

Unit 2 : Plasmas as Fluids

II.-1.

Ch. 6. Fluid Equations for a Plasma

* Consider the behavior of "an ensemble of charged particles," rather than "of individual charged particles."

6.1. Continuity Equation :

$$\frac{\partial}{\partial t} n + \vec{\nabla} \cdot (n \vec{u}) = S$$

(6.3)

volume source rate of particles:

"Conservation of particle numbers"
for $S = 0$

> 0 for ionization

< 0 for recombination

for instance.

6.2. Momentum Balance Equation :

* Consider the rate of change of momentum density in a differential element of volume.

* $\frac{\partial}{\partial t}(nm\vec{u}) = nq(\vec{E} + \vec{u} \times \vec{B}) + \dots$ (6.5)

Macroscopic Forces
on the element,
where $\vec{u} = \langle \vec{v} \rangle$.
Sum of forces on
individual particles.

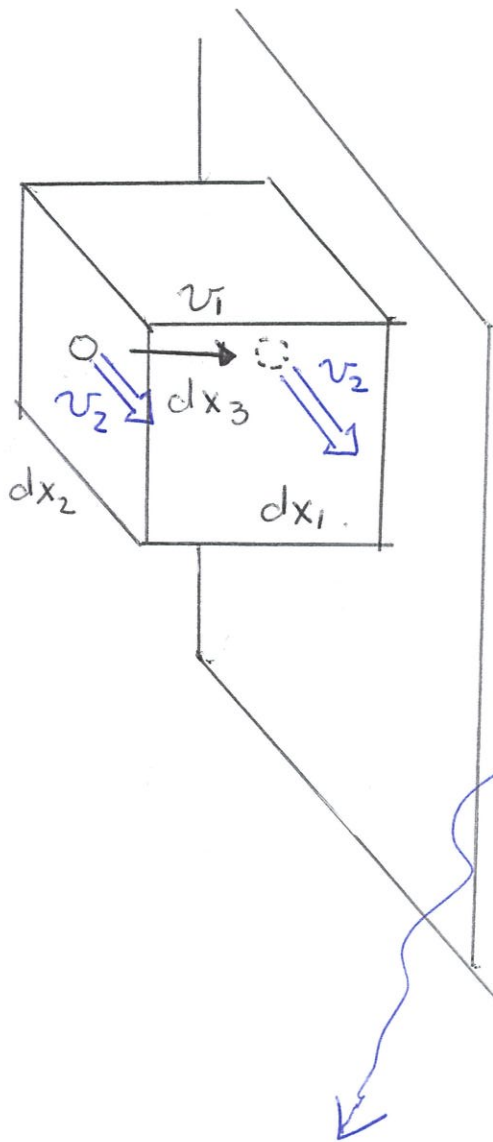
?
Contribution
from
"particles' flux
into/out of the vol. element
carry momentum."

* $f(\vec{x}, \vec{v})$: distribution function,
the relative probability of finding a particle with \vec{v}
at \vec{x} .

→ differential number of ptls in a phase space elt $d^3v d^3x$
located at (\vec{x}, \vec{v}) is " $f(\vec{x}, \vec{v}) d^3v d^3x$ "

* differential number of ptls carried per unit time across the
surface of constant x_1 by this elt in phase space is

" $f(\vec{x}, \vec{v}) d^3v d^3x / dt = v_1 f d^3v dx_2 dx_3$, " $dt = \frac{dx_1}{v_1}$ "



* Specific pts "O" in Fig. each carry x_2 -directed momentum " mv_2 ".

→

* differential amount of momentum in this direction per unit time across a surface of ~~of~~ constant x_1 by this elt. of phase space is

$$" mv_2 v_1 f(\vec{x}, \vec{v}) d^3v dx_2 dx_3$$

∞∞ The rate of change of x_2 -directed momentum, averaged over all the particles, is expressed in terms of the divergence of fluxes of momentum across the various surfaces:

$$\frac{\partial}{\partial t}(nmv_2) = -\frac{\partial}{\partial x_1}(mn \langle v_2 v_1 \rangle) - \frac{\partial}{\partial x_2}(mn \langle v_2 v_2 \rangle) - \frac{\partial}{\partial x_3}(mn \langle v_2 v_3 \rangle)$$

$\left(\begin{array}{l} \text{const } x_1, \\ \text{const } x_2, \\ \text{and " } x_3 \text{ respectively} \end{array} \right)$
 (6.6).

Momentum Balance Equation

II-4.

$$* \quad \frac{\partial}{\partial t} (nm u_i) = - \sum_{j=1}^3 \frac{\partial}{\partial x_j} (mn \langle v_i v_j \rangle) \quad (6.6)$$

* Pressure tensor :

$$P_{ij} \equiv mn \left(\langle v_i - u_i \rangle \langle v_j - u_j \rangle \right) \\ = mn \left(\langle v_i v_j \rangle - u_i u_j \right) \quad (6.7)$$

$$\therefore mn \langle v_i v_j \rangle = P_{ij} + mn u_i u_j, \text{ where } u_i \equiv \langle v_i \rangle.$$

* For drifting Maxwellian distribution function (i.e., $f(\vec{v}-\vec{u})$ is Maxwellian),

$$P_{ij} = nT \text{ for } i=j, \text{ and } P_{ij} = 0 \text{ for } i \neq j$$

* For drifting bi-Maxwellian f with different temperatures,

$$P_{ij} = \begin{bmatrix} nT_{\perp} & 0 & 0 \\ 0 & nT_{\perp} & 0 \\ 0 & 0 & nT_{\parallel} \end{bmatrix}, \quad (6.8)$$

$$* \frac{\partial}{\partial t} (nm u_i) = - \sum_j \frac{\partial P_{ij}}{\partial x_j} - m \sum_j \frac{\partial}{\partial x_j} (n u_i u_j)$$

or adding macroscopic Force

$$* \frac{\partial}{\partial t} (mn \vec{u}) = nq(\vec{E} + \vec{u} \times \vec{B}) - \vec{\nabla} \cdot \vec{P} - \vec{\nabla} \cdot (mn \vec{u} \vec{u}), \quad (6.11)$$

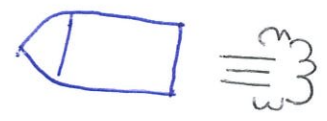
or

Using an identity: $\vec{\nabla} \cdot (n \vec{u} \vec{u}) = \vec{u} \vec{\nabla} \cdot (n \vec{u}) + n(\vec{u} \cdot \vec{\nabla}) \vec{u}$,
and the continuity equation,

$$* mn \left(\frac{\partial}{\partial t} + \vec{u} \cdot \vec{\nabla} \right) \vec{u} = nq(\vec{E} + \vec{u} \times \vec{B}) - \vec{\nabla} \cdot \vec{P} - m \sum \vec{u} \quad (6.12)$$

↓
convective derivative

$$\frac{d}{dt} = \left(\frac{\partial}{\partial t} + \vec{u} \cdot \vec{\nabla} \right)$$



Rocket consuming fuels.

* For relatively simple phenomena, simple form of \vec{P} can be used.

* But the form of \vec{P} gets more complicated for description of complex phenomena.

6.3, Equations of State

II-6,

$$\circ \quad \frac{\partial}{\partial t} n = -\vec{\nabla} \cdot (n \vec{u})$$

$$\circ \quad mn \frac{d}{dt} \vec{u} = -\vec{\nabla} \cdot \vec{p} + nq(\vec{E} + \vec{u} \times \vec{B})$$

"Hierarchy of Fluid Equations."

$$\circ \quad \frac{d}{dt} \vec{p} = \dots \vec{\nabla} \cdot (\text{heat-flux})$$

↓ ?

* To obtain a closed set of fluid equations, some approximation has to be made at some point. → "Fluid Closure."

* The simplest way to achieve the closure is to use the "equations of state" by relating \vec{p} to already used variables such as "n" and "B".

Equations of State : cont'd.

II-7

* For scalar pressure "P": $P = C n^\gamma$

γ : adiabatic exponent.

• $\gamma = 1$ for 'isothermal' compression; for "slow" compression compared to thermal conduction.

• $\gamma = \frac{2+N}{N}$ "N" number of degrees of freedom
for 'adiabatic' compression; for 'faster' than thermal conduction.

* If ^{compression is} slower than the collisional exchange of energy,
→ isotropic and $N=3 \rightarrow \gamma = 5/3$.

* If compression is faster than collisional exchange of energy,
→ anisotropic, $N=1$ and $\gamma=3$ for || direction,
 $N=2$ and $\gamma=2$ ⊥ "

"Double adiabatic" equations of state $\Pi=8$

* Compression that involves components both \parallel and \perp to magnetic field \vec{B} :

$$\perp: P_{\perp} = mn \left\langle \frac{v_{\perp}^2}{2} \right\rangle = n \langle \mu \rangle B \quad (6.17)$$

If the compression is fast compared to collisions but slower than gyration of particles, μ is conserved,

$$\Rightarrow \boxed{\frac{d}{dt} \left(\frac{P_{\perp}}{nB} \right) = 0} \quad (6.18)$$

$$\parallel: P_{\parallel} = mn \langle v_{\parallel}^2 \rangle, \quad J \propto v_{\parallel} L \quad (6.19)$$

Using conservation of ptls: $nV = nAL = \text{const}$,
 of magnetic flux: $BA = \text{const}$, $\Rightarrow L = \frac{V}{A} \propto \frac{B}{n}$.

Eq. (6.19) \rightarrow $\circ\circ$ $\boxed{\frac{d}{dt} \left(\frac{P_{\parallel} B^2}{n^3} \right) = 0}$ (A = area) (6.20) ,

* For pure perpendicular compression,

conservation of particles $\rightarrow nA = \text{const}$

" magnetic flux $\rightarrow BA = \text{const}$

$$\circ \circ \frac{d}{dt} \left(\frac{P_{\perp}}{nB} \right) = 0 \quad \text{reduces to} \quad \frac{d}{dt} \left(\frac{P_{\perp}}{n^2} \right) = 0,$$

which is consistent with $\gamma = 2$ for $N = 2$.

* For pure parallel compression in which B is unchanged,

$$\frac{d}{dt} \left(\frac{P_{\parallel} B^2}{n^3} \right) = 0 \quad \text{reduces to} \quad \frac{d}{dt} \left(\frac{P_{\parallel}}{n^3} \right) = 0,$$

which is consistent with $\gamma = 3$ for $N = 1$.

6.4. Two-fluid Equations

II-10.

- * There are always at least two species in any neutral plasma.
- * In momentum balance equation for each species, transfer of momentum between different species due to collisions should be taken into account.
- * Rate at which momentum per unit volume is gained by species " α " due to collisions with species β is given by

$$\boxed{\vec{R}_{\alpha\beta} = -m_{\alpha} n_{\alpha} \nu_{\alpha\beta} (\vec{u}_{\alpha} - \vec{u}_{\beta})} \quad (6.21)$$

where $\nu_{\alpha\beta}$: collision frequency: the rate at which the momentum of species α is transferred to species β .

- * Now, the momentum balance equation should be:

$$m_{\alpha} n_{\alpha} \left(\frac{\partial \vec{u}_{\alpha}}{\partial t} + (\vec{u}_{\alpha} \cdot \vec{\nabla}) \vec{u}_{\alpha} \right) = n_{\alpha} q_{\alpha} (\vec{E} + \vec{u}_{\alpha} \times \vec{B}) - \vec{\nabla} \cdot \vec{P}_{\alpha} - \sum_{\beta} \vec{R}_{\alpha\beta} \quad (6.24)$$

* From momentum conservation,

$$\vec{R}_{\beta\alpha} = -\vec{R}_{\alpha\beta},$$

This implies

$$\rightarrow m_\alpha n_\alpha v_{\alpha\beta} = m_\beta n_\beta v_{\beta\alpha}.$$

6.5. Plasma Resistivity

* Collisions between electrons and ions in a plasma will impede the acceleration of electrons in response to an electric field applied along (or in the absence of) a magnetic field.

* Neglecting small electron inertia (m_e) and assuming homogeneous electron pressure and velocity,

$$0 = -n_e e E_{\parallel} + R_{ei\parallel}, \quad \text{where } R_{ei\parallel} = -m_e n_e v_{ei} (u_{e\parallel} - u_{i\parallel}) \quad (6.24)$$

* Current density: $j_{\parallel} = -n_e e (u_{e\parallel} - u_{i\parallel})$ (6.26)

* From Eqs (6.24) and (6.25), we obtain

$$E_{\parallel} = - \frac{m_e v_{ei}}{e} (u_{e\parallel} - u_{i\parallel}) = \frac{m_e v_{ei}}{n_e e^2} j_{\parallel} = \eta j_{\parallel} \quad (6.26)$$

Taking into account of velocity distribution of electrons,

$$v_{ei} \rightarrow \langle v_{ei} \rangle \quad \text{and}$$

$$\eta = \frac{m_e \langle v_{ei} \rangle}{n_e e^2} \quad (6.27)$$

Then,

$$\vec{R}_{ei} = -m_e n_e \langle v_{ei} \rangle (\vec{u}_e - \vec{u}_i) = \eta n_e e \vec{j} \quad (6.28)$$

* Note that Eq. (6.28) can also be applied to the direction $\perp \vec{B}$:

$$\eta_{\perp} \approx 2 \eta_{\parallel}$$

because electron distribution can be distorted significantly from Maxwellian due to E_{\parallel} in \parallel direction to \vec{B} .

* Resistivity of fusion plasma is extremely low, lower than that of copper!