

Mass balance Reactors I

Today's lecture

- Mass balance
 - Principle
 - Applications
 - Steady state
- State of mixing
- Reactor analysis using mass balance
 - Completely mixed batch reactor

Principle behind

- Conservation of matter: matter (atoms) can neither be created nor destroyed
 - * exception (not relevant to this class!): $E = mc^2$

Mass balance without reactions

Simple accounting of materials:

$$(\text{Accumulation}) = (\text{Input}) - (\text{Output})$$

like in your bank account (when interest rate=0),

balance = deposit - withdrawal

Mass balance: Time as a factor

$$\left[(\text{Accumulation}) = (\text{Input}) - (\text{Output}) \right] / (\text{time})$$

$$\frac{dM}{dt} = \frac{d(in)}{dt} - \frac{d(out)}{dt}$$

rate of accumulation rate of input rate of output

- Solving a mass balance problem:
 - 1) Draw schematics, make assumptions, & define control volume (system boundary)
 - 2) Write a mass balance equation using time as a factor
 - 3) Use mathematics to solve the equation

Solving a mass balance problem

Q: Prof. Choi purchases and brings into his house 20 kg of consumer goods every week. Of this amount, 50% is eaten by him as food and eventually leaves the house as CO_2 and other materials. The rest is produced as solid wastes except for 1 kg that accumulates in his house. The solid wastes are classified as non-recyclables and recyclables which are at a mass ratio of 1:1. How many 20-L non-recyclable waste plastic bags should Prof. Choi purchase every year? Assume a density of 1 kg/L for the non-recyclable waste.

Mass balance: substances in water

$$\frac{dM}{dt} = \frac{d(in)}{dt} - \frac{d(out)}{dt}$$

For substances homogeneously distributed in water or air, $d(in)/dt$ and $d(out)/dt$ can be calculated as:

$$\frac{Mass}{Time} = C \cdot Q = \text{Mass flow rate}$$

C = concentration [M/L³]

Q = flow rate [L³/T]

Accordingly,

$$\frac{dM}{dt} = C_{in} \cdot Q_{in} - C_{out} \cdot Q_{out}$$

Mass balance: including reactions

(Accumulation) = (Input) – (Output) + (Reaction)

$$\frac{dM}{dt} = \frac{d(in)}{dt} - \frac{d(out)}{dt} + R$$

R = rate of change in mass due to reaction [M/T]

$$= rV \quad (V: \text{volume})$$

reaction rate, $r = -kC^n$ [M/L³/T] (n =reaction order)

for 1st order reaction, $r = -kC$

(most common in the environment)

Steady state

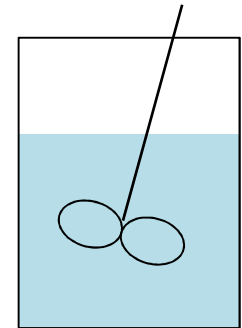
- $dM/dt = 0$
- No change in the amount of materials in the control volume, i.e., $M \neq f(t)$
cf) transient state: $M = f(t)$
- The mass balance equation gets simpler!
(No left-hand-side term)

Mass balance: including reactions

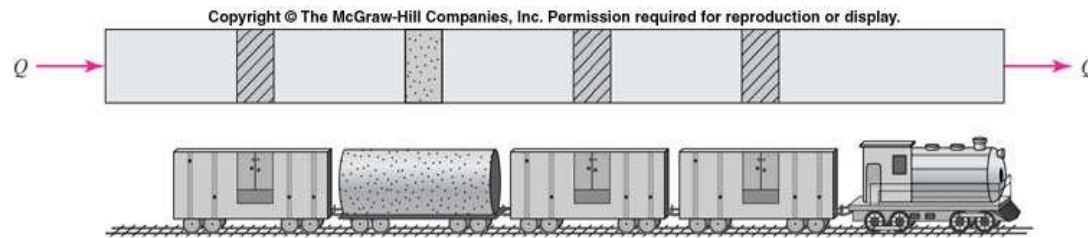
Q: A well-mixed sewage lagoon is receiving 430 m³/d of untreated sewage. The lagoon has a surface area of 10 ha and a depth of 1.0 m. The pollutant concentration in the sewage discharging into the lagoon is 180 mg/L. The pollutant degrades in the lagoon according to first-order kinetics with a reaction rate constant of 0.70 d⁻¹. Assuming no other water losses or gains and that the lagoon is completely mixed, find the steady-state concentration of the pollutant in the lagoon effluent.

The state of mixing

- Ideal models for mixing
 - **completely mixed systems:** entire system is homogeneous



- **plug flow systems:** no mixing in the direction of flow; homogeneous (completely mixed) in the direction perpendicular to the flow



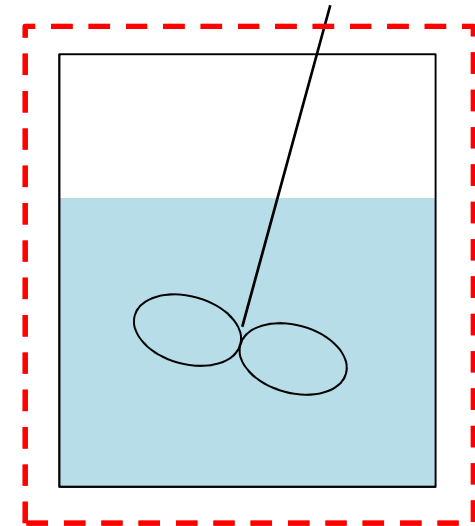
(b)

Reactor analysis – CMBR, 1st order reaction

- **Completely mixed batch reactor (CMBR)**

- Fill-and-draw type
- No flow in or flow out

- 1) draw schematics, define CV
- 2) write a mass balance eq.



$$V \frac{dC}{dt} = \cancel{\frac{d(in)}{dt}} - \cancel{\frac{d(out)}{dt}} + \underbrace{R}_{-kCV}$$

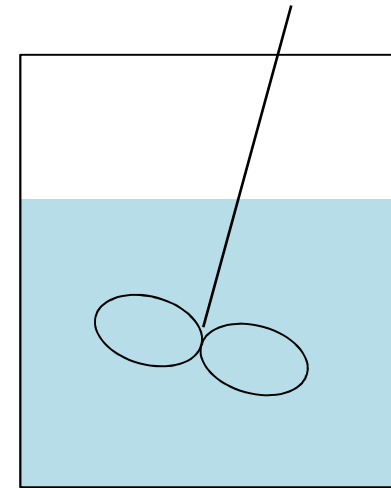
Reactor analysis - CMBR, 1st order reaction

3) solve the equation

$$\frac{dC}{dt} = -kC$$

integrating over $t=0$ to t_{final} :

$$\frac{C_{final}}{C_{initial}} = e^{-kt_{final}}$$



Reactor analysis - CMBR, 1st order reaction

Q: A contaminated soil is to be treated in a completely mixed lagoon. To determine the time it will take to treat the soil, a laboratory completely mixed batch reactor is tested to gather the following data. Assuming a first-order reaction, estimate the rate constant, k , and determine the time to achieve 99% reduction in the original concentration.

Time (days)	Contaminant concentration (mg/kg)
1	280
16	132

Suggested readings

[ENG] pp. 152 – 165, 167 – 170

[KOR] pp. 146 – 161, 163 – 166

Next class

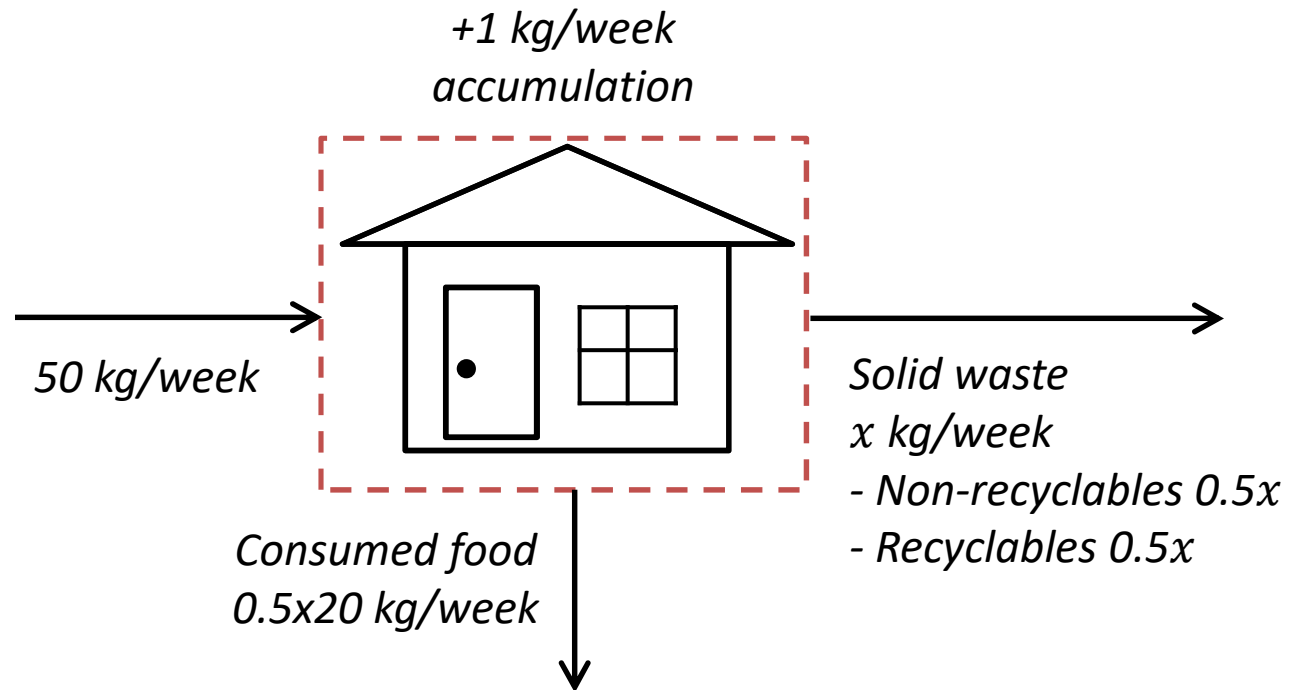
Reactors II

- More on reactor analysis – reactor with flow in & outs
- Hydraulic retention time
- Comparing the performance of different reactors

Slide#6 solution

i) Draw a schematic, make assumptions, define CV

Assume there's no inputs/outputs other than those given in the question.



ii) Write a mass balance eq.

$$\frac{dM}{dt} = \frac{d(in)}{dt} - \frac{d(out)}{dt}$$

iii) Arrange the eq. to a useful form

$$\frac{d(out)}{dt} = \frac{d(in)}{dt} - \frac{dM}{dt}$$

$$\frac{d(out)}{dt} = 20 \text{ kg/week} - 1 \text{ kg/week} = 19 \text{ kg/week}$$

$$= 0.5 \times 20 \text{ kg/week} + x$$

$$x = 9 \text{ kg/week}$$

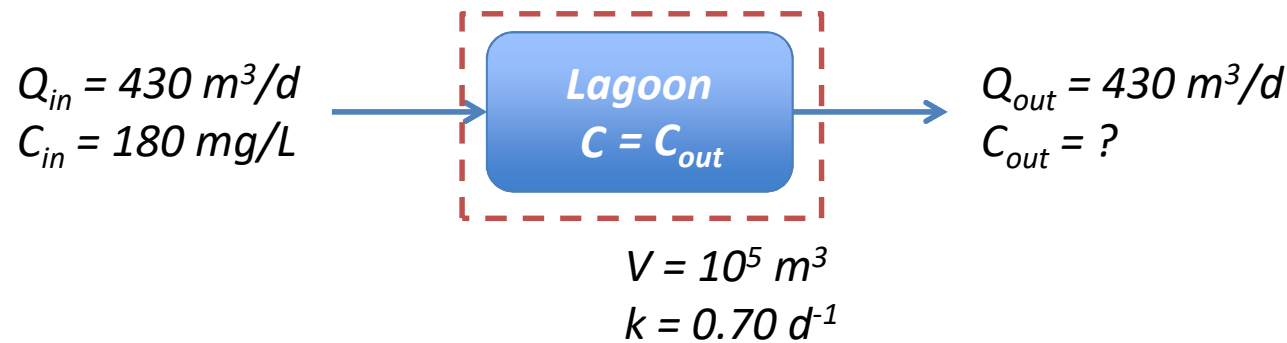
Non-recyclable waste produced every year

$$= 52 \text{ weeks/year} \times 0.5 \times 9 \text{ kg/week} = 234 \text{ kg/year} = 234 \text{ L/year}$$

$$\text{Plastic bags to be purchased every year} = 234 \text{ L} / (20 \text{ L/bag}) = \mathbf{11.7 \text{ bags}}$$

Slide#10 solution

i) Draw a schematic diagram, make assumptions, define CV



ii) Write a mass balance eq.

$$\frac{dM}{dt} = Q_{in}C_{in} - Q_{out}C_{out} - kC_{out}V$$

iii) Arrange the eq. to a useful form

$$C_{out} = \frac{Q_{in}C_{in}}{Q_{out} + kV} = \frac{430 \text{ m}^3/\text{d} \times 180 \text{ mg/L} \times 10^3 \text{ L/m}^3}{430 \text{ m}^3/\text{d} + 0.70 \text{ d}^{-1} \times 10^5 \text{ m}^3} = 1100 \text{ mg/m}^3 = \mathbf{1.1 \text{ mg/L}}$$

Slide#14 solution

$$-kt = \ln \frac{C_{final}}{C_{initial}}$$

$$k = -\frac{1}{t} \cdot \ln \frac{C_{final}}{C_{initial}} = -\frac{1}{15 d} \cdot \ln \frac{132}{280} = 0.0501 d^{-1}$$

$$t_{99\%} = -\frac{1}{k} \cdot \ln \frac{C_{final}}{C_{initial}} = -\frac{1}{0.0501 d^{-1}} \cdot \ln 0.01 = \mathbf{91.9 \text{ days}}$$

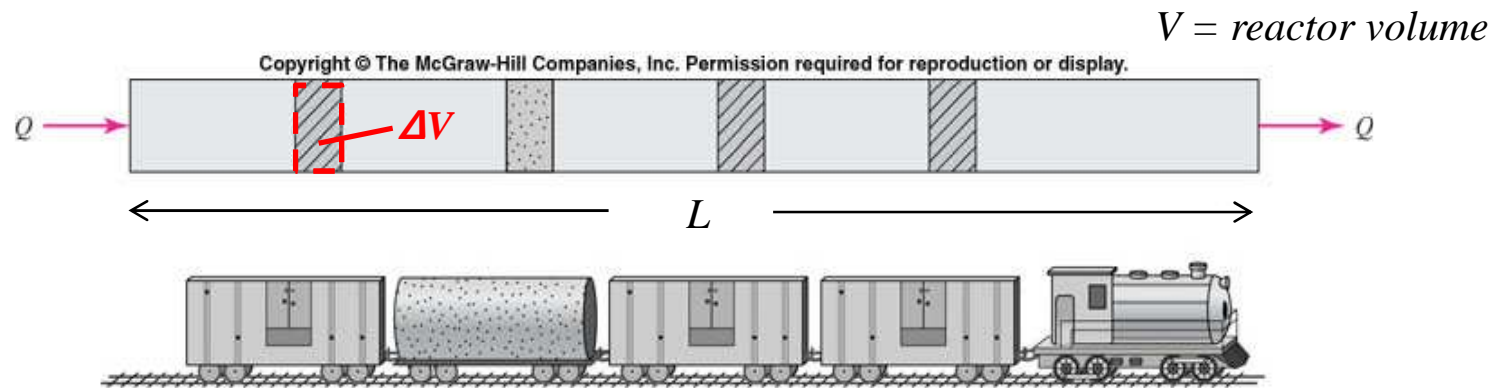
Reactors II

Today's lecture

- Reactor analysis using mass balance
 - Plug flow reactor
 - Completely mixed flow reactor
- Reactor analysis – wrapping up
 - Hydraulic retention time
 - PFR vs. CMFR

Reactor analysis – PFR, 1st order reaction

- Plug-flow reactor (PFR)



1) define control volume:

the moving “plug”: a very thin, homogeneous plate moving in the direction of flow

Reactor analysis – PFR, 1st order reaction

2) write a mass balance eq.:

$$\Delta V \frac{dC}{dt} = \frac{d(in)}{dt} - \frac{d(out)}{dt} + R$$

$-kC\Delta V$ (1st order)

3) arrange the equation: $\frac{dC}{dt} = -kC$

integrating over $t=0$ to t_0 ($= L/v_{flow} = V/Q$):

$$\frac{C_{out}}{C_{in}} = e^{-kt_0}$$

→ same form as the batch reactor!
(why??)

Reactor analysis – PFR, 1st order reaction

- Examples of PFRs



Disinfection



Rivers and streams

Reactor analysis - PFR

Q: In the U.S., a wastewater treatment plant must disinfect its effluent before discharging the wastewater to a stream. The wastewater contains 4.5×10^5 CFU/L of fecal coliform. The effluent standard for fecal coliform is 2×10^3 CFU/L. Assuming that the disinfection facility is a PFR, determine the length of pipe required if the velocity of the wastewater in the PFR is 0.75 m/s. Assume that the first-order reaction rate constant for destruction of the fecal coliforms is 0.23 min^{-1} .

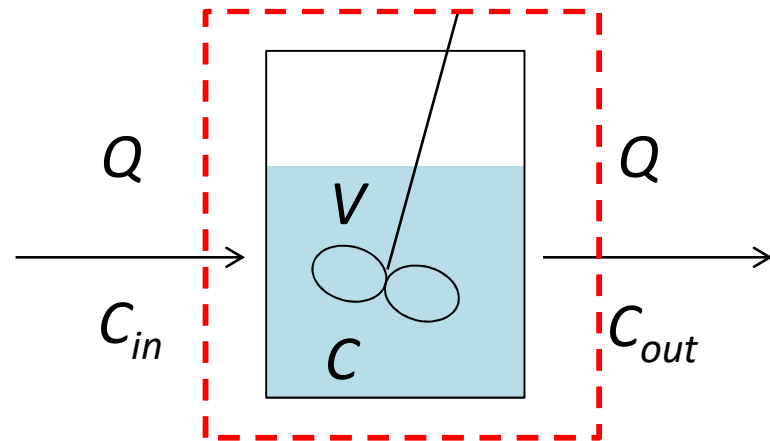
Reactor analysis – CMFR, 1st order reaction

- Completely mixed flow reactor (CMFR)
(continuous-flow stirred tank reactor, CSTR)

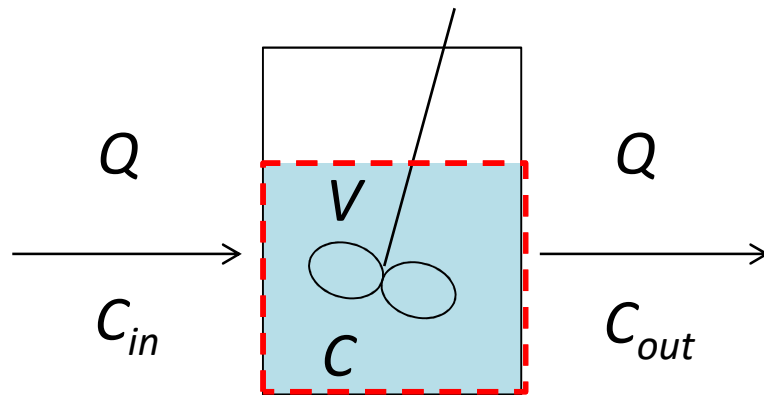
- 1) define control volume
- 2) write a mass balance eq.

$$V \frac{dC}{dt} = Q \cdot C_{in} - Q \cdot C_{out} - kCV \text{ (1st order)}$$

The diagram shows a mass balance equation for a control volume. The terms are: $V \frac{dC}{dt}$ (accumulation), $Q \cdot C_{in}$ (inflow), $Q \cdot C_{out}$ (outflow), and $-kCV$ (1st order reaction rate).



Reactor analysis – CMFR, 1st order reaction



Because of homogeneous mixing, $C = C_{out}$

$$V \frac{dC_{out}}{dt} = QC_{in} - QC_{out} - kC_{out}V$$

Reactor analysis – CMFR, 1st order reaction

3) arrange the equation:

$$V \frac{dC_{out}}{dt} = QC_{in} - QC_{out} - kC_{out}V$$

Special case I. No reaction, initial concentration = C_0

$$V \frac{dC_{out}}{dt} = QC_{in} - QC_{out} - kC_{out}V$$

$$\frac{dC_{out}}{dt} = \frac{1}{t_0}(C_{in} - C_{out}) \quad (t_0 = V/Q)$$

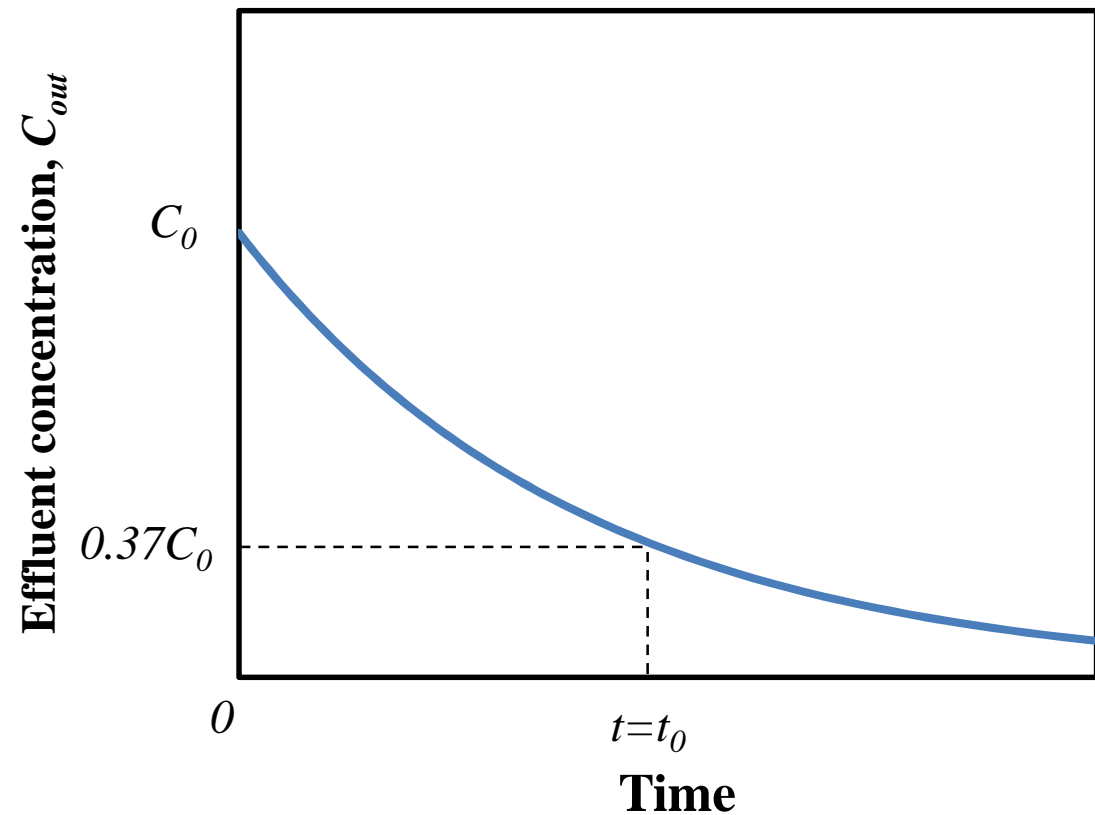
integrating over $t=0$ to t :

$$C_{out,t} = C_0 \left[\exp\left(-\frac{t}{t_0}\right) \right] + C_{in} \left[1 - \exp\left(-\frac{t}{t_0}\right) \right]$$

Reactor analysis – CMFR, 1st order reaction

when $C_{in} = 0$,

$$C_{out,t} = C_o \left[\exp\left(-\frac{t}{t_0}\right) \right]$$



Reactor analysis – CMFR, 1st order reaction

$$V \frac{dC_{out}}{dt} = QC_{in} - QC_{out} - kC_{out}V$$

Special case II. Steady state

$$V \frac{dC_{out}}{dt} = QC_{in} - QC_{out} - kC_{out}V$$

$$C_{out} = \frac{C_{in}}{1 + kt_0} \quad (t_0 = V/Q)$$

→ influent concentration (C_{in}) is reduced in the effluent by a factor of $(1+kt_0)$

Reactor analysis – CMFR, 1st order reaction

- Examples of CMFRs



Biological wastewater
treatment



Lake

Reactor analysis - CMFR

Q: Activated sludge is a key process for most wastewater treatment facilities. The process is often run as a CMFR. Assume a 400 m³-sized CMFR for an activated sludge process receiving 2000 m³/d of wastewater. If a terrorist dumped 10 kg of a non-biodegradable toxic chemical to the reactor, how long will it take for the toxic chemical concentration in the reactor to a safe level (1 mg/L)?

Reactor analysis - CMFR

Q: A chemical degrades in a steady-state CMFR according to first-order reaction kinetics. The upstream concentration of the chemical is 10 mg/L and the downstream concentration is 2 mg/L. Water is being treated at a rate of 29 m³/min. The volume of the tank is 580 m³. What is the rate of decay? What is the rate constant?

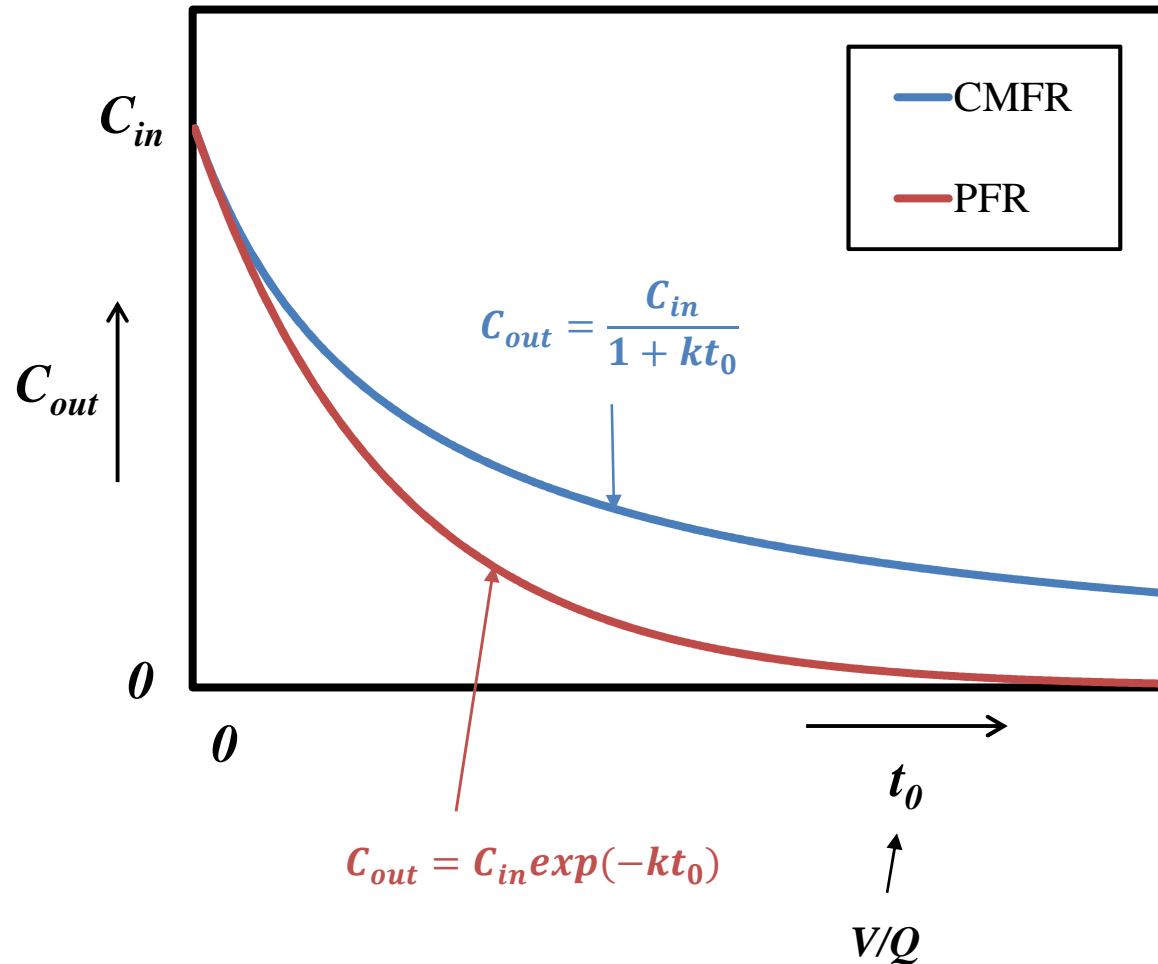
Hydraulic retention time

- Hydraulic retention time (HRT), t_0

$$t_0 = V / Q$$

- The average time the fluid particles spend in the reactor
- PFR: the time that fluid particles spend in a reactor is the same ($=t_0$) for all particles
- CMFR: the time that fluid particles spend in a reactor is different

PFR vs. CMFR



- At the same t_0 , PFR shows better performance
- Advantage of using CMFR: less sensitive to shock loads and toxic compounds

Suggested readings

[ENG] pp. 165 – 176

[KOR] pp. 161 – 173

Next class

Ecosystem

- Fundamental characteristics of ecosystems
- Human impact
- Bioaccumulation of hazardous chemicals
- Nutrient cycle
- Lake ecosystem

Slide#6 solution

$$\ln \frac{C_{out}}{C_{in}} = -kt_0 = -kL/v_{flow}$$

$$L = -\frac{v_{flow}}{k} \cdot \ln \frac{C_{out}}{C_{in}} = -\frac{0.75 \text{ m/s}}{0.23 \text{ min}^{-1}} \times 60 \text{ s/min} \times \ln \frac{2 \times 10^3 \text{ CFU/mL}}{4.5 \times 10^5 \text{ CFU/mL}}$$

= 1060 m

Slide#13 solution

Non-biodegradable → *no reaction*

$$C_{out,t} = C_0 \exp(-t/t_0)$$

$$t = -t_0 \cdot \ln \frac{C_{out,t}}{C_0}$$

$$C_0 = \frac{10 \text{ kg}}{400 \text{ m}^3} \times 10^6 \text{ mg/kg} \times 10^{-3} \text{ m}^3/\text{L} = 25 \text{ mg/L}$$

$$t_0 = \frac{V}{Q} = \frac{400 \text{ m}^3}{2000 \text{ m}^3/\text{d}} = 0.2 \text{ d}$$

$$t = -0.2 \text{ d} \cdot \ln \frac{1 \text{ mg/L}}{25 \text{ mg/L}} = \mathbf{0.64 \text{ day}}$$

Slide#14 solution

$$C_{out} = \frac{C_{in}}{1+kt_0}$$

$$k = \frac{1}{t_0} \left(\frac{C_{in}}{C_{out}} - 1 \right)$$

$$t_0 = \frac{580 \text{ m}^3}{29 \text{ m}^3/\text{min}} = 20 \text{ min}$$

$$k = \frac{1}{20 \text{ min}} \left(\frac{10 \text{ mg/L}}{2 \text{ mg/L}} - 1 \right) = \mathbf{0.20 \text{ min}^{-1}}$$

$$\text{rate of decay} = -r = -\left. \frac{dC}{dt} \right|_{\text{reaction}} = k \cdot C_{out}$$

$$= (0.20 \text{ min}^{-1}) \cdot (2 \text{ mg/L}) = \mathbf{0.40 \text{ mg/L} - \text{min}}$$