## Chapter 7

## Fluid Flow

## What is a fluid?

- Gas
- loosely associated molecules that are not close together and that travel through space for long distances (many times larger than the molecular diameter) before colliding with each other
- Liquid
- Molecules that are very close together (on the same order as their molecular diameter) and that are in collision with each other very frequently as they move around each other


## The Concept of Pressure

- Absolute pressure
- Gauge pressure
- Absolute pressure - Atmospheric pressure



## Example 7.1

- Absolute pressure
= Gauge pressure + Atmospheric pressure
= 34.0 psig + 14.2 psia (usually 14.7 psia)
$=48.2$ psia
- pounds $\left(1 b_{f}\right)$ per square inch (psi)
- psia
- psig
- $1 \mathrm{~atm}=14.7 \mathrm{psi}=760 \mathrm{mmHg}=101,300 \mathrm{~Pa}$


## Non-flowing (stagnant) Fluids



$$
P_{2}-P_{1}=\rho g\left(z_{1}-z_{2}\right)
$$

$\rho$ is fluid density
$z$ is distance UPWARD
1 and 2 are locations in the liquid

## Example

$$
P_{2}-P_{1}=\rho g\left(z_{1}-z_{2}\right)
$$

Example: The Titanic sank in $12,500 \mathrm{ft}$. What is the pressure (in $p s i$ ) where she lies?

Note: the density of sea water is $\sim 64.3 \mathrm{lb} b_{m} / t t^{3}$


## Principles of Fluid Flow

- Laminar flow

- Turbulent flow



## Principles of Fluid Flow



- Average velocity ( $v_{\text {avg }}$ )
- Volumetric flow rate
$\dot{V}=V_{\text {avg }} A_{c s}$
$A_{c s}$ : cross-sectional area
- Mass flow rate

$$
\rho \dot{V}=\dot{m}=\rho v_{a v g} A_{c s}
$$

## Mechanical Energy Equation

For steady-state incompressible flow (in the unit of energy per mass of fluid)

$$
\left(\frac{P}{\rho}+\frac{1}{2} \alpha v_{a v e}^{2}+g z\right)_{o u t}-\left(\frac{P}{\rho}+\frac{1}{2} \alpha v_{a v e}^{2}+g z\right)_{\text {in }}=w_{s}-w_{f}
$$



## Mechanical Energy

- Kinetic energy
- K.E.: $1 / 2 m\left(v^{2}\right)_{\text {avg }}$
- K.E. per mass: $1 / 2\left(\mathrm{v}^{2}\right)_{\text {avg }}=1 / 2 \alpha\left(\mathrm{v}_{\text {avg }}\right)^{2}$
- $\alpha$ : a conversion factor from $\left(\mathrm{v}_{\text {avg }}\right)^{2}$ to $\left(\mathrm{v}^{2}\right)_{\text {avg }}$
- Can be assumed to equal 1.0
- Potential energy
- P.E.: mgz
- P.E. per mass: gz
- Energy associated with pressure
- P : force/area, $\rho$ : mass/volume
- P/ $\rho$ : energy/mass


## Work and Friction

- Work ( $\mathrm{w}_{\mathrm{s}}$ )
- This kind of work is called "shaft work".
- Positive when work is done on the fluid (e.g., by a pump)
- Negative when the fluid does work on its environment (e.g., in a turbine)
- Friction ( $\mathrm{w}_{\mathrm{f}}$ )
- Always positive


## Mechanical Energy Equation

$$
\frac{P_{2}-P_{1}}{\rho}+\frac{1}{2} \alpha\left(v_{2}^{2}-v_{1}^{2}\right)+g\left(z_{2}-z_{1}\right)=w_{s}-w_{f}
$$

Increase in fluid mechanical energy (pressure + kinetic energy + potential energy)

Positive when Always positive work is done on the fluid

Note 1: each grouping of variables has units of energy per mass of fluid. To cast the equation in terms of "Power" (energy/time), multiply all terms by mass flow rate

## Special Case: No Friction or Shaft Work

$$
\frac{P_{2}-P_{1}}{\rho}+\frac{1}{2} \alpha\left(v_{2}^{2}-v_{1}^{2}\right)+g\left(z_{2}-z_{1}\right)=0
$$

Called the "Bernoulli Equation" after Daniel Bernoulli, a $19^{\text {th }}$ Century fluid mechanics expert

## For no work or friction

$$
\frac{P_{2}-P_{1}}{\rho}+\frac{1}{2} \alpha\left(v_{2}^{2}-v_{1}^{2}\right)+g\left(z_{2}-z_{1}\right)=0
$$

What happens to the pressure in a horizontal pipe when it expands to a larger diameter?


Which form(s) of energy is (are) decreasing, and which is (are) increasing?

## Example: Liquid Flow in an Expanding Pipe


a. What is the average velocity in the larger pipe?

$$
v_{\text {avg }, 2}=v_{\text {avg }, 1} A_{1} / A_{2}=v_{\text {avg }, 1} d_{1}^{2} / D_{2}^{2}=v_{\text {avg },} / 4=0.5 \mathrm{~m} / \mathrm{s}
$$

b. What is the pressure in the larger pipe?

$$
\begin{gathered}
\frac{P_{2}-P_{1}}{\rho}+\frac{1}{2} \alpha\left(v_{2}^{2}-v_{1}^{2}\right)+g\left(z_{2}-z_{1}\right)=0 \\
P_{2}-P_{1}=\frac{1}{2} \rho \alpha\left(v_{1}^{2}-v_{2}^{2}\right) \text { The Pressure Increases! }
\end{gathered}
$$

## Example: An Emptying Tank

Liquid in an open tank flows out through a small outlet near the bottom of the tank. Friction is negligible. What is the outlet velocity as a function of the height of the liquid in the tank?

$$
\begin{aligned}
& P_{1}=P_{2}=0 \\
& v_{1}=0 \quad v_{2}=v_{\text {out }} \\
& z_{2}-z_{1}=-h \\
& a \approx 1
\end{aligned}
$$



$$
\begin{gathered}
\frac{{\not P_{2}^{0}-P_{1}^{0}}_{0}^{\rho}+}{}+\frac{1}{2} \mathscr{d}\left(v_{2}^{1}-{\forall \forall_{1}^{2}}_{0}^{2}\right)+g\left(z_{2}^{-h}-z_{1}\right)=0 \\
\frac{1}{2} v_{\text {out }}^{2}-g h=0
\end{gathered}
$$

Torricelli's Equation

## The Effects of Fluid Friction

The mechanical energy equation says that friction $\left(w_{f}\right)$ causes mechanical energy to decrease.

Friction is produced in flowing fluid, because fluid molecules...

- Flow past solid boundaries

- Flow past other fluid molecules


## Friction in liquid flow through horizontal constant-diameter pipe:



| $v_{1}=v_{2}$ |  |
| :--- | :--- |
| $z_{2}-z_{1}=0$ | $\frac{P_{2}-P_{1}}{\rho}+\frac{1}{2} \alpha\left(\underline{v}_{2}^{2}-{v_{1}}^{2}\right)+g\left(z_{2}-z_{1}\right)=-w_{f}$ |
|  | $P_{2}=P_{1}-\rho w_{f}$ |

Friction in liquid pipe flow reduces pressure (not velocity)

## Pumps



Example 7.8
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$$
\begin{gathered}
\frac{P_{2}-P_{1}}{\rho}+\frac{1}{2} \alpha\left({\underline{v_{2}}}^{2}-v_{1}^{2}\right)^{0}+g\left(\underline{z}_{2}-z_{1}\right)=w_{s}-w_{f} \\
P_{2}=P_{1}+\rho w_{\text {pump }}-\rho w_{f}
\end{gathered}
$$

## Pumps



## Power delivered to the fluid <br> Pump Efficiency = <br> Power to operate the pump

## Turbines

- The calculated power
- Power extracted from the fluid using a perfect turbine
- Actual power delivered by the turbine is smaller than that value. (friction loss, mechanical inefficiencies, etc.)


## Power delivered by the turbine <br> Turbine Efficiency = <br> Power extracted from the fluid

## Chapter 8

## Mass Transfer

## Mass Transfer

- Molecular Diffusion
- Concentration difference
- Mass Convection
- By bulk fluid flow


## Molecular Diffusion

- Random movement (in liquids, called Brownian motion)
- Molecules of one species (A) moving through a stationary medium of another species(B)

a



## Fick's Law


("A" diffusing through "B")

$$
\dot{N}_{A}=-D_{A B} A \frac{c_{A, 2}-c_{A, 1}}{x_{2}-x_{1}}
$$

$\dot{N}_{A}=$ moles of " $A$ " transferred per time from " 1 " to " 2 "
$D_{A B}=$ "diffusivity" of " $A$ " diffusing through " $B$ "
$A=$ area through which diffusion occurs (cross-section)

## Fick's Law

$$
\dot{N}_{A}=-D_{A B} A \frac{c_{A, 2}-c_{A, 1}}{x_{2}-x_{1}}
$$

Transfer rate $=$ Driving force $/$ Resistance
Analogy with Ohm's Law

$$
I=\frac{V}{R} \quad \dot{N}_{A}=\frac{c_{A, 1}-c_{A, 2}}{R}=\frac{c_{A, 1}-c_{A, 2}}{\left(\frac{x_{2}-x_{1}}{D_{A B} A}\right)}
$$

What molecular variables affect $D_{A B}$ ? molecular size, shape, charge, temperature

## Diffusion in Contact Lens

- "Hard lenses" (polymethylmethacrylate)
- physically uncomfortable
- inadequate oxygen diffusion (irritation, inflammation)
- "Soft lenses" (hydrocarbon hydrogels)
- physically more comfortable
- inadequate oxygen diffusion
- "Oxygen permeable" (siloxane)
- physically uncomfortable
- better oxygen diffusion
- Latest (siloxane hydrogels)
- physically more comfortable
- better oxygen diffusion


## Mass Convection

- Flow-enhanced transfer of one species moving through another species.



## Mass Transfer across Phase Boundaries

- Mass convection + Molecular diffusion
- Mass convection >> Molecular diffusion
- Phase boundaries
- Liquid/Gas, Solid/Liquid, Liquid/Liquid


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## Mass Transfer across Phase Boundaries

Phase Boundary or Interface

Figure 8.5

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$h_{m}=$ mass-transfer coefficient
$c_{A 1}=$ concentration of " $A$ " at the phase boundary in phase II


## Mass Transfer across Phase Boundaries

$$
\dot{N}_{A}=h_{m} A\left(c_{A, 1}-C_{A, 2}\right)
$$

Analogy with Ohm's Law

$$
I=\frac{V}{R} \quad \dot{N}_{A}=\frac{C_{A, 1}-C_{A, 2}}{R}=\frac{C_{A, 1}-C_{A, 2}}{\left(\frac{1}{h_{m} A}\right)}
$$

What variables affect $h_{m}$ ?

- flow patterns (depends on geometry, etc.)
- molecular size
- molecular shape
- molecular charge
- temperature

Ex. 8.1. The level of a lake drops throughout the summer due to water evaporation.
(a) How much volume will the lake lose per day to to evaporation?
(b) How long will it take for the water level to drop 1 m ?

| conc. of water at the water surface | $1.0 \times 10^{-3} \mathrm{kgmol} / \mathrm{m}^{3}$ |
| :--- | :--- |
| conc. of water in the wind | $0.4 \times 10^{-3} \mathrm{kgmol} / \mathrm{m}^{3}$ |
| area of the lake | $1.7 \mathrm{mi} i^{2}$ |
| mass transfer coefficient | $0.012 \mathrm{~m} / \mathrm{s}$ |
| density of the lake water | $1000 \mathrm{~kg} / \mathrm{m}^{3}$ |

## Multi-Step Mass Transfer

- Membrane Separation



## Membrane Separation



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## Membrane Separation

Solving for the concentration differences

$$
\dot{N}_{A}=D_{A, m} A \varepsilon_{\text {pore }} \frac{c_{A_{m, i}}-c_{A_{m, O}}}{\Delta x_{m}}
$$

$$
\begin{aligned}
& c_{A_{i}}-c_{A_{m, i}}=\frac{\dot{N}_{A}}{h_{m_{i}} A} \\
& c_{A_{m, i}}-c_{A_{m, o}}=\frac{\dot{N}_{A} \Delta x_{m}}{D_{A, m} A \varepsilon_{\text {pore }}} \\
& c_{A_{m, o}}-c_{A_{0}}=\frac{\dot{N}_{A}}{h_{m_{o}} A}
\end{aligned}
$$

Summing these...
$c_{A_{i}}-c_{A_{o}}=\dot{N}_{A}\left(\frac{1}{h_{m_{i}} A}+\frac{\Delta x_{m}}{D_{A, m} A \varepsilon_{\text {pore }}}+\frac{1}{h_{m_{o}} A}\right)$

## Membrane Separation

$$
\dot{N}_{A}=\frac{c_{A_{i}}-C_{A_{o}}}{\frac{1}{h_{m_{i}} A}+\frac{\Delta x_{m}}{D_{A, m} A \varepsilon_{\text {pore }}}+\frac{1}{h_{m_{o}} A}}=\frac{\text { overall driving force }}{\sum \text { resistances }}
$$

Concept: Limiting Resistance

$$
\begin{aligned}
\text { Total Resistance }=\frac{1}{h_{m_{i}} A}+\frac{\Delta x_{m}}{D_{A, m} A \varepsilon_{p o r e}}+\frac{1}{h_{m_{o}} A} \\
\quad \begin{array}{l}
\text { convection } \\
=\begin{array}{l}
\text { resistance on } \\
\text { the inlet side }
\end{array}+\begin{array}{l}
\text { resfistance in } \\
\text { the membrane }
\end{array} \quad \text { renvection } \\
\text { the outlet side }
\end{array}
\end{aligned}
$$

If one resistance >> the others, changing the others will not change the total resistance significantly

Ex. 8.2. Liquid $B$ flows on one side of a membrane, and liquid $C$ flows along the other side. Species A present in both liquids transfers from liquid $B$ into liquid $C$.
(a) What is the transfer rate of $A$ from $B$ to $C$ ?
(b) Calculate the limiting resistance.
conc. of $A$ in liquid $B$ conc. of $A$ in liquid $C$ thickness of the membrane diffusivity of $A$ in the membrane area of membrane porosity of membrane mass transfer coefficient on side B $\quad 7.0 \times 10^{-4} \mathrm{~m} / \mathrm{s}$ mass transfer coefficient on side C $\quad 3.0 \times 10^{-4} \mathrm{~m} / \mathrm{s}$


Ex. 8.3. In patient with severe kidney disease, urea must be removed from the blood with a hemodialyzer. In that device, the blood passes by special membranes through which urea can pass. A salt solution (dialysate) flows on the other side of the membrane to collect the urea and to maintain the desired concentration of vital salts in the blood.
(a) What is the initial removal rate of urea? (Note. This rate will decrease as the urea concentration in the blood decrease.)
(b) One might be tempted to try to increase the removal rate of urea by developing better hemodialyzer membrane. Is such an effort justified?

Blood side
mass transfer coeff. for the urea urea conc. within the dialyzer
Dialysate side
mass transfer coeff. for the urea urea conc. within the dialyzer
Membrane
thickness
diffusivity of urea in the membrane
total membrane area
porosity
$0.0019 \mathrm{~cm} / \mathrm{s}$
$0.020 \mathrm{gmol} / \mathrm{l}$
$0.0011 \mathrm{~cm} / \mathrm{s}$
$0.003 \mathrm{gmol} / \mathrm{l}$
0.0016 cm
$1.8 \times 10^{-5} \mathrm{~cm}^{2} / \mathrm{s}$
$1.2 m^{2}$
20\%

