lower Early voltage and β.**

MOS Cascode Amplifier

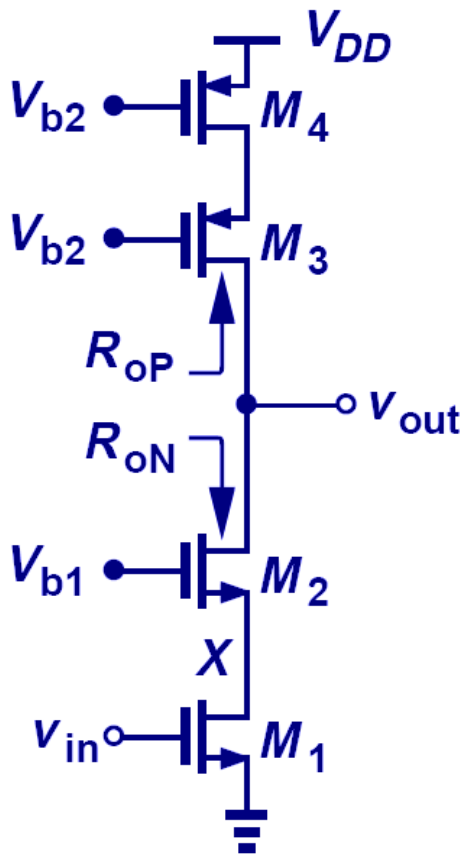


$$A_v = -G_m R_{out}$$

$$A_v \approx -g_{m1}\left[(1+g_{m2}r_{O2})r_{O1} + r_{O2}\right]$$

$$A_v \approx -g_{m1}r_{O1}g_{m2}r_{O2}$$

Improved MOS Cascode Amplifier



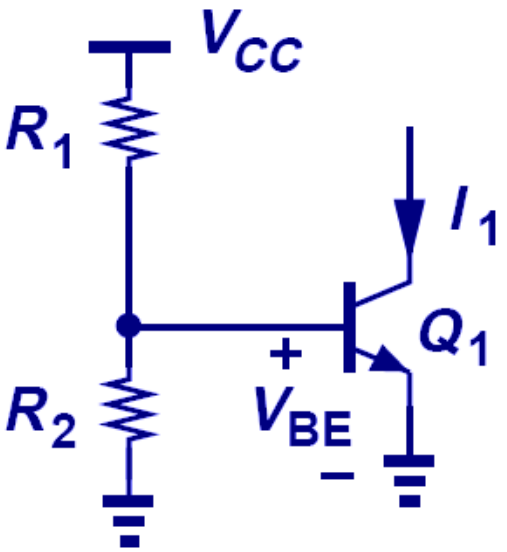
$$R_{on} \approx g_{m2} r_{O2} r_{O1}$$

$$R_{op} \approx g_{m3} r_{O3} r_{O4}$$

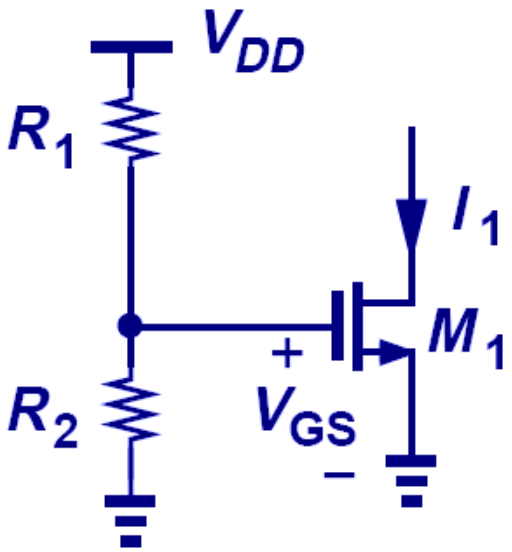
$$R_{out} = R_{on} \parallel R_{op}$$

- **Similar to its bipolar counterpart, the output impedance of a MOS cascode amplifier can be improved by using a PMOS cascode current source.**

Temperature and Supply Dependence of Bias Current



(a)



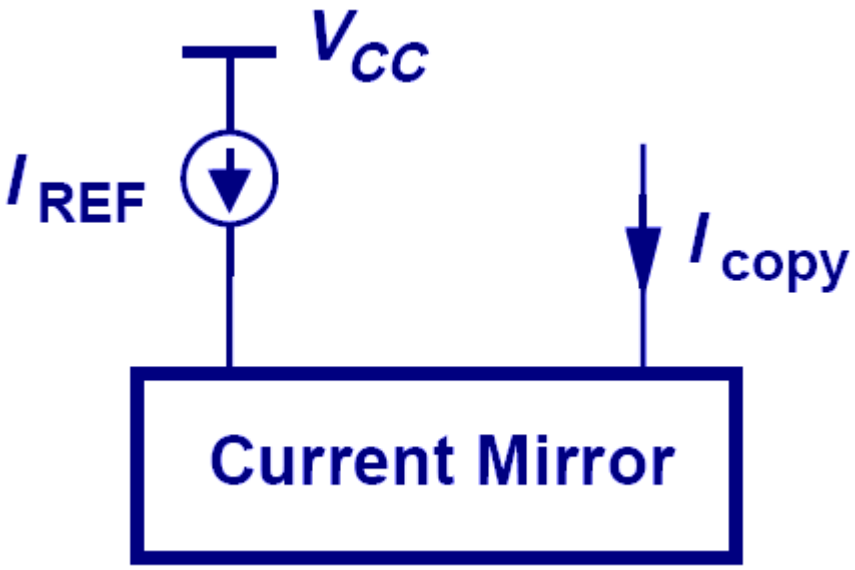
(b)

$$R_2 V_{CC}/(R_1+R_2) - I_1/\beta \cdot (R_1 \| R_2) = V_T \ln(I_1/I_S)$$

$$I_1 = \frac{1}{2}\mu_n C_{ox}\frac{W}{L}\left(\frac{R_2}{R_1+R_2}V_{DD} - V_{TH}\right)^2$$

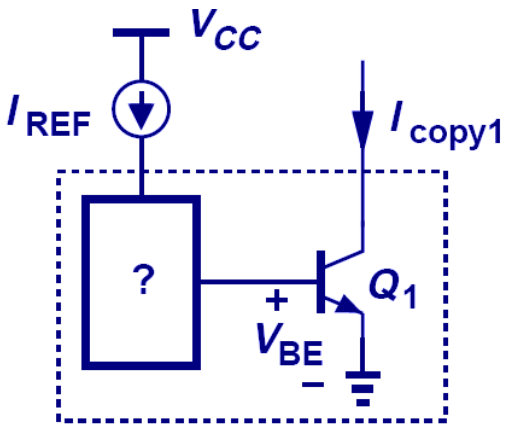
- Since V_T, I_S, μ_n, and V_{TH} all depend on temperature, I_1 for both bipolar and MOS depends on temperature and supply.

Concept of Current Mirror

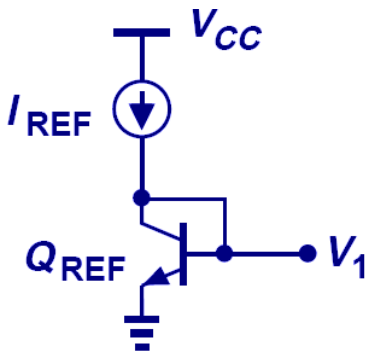


- **The motivation behind a current mirror is to sense the current from a "golden current source" and duplicate this "golden current" to other locations.**

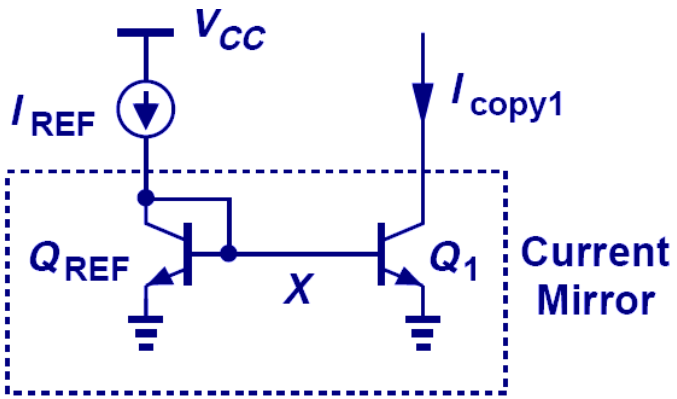
Bipolar Current Mirror Circuitry



(a)



(b)

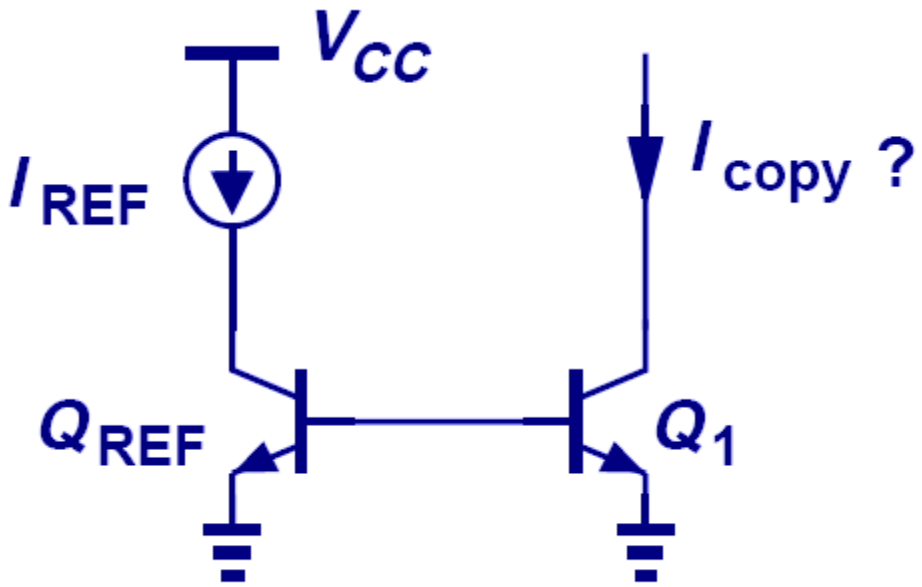


(c)

$$I_{copy} = \frac{I_{S1}}{I_{S,REF}} I_{REF}$$

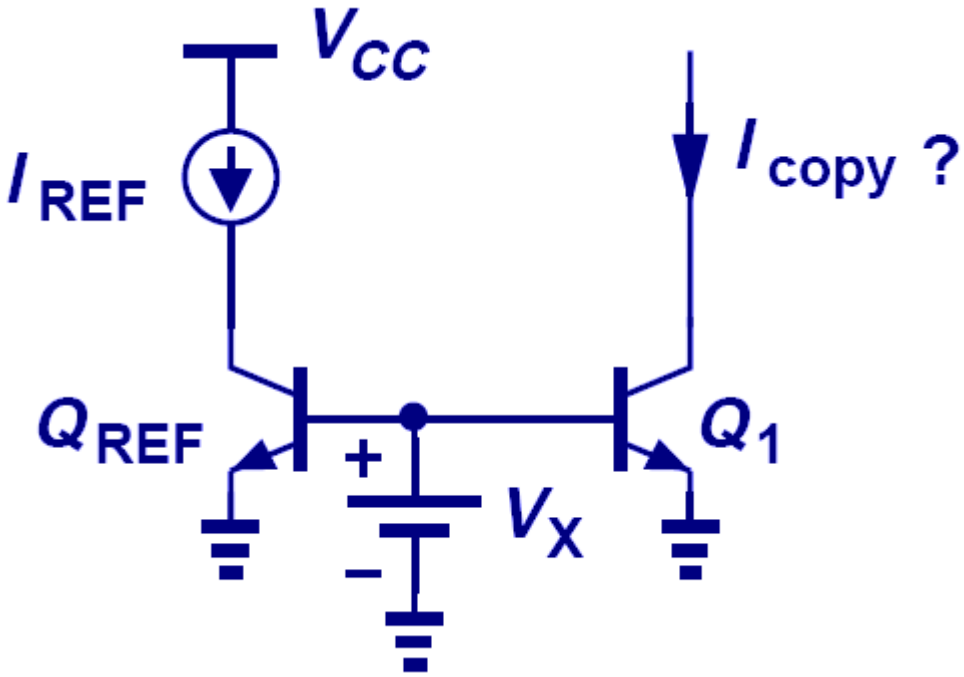
- **The diode-connected Q_{REF} produces an output voltage V_1 that forces $I_{copy1} = I_{REF}$, if $Q_1 = Q_{REF}$.**

Bad Current Mirror Example I



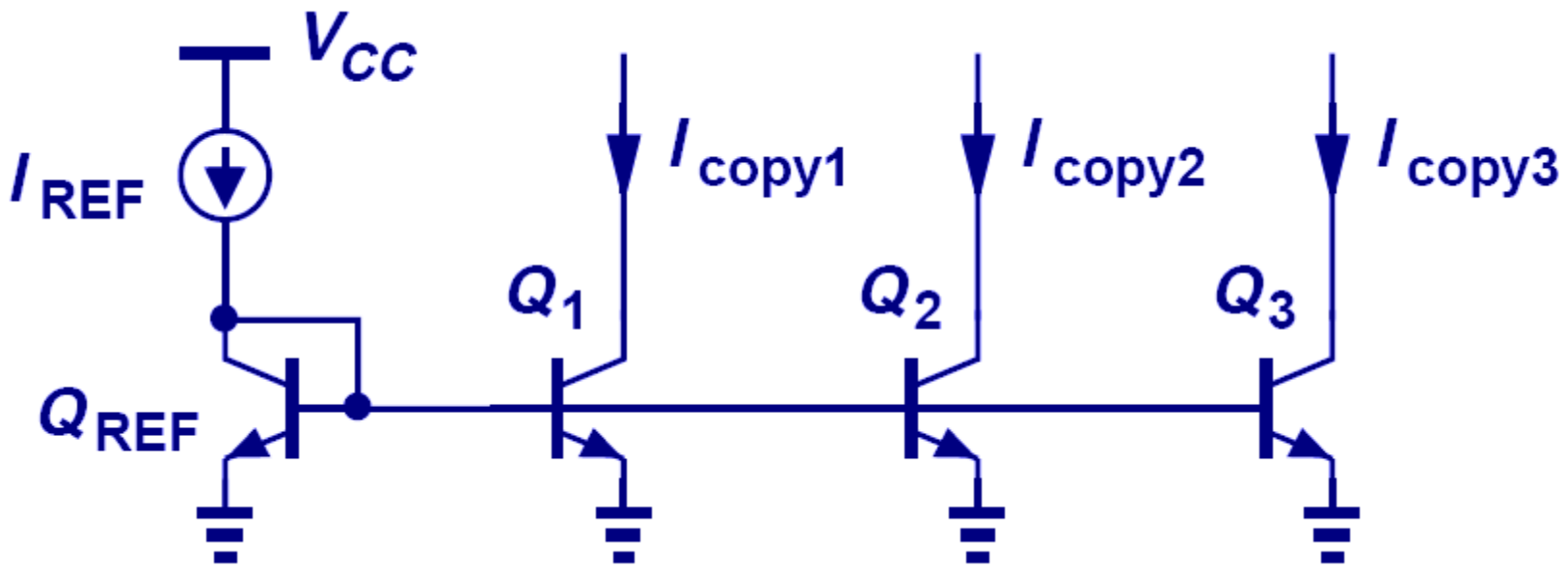
- **Without shorting the collector and base of Q_{REF} together, there will not be a path for the base currents to flow, therefore, I_{copy} is zero.**

Bad Current Mirror Example II



- **Although a path for base currents exists, this technique of biasing is no better than resistive divider.**

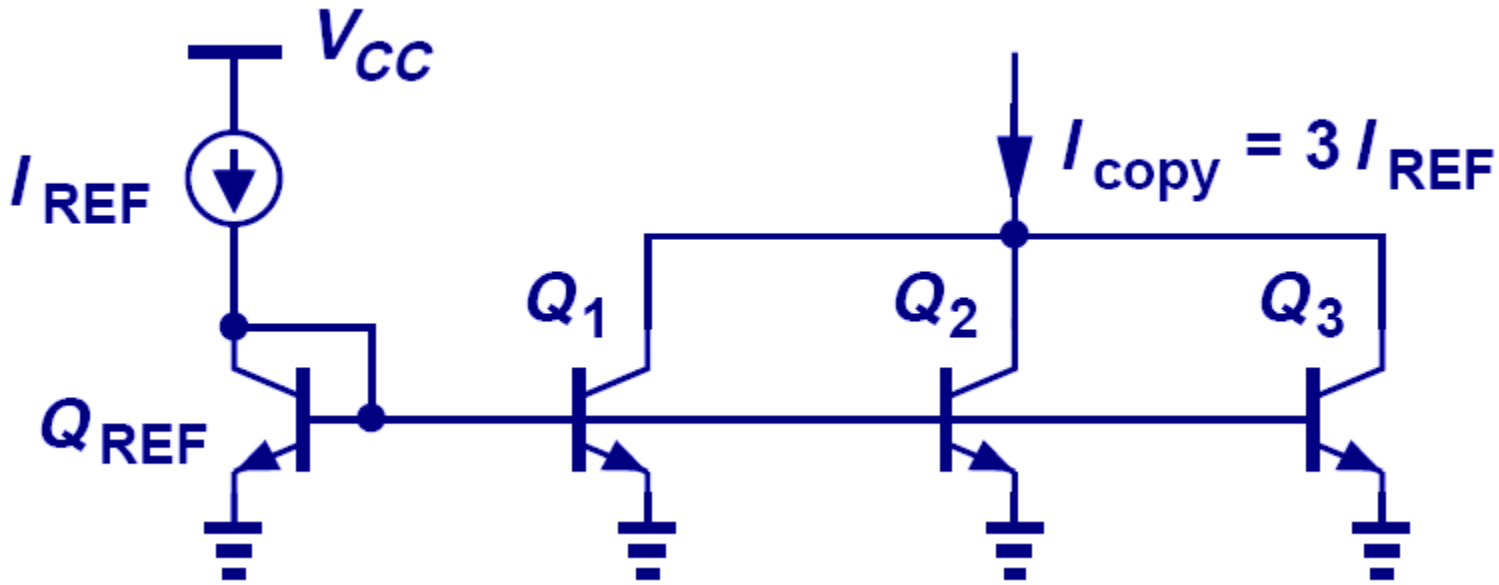
Multiple Copies of I_{REF}



$$I_{copy,j} = \frac{I_{S,j}}{I_{S,REF}} I_{REF}$$

- **Multiple copies of I_{REF} can be generated at different locations by simply applying the idea of current mirror to more transistors.**

Current Scaling

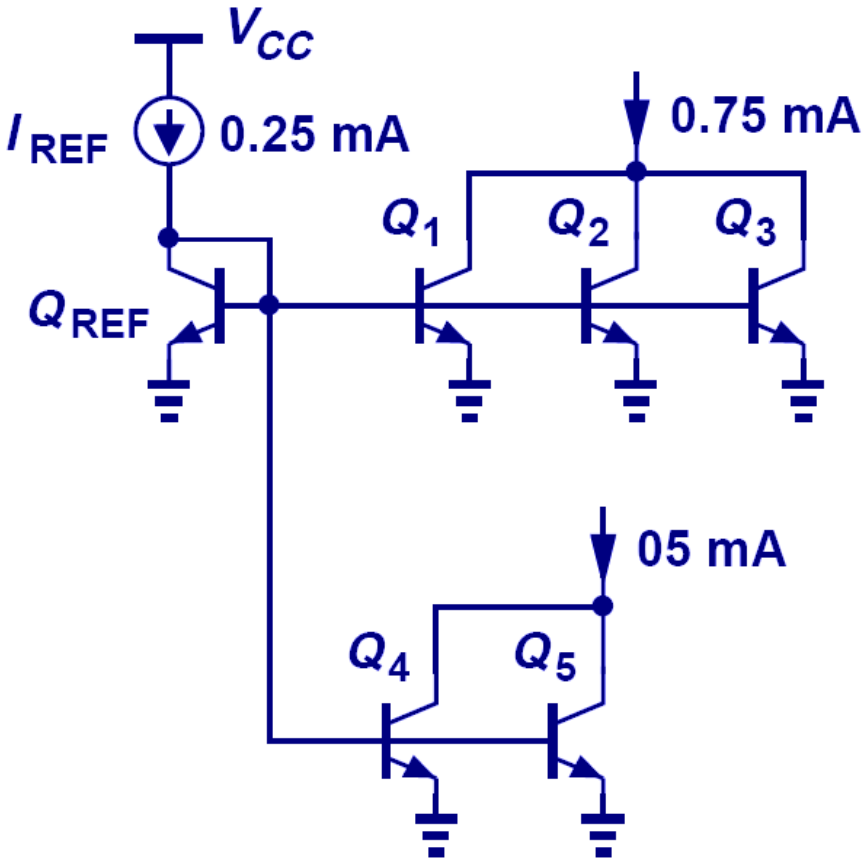


$$I_{copy,j} = nI_{REF}$$

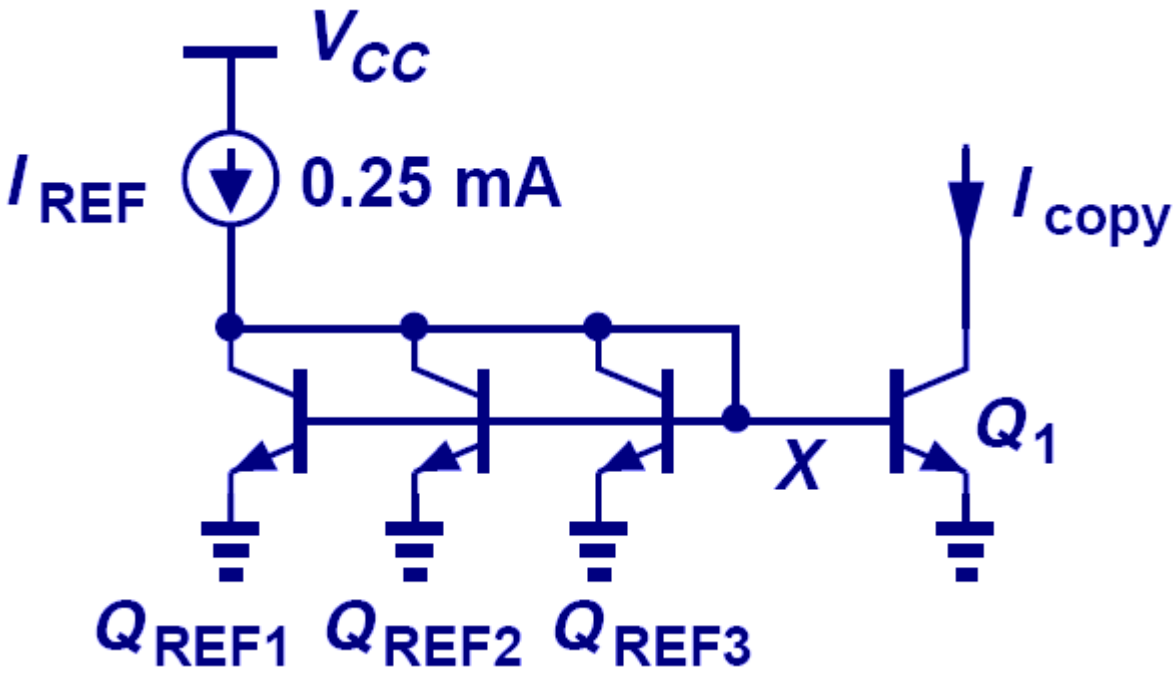
- By scaling the emitter area of Q_j n times with respect to Q_{REF}, $I_{copy,j}$ is also n times larger than I_{REF}. This is equivalent to placing n unit-size transistors in parallel.

Example 9.14 : Scaled Current

- **A multistage amplifier incorporates two current sources of values 0.75mA and 0.5mA. Using a bandgap reference current of 0.25mA, design the require current sources. Neglect the effect of the base current for now.**



Fractional Scaling

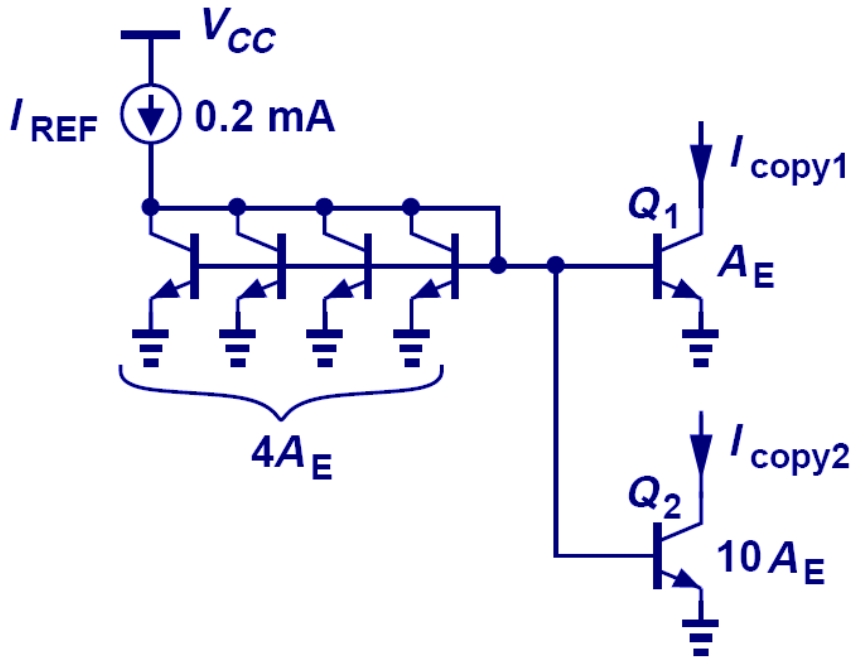


$$I_{copy} = \frac{1}{3} I_{REF}$$

- A fraction of I_{REF} can be created on Q_1 by scaling up the emitter area of Q_{REF}.

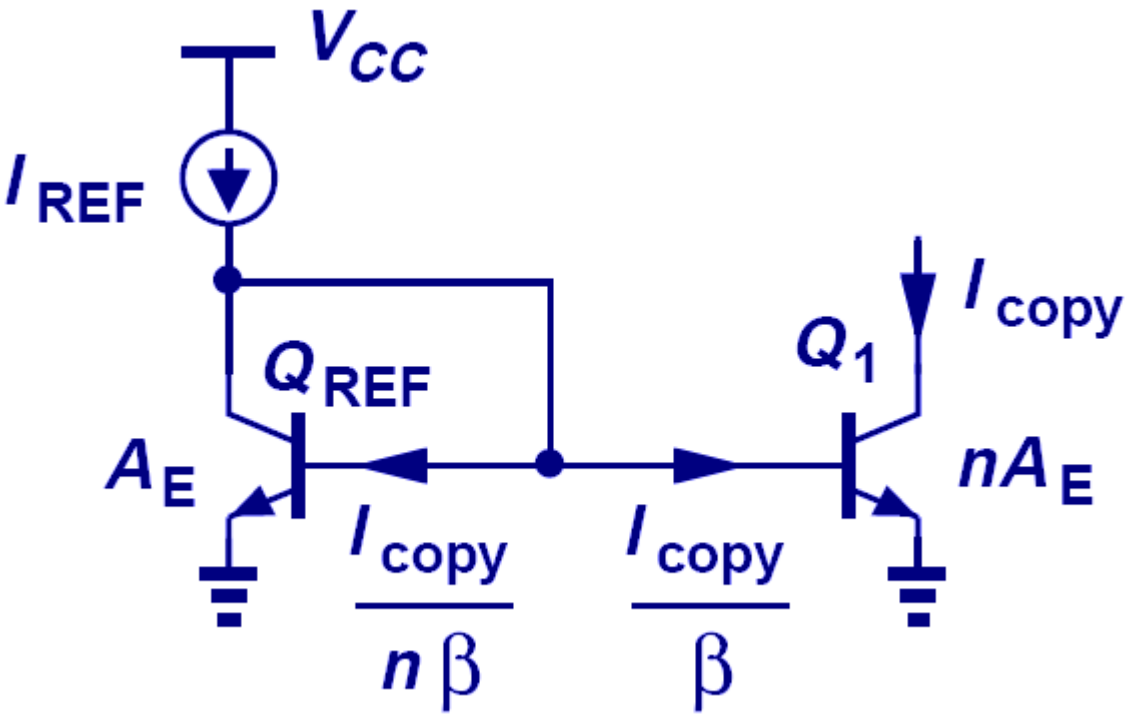
Example 9.15 : Different Mirroring Ratio

- It is desired to generate two currents equal to 50uA and 500uA from a reference of 200uA. Design the current mirror circuit.



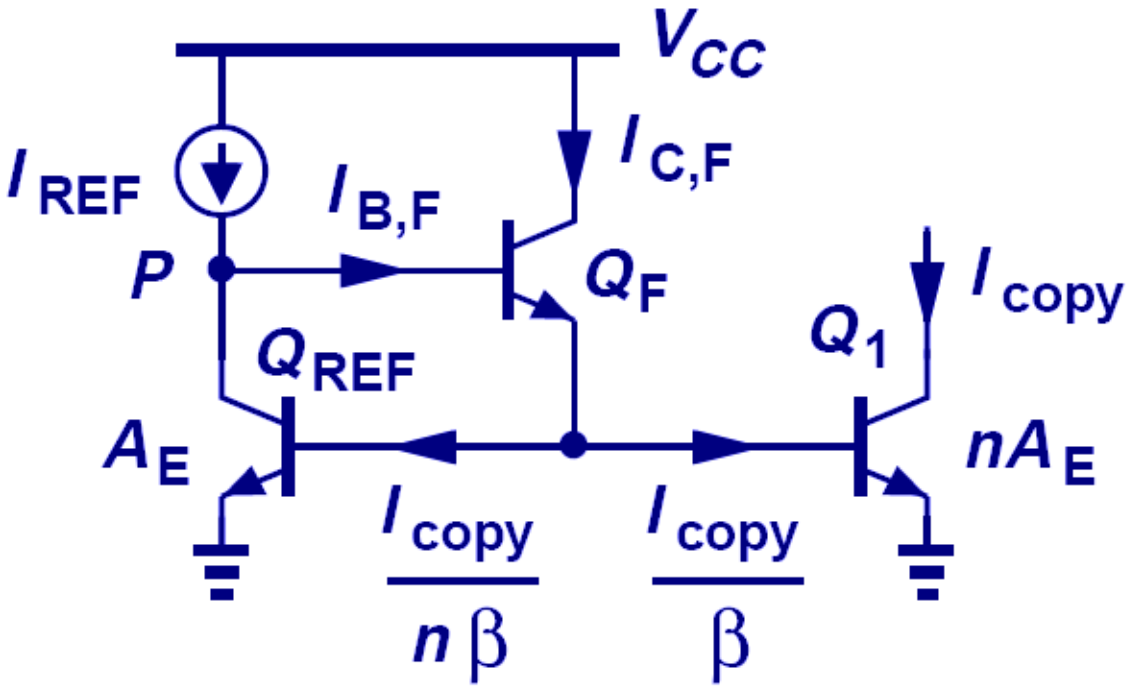
- Using the idea of current scaling and fractional scaling, I_{copy2} is 0.5mA and I_{copy1} is 0.05mA respectively. All coming from a source of 0.2mA.

Mirroring Error Due to Base Currents



$$I_{copy} = \frac{nI_{REF}}{1+\frac{1}{\beta}(n+1)}$$

Improved Mirroring Accuracy

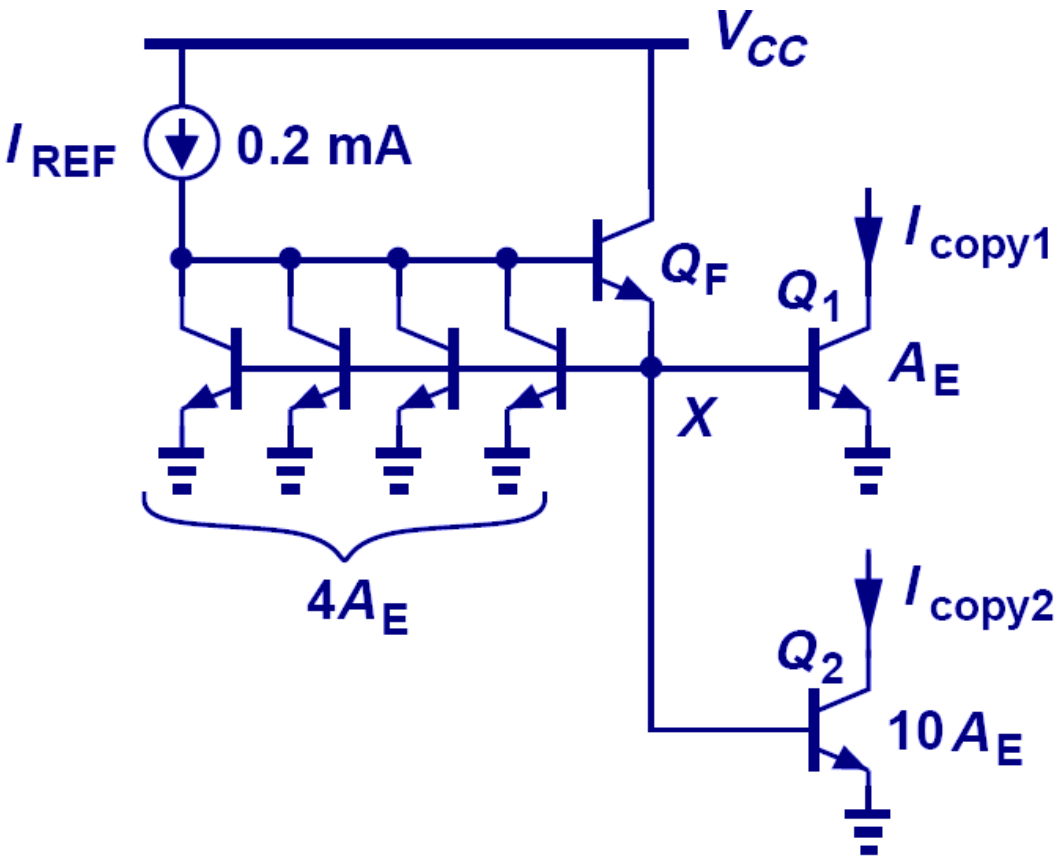


$$I_{copy} = \frac{nI_{REF}}{1 + \frac{1}{\beta^2}(n+1)}$$

- Because of Q_F, the base currents of Q_{REF} and Q_1 are mostly supplied by Q_F rather than I_{REF}. Mirroring error is reduced β times.

Example 9.16 : Different Mirroring Ratio Accuracy

- Compute the I_{copy1} and I_{copy2} in this figure before and after adding a follower.



Before :

$$I_{copy1} = \frac{I_{REF}}{4 + \frac{15}{\beta}}$$

$$I_{copy2} = \frac{10 I_{REF}}{4 + \frac{15}{\beta}}$$

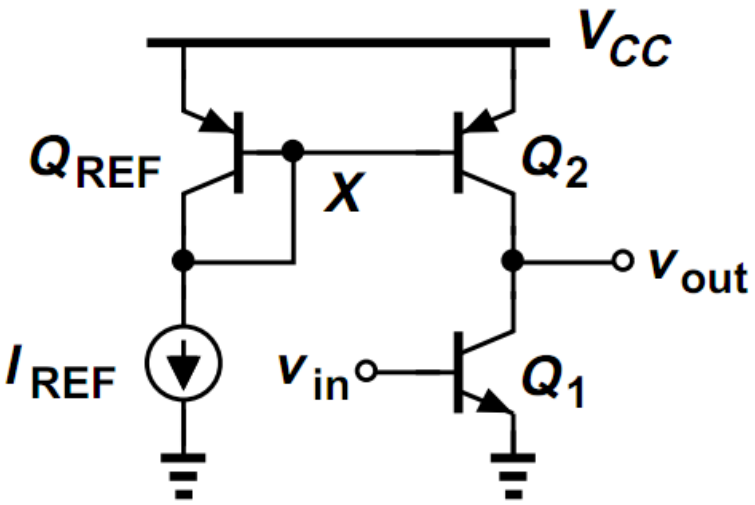
After :

$$I_{copy1} = \frac{I_{REF}}{4 + \frac{15}{\beta^2}}$$

$$I_{copy2} = \frac{10 I_{REF}}{4 + \frac{15}{\beta^2}}$$

Example 9.17 : Different Mirroring Ratio Accuracy

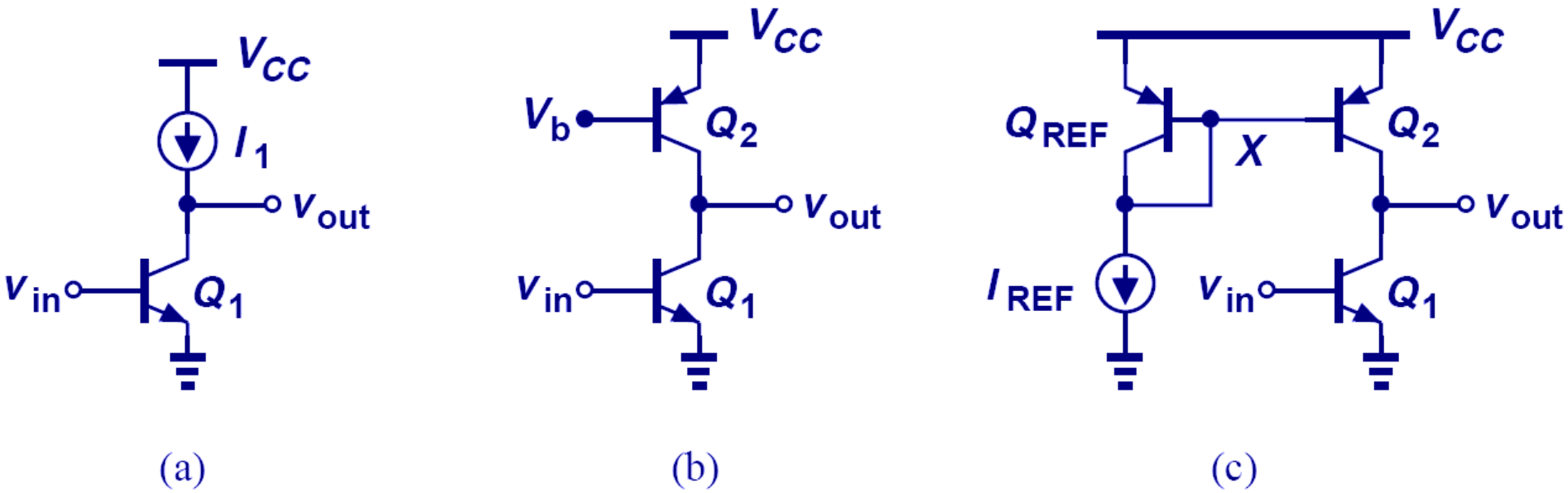
- Design this circuit for a voltage gain 100 and a power budget of 2mW. Assume $V_{A,npn}$ = 5V, $V_{A,pnp}$ = 4V, I_{REF} = 100uA, and V_{CC} = 2.5V.



$$A_v = -g_{m1}(r_{O1}||r_{O2})$$
$$= -\frac{1}{V_T} \cdot \frac{V_{A,npn}V_{A,pnp}}{V_{A,npn}+V_{A,pnp}}$$
$$= -85.5.$$

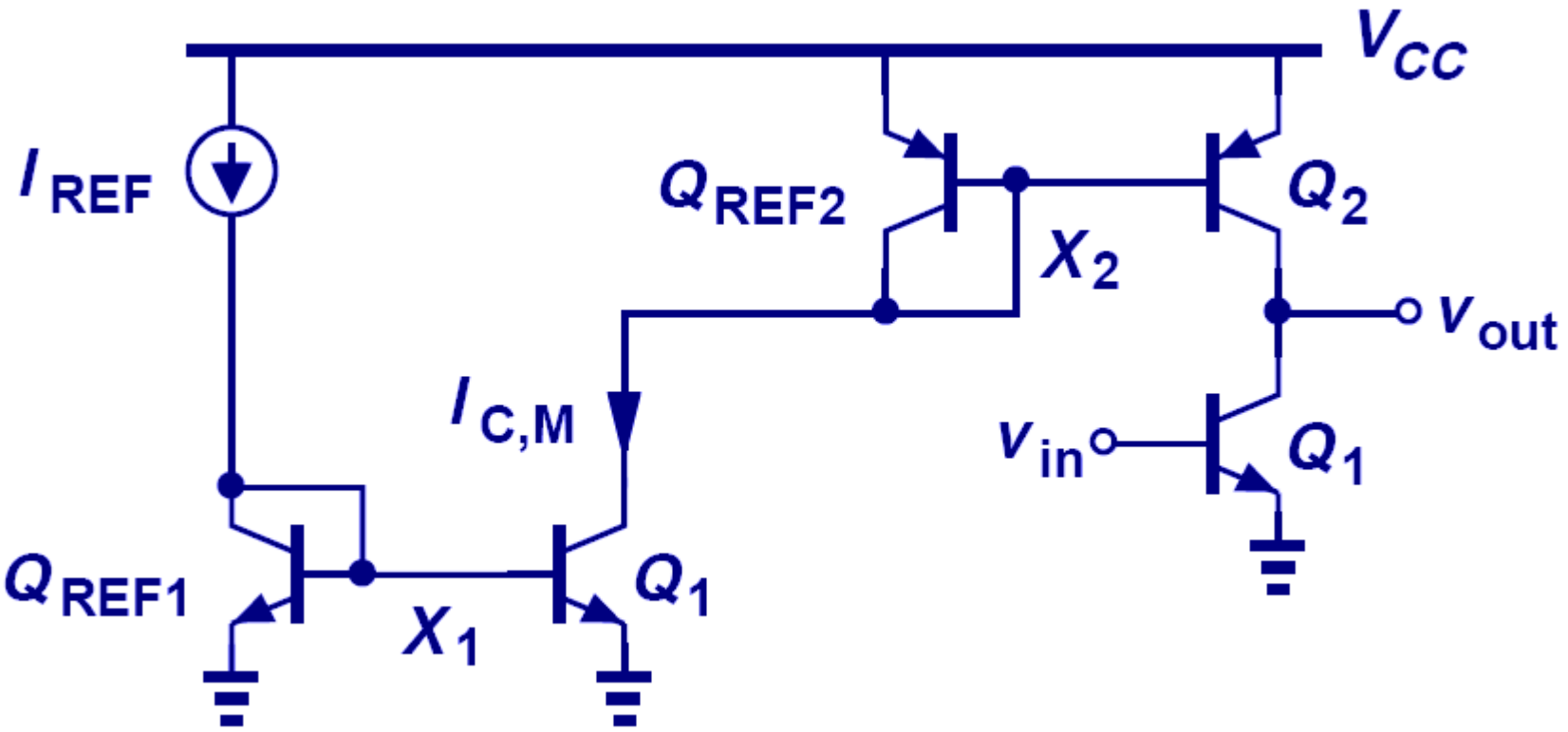
- The gain is smaller than 100 because low Early voltages and V_T, a fundamental constant of the technology, independent of the bias current.

PNP Current Mirror

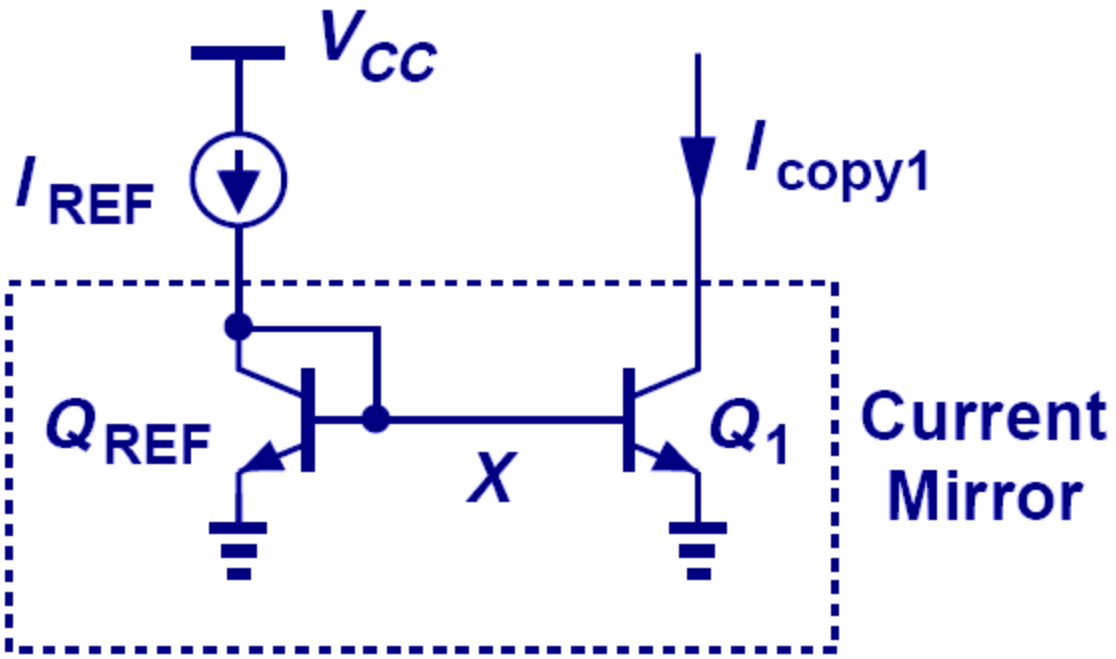


- **PNP current mirror is used as a current source load to an NPN amplifier stage.**

Generation of I_{REF} for PNP Current Mirror

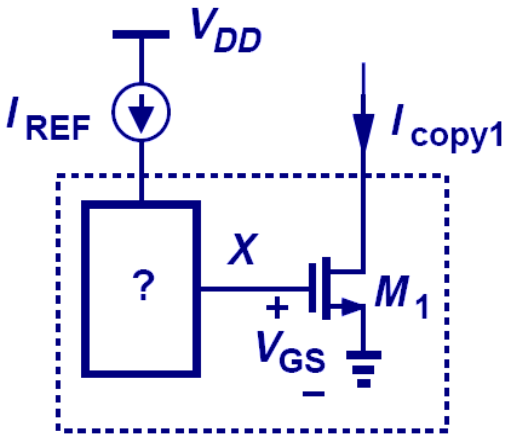


Current Mirror with Discrete Devices

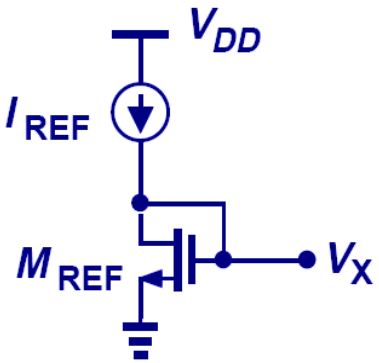


- Let Q_{REF} and Q_1 be discrete NPN devices. I_{REF} and I_{copy1} can vary in large magnitude due to I_S mismatch.

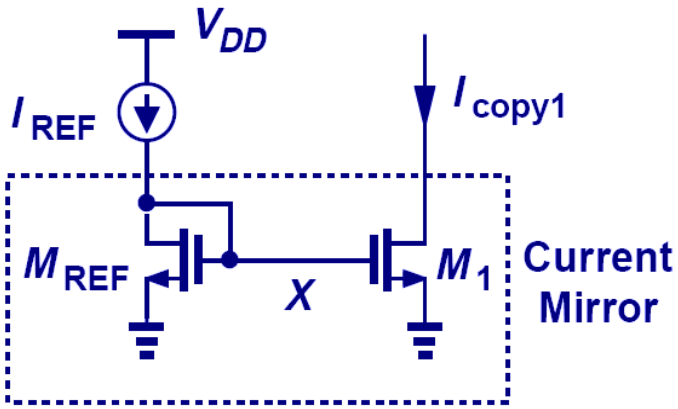
MOS Current Mirror



(a)



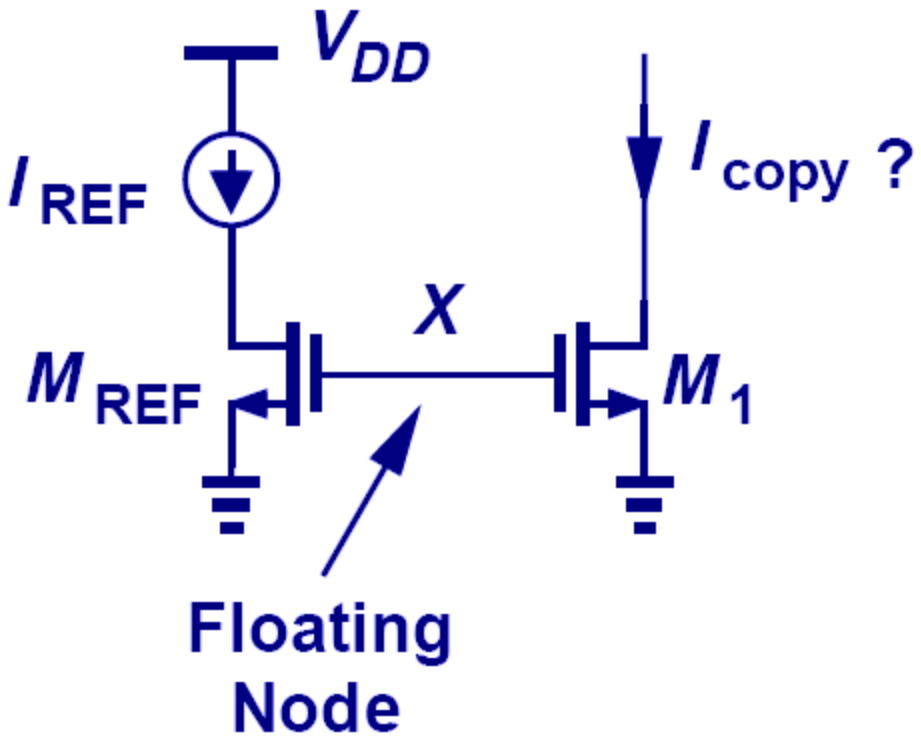
(b)



(c)

- **The same concept of current mirror can be applied to MOS transistors as well.**

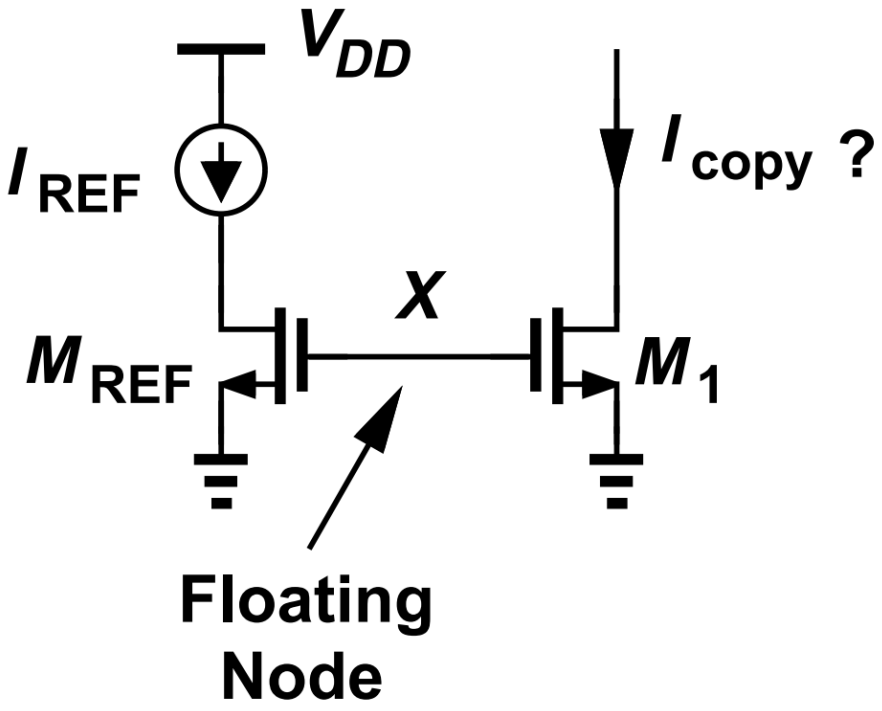
Bad MOS Current Mirror Example



- This is not a current mirror since the relationship between V_X and I_{REF} is not clearly defined.
- The only way to clearly define V_X with I_{REF} is to use a diode-connected MOS since it provides square-law I-V relationship.

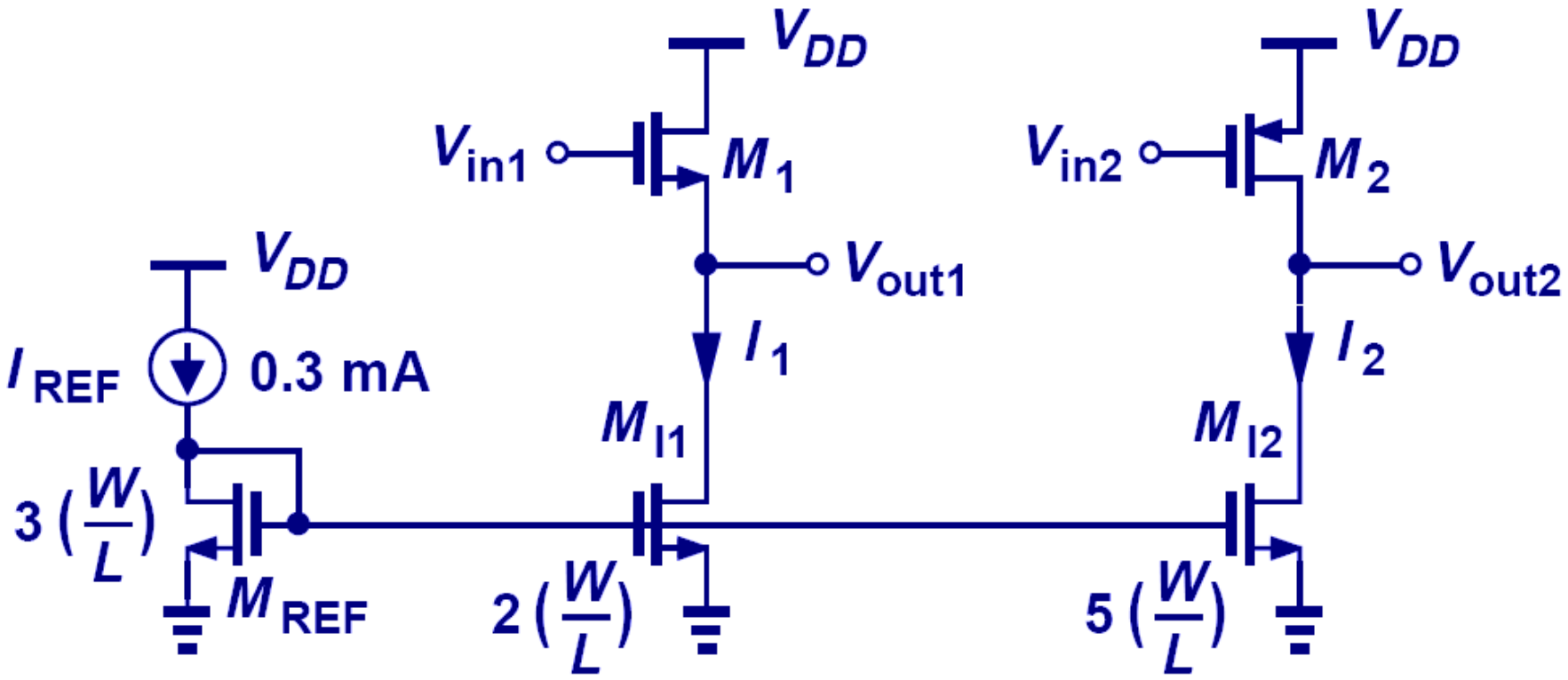
Example 9.20 : Current Mirror ?

- Is this current mirror? Explain what happens.



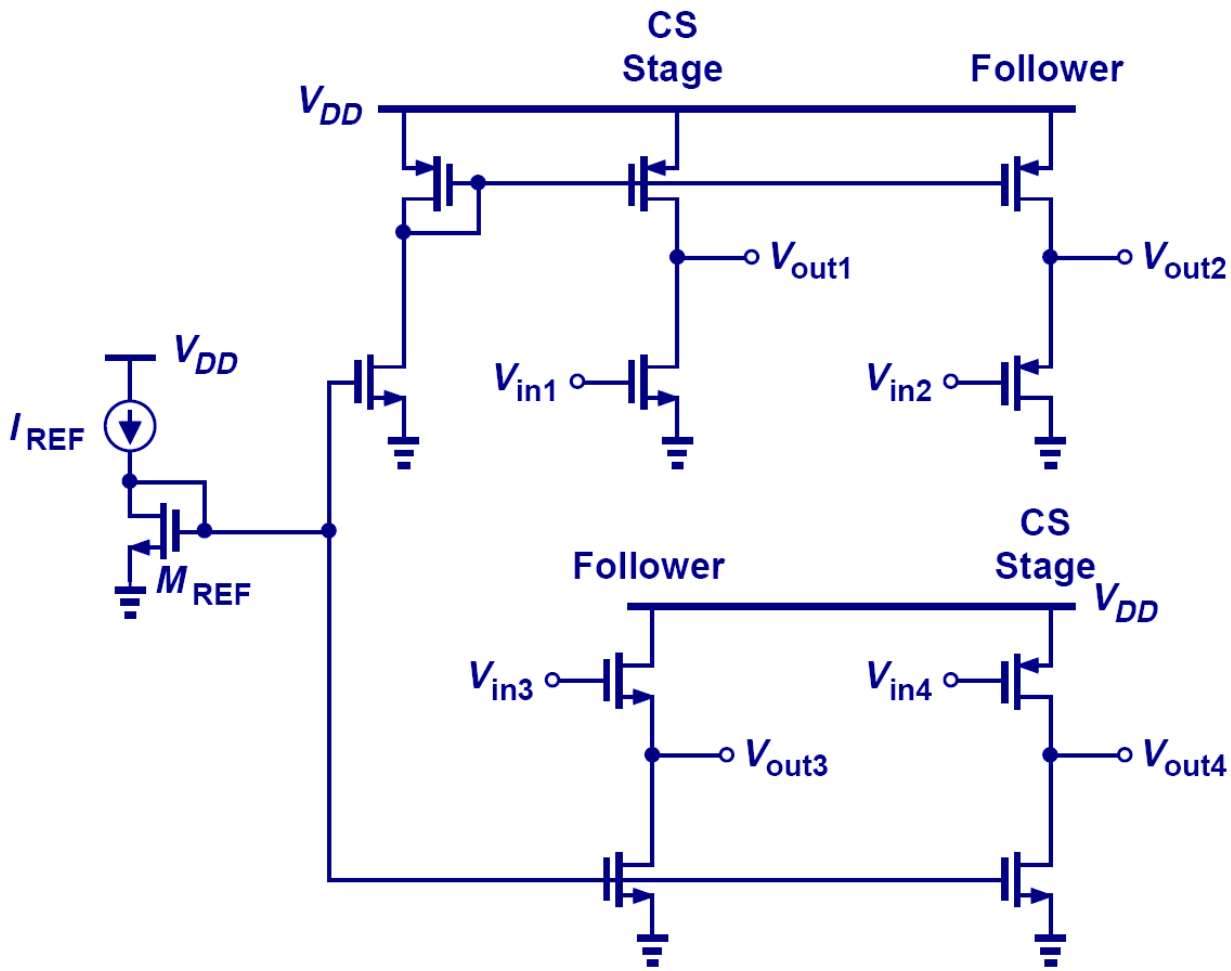
- This circuit is not a current mirror because the gates of M_{REF} and M_1 are floating.

Example 9.21 : Current Scaling



- **Similar to their bipolar counterpart, MOS current mirrors can also scale I_{REF} up or down (I_1 = 0.2mA, I_2 = 0.5mA).**

CMOS Current Mirror



- **The idea of combining NMOS and PMOS to produce CMOS current mirror is shown above.**