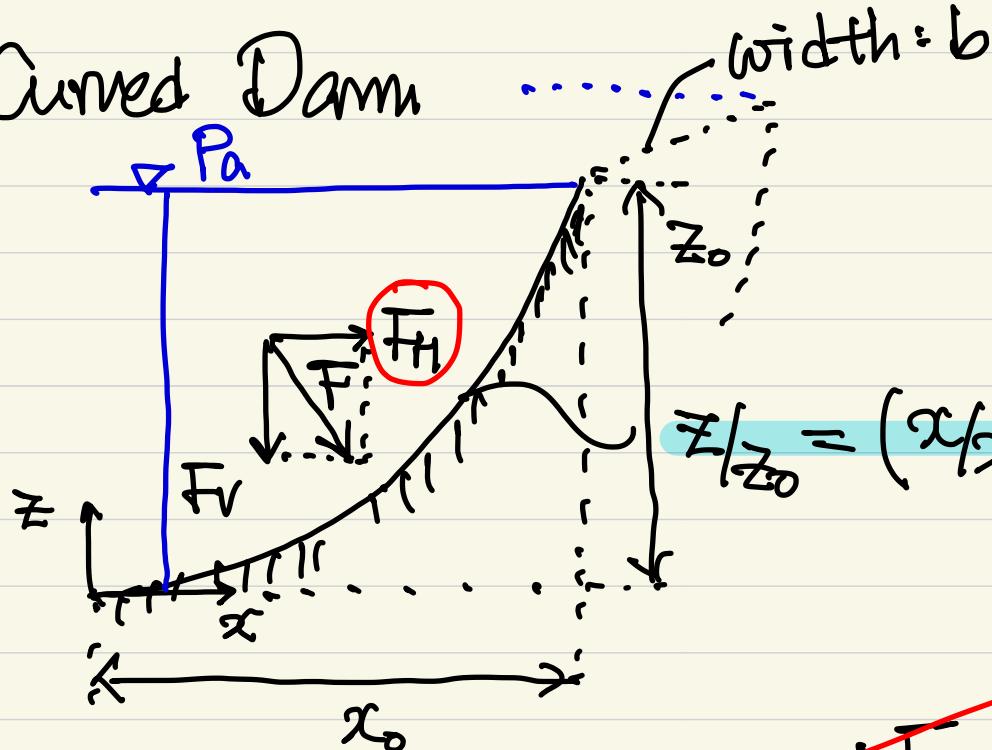


· 중간 평가 #1 : 10/11 (회) 11:00 ~ 12:30 (1, 2장)
 (301종 204회, 305회)

ex) Curved Dam



• $P_a \approx 0$ ★

• $F_H = \rho g h c_g \cdot A_{proj}$

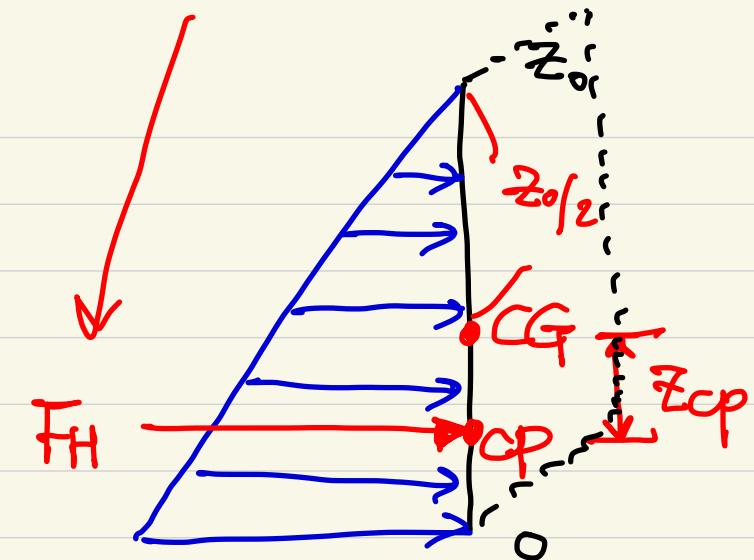
$$= \rho g \cdot \frac{z_0}{z} (z_0 \cdot b)$$

$$= \frac{1}{2} \rho g b z_0^2$$

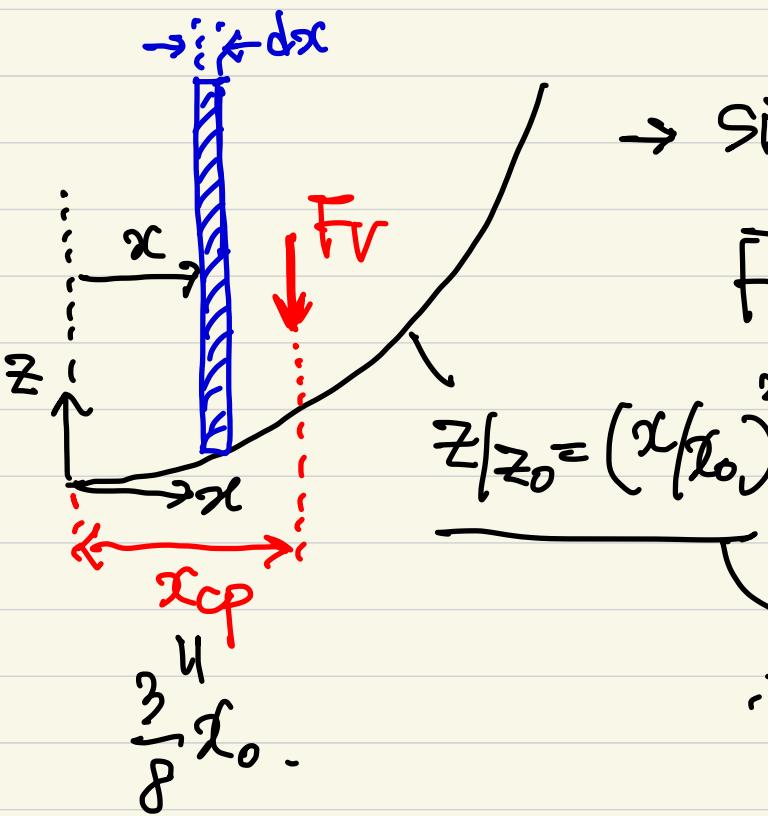
• $F_v = \rho g V$

$$= \rho g \int_{0}^{x_0} (z_0 - z) b \cdot dx$$

$$= \frac{2}{3} \rho g b z_0^2$$

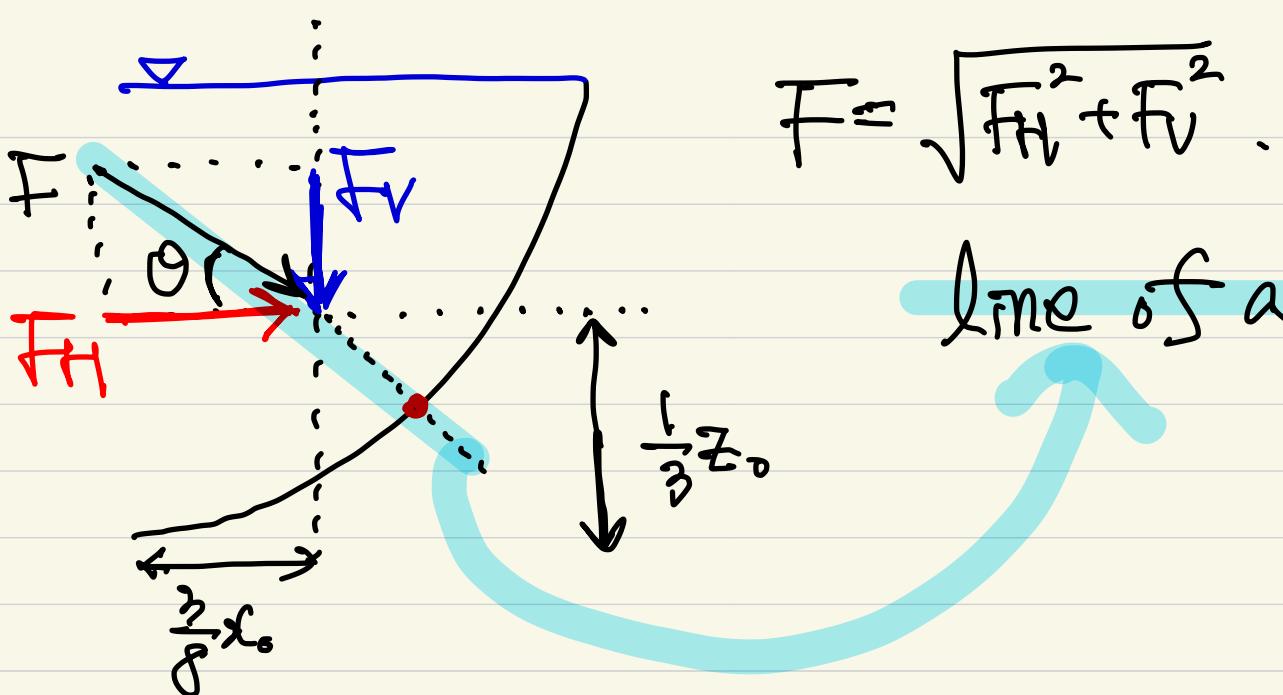


$$\begin{aligned}
 \overbrace{F_H - Z_{cp}}^{\text{green blob}} &= -\rho g \sin \theta \cdot \frac{I_{xx}}{\frac{1}{12} b z_0^3} \\
 &= 1 \cdot \frac{1}{12} b z_0^3 \\
 \rightarrow Z_{cp} &= -\frac{1}{f} z_0. \quad (\text{or } \frac{1}{3} z_0 \text{ from the bottom})
 \end{aligned}$$



→ similarly for F_V .

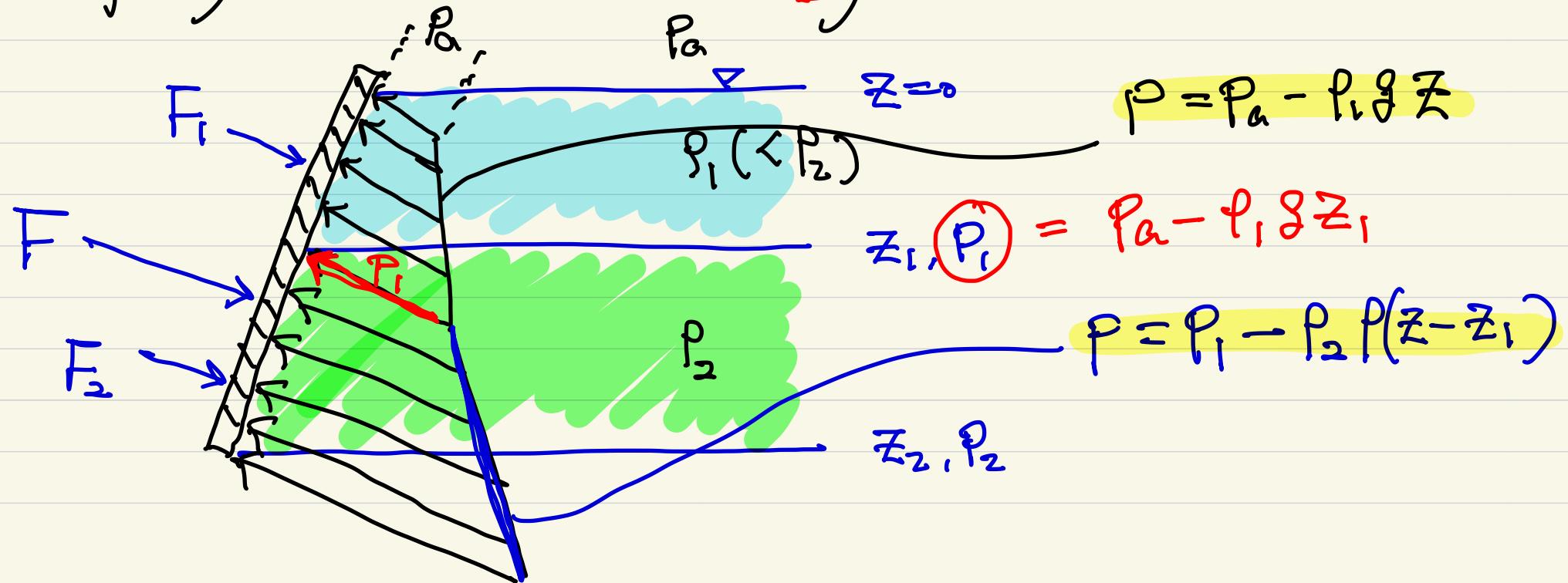
$$\begin{aligned}
 \overbrace{F_V \cdot x_{cp}}^{\text{green blob}} &= \int_0^{x_0} \rho g (z_0 - z) b \cdot x \cdot dx \\
 \therefore x_{cp} &= \frac{3}{f} x_0.
 \end{aligned}$$



$$F = \sqrt{F_H^2 + F_V^2}$$

line of action.

2.1 Hydrostatic forces in layered fluids.



$$\therefore F = \sum_i F_i = \sum_i P_{CG,i} \cdot A_i$$

$$Y_{CP,i} = - \frac{P_i g \sin \theta_i \cdot I_{xx,i}}{P_{CG,i} \cdot A_i}$$

$$X_{CP,i} = - \frac{P_i g \sin \theta_i \cdot I_{xy,i}}{P_{CG,i} \cdot A_i}$$

→ Moment summation.

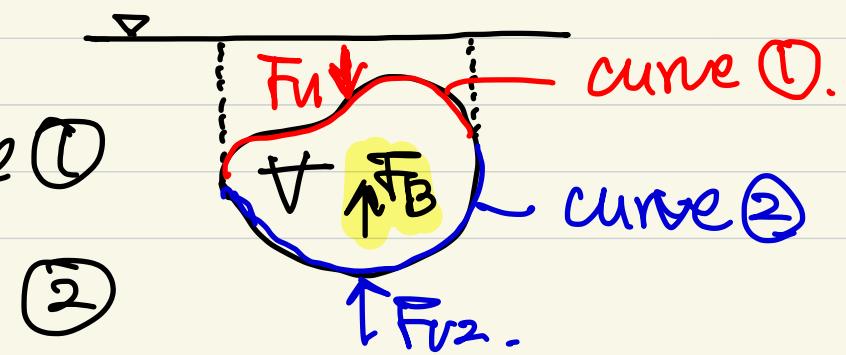
$$F \cdot Y_{CP} = \sum_i F_i \cdot Y_{CP,i}$$

$$F \cdot X_{CP} = \sum_i F_i \cdot X_{CP,i}$$

2.F Buoyancy and Stability (Archimedes Law).

- ① A body immersed in a fluid experiences a vertical buoyant force equal to the weight of the fluid it displaces.

- F_{V1} : fluid weight above curve ①
- F_{V2} :



$$\Rightarrow F_B = F_{V2} - F_{V1} = \rho_f g V \quad (\text{weight of the body})$$

$W = \rho_b \cdot g V$

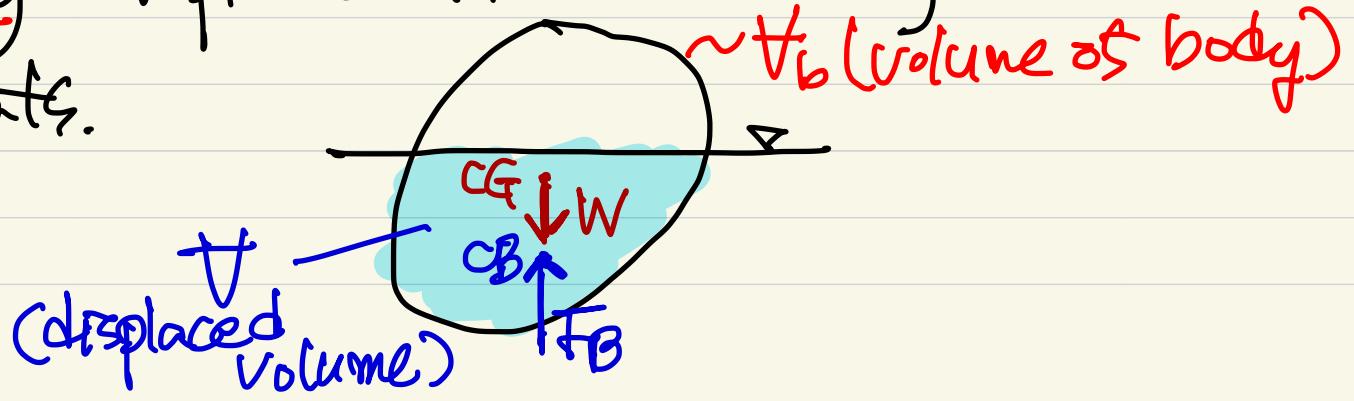
If $\rho_b = \rho_f$

: neutrally buoyant.

- line of action of the F_B passes through the center of volume, if ρ is uniform.

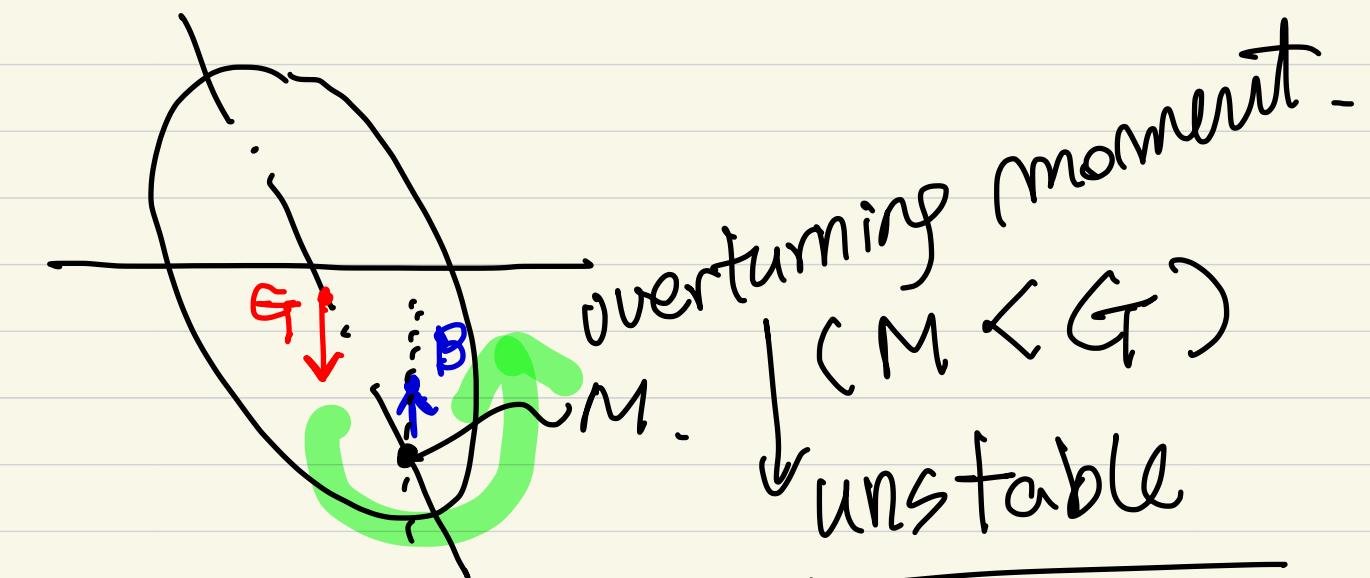
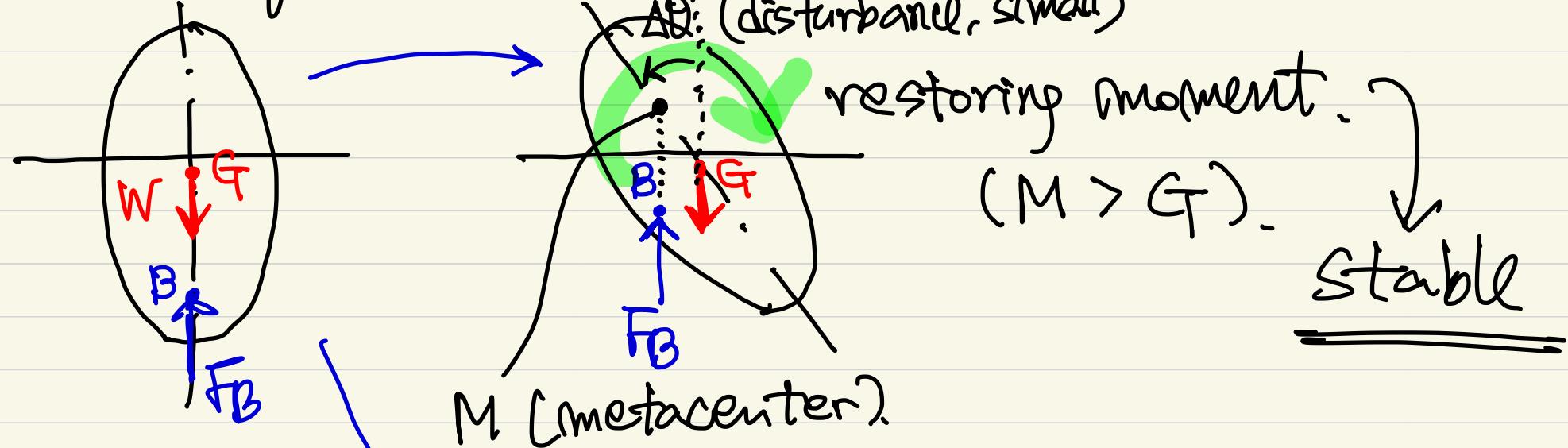
→ CB (center of buoyancy) may or may not correspond to actual CM.

- ② A floating body displaces its own weight in the fluid it floats.



$$F_B = f_f g T = W = P_b g T / b. \quad (\epsilon \ll 1)$$

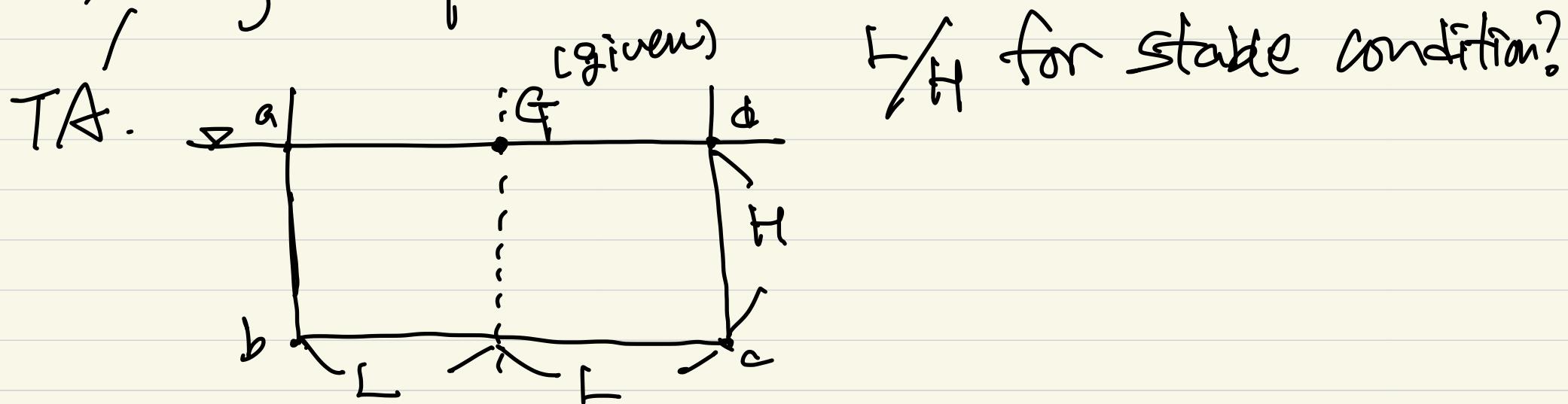
* Stability. (response to a disturbance).



\bar{MG} : metacentric height.

(property of the cross-section for the given weight). → indication of the stability ($\bar{MG} > 0$ for the stable condition)

ex) Barge ship.



2.9. Pressure distribution in rigid-body motion.

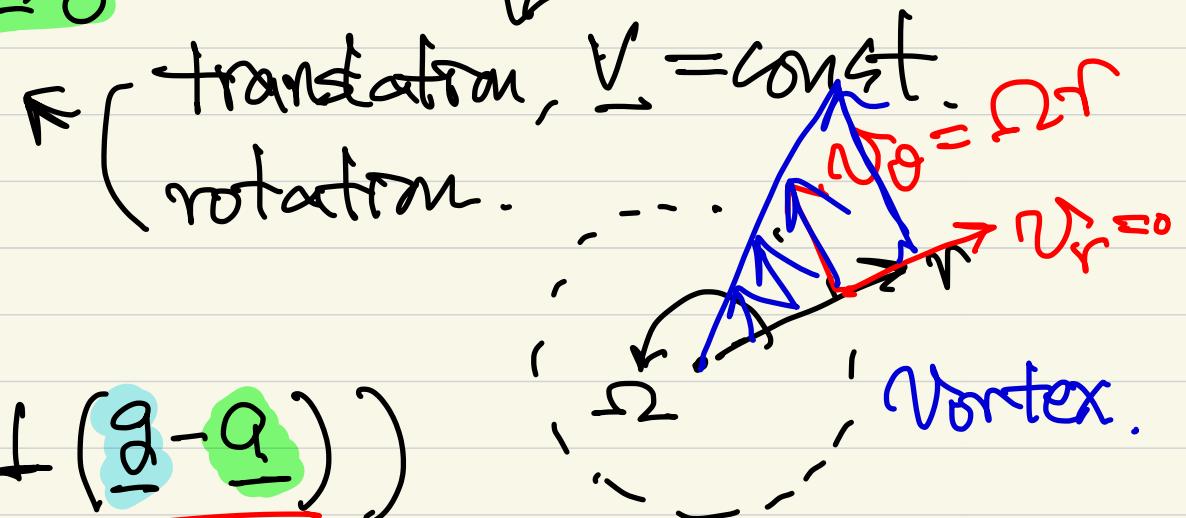
$$\nabla p = \rho(\underline{g} - \underline{a}) + \mu \nabla^2 \underline{V}$$

↑
 중력
 험력
 풍속
 $\nabla^2 V = 0$

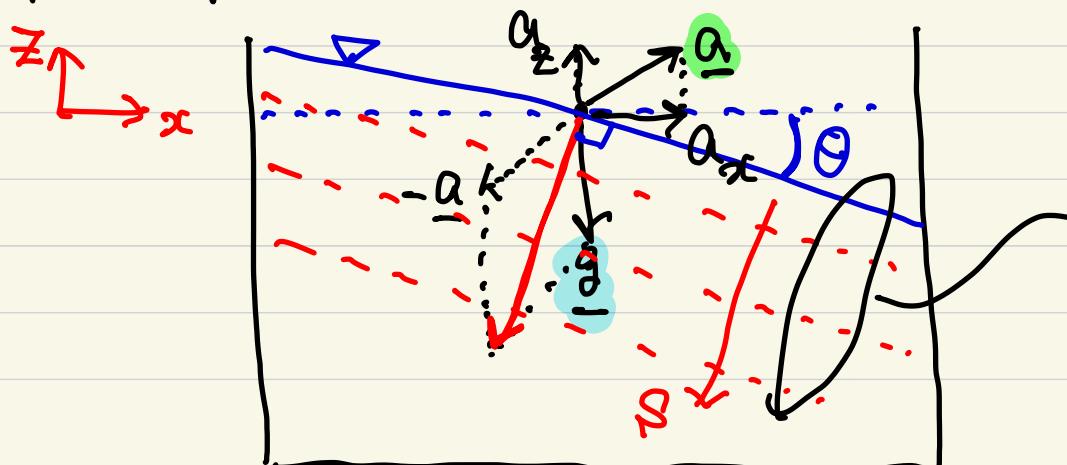
(no relative motion between particles)

$$\therefore \nabla p = \rho(\underline{g} - \underline{a}).$$

(line of constant $P \perp (\underline{g} - \underline{a})$)



* Uniform linear acceleration.

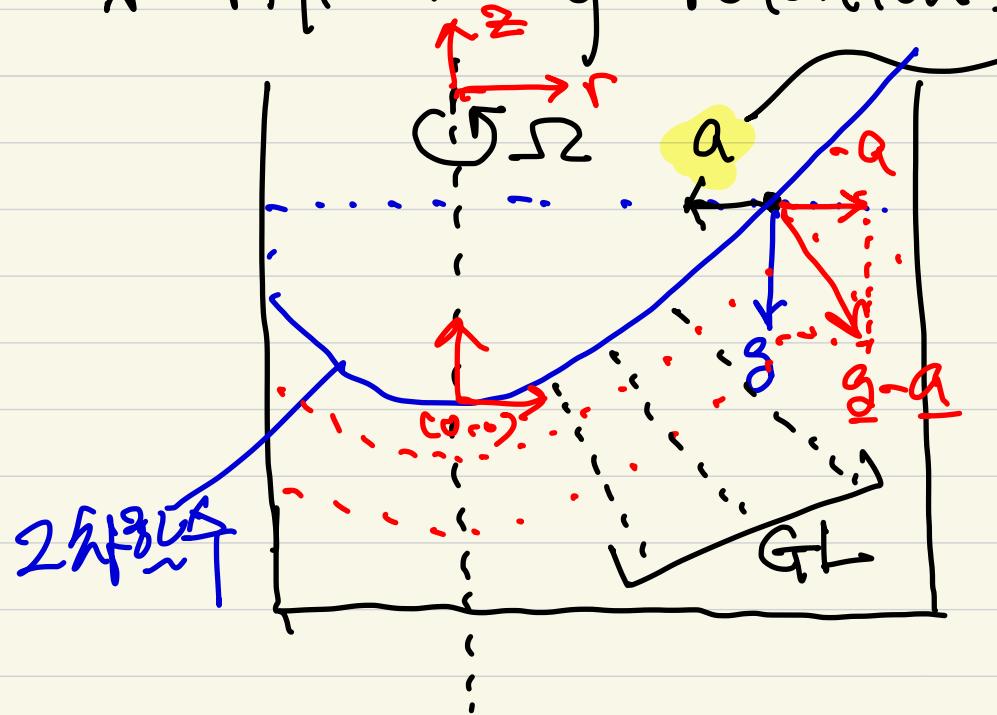


lines of constant pressure.

$$\cdot \tan\theta = \frac{a_x}{g+a_z} \rightarrow \theta = \tan^{-1} \frac{a_x}{g+a_z}$$

$$\cdot \Delta P = \rho g z \rightarrow \frac{dp}{ds} = \rho \sqrt{a_x^2 + (g+a_z)^2}$$

* rigid-body rotation.



centripetal acceleration.

$$\nabla P = \rho (g - a)$$

$$a = \frac{\Omega}{r} \times (\Omega \times r) = -r\Omega^2 \hat{i}_r$$

$$\frac{\Omega}{r} = \Omega \cdot \hat{i}_k$$

$$\nabla P = \left[\frac{\partial P}{\partial r} \hat{i}_r + \frac{\partial P}{\partial z} \hat{i}_k \right] = \rho (g - a) = \left[-\rho g \hat{i}_r \right] + \left[\rho r \Omega^2 \hat{i}_r \right]$$

$$g = -g \hat{i}_k$$

Euler eq.

$$\therefore \frac{\partial P}{\partial r} = \rho r \Omega^2, \quad \frac{\partial P}{\partial z} = -\rho g. \quad \Rightarrow P(r, z)$$

$$\rightarrow P(r, z) = \frac{1}{2} \rho r^2 \Omega^2 - \rho g z + C.$$

① $(r, z) = (0, 0)$ (free surface), $P = P_a$.

$$\therefore C = P_a.$$

$$\therefore P = P_a - \rho g z + \frac{1}{2} \rho r^2 \Omega^2.$$

\hookrightarrow surface of constant pressure (P_1)

\checkmark $\therefore \check{z} = \frac{P_a - P_1}{\rho g} + \frac{\Omega^2 r^2}{2g}$: paraboloids of revolution.

if $P_1 = P_a$. $\check{z} = \frac{\Omega^2 r^2}{2g} \rightarrow$ free surface.

- Lines orthogonal to the constant-pressure surfaces. (i.e., pressure-gradient surfaces).

$$\Rightarrow \frac{dz}{dr} \Big|_{GL} = - \frac{1}{(\frac{dz}{dr})_p = \text{const}} = - \frac{1}{r\Omega^2/g}.$$

(gradient line)

$$\therefore \frac{dz}{dr} \Big|_{GL} = - \frac{g}{r\Omega^2} \Rightarrow r \approx C_i \cdot \exp\left(-\frac{\Omega^2 t}{g}\right)$$

in the absence of friction and Coriolis effects, ..

the particles will follow these lines!

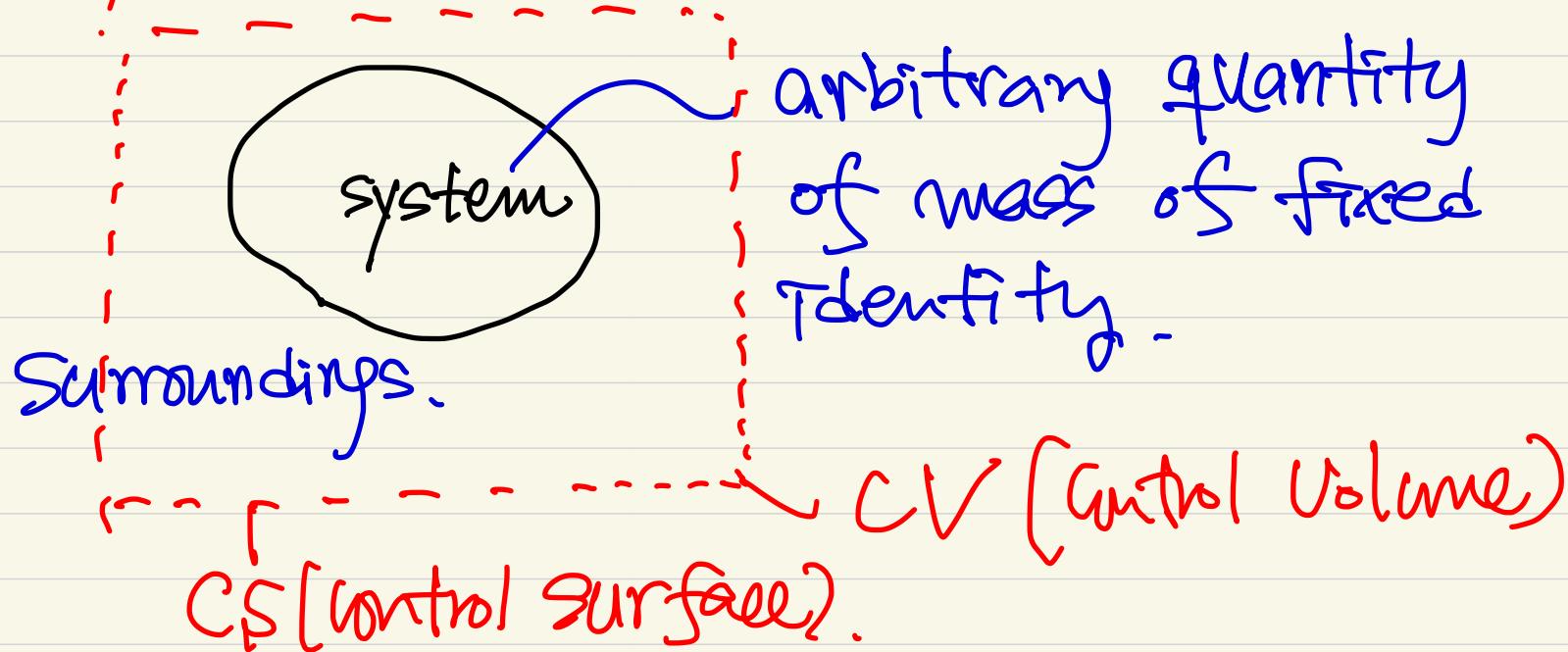
Depending on their density, small particles/bubbles
will fall/rise along these exponential lines.

Lecture #1. 10/11. 11:00 - 12:30. 305, 204f.

CH.3 Integral relation for a Control Volume.

3.1. Basic Physical Laws of Fluid Mechanics.

* System vs. Control Volume.



⇒ Law of mechanics : Interaction between system and surroundings.



i) Conservation of mass : $M_{sys} = \text{constant}$, $\frac{dM}{dt} = 0$.

✓ 2)

“

$$\text{Momentum. : } \underline{F} = m\underline{a} = m \frac{d\underline{v}}{dt}$$
$$= \frac{d}{dt}(m\underline{v})$$

3)

“

angular mtm

$$: \underline{M} = \frac{d}{dt}(\underline{\underline{H}}) . \quad \underline{\underline{H}} = \sum (\underline{r} \times \underline{v}) \sin.$$

↓
(total moment)

✓ 4)

“

energy : $dE = \oint Q - \oint W$.

$$\left(\frac{dE}{dt} = \frac{dQ}{dt} - \frac{dW}{dt} \right).$$

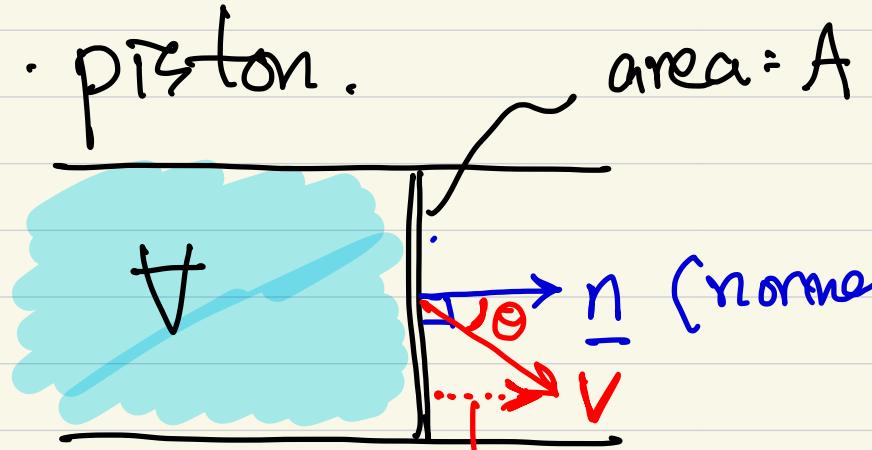
5) 2ND law of thermodynamics : $ds \geq \frac{dQ}{T}$

6) state equations, $P = P(S, T)$, $e = e(P, T)$

→ Control Volume form.

* Volume and mass flow rate.

• piston.



(normal vector).

$$\begin{aligned} dV &= (\underline{V} \cdot d\underline{E}) \cdot A \\ \therefore \frac{dV}{dt} &= VA \\ \underline{V} \cdot \underline{\cos\theta} \Rightarrow dV &= (\underline{V} \cdot \underline{\cos\theta}) dt \cdot A \\ &= (\underline{V} \cdot \underline{\Omega}) dt A \end{aligned}$$