## 1.3.2 Ideal solution

1





## 1.3.2 Ideal solution



 $G = X_A G_A + X_B G_B + RT(X_A \ln X_A + X_B \ln X_B)$ 

## 1.3.4. Chemical Potential

Partial molar quantity (아주 작은 양이 add 되었을 때 변하는 성질)  $\bar{Q}_i = \left(\frac{\partial Q_i}{\partial n_i}\right)_{T,P,n_j}$ 

Partial Molar Quantity of Free energy  $\rightarrow$  Chemical Potential <sup>Whole System</sup>  $\mu_A = \left(\frac{\partial G^U}{\partial n_A}\right)_{T,P,n_B} G$ : molar free *E* (independent of size)

For binary solution at T, P, const.  $dG' = \mu_A dn_A + \mu_B dn_B$ 

#### If T, P change & multi components $dG' = -SdT + VdP + \mu_A dn_A + \mu_B dn_B + \mu_C dn_C + \dots$

For molar quantity

 $G = \mu_A X_A + \mu_B X_B (Jmol^{-1})$ (:: 1 mol of original phase,  $X_A$  mol,  $X_B$  mol.  $dn_A : dn_B = X_A : X_B$ )



## 1.3.2 Ideal solution

### For molar quantity

$$G = \mu_A X_A + \mu_B X_B$$

$$\left(\frac{\partial G}{\partial X_A}\right)_{T,P,X_B} = \mu_A$$



For ideal solution,

 $G = X_A G_A + X_B G_B + RT(X_A \ln X_A + X_B \ln X_B)$ 

$$\mu_A = \left(\frac{\partial G}{\partial X_A}\right)_{T,P,X_B} = G_A + RT \ln X_A$$

 $\mu_B = G_B + RT \ln X_B$ 



$$\begin{pmatrix} \frac{\partial G}{\partial X_A} \end{pmatrix}_{T,P,X_B} = \mu_A = G_A + RT \ln X_A \\ \mu_B = G_B + RT \ln X_B \end{cases}$$

$$\cdot \quad dG' = -SdT + VdP + \sum \mu_i dn_i \\ \cdot \quad dG^M = \mu_A dX_A + \mu_B dX_B - 1 \\ \cdot \quad G^M = X_A \mu_A + X_B \mu_B - 2 \\ \cdot \quad \frac{dG^M}{dx_A} = \mu_A - \mu_B - 3 \left( \frac{dG^M}{dx_B} = \mu_B - \mu_A \right) \\ \cdot \quad (3) \times X_B \to X_B \frac{\partial G^M}{\partial x_A} = \mu_A X_B - \mu_B X_B \cdot (4) \\ \cdot \quad (2) + (4) \to G^M + X_B \frac{\partial G^M}{\partial x_A} = \mu_A (X_A + X_B) = \mu_A \cdot (5) \\ \cdot \quad \mu_A = G^M + X_A \frac{\partial G^M}{\partial x_B} - (7) \\ (\text{intercept at } X_B = 1) = G^M_{at} x_B + X_A \cdot slope = G^M + X_A \frac{\partial G^M}{\partial x_B} \\ from (7) = \mu_B \\ by (3)' \text{ intercept at } X_B = 0 \end{cases}$$





### **1.4** Regular solutions (Quasi- chemical model)



- $\Delta H^M = 0$  $\Delta H^M > 0$
- $\Delta H^M > 0$  $\Delta H^M < 0$

Ideal Endothermic Exothermic

### Quasi- chemical approach

✓ 
$$\Delta H^M$$
 is only due to the bonding E.  
( $\Delta V^M = 0$ , vol of A ≅ B)

✓ Interatomic bonding E, distance maintained the same



## **1.3.3. Regular solutions**

when A&B are mixed:

$$\Delta H_{Mix} = P_{AB} \left[ \varepsilon_{AB} - \frac{1}{2} (\varepsilon_{AA} + \varepsilon_{BB}) \right] = P_{AB} \varepsilon$$

E: difference between A-B to aveg. of AA. BB

(1) 
$$\varepsilon = 0$$
  $\Delta H^M = 0$  Ideal solution  
# of bonds # atom  
 $P_{AB} = N_A Z X_A X_B$  (random solution)  
Avogadro's #  
(2)  $\varepsilon > 0$   $\Delta H^M > 0$   $P_{AB}$  ↑, 다른 종류의 atom이 둘려 쌓여지길 선호함  
(3)  $\varepsilon < 0$   $\Delta H^M < 0$   $P_{AB} \downarrow$ , 같은 종류의 atom이 둘려 쌓여지길 선호함  
(less random)

### 1.3.3. Regular solutions (Quasi-chemical model)



 $\Delta G_{Mix}$ , always decrease for small  $X_B$ 



## 1.3.3. Regular solutions (Quasi-chemical model)

### **\*** The Effect of $\Delta H_{mix}$ and T on $\Delta G_{mix}$





## **1.3.5 Regular solution**





Total free energy of alloy (1-39)

 $G^M$  $=\widetilde{X_{A}G_{A}^{\circ}+X_{B}G_{R}^{\circ}}+\widetilde{\Omega X_{A}X_{B}+RT(X_{A}lnX_{A}+X_{B}lnX_{B})}$  $= X_A \left[ G_A^{\circ} + \Omega (1 - X_A)^2 + RT \ln X_A \right]$  $+ X_B \left[ G_B^{\circ} + \Omega (1 - X_B)^2 + RT ln X_B \right]$  $(X_A X_B = X_A^2 X_B + X_B^2 X_A)$  $= \mu_A X_A + \mu_B X_B$ 

 $\therefore \begin{cases} \mu_A = G_A^{\circ} + \Omega(1 - X_A)^2 + RT \ln X_A \\ \mu_B = G_B^{\circ} + \Omega(1 - X_B)^2 + RT \ln X_B \end{cases}$ 



### Activity

 $\mu_A = G_A + RT ln a_A$ 

for regular solution

 $\gamma_A = \frac{a_A}{X_A}$ : activity coefficient

$$ln\left(\frac{a_A}{X_A}\right) = \frac{\Omega}{RT}(1 - X_A)^2$$
$$ln\left(\frac{a_B}{X_B}\right) = \frac{\Omega}{RT}(1 - X_B)^2$$



$$RT ln \gamma_A = \Omega X_B^2$$







For dilute solution.

$$\gamma_B = \frac{a_B}{X_B} = const$$
 (Henry's law)  
 $\gamma_A = \frac{a_A}{X_A} = 1$  (Raoult's law)



# 1.3.6 Real Solutions



Actual arrangement in real solution

 $\rightarrow$  Compromise between  $\Delta E \& \Delta S$  for min G

- $\begin{cases} \varepsilon < 0 & G \downarrow \text{ by increasing A} B \text{ bonds} & \rightarrow \text{ ordering} \\ \varepsilon > 0 & G \uparrow \text{ by increasing A} A, B B \text{ bonds} & \rightarrow \text{ clustering} \end{cases}$
- Ordering & clustering tendency ↓ as T ↑
- $\Delta V^M \neq 0$  (size dependence) Size difference  $\rightarrow$  interstitial solid solution

Strong chemical bonding force  $\rightarrow$  <u>intermediate phase</u> formation



### 1.3.7. Ordered Phases - SPO parameter



(a) Random A-B solution with a total of 100 atoms and  $X_A = X_B = 0.5$ ,  $P_{AB} \sim 100$ , S = 0. (b) Same alloy with short-range order  $P_{AB} = 132$ ,  $P_{AB}(\max) \sim 200$ , S = 0.32.

If  $\Omega < 0$ , and  $\# P_{AB}$  is greater.  $\rightarrow$  short range order (S) (vs. long range order)

$$S = \frac{P_{AB} - P_{AB}(random)}{P_{AB}(max) - P_{AB}(random)}$$



### 1.3.8. Intermediate Phases



♦ When small composition deviation cause rapid rise of *G*→ intermetallic compound.
Usually stoichiometric  $A_m B_n (m, n : integer)$ 



### Ordered structures in Cu-Au system





## **1.4 Equilibrium in Heterogeneous Systems**

### The Molar Free Energy of Two-phase Mixture





## **1.4 Equilibrium in Heterogeneous Systems**





## \* A Simple Phase Diagram

- 1 Completely miscible
- ② Miscibility Gap
  - Liquid phase (ideal)
  - Solid phase ( $\Delta H_{mix} > 0 \rightarrow A$ , B dislike)
- ③ Ordered Alloy
  - $\Delta H_{mix} < 0$
- (4) Simple Eutectic
  - Miscibility gap extend into liquid phase

(5) Phase diagram containing intermediate phase



### \* A Simple Phase Diagram





## 1.5 Binary Phase Diagrams(Summary)





 $T_1$ 



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**\*** System with a Miscibility Gap ( $\Delta H_{mix}^s > \Delta H_{mix}^L = 0$ )





## **\*** Ordered Alloys ( $\Delta H^s_{mix} < 0$ )







### Eutectic Phase Diagram with Same Crystal Structure





### Eutectic Phase Diagram with Different Crystal Structure





### More Complex Phase Diagram





Phase Diagrams Containing Intermediate Phases



Minimum G



### The Effect of Temperature on Solid Solubility





### Equilibrium Vacancy Concentration





## **1.6 The Influence of Interfaces on Equilibrium**

The effect of interfacial energy on the solubility of small particles.



Phase  $\beta$  in  $\alpha$ 

✓ Gibbs – Thompson Effect :

Extra pressure due to the curvature of  $\alpha/\beta$  interface



Phase Transformation in Materials

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## 1.6 The Influence of Interfaces on Equilibrium

### **\therefore** Transfer of d*n* mol of $\beta$ from large to small particle.



 $dG = \Delta G_r \cdot dn$ 

 $(\Delta G_r:$  molar free energy difference

between two particles)

 $dG = \gamma dA$ 

( $\because$  Large particle  $\rightarrow$  unchanged, small  $\rightarrow$  changed)

 $\gamma dA = \Delta G_r \cdot dn$ 

$$\Delta G_r = \gamma \frac{dA}{dn}$$

$$n = \frac{4\pi r^2}{3V_m}, A = 4\pi r^2, \frac{dA}{dn} = \frac{\frac{dA}{dr}}{\frac{dA}{dr}} = \frac{2V_m}{r}$$

 $\therefore \ \Delta G_r = \frac{2\gamma V_m}{r}$ 

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## 1.6 The influence of interfaces on Equilibrium

The effect of interfacial energy on the solubility of small particles



Typical value :  $\gamma = 200 \ mJ/m^2$ ,  $V_m = 10^{-5} \ m^3$ 

$$\frac{X_r}{X_{\infty}} \approx 1 + \frac{1}{r(nm)} (10 \text{ nm} \rightarrow \frac{X_r}{X_{\infty}} = 1.1 (10 \% \text{ diff}))$$

